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Decentralized Output-Feedback Adaptive Event-Triggered Control for Interconnected Nonlinear Delay Systems with Actuator Failures

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Abstract: This paper investigates decentralized adaptive event-triggered fault-tolerant control for interconnected nonlinear delay systems with actuator failures. The actuator failures suffered include loss of effectiveness and bias faults. A control scheme based on the K-filter is proposed, which effectively compensates for the effects of unknown actuator failures. A hyperbolic tangent function and neural network are introduced to approximate the unknown interconnection and nonlinear delay function. By introducing the dynamic surface control method, the “explosion of complexity” issue is addressed. Furthermore, our proposed controller can ensure that all states of the corresponding closed-loop system are semi-globally uniformly ultimately bounded and that the tracking error can converge to a small neighborhood of zero. Meanwhile, Zeno behavior can be effectively avoided. Finally, the validity of the proposed control scheme is verified using a simulation example.

Keywords: decentralized adaptive control; backstepping technique; fault-tolerant control; event-triggered control; nonlinear delay system



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1. Introduction

In recent years, adaptive control for nonlinear systems has been widely studied. Because neural networks (NNs) and fuzzy logic systems (FLSs) have strong approximation ability, they are used to approximate unknown nonlinear functions. As typical nonlinear systems, interconnected nonlinear systems are popular because of their broad application. Interconnected nonlinear systems have nonlinear and uncertain characteristics, which lead to difficulties in controller design. To address these problems, a decentralized control structure has been proposed, which naturally reduces the computational burden associated with centralized control. Hence, some researchers have proposed some adaptive decentralized control methods for interconnected nonlinear systems [1,2]. In [3], an adaptive decentralized control method for interconnected nonlinear systems with unmodeled dynamics was proposed. The adaptive fuzzy decentralized output-feedback control problem for switched interconnected nonlinear systems was first investigated in [4]. A decentralized backstepping control method for interconnected systems with non-triangular structural uncertainties was investigated in [5]. In practice, time-varying delay characteristics are common, significantly impacting the stability and performance of the system. The traditional linear theory cannot describe and deal with these delay characteristics. To address this issue, an adaptive decentralized control method based on NNs for interconnected nonlinear systems with time delays was proposed in [6]. The decentralized output-feedback control problem for interconnected nonlinear systems with input delays and saturation was studied in [7].

The occurrence of actuator failures is common in modern industrial control systems, which affects the stability of the system. Consequently, it is of great theoretical and practical

significance to study fault-tolerant control (FTC) of nonlinear systems [8,9]. In recent years, many effective FTC methods have been developed to address the above-mentioned problems. In [10], an adaptive fuzzy fault-tolerant control method was proposed for the cascade chemical reactor system. In [11,12], adaptive FTC methods were developed for a class of single-input single-output (SISO) nonlinear systems. In the existing literature [13–16], the focus has gradually shifted from SISO nonlinear systems to multi-input multiple-output (MIMO) nonlinear systems with the same actuator failures mentioned in [11,12]. It can be seen that the above works are based on continuous control methods to address the control problem of nonlinear systems with actuator failures, including loss of effectiveness and bias faults. However, few researchers have addressed the control problem of interconnected nonlinear delay systems with such actuator failures using the discrete control method.

In recent years, event-triggered control has become a research hotspot. Compared with the continuous control method, event-triggered control can save limited communication bandwidth while ensuring system performance. As a result, event-triggered control has been extensively studied. In [17], the adaptive event-triggered control problem for a class of uncertain nonlinear systems was considered, in which the assumption of the input-to-state stability is no longer needed. In [18], an adaptive NN event-triggered control method for switched nonlinear systems was proposed, in which the restrictions on nonlinear functions no longer need to be considered. In [19], the adaptive event-triggered control problem for a more general nonlinear system was considered, considering cases with unmodeled dynamics and nonlinear time delays. Furthermore, the authors of [20] proposed an encoding–decoding mechanism that further saves communication resources based on an event-triggered mechanism. As far as we know, event-triggered control has good flexibility and responsiveness, helping to reduce wear and failure to a certain extent. Nevertheless, constructing an event-triggered controller for interconnected nonlinear systems with actuator faults remains a challenge. Therefore, this issue becomes the second motivation for this study.

Based on the above discussion, this paper investigates the output-feedback adaptive event-triggered tracking control problem for a class of uncertain nonlinear large-scale interconnected systems with actuator failures and time-varying delays. Although the above-mentioned articles have been well studied, addressing the coupling problem between the interconnection and time-varying delay components becomes important. Moreover, effectively saving communication resources and designing a decentralized adaptive event-triggered fault-tolerant control scheme under the premise of ensuring system performance is particularly important. The main contributions of this paper can be summarized as follows:

1. Compared with the literature [13,14,21,22], a new fault-tolerant control strategy based on the K-filter is proposed. The unmeasured states are well estimated, and the actuator failures are compensated for. The interconnected nonlinear function and nonlinear delay function are approximated by introducing a hyperbolic tangent function and NNs.
2. A decentralized adaptive event-triggered controller is developed to ensure that all closed-loop signals are bounded and that tracking errors can converge to a small neighborhood of zero. Furthermore, by utilizing dynamic surface control and backstepping technology, the “explosion of complexity” issue is addressed.
3. Compared with the continuous control method [4,5,7], our proposed event-triggered control method can effectively reduce communication resources. It is proven through theoretical analysis that the Zeno phenomenon is avoided.

This paper is organized as follows. Problem description and preliminaries are provided in Section 2. In Section 3, the state observer, and the decentralized event-triggered controller are designed, and the system stability is analyzed. In Section 4, simulation results are shown. Conclusions are presented in Section 5.

Notations: \mathfrak{R} denotes the set of real numbers; \mathfrak{R}^{n_i} denotes the n_i -dimensional Euclidean space; and $\mathfrak{R}^{n_i \times n_i}$ denotes the real $n_i \times n_i$ matrix space. $E[\cdot]$ is usually the symbol used to denote the expected value or expected absolute value in mathematics.

2. Problem Description and Preliminaries

In this paper, we consider the following interconnected nonlinear delay systems with actuator failures in the form of:

$$\begin{cases} \dot{x}_i = A_i x_i + \Psi_i(y_i)\theta_i + B_i u_i + h_i(y_1, \dots, y_N, t) \\ \quad + f_i(y_i(t), y_i(t - m_{i,1}(t)), \dots, y_i(t - m_{i,n_i}(t))), \\ y_i = x_{i,1}, i = 1, \dots, N, \end{cases} \quad (1)$$

where $A_i = \begin{bmatrix} 0 & I_{n_i-1} \\ 0 & 0 \end{bmatrix} \in \mathfrak{R}^{n_i \times n_i}$; $B_i = [0, \dots, 0, 1]^T \in \mathfrak{R}^{n_i}$; and $x_i = [x_{i,1}, \dots, x_{i,n_i}]^T \in \mathfrak{R}^{n_i}$; $u_i \in \mathfrak{R}$; and $y_i \in \mathfrak{R}$ are the unmeasurable system states, control input with actuator failure, and output of the i -th subsystem, respectively. $\theta_i \in \mathfrak{R}^{p_i}$ is an unknown parameter, and $\Psi_i(y_i) = [\Psi_{i,1}(y_i), \dots, \Psi_{i,n_i}(y_i)]^T \in \mathfrak{R}^{n_i \times p_i}$ with $\Psi_{i,j}(y_i) \in \mathfrak{R}^{p_i}$ is known as the smooth function vector. $h_i = [h_{i,1}, \dots, h_{i,n_i}]^T \in \mathfrak{R}^{n_i}$ is the unknown smooth nonlinear interconnected function vector, where h_i and $h_{i,j}$ represent $h_i(y_1, \dots, y_N, t)$ and $h_{i,j}(y_1, \dots, y_N, t)$, respectively. $f_i = [f_{i,1}, \dots, f_{i,n_i}]^T \in \mathfrak{R}^{n_i}$ is the unknown smooth time-varying nonlinear delay function vector, where $f_{i,j}$ represents $f_{i,j}(y_i(t), y_i(t - m_{i,j}(t)))$, and $m_{i,j}(t)$ is the time-varying delay function. Here, $0 < m_{i,j} < \bar{m}_{i,j} < \infty$ and $|\dot{m}_{i,j}| < m_{i,j}^* < 1$.

