

Carbon Dioxide: A Raw Material for Cementitious Mortar [†]

Alessandro P. Fantilli ^{1,*} , Riccardo Calvi ², Edoardo Quietì ² and Pier Luigi Radavelli ²¹ Politecnico di Torino—DISEG, 10129 Torino, Italy² SIAD s.p.a., 24126 Bergamo, Italy; riccardo_calvi@siad.eu (R.C.); edoardo_quietì@siad.eu (E.Q.); pier_luigi_radavelli@siad.eu (P.L.R.)

* Correspondence: alessandro.fantilli@polito.it; Tel.: +39-011-0904900

[†] Presented at International Conference on Raw Materials and Circular Economy, Athens, Greece, 5–9 September 2021.

Abstract: Buildings and infrastructures can absorb CO₂ from the atmosphere because of the carbonation process that affects the calcium hydroxide of concrete elements. The aim of this research project is to initiate the absorption at casting by adding dry ice pellets to cement-based mortars. Test results demonstrate that the flexural and compressive strength of the mortars are not modified by this addition. Conversely, due to the presence of CO₂, the standard deviation of strength reduces with respect to that measured in plain mortars. Thus, carbon dioxide can be considered a valuable resource that improves the mechanical behavior of construction materials.

Keywords: cementitious mortar; dry ice pellets; compressive test; three-point bending test



Citation: Fantilli, A.P.; Calvi, R.; Quietì, E.; Radavelli, P.L. Carbon Dioxide: A Raw Material for Cementitious Mortar. *Mater. Proc.* **2021**, *5*, 2. <https://doi.org/10.3390/materproc2021005002>

Academic Editors: Anthimos Xenidis, Evangelos Tzamos and Konstantinos Simeonidis

Published: 22 October 2021

Publisher's Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

1. Introduction

Among all the materials, cement and steel are two of the most important sources of carbon dioxide. It is sufficient to think that cement manufacture releases about 7% of global CO₂, half of which can be attributed to the construction industry [1]. On the other hand, cement-based composites are prone to carbonate and, therefore, tend to absorb the carbon dioxide from the atmosphere. Hence, to compensate for the emission of cement production, some procedures have been proposed with the aim of absorbing carbon dioxide during the production of cementitious composites. More precisely, three different carbonation approaches can be found in the current literature.

The first, called Solidia Cement [2], a specific binder composed of calcium silicate with a low lime content, is more capable of absorbing CO₂ than ordinary Portland cement. When using this approach, concrete must be exposed to carbon dioxide for at least 48 h. In the second approach, called pre-carbonation [3], the goal is to obtain limestone by carbonating the calcium hydroxide. Then, the mixture of water and limestone is added to the concrete components (i.e., cement, water, aggregate, and additives). Finally, in the so-called “CarbonCure” method, carbon dioxide is added when concrete components are mixed [4].

Following the last approach, Fantilli et al. [5] have recently introduced a new cement-based mortar in which carbon dioxide, in the form of dry ice pellets, is added to the mixture like a raw material. By means of this addition, the maximum content of CO₂ that is absorbed by the mortar system is equal to 1.6% of the mass of the CEM I binder. Nevertheless, to consider carbon dioxide an effective raw material, like those currently used to cast cement-based products, it is necessary not only to simplify the procedure for absorbing CO₂ but also to demonstrate that CO₂ can improve the performance of mortars.

For these reasons, a new experimental campaign, performed on 60 mortar prisms, tested in bending moment and compression (in accordance with EN 196-1 [6]), is described in the following sections. The aim was to measure the effect induced by the addition of carbon dioxide both on the strengths, in bending and compression, and on the statistical distribution of these mechanical performances.