Actuator failures with loss of effectiveness and bias faults can be modeled as

$$u_i = \aleph_i v_i + u_{i,h} \quad (2)$$

where u_i is the output of the i -th local actuator; v_i is our designed input; \aleph_i is the unknown actuator efficiency factor satisfying $0 < \underline{\aleph}_i < \aleph_i \leq 1$; and $u_{i,h}$ is the uncertain bounded bias function.

Definition 1. Consider the following nonlinear system:

$$dZ(t) = f(Z(t))dt. \quad (3)$$

The trajectory $Z(t)$ of system (3) is said to be semi-globally uniformly ultimately bounded (SGUUB) at the p -th moment if for some compact set $\Omega \in \mathfrak{R}^n$ and any initial state $Z_0 = Z(t_0)$, there exists a constant $\varepsilon > 0$, and a time constant $T = T(\varepsilon, Z_0)$ such that $E\left[|Z(t)^p|\right] < \varepsilon$ for all $t > t_0 + T$. When $p = 2$, it is usually called SGUUB in the mean square.

Our control objective is to develop a decentralized adaptive event-triggered output-feedback controller in the form of (67) for system (1) with actuator faults (2) such that all states of the resulting closed-loop system are SGUUB and the tracking error can converge to a small neighborhood of zero.

To achieve the objective, some assumptions and lemmas are given below.

Assumption 1. The desired trajectories $y_{i,r}$ and $\dot{y}_{i,r}$ are available and bounded for $i = 1, \dots, n_i$.

Assumption 2 ([23]). For $i = 1, \dots, N, j = 1, \dots, n_i$, the interconnected nonlinear function $h_{i,j}$ satisfies

$$|h_{i,j}|^2 \leq \sum_{\gamma=1}^N (y_\gamma h_{i,j,\gamma}(y_\gamma))^2, \quad (4)$$

where $h_{i,j,\gamma}(y_\gamma) \geq 0$ denotes the unknown smooth function.

Assumption 3 ([24]). The nonlinear functions $f_{i,j}(\cdot)$ satisfy the following inequalities for $j = 1, \dots, n_i$

$$|f_{i,j}(y_i(t), y_i(t - m_{i,j}(t)))|^2 \leq a_{i,j,1} \bar{f}_{i,j,1}(y_i(t)) + a_{i,j,2} \bar{f}_{i,j,2}(y_i(t - m_{i,j}(t))), \quad (5)$$

where $a_{i,j,1}$ and $a_{i,j,2}$ are positive constants. $\bar{f}_{i,j,p}(\cdot)$ represents the uncertain smooth function, where $\bar{f}_{i,j,p}(0) = 0$ for $i = 1, \dots, N, j = 1, \dots, n_i, p = 1, 2$. Additionally, $\bar{f}_{i,j,p}(\cdot)$ satisfies

$$\bar{f}_{i,j,p}(\tilde{y}_i(t) + y_{i,r}(t)) \leq \tilde{y}_i(t) f_{i,j,p}^*(\tilde{y}_i(t)) + \eta_{i,j,p}(y_{i,r}(t)), \quad (6)$$

where $\tilde{y}_i(t)$ and $y_{i,r}(t)$ are variables, $f_{i,j,p}^*$ represents the uncertain functions, and $\eta_{i,j,p}(y_{i,r}(t))$ represents the bounded functions for a bounded variable $y_{i,r}(t)$ with $\eta_{i,j,p}(0) = 0$.

Lemma 1 ([25]). There exists a constant $\nu > 0$ and a variable $\lambda \in \mathfrak{R}$ such that

$$0 \leq |\lambda| - \lambda \tanh\left(\frac{\lambda}{\nu}\right) \leq 0.2785\nu. \quad (7)$$

Lemma 2 ([26]). Define the set $S_{\omega_i} = \{\lambda_i \mid |\lambda_i| < 0.2554\omega_i\}, i = 1, \dots, N$. For $\lambda_i \notin S_{\omega_i}$, the inequality $1 - 16 \tanh^2(\lambda_i/\omega_i) \leq 0$ holds, where $\omega_i > 0$ is a constant.

Lemma 3 ([27]). For the continuous function $F(Z)$ on the compact set Ω_Z , a radial basis function neural network (NN) exists such that

$$F(Z) = (\vartheta^*)^T S(Z) + \varepsilon^*(Z), \forall Z \in \Omega_Z \quad (8)$$

where $\vartheta^* = [\vartheta_1^*, \vartheta_2^*, \dots, \vartheta_N^*]^T$ is the ideal weight vector and $S(Z) = [S_1(Z), S_2(Z), \dots, S_N(Z)]^T$, with $S_i(Z)$ being the Gaussian function. The number of NN nodes is $N > 1$, and ε^* is the bounded approximation error with $|\varepsilon^*| \leq \bar{\varepsilon}$.

Lemma 4. For any constant $\chi > 0$ and any variable $x \in \mathfrak{R}$, the following inequality holds

$$0 \leq |x| - \frac{x^2}{\sqrt{x^2 + \chi^2}} \leq \chi. \quad (9)$$

3. Main Results

In this section, the main results are presented. First, a K-filter is constructed to estimate the unmeasured states. Then, the intermediate design steps are given. Subsequently, a decentralized event-triggered controller is designed. Finally, the system stability is analyzed.

3.1. State Observer Design

To obtain the unmeasurable states, we design a K-filter utilizing the output signal y_i and control signal u_i for the i -th subsystem

$$\dot{\Lambda}_i = A_{ci}\Lambda_i + K_i y_i, \quad (10)$$

$$\dot{\Xi}_i = A_{ci}\Xi_i + \Psi_i(y_i), \quad (11)$$

$$\dot{\xi}_i = A_{ci}\xi_i + B_i v_i, \quad (12)$$

where $K_i = [k_{i,1}, \dots, k_{i,n_i}]^T \in \mathfrak{R}^{n_i}$ such that all the eigenvalues of $A_{ci} = A_i - K_i E_1^T$ are in the open left-half plane; $E_1 = [1, 0, \dots, 0]^T \in \mathfrak{R}^{n_i}$; and v_i is the same as v_i in (2). Then, the state estimate of the i -th subsystem for system (1) can be expressed as

$$\hat{x}_i = \Lambda_i + \Xi_i \theta_i + \aleph_i \xi_i. \quad (13)$$

Remark 1. On the one hand, the K-filter based on actuator failures is constructed to address the coupling problem of unknown states and actuator effectiveness loss. On the other hand, the K-filter updates the state estimates recursively, avoiding redundant calculations and improving computational efficiency.

The observer error is defined as $\tilde{x}_i = [\tilde{x}_{i,1}, \dots, \tilde{x}_{i,n_i}]^T = x_i - \hat{x}_i$. Its derivative is

$$\dot{\tilde{x}}_i = A_{ci}\tilde{x}_i + B_i u_{i,h} + h_i + f_i. \tag{14}$$

For the error system, we consider the following Lyapunov function

$$V_{i,0} = \tilde{x}_i^T P_i \tilde{x}_i, \tag{15}$$

where P_i is a positive definite matrix such that $A_{ci}^T P_i + P_i A_{ci} = -Q_i$, with Q_i being a positive definite matrix to be determined in stability analysis.

Then, taking the time derivative of $V_{i,0}$ along (14), one has

$$\dot{V}_{i,0} = \tilde{x}_i^T (A_{ci}^T P_i + P_i A_{ci}) \tilde{x}_i + 2\tilde{x}_i^T P_i (B_i u_{i,h} + h_i + f_i). \tag{16}$$

Using Young’s inequality, one can obtain the following equalities:

$$2\tilde{x}_i^T P_i B_i u_{i,h} \leq \|P_i\|^2 |\tilde{x}_i|^2 + \bar{u}_{i,h}^2, \tag{17}$$

$$2\tilde{x}_i^T P_i h_i \leq \|P_i\|^2 |\tilde{x}_i|^2 + \|h_i\|^2, \tag{18}$$

$$2\tilde{x}_i^T P_i f_i \leq \|P_i\|^2 |\tilde{x}_i|^2 + \|f_i\|^2. \tag{19}$$

Substituting (17), (18), and (19) into (16) yields

$$\dot{V}_{i,0} \leq -\tilde{x}_i^T (Q_i - 3\|P_i\|^2) \tilde{x}_i + \bar{u}_{i,h}^2 + \|h_i\|^2 + \|f_i\|^2. \tag{20}$$

3.2. Intermediate Design Steps

Let $\Lambda_{i,2}$, $\Xi_{i,2}$, $\zeta_{i,2}$, and $\tilde{x}_{i,2}$ denote the second entries of Λ_i , Ξ_i , ζ_i , and \tilde{x}_i , respectively. Based on the design procedure similar to [28], we have

$$\dot{y}_i = \Lambda_{i,2} + \Xi_{i,2}^T \theta_i + \zeta_{i,2} + \tilde{x}_{i,2} + \Psi_{i,1}^T(y_i) \theta_i + h_{i,1} + f_{i,1}, \tag{21}$$

$$\dot{\zeta}_{i,j} = \zeta_{i,j} - k_{i,j} \zeta_{i,1}, j = 2, \dots, n_i - 1, \tag{22}$$

$$\dot{\zeta}_{i,n_i} = v_i - k_{i,n_i} \zeta_{i,1}, \tag{23}$$

where v_i is the same as v_i in (2).

Then, we formulate the following coordinate changes:

$$z_{i,1} = y_i - y_{i,r}, \tag{24}$$

$$z_{i,j} = \zeta_{i,j} - \zeta_{i,j}, j = 2, \dots, n_i, \tag{25}$$

where $\zeta_{i,j} (j = 2, \dots, n_i)$ represents the output of the first-order low-pass filters. These filters for $i = 1, \dots, N, j = 1, \dots, n_i - 1$ are described as follows:

$$\kappa_{i,j+1} \dot{\zeta}_{i,j+1} = \alpha_{i,j} - \zeta_{i,j+1}, \zeta_{i,j+1}(0) = \alpha_{i,j}(0), \tag{26}$$

where $\kappa_{i,j+1}$ is a design parameter.

Remark 2. In the backstepping control approach, the design of the control law involves the utilization of states as virtual control signals. Each step of the design necessitates both the virtual control signals and their corresponding derivatives. Theoretically, the calculation of the virtual control signal derivatives is simple. However, it can be quite complicated and tedious in applications

when n is greater than three because the control signal α_{i,n_i} will include the derivative of α_{i,n_i-1} , the second derivative of α_{i,n_i-2} , and the third derivative of α_{i,n_i-3} , thereby causing the “explosion of complexity” problem. To address this problem, a dynamic surface control method was proposed in [29–31].

Define the difference between the virtual controller and the first-order low-pass filter as follows:

$$\Pi_{i,j} = \zeta_{i,j} - \alpha_{i,j-1}. \tag{27}$$

Remark 3. According to [32], the boundary layer errors $\zeta_{i,j} - \alpha_{i,j-1}$ will converge asymptotically to zero only if $\kappa_{i,j}$ is very small. Thus, we should set $\kappa_{i,j}$ to a small constant in the simulation example. Additionally, the boundedness of $\zeta_{i,j} - \alpha_{i,j-1}$ is guaranteed by introducing the boundary layer error.

Concerning the unknown parameters, we introduce

$$\beta_{i,1} = \frac{1}{\aleph_i}, \beta_{i,2} = \sup\{\aleph_i^2\}, \tag{28}$$

where $\hat{\beta}_{i,1}$ and $\hat{\beta}_{i,2}$ are the estimations of $\beta_{i,1}$ and $\beta_{i,2}$, respectively. $\tilde{\beta}_{i,1} = \beta_{i,1} - \hat{\beta}_{i,1}$ and $\tilde{\beta}_{i,2} = \beta_{i,2} - \hat{\beta}_{i,2}$ are the corresponding estimation errors.

Step $i, 1$: Based on (21) and (24), one has

$$\dot{z}_{i,1} = \Lambda_{i,2} + \Xi_{i,2}^T \theta_i + \Psi_{i,1}^T \theta_i + \tilde{x}_{i,2} + \aleph_i \zeta_{i,2} + h_{i,1} + f_{i,1} - \dot{y}_{i,r}, \tag{29}$$

Construct the Lyapunov function $V_{i,1}$ as

$$V_{i,1} = V_{i,0} + \frac{1}{2} z_{i,1}^2 + \frac{1}{2} \Pi_{i,2}^2 + \frac{1}{2} \tilde{\theta}_i^T \Gamma_i^{-1} \tilde{\theta}_i + \frac{1}{2} \tilde{\theta}_i^2 + \frac{\aleph_i}{2} \tilde{\beta}_{i,1}^2 + \frac{1}{2} \tilde{\beta}_{i,2}^2, \tag{30}$$

where $\tilde{\theta}_i$ denotes the estimation of θ_i , with $\hat{\theta}_i = \theta_i - \tilde{\theta}_i$, and $\Gamma_i > 0$ is a design parameter.

The time derivative of $V_{i,1}$ can be obtained as follows:

$$\begin{aligned} \dot{V}_{i,1} &= \dot{V}_{i,0} + z_{i,1}(\Lambda_{i,2} + \Omega_i^T \theta_i + \tilde{x}_{i,2} + h_{i,1} + f_{i,1} + \aleph_i(z_{i,2} + \Pi_{i,2} + \alpha_{i,1}) - \dot{y}_{i,r}) \\ &\quad + \Pi_{i,2} \dot{\Pi}_{i,2} - \tilde{\theta}_i^T \Gamma_i^{-1} \dot{\tilde{\theta}}_i - \tilde{\theta}_i^T \dot{\tilde{\theta}}_i - \aleph_i \tilde{\beta}_{i,1} \dot{\hat{\beta}}_{i,1} - \tilde{\beta}_{i,2} \dot{\hat{\beta}}_{i,2} \\ &\leq -\tilde{x}_i^T (Q_i - 3\|P_i\|^2) \tilde{x}_i + \tilde{u}_{i,h}^2 + \|h_i\|^2 + \|f_i\|^2 + z_{i,1}(\Lambda_{i,2} + \Omega_i^T \theta_i + \tilde{x}_{i,2} \\ &\quad + h_{i,1} + f_{i,1} + \aleph_i(z_{i,2} + \Pi_{i,2} + \alpha_{i,1}) - \dot{y}_{i,r}) + \Pi_{i,2} \dot{\Pi}_{i,2} - \tilde{\theta}_i^T \Gamma_i^{-1} \dot{\tilde{\theta}}_i - \tilde{\theta}_i^T \dot{\tilde{\theta}}_i \\ &\quad - \aleph_i \tilde{\beta}_{i,1} \dot{\hat{\beta}}_{i,1} - \tilde{\beta}_{i,2} \dot{\hat{\beta}}_{i,2}, \end{aligned} \tag{31}$$

where $\Omega_i = \Xi_{i,2} + \Psi_{i,1}$.

According to Young’s inequality and Assumption 2, one has

$$\|h_i\|^2 \leq \sum_{\gamma=1}^N \sum_{j=1}^{n_i} (y_\gamma h_{i,j,\gamma}(y_\gamma))^2 \leq y_i^2 \sum_{\gamma=1}^N \sum_{j=1}^{n_i} (\tilde{h}_{i,j,\gamma}(y_i))^2, \tag{32}$$

$$\begin{aligned} z_{i,1} h_{i,1} &\leq \frac{1}{2} z_{i,1}^2 + \frac{1}{2} \|h_{i,1}\|^2 \leq \frac{1}{2} z_{i,1}^2 + \frac{1}{2} \sum_{\gamma=1}^N (y_\gamma h_{i,1,\gamma}(y_\gamma))^2 \\ &\leq \frac{1}{2} z_{i,1}^2 + \frac{1}{2} y_i^2 \sum_{\gamma=1}^N (\tilde{h}_{i,1,\gamma}(y_i))^2, \end{aligned} \tag{33}$$

where $\tilde{h}_{i,j,\gamma}$ for $j = 1, \dots, n_i$ are smooth nonlinear functions.