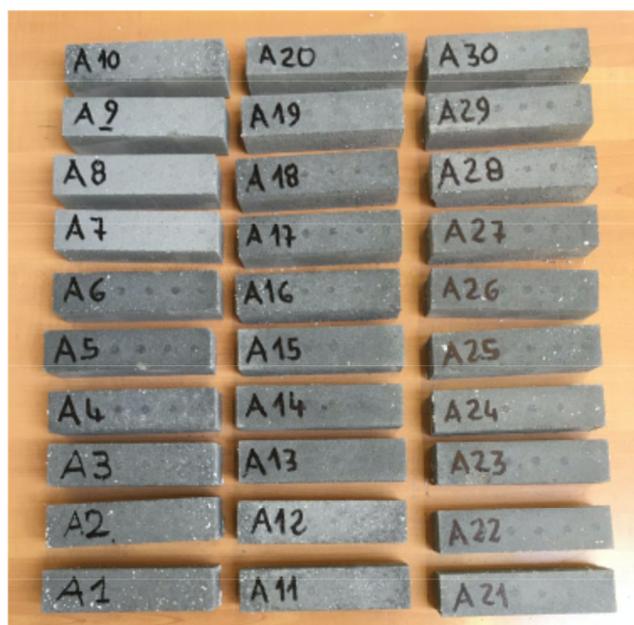
2. Material and Methods

Cement, tap water, normalized sand, and CO₂ were the components of the mortars herein investigated. The type of cement was CEM I 42.5R, whereas the carbon dioxide was provided by SIAD s.p.a in the form of dry ice pellets (with a diameter of 3 mm). Dry ice was obtained through the expansion of liquid carbon dioxide. During this physical conversion, each kilogram of liquid CO₂ formed about 0.6–0.52 kg of gas and 0.4–0.48 kg of solids, in the form of snow carbon dioxide. Such snow was successively compressed to form the pellets, which were added to cement-based mortars at a temperature of about –78 °C. The mixture also included CEN Standard sand consisting of siliceous rounded particles, whose size distribution lies within the limits given by EN 196-1 [6].

With all the above-mentioned materials, two series of mortars were cast. As shown in Table 1, in the mortar called B- Carbon, 72 g of CO₂ (i.e., 1.6% of the mass of the cement) were added with respect to the standard mortar (called A-plain). With each mortar, 30 prisms (40 × 40 × 160 mm³) were cast (see Figure 1) by means of polystyrene molds. The specimens were cured in the molds for 28 days at a constant temperature of 20 °C (relative humidity = 50%) and, after demolding, were tested in three-point bending and compression following the EN 196-1 [6] rules.

Table 1. The mortars used to cast the specimens.

Series	Cement (g)	Water (g)	Sand (g)	CO ₂ (g)	CO ₂ /Cement (%)
A-Plain	4500	2250	13,500	0	0
B-Carbon	4500	2250	13,500	72	1.6



(a)



(b)

Figure 1. The prisms tested in three-point bending and compression following the EN 196-1 [6] rules: (a) the prisms of the series A-plain; (b) the prisms of the series B-carbon.

3. Results and Discussion

From the three-point bending tests, the flexural strength σ_{flex} of all the 30 specimens of each mortar was measured, whereas the compressive strength σ_c was obtained with the uniaxial compression test. The latter was performed on 60 halves of the prisms previously tested in bending.

Figure 2 illustrates the statistical distributions of both σ_{flex} and σ_c , related to the mortar of series A-Plain (Figure 2a,b) and to that of series B-Carbon (Figure 2c,d), respectively.