Then, one can have

$$\begin{aligned} \dot{V}_{i,1} \leq & -\tilde{x}_i^T \left(Q_i - 3\|P_i\|^2 \right) \tilde{x}_i + \bar{u}_{i,h}^2 + \|f_i\|^2 + \frac{1}{2}z_{i,1}^2 + \Pi_{i,2}\dot{\Gamma}_{i,2} + z_{i,1}(\Lambda_{i,2} + \Omega_i^T\theta_i \\ & + \tilde{x}_{i,2} + f_{i,1} + \aleph_i(z_{i,2} + \Pi_{i,2} + \alpha_{i,1}) - \dot{y}_{i,r}) - \tilde{\theta}_i^T \Gamma_i^{-1} \dot{\hat{\theta}}_i + y_i^2 \sum_{\gamma=1}^N \sum_{j=1}^{n_i} (\tilde{h}_{i,j,\gamma}(y_i))^2 \\ & + \frac{1}{2}y_i^2 \sum_{\gamma=1}^N (\tilde{h}_{i,1,\gamma}(y_i))^2 - \tilde{\theta}_i^T \hat{\theta}_i - \aleph_i \tilde{\beta}_{i,1} \hat{\beta}_{i,1} - \tilde{\beta}_{i,2} \hat{\beta}_{i,2}. \end{aligned} \tag{34}$$

Choose the Lyapunov candidate function as

$$V_{i,\tau} = \frac{3a_{i,1,2}e^{\lambda_i \bar{m}_{i,1}}}{2(1 - m_{i,1}^*)} \int_{t-m_{i,1}(t)}^t c_{i,1}(s)ds + \sum_{j=2}^{n_i} \frac{a_{i,j,2}e^{\lambda_i \bar{m}_{i,j}}}{1 - m_{i,j}^*} \int_{t-m_{i,j}(t)}^t c_{i,j}(s)ds, \tag{35}$$

where $c_{i,j}(s) = e^{-\lambda_i(t-s)}z_{i,1}(s)f_{i,j,2}^*(z_{i,1}(s))$ and λ_i is a design parameter, whose time derivative is

$$\begin{aligned} \dot{V}_{i,\tau} \leq & -\lambda_i V_{i,\tau} + \frac{3a_{i,1,2}e^{\lambda_i \bar{m}_{i,1}}}{2(1 - m_{i,1}^*)} z_{i,1}(t)f_{i,1,2}^*(z_{i,1}(t)) - \frac{3}{2}a_{i,1,2}z_{i,1}(t_{i,1}^m)f_{i,1,2}^*(z_{i,1}(t_{i,1}^m)) \\ & + \sum_{j=2}^{n_i} \frac{a_{i,j,2}e^{\lambda_i \bar{m}_{i,j}}}{1 - m_{i,j}^*} z_{i,1}f_{i,j,2}^*(z_{i,1}(t)) - \sum_{j=2}^{n_i} a_{i,j,2}z_{i,1}(t_{i,j}^m)f_{i,j,2}^*(z_{i,1}(t_{i,j}^m)), \end{aligned} \tag{36}$$

where we define $t_{i,j}^m = t - m_{i,j}(t)$.

Let $W_{i,1} = V_{i,1} + V_{1,\tau}$. Then, the derivative of $W_{i,1}$ can be obtained as follows:

$$\begin{aligned} \dot{W}_{i,1} \leq & -\tilde{x}_i^T \left(Q_i - 3\|P_i\|^2 \right) \tilde{x}_i + \bar{u}_{i,h}^2 + \|f_i\|^2 + \frac{1}{2}z_{i,1}^2 + \Pi_{i,2}\dot{\Gamma}_{i,2} + z_{i,1}(\Lambda_{i,2} + \Omega_i^T\theta_i \\ & + \tilde{x}_{i,2} + f_{i,1} + \aleph_i(z_{i,2} + \Pi_{i,2} + \alpha_{i,1}) + \frac{16}{z_{i,1}} \tanh^2\left(\frac{z_{i,1}}{\omega_i}\right) G_i - \dot{y}_{i,r}) \\ & + \left(1 - 16 \tanh^2\left(\frac{z_{i,1}}{\omega_i}\right) \right) G_i - \tilde{\theta}_i^T \Gamma_i^{-1} \dot{\hat{\theta}}_i - \tilde{\theta}_i^T \hat{\theta}_i - \aleph_i \tilde{\beta}_{i,1} \hat{\beta}_{i,1} - \tilde{\beta}_{i,2} \hat{\beta}_{i,2} - \lambda_i V_{i,\tau} \\ & + \frac{3a_{i,1,2}e^{\lambda_i \bar{m}_{i,1}}}{2(1 - m_{i,1}^*)} z_{i,1}(t)f_{i,1,2}^*(z_{i,1}(t)) - \frac{3}{2}a_{i,1,2}z_{i,1}(t_{i,1}^m)f_{i,1,2}^*(z_{i,1}(t_{i,1}^m)) \\ & + \sum_{j=2}^{n_i} \frac{a_{i,j,2}e^{\lambda_i \bar{m}_{i,j}}}{1 - m_{i,j}^*} z_{i,1}f_{i,j,2}^*(z_{i,1}(t)) - \sum_{j=2}^{n_i} a_{i,j,2}z_{i,1}(t_{i,j}^m)f_{i,j,2}^*(z_{i,1}(t_{i,j}^m)). \end{aligned} \tag{37}$$

where $G_i = \frac{1}{2} \sum_{\gamma=1}^N (y_i \tilde{h}_{i,1,\gamma}(y_i))^2 + \sum_{\gamma=1}^N \sum_{j=1}^{n_i} (y_i \tilde{h}_{i,j,\gamma}(y_i))^2$.

Next, the unknown nonlinear delay functions and interconnection terms in the Lyapunov function $W_{i,1}$ are approximated using NNs.

According to Assumption 3 and Young’s inequality, one has

$$\begin{aligned}
z_{i,1}f_{i,1} &\leq \frac{1}{2}z_{i,1}^2 + \frac{1}{2}f_{i,1}^2 \\
&\leq \frac{1}{2}z_{i,1}^2 + \frac{1}{2}a_{i,1,1}z_{i,1}(t)f_{i,1,1}^*(z_{i,1}(t)) + \frac{1}{2}a_{i,1,1}\eta_{i,1,1}(y_{i,r}(t)) \\
&\quad + \frac{1}{2}a_{i,1,2}\eta_{i,1,2}(y_{i,r}(t_{i,1}^m)) + \frac{1}{2}a_{i,1,2}z_{i,1}(t_{i,1}^m)f_{i,1,2}^*(z_{i,1}(t_{i,1}^m)), \quad (38)
\end{aligned}$$

$$\begin{aligned}
\|f_i\|^2 &\leq \sum_{j=1}^{n_i} (a_{i,j,1}z_{i,1}(t)f_{i,j,1}^*(z_{i,1}(t)) + a_{i,j,1}\eta_{i,j,1}(y_{i,r}(t)) \\
&\quad + a_{i,j,2}z_{i,1}(t_{i,j}^m)f_{i,j,2}^*(z_{i,1}(t_{i,j}^m)) + a_{i,j,2}\eta_{i,j,2}(y_{i,r}(t_{i,j}^m))). \quad (39)
\end{aligned}$$

Let $F(Z_i) = \frac{3}{2}a_{i,1,1}f_{i,1,1}^*(z_{i,1}(t)) + \frac{3a_{i,1,2}e^{\lambda_i m_{i,1}}}{2(1-m_{i,1}^*)}f_{i,1,2}^*(z_{i,1}(t)) + \sum_{j=2}^{n_i} \frac{a_{i,j,2}e^{\lambda_i m_{i,j}}}{1-m_{i,j}^*}f_{i,j,2}^*(z_{i,1}(t)) + \sum_{j=2}^{n_i} a_{i,j,1}f_{i,j,1}^*(z_{i,1}(t)) + \frac{16}{z_{i,1}}\tanh^2(\frac{z_{i,1}}{\varpi_i}))G_i$. According to Lemma 3, we can obtain $F(Z_i) = \vartheta_i^T S_i(Z_i) + \varepsilon_i$, where $Z_i = z_{i,1}$.

Remark 4. According to Assumptions 2 and 3, both the interconnected nonlinear function and the time-vary nonlinear function can be represented by smooth functions about y_i . Therefore, in this paper, we choose to eliminate the influence of the interconnected nonlinear function and time-varying nonlinear function in the first step related to y_i and approximate the nonlinear function using NNs.

Using Young's inequality, one has

$$z_{i,1}\tilde{x}_{i,2} \leq \frac{1}{2}z_{i,1}^2 + \frac{1}{2}\|x_i\|^2, \quad (40)$$

$$\aleph_{iz_{i,1}}(z_{i,2} + \Pi_{i,2}) \leq \frac{3}{2}\beta_{i,2}z_{i,1}^2 + \frac{1}{4}z_{i,2}^2 + \frac{1}{2}\Pi_{i,2}^2, \quad (41)$$

$$z_{i,1}F(Z_i) \leq z_{i,1}\vartheta_i^T S_i(Z_i) + \frac{1}{2}z_{i,1}^2 + \frac{1}{2}\varepsilon_i^2. \quad (42)$$

Construct the stabilizing function as follows:

$$\alpha_{i,1} = -\frac{z_{i,1}\hat{\beta}_{i,1}^2\bar{\alpha}_{i,1}^2}{\sqrt{z_{i,1}^2\hat{\beta}_{i,1}^2\bar{\alpha}_{i,1}^2 + \chi_i^2}}, \quad (43)$$

where χ_i is a positive design parameter. With the aid of Lemma 4, we obtain

$$\aleph_{iz_{i,1}}\alpha_{i,1} = -\frac{\aleph_{iz_{i,1}}z_{i,1}^2\hat{\beta}_{i,1}^2\bar{\alpha}_{i,1}^2}{\sqrt{z_{i,1}^2\hat{\beta}_{i,1}^2\bar{\alpha}_{i,1}^2 + \chi_i^2}} \leq -\aleph_{iz_{i,1}}\hat{\beta}_{i,1}\bar{\alpha}_{i,1} + \aleph_i\chi_i. \quad (44)$$

Choose the virtual control signal and adaptive laws as follows:

$$\bar{\alpha}_{i,1} = d_{i,1}z_{i,1} + 2z_{i,1} + \Lambda_{i,2} - \dot{y}_{i,r} + \Omega_i^T\hat{\theta}_i + \frac{3}{2}\hat{\beta}_{i,2}z_{i,1} + \hat{\vartheta}_i^T S_i(Z_i), \quad (45)$$

$$\hat{\theta}_i = \Gamma_i\Omega_i z_{i,1} - \varsigma_i\Gamma_i\hat{\theta}_i, \quad (46)$$

$$\dot{\hat{\vartheta}}_i = -\hat{\vartheta}_i + z_{i,1}S_i(Z_i), \quad (47)$$

$$\dot{\hat{\beta}}_{i,1} = z_{i,1}\bar{\alpha}_{i,1} - \hat{\beta}_{i,1}, \quad (48)$$

$$\dot{\hat{\beta}}_{i,2} = \frac{3}{2}z_{i,1}^2 - \hat{\beta}_{i,2}, \quad (49)$$

where $\varsigma_i > 0$ is a design parameter.

Remark 5. The K -filter based on actuator failures is constructed, which draws attention to the effect of actuator failures when constructing the $i, 1$ -th virtual controller. This makes it difficult for

us to construct a virtual controller. The stabilizing function and an adaptive law $\beta_{i,1}$ are introduced to address the problem of actuator failures.

The dynamics of the boundary layer error are given as follows:

$$\dot{\Pi}_{i,2} = -\frac{\Pi_{i,2}}{\kappa_{i,2}} + M_{i,2}, \tag{50}$$

where $M_{i,2}$ is a positive design parameter.

Substituting (38)–(50) into (37), one has

$$\begin{aligned} W_{i,1} \leq & -\tilde{x}_i^T(Q_i - 3\|P_i\|^2 - \frac{1}{2})\tilde{x}_i + \tilde{u}_{i,h}^2 - \frac{\Pi_{i,2}^2}{\kappa_{i,2}} + \frac{1}{2}\Pi_{i,2}^2 + M_{i,2}\Pi_{i,2} - d_{i,1}z_{i,1}^2 + \aleph_i\chi_i \\ & + \varsigma_i\tilde{\theta}_i^T\hat{\theta}_i + \tilde{\theta}_i^T\hat{\theta}_i + \aleph_i\tilde{\beta}_{i,1}\hat{\beta}_{i,1} + \tilde{\beta}_{i,2}\hat{\beta}_{i,2} - \lambda_i V_{i,\tau} + \frac{1}{2}\epsilon_i^2 + \frac{1}{4}z_{i,2}^2 + \frac{3}{2}a_{i,1,1}\eta_{i,1,1}(y_{i,r}(t)) \\ & + \frac{3}{2}a_{i,1,2}\eta_{i,1,2}(y_{i,r}(t_{i,1}^m)) + \sum_{j=2}^{n_i} (a_{i,j,1}\eta_{i,j,1}(y_{i,r}(t)) + a_{i,j,2}\eta_{i,j,2}(y_{i,r}(t_{i,j}^m))) \\ & + (1 - 16\tanh^2(\frac{z_{i,1}}{\omega_i}))G_i. \end{aligned} \tag{51}$$

Step i, j : Based on (22) and (25), one has

$$\dot{z}_{i,j} = z_{i,j+1} + \Pi_{i,j+1} + \alpha_{i,j} - k_{i,j}\zeta_{i,1} - \dot{\zeta}_{i,j}. \tag{52}$$

Construct the Lyapunov function $V_{i,j}$ as follows:

$$V_{i,j} = \frac{1}{2}z_{i,j}^2 + \frac{1}{2}\Pi_{i,j+1}^2, \tag{53}$$

and in view of (52), differentiating $V_{i,j}$ yields

$$\dot{V}_{i,j} = z_{i,j}(z_{i,j+1} + \Pi_{i,j+1} + \alpha_{i,j} - k_{i,j}\zeta_{i,1} - \dot{\zeta}_{i,j}) + \Pi_{i,j+1}\dot{\Pi}_{i,j+1}, \tag{54}$$

Choose the virtual control law and the dynamics of the boundary layer error as follows:

$$\alpha_{i,j} = -d_{i,j}z_{i,j} - c_{i,j}z_{i,j} + k_{i,j}\zeta_{i,1} + \dot{\zeta}_{i,j}, \tag{55}$$

$$\dot{\Pi}_{i,j+1} = -\frac{\Pi_{i,j+1}}{\kappa_{i,j+1}} + M_{i,j+1}. \tag{56}$$

Substituting (55) and (56) into (54), one has

$$\dot{V}_{i,j} \leq -d_{i,j}z_{i,j}^2 - (c_{i,j} - 1)z_{i,j}^2 + \frac{1}{2}z_{i,j+1}^2 - \frac{\Pi_{i,j+1}^2}{\kappa_{i,j+1}} + \frac{1}{2}\Pi_{i,j+1}^2 + M_{i,j+1}\Pi_{i,j+1}. \tag{57}$$

Step i, n_i : Based on (23) and (25), one has

$$\dot{z}_{i,n_i} = v_i - k_{i,n_i}\zeta_{i,1} - \dot{\zeta}_{i,n_i}, \tag{58}$$

where v_i is the same as v_i in (2).

Construct the Lyapunov function V_{i,n_i} as

$$V_{i,n_i} = \frac{1}{2}z_{i,n_i}^2 + \frac{1}{2}\tilde{\Phi}_i^2, \tag{59}$$

where $\tilde{\Phi}_i = \Phi_i - \hat{\Phi}_i$, with $\hat{\Phi}_i$ being the estimation of $\Phi_i = \sup_{t \geq 0} \left| \frac{\tau_{i,2}(t)\phi_i}{1 + \tau_{i,1}(t)\delta_i} \right|$.

According to (58) and (59), differentiating V_{i,n_i} yields

$$\dot{V}_{i,n_i} = z_{i,n_i}(v_i - k_{i,n_i}\xi_{i,1} - \dot{\zeta}_{i,n_i}) - \tilde{\Phi}_i \dot{\hat{\Phi}}_i. \tag{60}$$

Choose the virtual control law as follows:

$$\alpha_{i,n_i} = -d_{i,n_i}z_{i,n_i} - c_{i,n_i}z_{i,n_i} + k_{i,n_i}\xi_{i,1} + \dot{\zeta}_{i,n_i}. \tag{61}$$

Substituting (61) into (60), one has

$$\begin{aligned} \dot{V}_{i,n_i} &\leq -d_{i,n_i}z_{i,n_i}^2 - c_{i,n_i}z_{i,n_i}^2 + z_{i,n_i}(v_i - \alpha_{i,n_i}) \\ &\quad - \tilde{\Phi}_i \dot{\hat{\Phi}}_i. \end{aligned} \tag{62}$$

3.3. Event-Triggered Controller

In this section, an event-triggered controller is designed to stabilize interconnected nonlinear delay systems with actuator failures. On the premise of maintaining system performance, unnecessary communication resources are reduced.

The local actual control law and event-triggered mechanism are designed as follows:

$$v_i(t) = \omega_i(t_{i,k}), \forall t \in [t_{i,k}, t_{i,k+1}) \tag{63}$$

$$t_{i,k+1} = \inf\{t > t_{i,k+1} \mid |e_i(t)| \geq \delta_i |v_i(t)| + \phi_i\}, \tag{64}$$

where $\omega_i = \omega_i(t)$ is an intermediate continuous control law, which is given later; $e_i(t) = \omega_i(t) - v_i(t)$ denotes the measurement error; and $\delta_i (0 < \delta_i < 1)$ and $\phi_i > 0$ are design parameters.