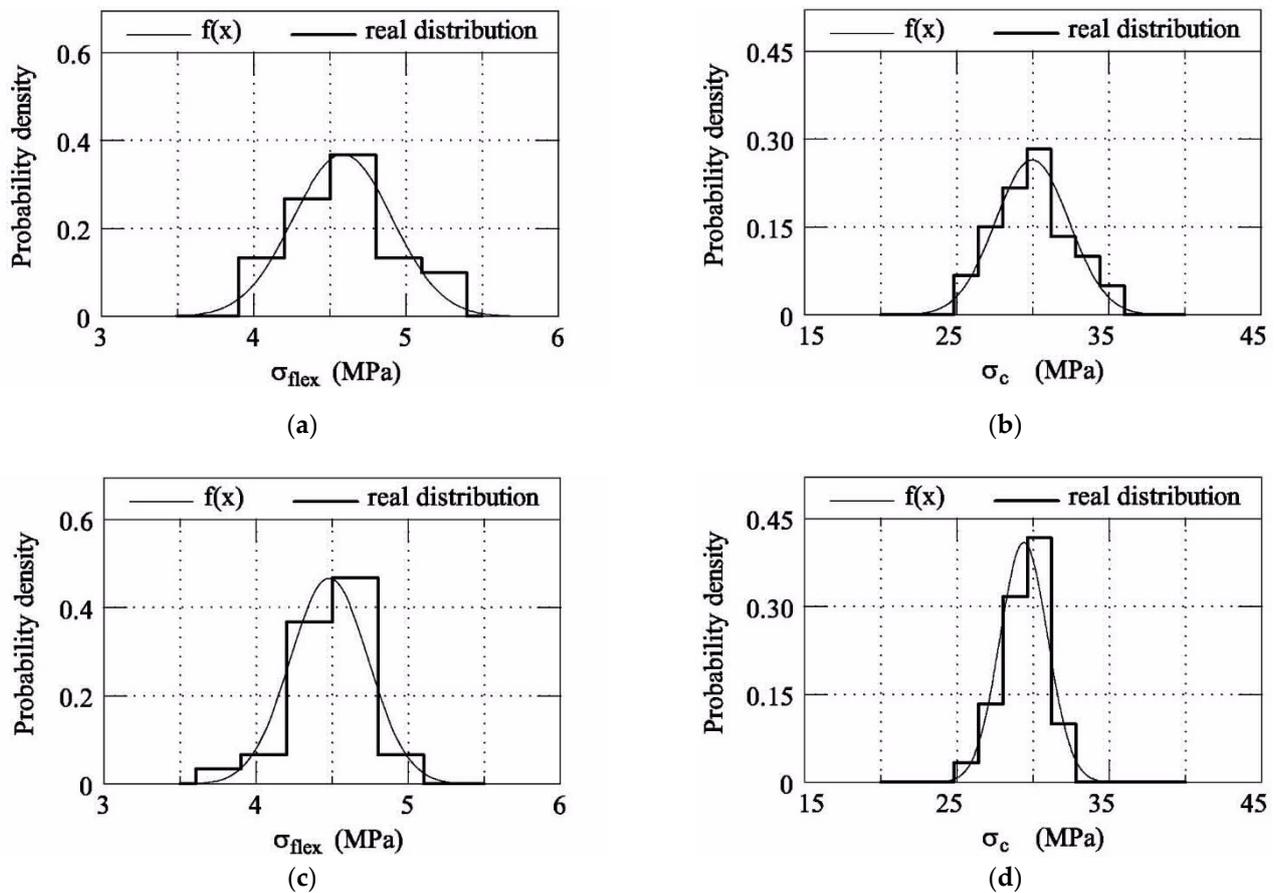


Figure 2. The statistical distributions of strength: (a) flexural strength in the mortar A-Plain; (b) compressive strength in the mortar A-Plain; (c) flexural strength in the mortar B-Carbon; (d) compressive strength in the mortar B-Carbon.

With respect to the series A-Plain, the use of CO_2 (in the series B-Carbon) does not modify the modal values of both compressive and flexural strength, but the probability density increases. Moreover, the dispersion of strength around the modal values tends to reduce in the mortars containing CO_2 . To better quantify these aspects, the density probability function $f(x)$ of the normal Gaussian distribution $f(x)$ can be computed (when the variable x is equal to σ_{flex} and σ_c , respectively) and is depicted in Figure 2:

$$f(x) = \frac{1}{\delta\sqrt{2\pi}} e^{-\frac{(x-\mu)^2}{2\delta^2}}, \quad (1)$$

The average value μ and the corresponding standard deviation δ are:

$$\mu = \frac{\sum_{i=1}^n x_i}{n} \quad \delta = \frac{1}{n-1} \sum_{i=1}^n (x_i - \mu)^2 \quad (2)$$

where N = number of specimens used to measure the strength (i.e., $N = 30$ in bending and $N = 60$ in compression). For both the series, the values of μ and δ are reported in Table 2.

Table 2. The statistical parameters of the mortars investigated herein.

Mechanical Property	σ_{flex}		σ_c	
	A-Plain	B-Carbon	A-Plain	B-Carbon
μ (MPa)	4.59	4.48	30.0	29.4
δ (MPa)	0.319	0.250	2.40	1.53
Degree of freedom	29		59	
F-test	F = 1.63 < $f_{0.05} = 1.86$		F = 2.44 < $f_{0.05} = 1.54$	
Equal variances	Yes		No	

The average values of compressive and flexural strength are nearly the same in both the mortars, whereas the lowest values of the standard deviation are those of the mortar B-Carbon, in which CO₂ is added. These results are in accordance with those obtained by Monkman & Cail [7], regarding the compressive strength of concrete samples in which CO₂ was added using the CarbonCure procedure. Moreover, the results of the F-test [8], summarized in Table 2, show that *F* is smaller than the critical value in the 95% confidence interval ($f_{0.05}$) only in the case of flexural strength. On the contrary, the compressive strength of A-plain and B-carbon do not have equal variance with a 95% confidence interval. As σ_c is the most important parameter that characterizes cement-based mortars, it is clear that statistically significant differences exist when dry ice pellets are added to a mortar system.

4. Conclusions

According to the experimental results illustrated in the previous sections, the following conclusions can be drawn:

- Carbon dioxide can be absorbed by cement-based mortars through a very simple approach, which can be easily implemented at the construction site. Specifically, CO₂, in the form of dry ice pellets, was added to concrete mixture like a common additive.
- If the mass of the added CO₂ is 1.6% of the cement, the average values of both flexural and compressive strength of the cementitious mortars are not modified.
- However, such a content of carbon dioxide leads to a remarkable reduction in strength distribution (i.e., a reduction in the standard deviation) with respect to that measured in plain mortars.
- The analysis of variance shows significant improvements in the mortars containing CO₂. Accordingly, the latter can be considered as a raw material for cement-based composites.

The effect produced by the addition of carbon dioxide on mortars containing other types of cement as well as other waste materials will be investigated in future experimental and theoretical analyses.

Author Contributions: Conceptualization, A.P.F.; methodology, A.P.F., E.Q., and P.L.R.; validation, A.P.F., E.Q., P.L.R., and R.C.; investigation, A.P.F.; resources, E.Q., P.L.R., and R.C.; data curation, A.P.F.; writing—original draft preparation, A.P.F.; review and editing, A.P.F., E.Q., P.L.R., and R.C. All authors have read and agreed to the published version of the manuscript.

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: Not applicable.

References

1. Monteiro, P.J.M.; Miller, S.A.; Horvath, A. Towards sustainable concrete. *Nat. Mater.* **2017**, *16*, 698–699. [CrossRef]
2. Sahu, S.; Meiningner, R.C. Sustainability and Durability of Solidia Cement Concrete. *ACI Concr. Int.* **2020**, *42*, 29–34.
3. Qian, X.; Wang, J.; Fang, Y.; Wang, L. Carbon dioxide as an admixture for better performance of OPC-based concrete. *J. CO₂ Util.* **2018**, *25*, 31–38. [CrossRef]

4. Monkman, S.; MacDonald, M. On carbon dioxide utilization as a means to improve the sustainability of ready-mixed concrete. *J. Clean. Product.* **2017**, *167*, 365–375. [[CrossRef](#)]
5. Fantilli, A.P.; Calvi, R.; Quietì, E. Carbon dioxide dry ice pellets as additive of cement-based pastes and mortars. In Proceedings of the XI International Symposium on Environmental Engineering, Turin, Italy, 29 June–2 July 2021.
6. UNI EN 196-1. *Methods of Testing Cement—Part 1: Determination of Strength*; European Committee for Standardization: Brussels, Belgium, 2005.
7. Monkman, S.; Cail, K. Waste CO₂ upcycling as a means to improve ready mixed concrete sustainability. In Proceedings of the 15th International Congress on the Chemistry of Cement, Prague, Czech Republic, 16–20 September 2019.
8. Fisher, R.A. *Statistical Methods for Research Workers*, 1st ed.; Oliver & Boyd: Edinburgh, UK, 1925.