According to the above event-triggered mechanism, $|\omega_i(t) - v_i(t)| \leq \delta_i |v_i(t)| + \phi_i$ holds all the time. When $\tau_{i,1}(t)$ and $\tau_{i,2}(t)$ satisfy $|\tau_{i,1}(t)| \leq 1$ and $|\tau_{i,2}(t)| \leq 1$, respectively, we obtain

$$v_i(t) = \frac{\omega_i(t)}{1 + \tau_{i,1}(t)\delta_i} - \frac{\tau_{i,2}(t)\phi_i}{1 + \tau_{i,1}(t)\delta_i}, \tag{65}$$

with $\tau_{i,1}(t)$ and $\tau_{i,2}(t)$ satisfying

$$\begin{cases} \tau_{i,1}(t) = \tau_{i,2}(t) = \tau_i(t), v_i(t) \geq 0, \\ \tau_{i,1}(t) = \tau_i(t), \tau_{i,2}(t) = -\tau_i(t), v_i(t) < 0, \end{cases} \tag{66}$$

where $\tau_i(t)$ is any number in $[-1, 1]$.

The control protocol and adaptive law are designed as follows:

$$\omega_i(t) = -(1 + \delta_i) \left(\alpha_{i,n_i} \tanh\left(\frac{z_{i,n_i}\alpha_{i,n_i}}{v_i}\right) + \hat{\Phi}_i \tanh\left(\frac{z_{i,n_i}\hat{\Phi}_i}{v_i}\right) \right), \tag{67}$$

$$\dot{\hat{\Phi}}_i = |z_{i,n_i}| - \hat{\Phi}_i. \tag{68}$$

3.4. Stability Analysis and Avoidance of Zeno Behavior

For the stability analysis, we choose the total Lyapunov function V as $V = \sum_{i=1}^N (W_{i,1} + \sum_{j=2}^{n_i} V_{i,j})$.

Theorem 1. Consider a closed-loop system consisting of interconnected nonlinear systems (1); actuator failures (2); the K-filter (10)–(12); the adaptive controller designed in (45), (55), (61), and (67); and the event-triggered mechanisms (63)–(64). Then, all the signals in the closed-loop system are SGUUB, and the tracking error can converge to a small neighborhood of zero. Additionally, Zeno behavior can be effectively avoided.

Proof of Theorem 1. As $|\tau_{i,1}(t)| \leq 1$, then $1 - \delta_i \leq 1 + \tau_{i,1}(t)\delta_i \leq 1 + \delta_i$ and $\frac{1+\delta_i}{1+\tau_{i,1}(t)\delta_i} \geq 1$. Since $z_{i,n_i}\alpha_{i,n_i} \tanh(\frac{z_{i,n_i}\alpha_{i,n_i}}{v_i}) > 0$ and $z_{i,n_i}\hat{\Phi}_i \tanh(\frac{z_{i,n_i}\hat{\Phi}_i}{v_i}) > 0$, one has

$$\frac{z_{i,n_i}\omega_i(t)}{1 + \tau_{i,1}(t)\delta_i} \leq -z_{i,n_i}\alpha_{i,n_i} \tanh(\frac{z_{i,n_i}\alpha_{i,n_i}}{v_i}) - z_{i,n_i}\hat{\Phi}_i \tanh(\frac{z_{i,n_i}\hat{\Phi}_i}{v_i}). \tag{69}$$

According to Lemma 1, the following inequality can be obtained:

$$\frac{z_{i,n_i}\omega_i(t)}{1 + \tau_{i,1}(t)} \leq -|z_{i,n_i}\alpha_{i,n_i}| - |z_{i,n_i}|\hat{\Phi}_i + 0.557v_i, \tag{70}$$

Substituting (65) and (70) into (62), we can obtain

$$\begin{aligned} \dot{V}_{i,n_i} &\leq -d_{i,n_i}z_{i,n_i}^2 - c_{i,n_i}z_{i,n_i}^2 - |z_{i,n_i}\alpha_{i,n_i}| - |z_{i,n_i}|\hat{\Phi}_i - \frac{z_{i,n_i}\tau_{i,2}(t)\phi_i}{1 + \tau_{i,1}(t)\delta_i} - z_{i,n_i}\alpha_{i,n_i} \\ &\quad - \tilde{\Phi}_i(|z_{i,n_i}| - \hat{\Phi}_i) + 0.557v_i \\ &\leq -d_{i,n_i}z_{i,n_i}^2 - c_{i,n_i}z_{i,n_i}^2 + \tilde{\Phi}_i\hat{\Phi}_i + 0.557v_i. \end{aligned} \tag{71}$$

According to (51), (57), and (71), differentiating V yields

$$\begin{aligned} \dot{V} &\leq \sum_{i=1}^N (-\tilde{x}_i^T(Q_i - 3\|P_i\|^2 - \frac{1}{2})\tilde{x}_i + \tilde{u}_{i,h}^2 - \sum_{j=2}^{n_i} (\frac{\Pi_{i,j}^2}{\kappa_{i,j}} - \frac{1}{2}\Pi_{i,j}^2 - M_{i,j}\Pi_{i,j}) - \sum_{j=1}^{n_i} d_{i,j}z_{i,j}^2 \\ &\quad + \aleph_i\chi_i + \varsigma_i\tilde{\theta}_i^T\hat{\theta}_i + \tilde{\theta}_i^T\hat{\theta}_i + \aleph_i\tilde{\beta}_{i,1}\hat{\beta}_{i,1} + \tilde{\beta}_{i,2}\hat{\beta}_{i,2} + \tilde{\Phi}_i\hat{\Phi}_i - \lambda_i V_{i,\tau} + 0.557v_i + \frac{1}{2}\tilde{\epsilon}_i^2 \\ &\quad - (c_{i,2} - \frac{5}{4})z_{i,2}^2 - \sum_{j=3}^{n_i-1} (c_{i,j} - \frac{3}{2})z_{i,j}^2 - (c_{i,n_i} - \frac{1}{2})z_{i,n_i}^2 + \frac{3}{2}a_{i,1,1}\eta_{i,1,1}(y_{i,r}(t)) \\ &\quad + \frac{3}{2}a_{i,1,2}\eta_{i,1,2}(y_{i,r}(t_{i,1}^m)) + \sum_{j=2}^{n_i} (a_{i,j,1}\eta_{i,j,1}(y_{i,r}(t)) + a_{i,j,2}\eta_{i,j,2}(y_{i,r}(t_{i,j}^m))) \\ &\quad + (1 - 16\tanh^2(\frac{z_{i,1}}{\omega_i}))G_i). \end{aligned} \tag{72}$$

The following inequalities are established by choosing an appropriate positive definite matrix Q_i , $\kappa_{i,j}$, and $c_{i,j}$ for $j = 2, \dots, n_i$

$$\begin{aligned} -\tilde{x}_i^T(Q_i - 3\|P_i\|^2 - \frac{1}{2})\tilde{x}_i &\leq -\lambda_{\min}(Q_i - 3\|P_i\|^2 - \frac{1}{2})\|x_i\|^2 \\ &\leq -\bar{\mu}_i\|x_i\|^2, \end{aligned} \tag{73}$$

$$\begin{aligned} -(\frac{\Pi_{i,j}^2}{\kappa_{i,j}} - \frac{1}{2}\Pi_{i,j}^2 - M_{i,j}\Pi_{i,j}) &\leq -(\frac{1}{\kappa_{i,j}} - 1)\Pi_{i,j}^2 + \frac{1}{2}M_{i,j}^2 \\ &\leq -l_{i,j}\Pi_{i,j}^2 + \frac{1}{2}M_{i,j}^2, \end{aligned} \tag{74}$$

where $\bar{\mu}_i > 0$ and $l_{i,j} > 0$ are parameters, and $c_{i,2} > \frac{5}{4}$, $c_{i,j} > \frac{3}{2}$, and $c_{i,n_i} > \frac{1}{2}$.

According to Lemma 2, $(1 - 16\tanh^2(\frac{z_{i,1}}{\omega_i}))G_i \leq 0$ for $z_{i,1} \notin S_{\omega_i}$; For $z_{i,1} \in S_{\omega_i}$, $(1 - 16\tanh^2(\frac{z_{i,1}}{\omega_i}))G_i \leq \bar{Y}_i^*$ with $\bar{Y}_i^* > 0$ being a constant. In conclusion, for convenience, $(1 - 16\tanh^2(\frac{z_{i,1}}{\omega_i}))G_i \leq \bar{Y}_i$ with $\bar{Y}_i \geq \bar{Y}_i^* \geq 0$ for $z_{i,1} \in \mathfrak{R}$.

Then, adopting Young’s inequalities yields

$$\begin{aligned} \dot{V} &\leq \sum_{i=1}^N (-\bar{\mu}_i \|x_i\|^2 - \sum_{j=1}^{n_i} d_{i,j} z_{i,j}^2 - \sum_{j=2}^{n_i} l_{i,j} \Pi_{i,j} - \frac{\zeta_i}{2} \tilde{\theta}_i^T \tilde{\theta}_i - \frac{1}{2} \tilde{\theta}_i^T \tilde{\theta}_i - \frac{\aleph_i}{2} \tilde{\beta}_{i,1}^2 - \frac{1}{2} \tilde{\beta}_{i,2}^2 \\ &\quad - \frac{1}{2} \Phi_i^2 - \lambda_i V_{i,\tau} + \Delta_i) \\ &\leq -cV + \bar{\Delta}, \end{aligned} \tag{75}$$

where $\Delta_i = \bar{u}_{i,h}^2 + \sum_{j=2}^{n_i} M_{i,j}^2 + \aleph_i \chi_i + \frac{\zeta_i}{2} \hat{\theta}_i^T \hat{\theta}_i + \frac{1}{2} \hat{\theta}_i^T \hat{\theta}_i + \frac{\aleph_i}{2} \hat{\beta}_{i,1}^2 + \frac{1}{2} \hat{\beta}_{i,2}^2 + \frac{1}{2} \Phi_i^2 + \frac{1}{2} \bar{\epsilon}_i^2 + 0.557\nu_i + \frac{3}{2} a_{i,1,1} \eta_{i,1,1}(y_{i,r}(t)) + \frac{3}{2} a_{i,1,2} \eta_{i,1,2}(y_{i,r}(t_{i,1}^m)) + \sum_{j=2}^{n_i} (a_{i,j,1} \eta_{i,j,1}(y_{i,r}(t)) + a_{i,j,2} \eta_{i,j,2}(y_{i,r}(t_{i,j}^m))) + \bar{Y}_i$, $c = \min\{\bar{\mu}_i, d_{i,j}, l_{i,j}, \frac{\zeta_i}{\Gamma_i}, \lambda_i, i = 1, \dots, N, j = 1, \dots, n_i\}$, and $\bar{\Delta} = \sum_{i=1}^N \Delta_i$. Therefore, following a similar analysis to [21], all the closed-loop signals are SGUUB.

From (75), we obtain that $V(t) \leq e^{-ct} V(0) + (\bar{\Delta}/c) \times (1 - e^{-ct})$. As a result, $z_{i,j}$, $\hat{\theta}_i$, $\hat{\beta}_{i,1}$, and $\hat{\beta}_{i,2}$ are also bounded.

As $z_{i,1} = y_i - y_{i,r}$, $z_{i,1}$ and $y_{i,r}$ is bounded, y_i is bounded. Since A_{ci} is Hurwitz, Λ_i and Ξ_i are bounded. From the backstepping procedure, $\alpha_{i,j}$ and u_i are bounded. By following a similar analysis to [33], system (1) is rephrased as

$$\dot{x}_i = A_{ci} x_i + \Psi_i(y_i) \theta_i + B_i u_i + h_i(y_1, \dots, y_N, t) + K_i y_i. \tag{76}$$

Because y_i and u_i are bounded and A_{ci} is Hurwitz, x_i is bounded. As a result, all the closed-loop signals are bounded.

Now, we show that the proposed controller can avoid Zeno behavior, i.e., for the i -th subsystem, there exists a positive number t_i^* such that $\{t_{i,k+1} - t_{i,k}\} \geq t_i^* (k \in \mathbb{R}^+)$. Since $e_i(t) = \omega_i(t) - v_i(t), \forall t \in [t_{i,k}, t_{i,k+1})$, one has

$$\frac{d}{dt} |e_i| = \frac{d}{dt} (e_i * e_i)^{\frac{1}{2}} = \text{sign}(e_i) \dot{e}_i \leq |\omega_i|. \tag{77}$$

From (61) and (67), ω_i is differentiable, and $\dot{\omega}_i$ is a function consisting of all the bounded closed-loop signals. Therefore, there exists a constant $\ell_i > 0$ such that $|\omega_i| \leq \ell_i$. Since $e_i(t_{i,k}) = 0$ and $\lim_{t \rightarrow t_{i,k+1}} e_i(t) = \phi_i$, it is obtained that the lower bound of t_i^* must satisfy $t_i^* \geq \frac{\phi_i}{\ell_i}$. Therefore, Zeno behavior is avoided. \square

4. Simulation Example

In this section, a simulation example is provided to verify the theoretical result. We consider interconnected nonlinear delay systems with actuator failures. The system model is given by

$$\begin{cases} \dot{x}_{1,1} = x_{1,2} + \Psi_{1,1} \theta_1 + h_{1,1} + f_{1,1}, \\ \dot{x}_{1,2} = u_1 + \Psi_{1,2} \theta_1 + f_{1,2}, \\ y_1 = x_{1,1}, \\ \dot{x}_{2,1} = x_{2,2} + \Psi_{2,1} \theta_2 + h_{2,1} + f_{2,1}, \\ \dot{x}_{2,2} = u_2 + \Psi_{2,2} \theta_2 + f_{2,2}, \\ y_2 = x_{2,1}, \end{cases} \tag{78}$$

where θ_1 and θ_2 are unknown constants, but they are set as $\theta_1 = 1$ and $\theta_2 = 1$.

The nonlinear functions in (78) are given as $\Psi_{1,1} = 0.2 \sin(x_{1,1}^2), \Psi_{1,2} = 0.15x_{1,1}^2, \Psi_{2,1} = 0.2 \cos(x_{2,1}^2), \Psi_{2,2} = 0.15x_{2,1} \sin(x_{2,1}), h_{1,1} = 0.1 \sin(x_{1,1}) \cos(x_{2,1}), h_{2,1} = 0.2 \sin(x_{1,1}^2 x_{2,1}), f_{1,1} = 0.3 \sin(x_{1,1}^2(t - m_{1,1}(t))), f_{1,2} = 0.2x_{1,1}(t - m_1(t)) \sin(x_{1,1}x_{1,1}(t - m_{1,2}(t))), f_{2,1} = 0.15 \cos(x_{2,1}(t - m_{2,1}(t))),$ and $f_{2,2} = 0.2x_{2,1}^2(t - m_{2,2}(t))$, where $m_{1,1}(t) = m_{1,2}(t) = m_{2,1}(t) = m_{2,2}(t) = 0.1(1 + \sin(t))$ are the time-varying delay functions.

The initial values of the variables are given as $x_{1,1} = 0.1, x_{1,2} = 0.2, x_{2,1} = 0.1, x_{2,2} = 0.2, \hat{\theta}_1 = 1.2, \hat{\theta}_2 = 1.2, [\Lambda_{1,1}, \Lambda_{1,2}, \Lambda_{2,1}, \Lambda_{2,2}] = [0, 0, 0, 0], [\Xi_{1,1}, \Xi_{1,2}, \Xi_{2,1}, \Xi_{2,2}] = [0, 0, 0, 0], [\zeta_{1,1}, \zeta_{1,2}, \zeta_{2,1}, \zeta_{2,2}] = [0, 0, 0, 0], \vartheta_1 = \vartheta_2 = [0, \dots, 0]^T, \hat{\beta}_{1,1} = \hat{\beta}_{1,2} = \hat{\beta}_{2,1} = \hat{\beta}_{2,2} = 1, \zeta_{1,2} = \zeta_{2,2} = 0, \text{ and } \hat{\Phi}_1 = \hat{\Phi}_2 = 0$. Then, $S_i(Z_i) = [\mu_{F_{i,1}}, \dots, \mu_{F_{i,\sigma}}]^T$ is the basis function vector, with $\mu_{F_{i,\sigma}}$ being the Gaussian function in the following form:

$$\mu_{F_{i,\sigma}} = e^{-0.25(Z_i - 5 + \sigma)^2}, \sigma = 1, \dots, 9, i = 1, 2, \tag{79}$$

where σ is the center of the neural network. The desired trajectory signal of each subsystem is chosen as $y_{i,r} = 2 \sin(0.5t), i = 1, 2$.

The design parameters are $k_{1,1} = 20, k_{1,2} = 10, k_{2,1} = 17, k_{2,2} = 10, \kappa_{1,1} = 0.1, \kappa_{2,1} = 0.1, d_{1,1} = 45, d_{1,2} = 45, d_{2,1} = 45, d_{2,2} = 45, v_1 = 1.2, v_2 = 1.5, \varsigma_1 = 2, \varsigma_2 = 2, \chi_1 = 0.01, \chi_2 = 0.01, M_{1,2} = 1, \text{ and } M_{2,2} = 1$.

Actuator 1 with loss of effectiveness is described as $u_1(t) = 0.6v_1(t), t > 7$ s, and actuator 2 with loss of effectiveness and bias faults is described as $u_2(t) = 0.8v_2(t) + 0.5, t > 12$ s. Based on the above analysis, the verification results are given in Figures 1–5. The output of the two subsystems is given in Figures 1 and 2. Figures 3 and 4 depict the input and output signals of the two actuators. It is worth noting that the moment when the actuator failure occurred is marked with *. The time intervals of the triggering events are shown in Figure 5. Obviously, all the closed-loop signals are bounded and Zeno behavior is avoided.

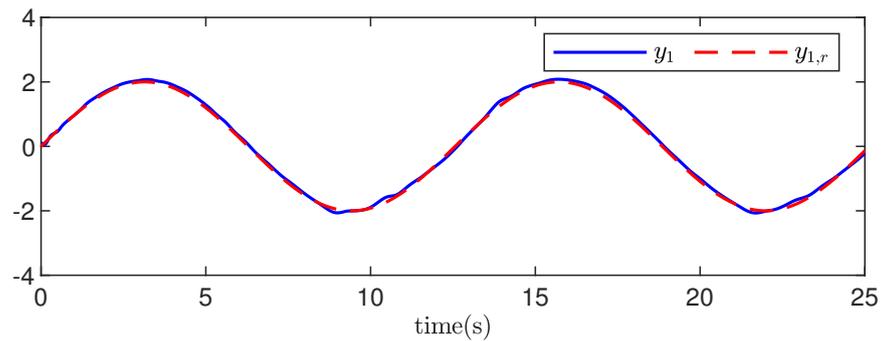


Figure 1. The output of the first subsystem.

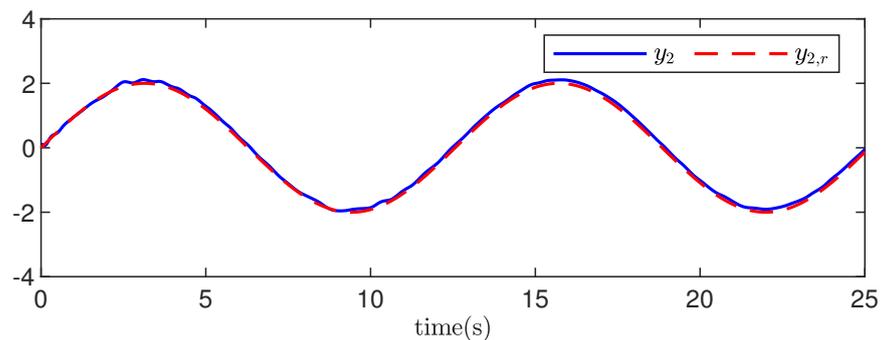


Figure 2. The output of the second subsystem.

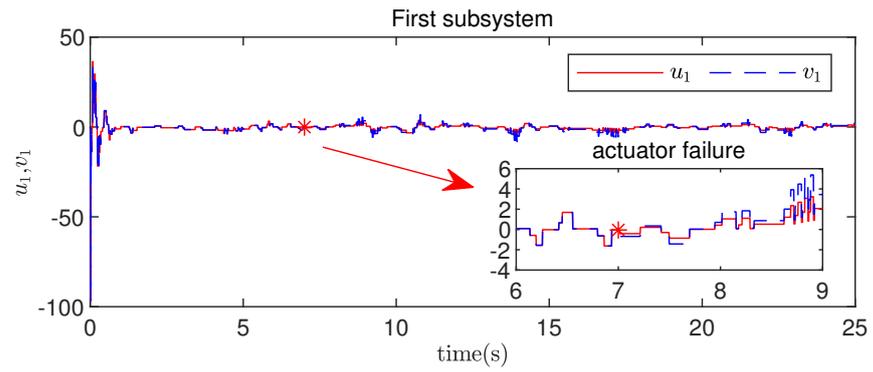


Figure 3. Input and output signals of actuator 1.

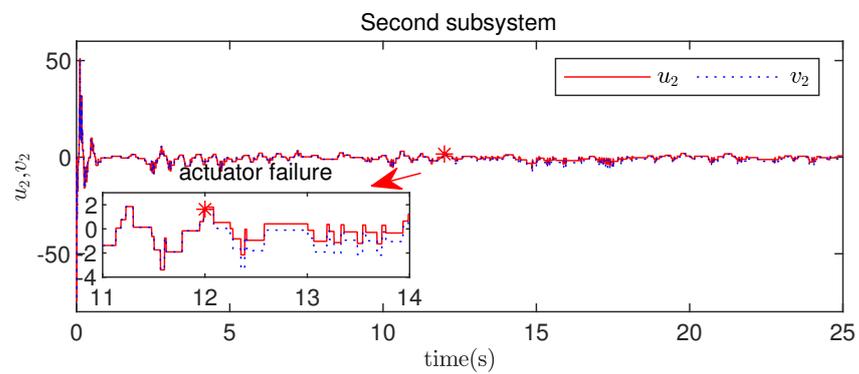


Figure 4. Input and output signals of actuator 2.

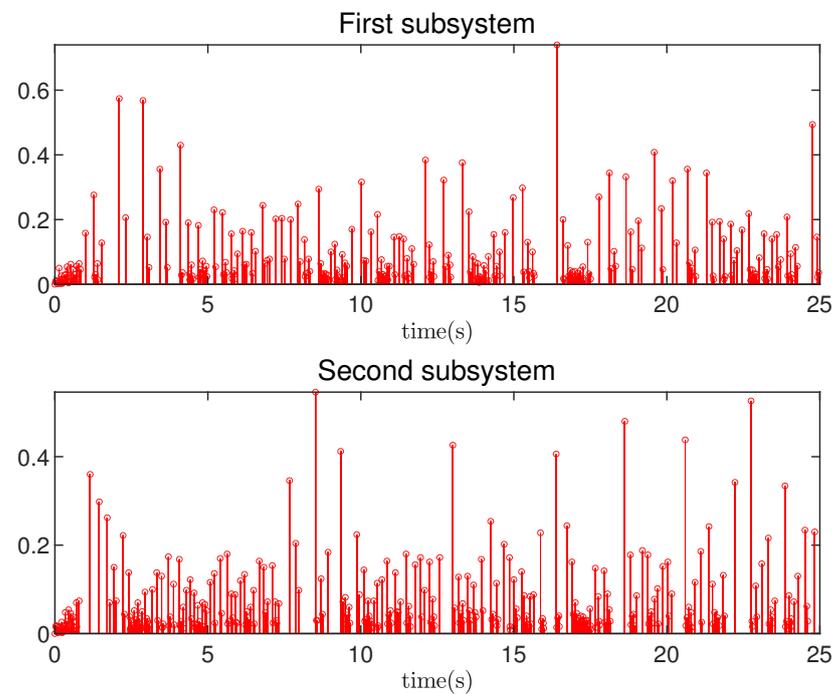


Figure 5. Time intervals of triggering events.

5. Conclusions

In this paper, a decentralized observer-based event-triggered fault-tolerant control scheme was derived for interconnected nonlinear delay systems. Our proposed event-triggered controller ensures that all system states are SGUUB. The problem of the “explosion

of complexity” is addressed by introducing first-order low-pass filters. The property of hyperbolic tangent functions and the approximation capability of NNs are used to handle interconnected nonlinear functions and time-varying delays. According to the simulation example, the Zeno phenomenon is avoided. In the future, it would be interesting to study dual-channel event-triggered control for interconnected nonlinear systems with actuator failures and denial-of-service attacks.

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