

Article

The Influence of Micro-Oxygen Addition on Desulfurization Performance and Microbial Communities during Waste-Activated Sludge Digestion in a Rusty Scrap Iron-Loaded Anaerobic Digester

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Abstract: In this study, micro-oxygen was integrated into a rusty scrap iron (RSI)-loaded anaerobic digester. Under an optimal RSI dosage of 20 g/L, increasing O_2 levels were added stepwise in seven stages in a semi-continuous experiment. Results showed the average methane yield was 306 mL/g COD (chemical oxygen demand), and the hydrogen sulphide (H_2S) concentration was 1933 ppmv with RSI addition. O_2 addition induced the microbial oxidation of sulphide by stimulating sulfur-oxidizing bacteria and chemical corrosion of iron, which promoted the generation of FeS and Fe₂S₃. In the 6th phase of the semi-continuous test, deep desulfurization was achieved without negatively impacting system performance. Average methane yield was 301.1 mL/g COD, and H₂S concentration was 75 ppmv. Sulfur mass balance was described, with 84.0%, 11.90% and 0.21% of sulfur present in solid, liquid and gaseous phases, respectively. The Polymerase Chain Reaction-Denaturing Gradient Gel Electrophoresis (PCR-DGGE) analysis revealed that RSI addition could enrich the diversity of hydrogenotrophic methanogens and iron-reducing bacteria to benefit methanogenesis and organic mineralization, and impoverish the methanotroph (Methylocella silvestris) to reduce the consumption of methane. Micro-oxygen supplementation could enhance the diversity of iron-oxidizing bacteria arising from the improvement of Fe(II) release rate and enrich the sulphur-oxidising bacteria to achieved desulfurization. These results demonstrated that RSI addition in combination with micro-oxygenation represents a promising method for simultaneously controlling biogas H₂S concentration and improving digestion performance.

Keywords: micro-oxygen; anaerobic digestion; chemical corrosion; average methane yield; sulfur-oxidizing bacteria; desulfurization efficiency; sulfur balance

1. Introduction

As the by-product of wastewater treatment plants (WWTPs) the output of waste activated sludge generated in biological wastewater treatment processes has increased continuously in the recent decade. Wet sludge production in China was estimated to reach 33.59 million tons (based on a moisture content of 80%) by the end of 2015. Activated sludge has a complex composition, containing a variety of bacteria and organic materials, and its improper disposal and accumulation is bound to cause secondary pollution.





on the anaerobic digestion of activated sludge.

Anaerobic treatment processes have been widely applied to the treatment of organic solid waste due to their low operational costs and high solids reduction efficiency [1–3]. Under anaerobic conditions, organic matter is initially hydrolyzed and then fermented into volatile fatty acids (VFAs) such as acetic acid, as well as hydrogen, which represent substrates for methanogenic archaea for methane production [4]. However, the application of anaerobic digestion of sludge is often limited by low methane yield and sludge reduction rates [5], and the limiting factors are generally associated with the slow hydrolysis of sludge [6]. To accelerate the sludge digestion, various pre-treatments

mechanical methods [9]. The operating cost of the present pretreatment is high and often unattractive for practical application. Zero-valent iron (ZVI), which is a cheap reductant, has been widely applied to accelerate hydrolysis-acidification of the anaerobic digestion of sludge [10,11]. ZVI addition is associated with a resulting decline in oxidation-reduction potential (ORP) when added into anaerobic systems, enabling a more favorable environment for anaerobic biological processes [12]. Rusty scrap iron (RSI) is an abandoned iron material covered by a layer of iron oxide (rust) on its surface, which may represent an economic alternative. However, in previous work, little research has investigated the effect of RSI

have been used to improve the hydrolysis of the sludge, including thermal [7], chemical [8] and

The issue of the quality and quantity of biogas is equally important. Biogas contains several pollutants formed during the anaerobic digestion of sludge, predominantly in the form of toxic hydrogen sulphide (H₂S), with concentrations ranging from 0.1% to 1.0% v/v (1000–10,000 ppmv) [13]. H₂S can be released during the anaerobic digestion process by specific microorganisms such as sulfate-reducing bacteria (SRB), due to the existence of sulfur-containing compounds in substrates [14]. This leads to many problems, such as inhibited anaerobic digestion process, reduced biogas production, and poor biogas quality [15]. Consequently, H₂S production must be prevented, or H₂S must be removed from the biogas.

Recently, biological treatment processes to eliminate hydrogen sulphide have been shown to lower operational costs compared to traditional physico-chemical processes and lower chemical utilization or eliminate it altogether [16]. The application of micro-oxygenation technology is a key step to achieve biological treatment of hydrogen sulphide. Biological removal is based on the utilization of sulphur-oxidising bacteria (SOB) able to metabolize hydrogen sulphide to obtain energy when oxygen is present as an electron acceptor. The biological oxidation takes place in stages, through several redox intermediates as shown in Equation (1) [17]. The main reactions carried out by SOB are shown below:

$$HS^{-} \to S^{0} \to S_{2}O_{3}^{2-} \to S_{4}O_{6}^{2-} \to SO_{4}^{2-}$$
(1)

$$H_2S + 0.5O_2 \rightarrow S^0 + H_2O; \Delta G^0 = -209.4 \text{ kJ/reaction}$$
 (2)

$$S^{0} + 1.5O_{2} + H_{2}O \rightarrow SO_{4}^{2-} + 2H^{+}; \Delta G^{0} = -587.41 \text{ kJ/reaction}$$
 (3)

$$H_2S + 2O_2 \rightarrow SO_4^{2-} + 2H^+; \Delta G^0 = -798.2 \text{ kJ/reaction}$$
 (4)

$$S_2O_3^{2-} + H_2O + 2O_2 \rightarrow 2SO_4^{2-} + 2H^+; \Delta G^0 = -818.3 \text{ kJ/reaction}$$
 (5)

At this point, it should be noted that H_2S oxidation in biological systems occurs concurrently with chemical reactions [18]. Currently, the study of biological technologies on hydrogen sulphide remove mainly focused on biotrickling filters [19,20] and bioscrubbers [21] that employ pure cultures developed in the presence of hydrogen sulphide, oxygen and nutrients.

An additive that could increase anaerobic digestion methane yields would be important for a transition to renewable energies [22]. In previous study, RSI as an additive to enhance the performance of anaerobic digestion. In this study, the effect of the limited oxygen supply to the RSI-loaded anaerobic digester on the anaerobic digestion performance and biogas desulfurization was explored. The possible control mechanism of H_2S in biogas by the coupling of RSI with micro-oxygen was proposed. Additional studies have described the shifts in microbial communities in response to

ambient temperature change [23], but did not assess micro-oxygenation in combination with RSI. In this work, providing more comprehensive insights into the digester ecosystem and the changes in microbial community structure under this circumstances.

2. Materials and Methods

2.1. Substrates, Inoculant and Rusty Scrap Iron

The waste-activated sludge (WAS) used in this study originated from the Jianning Economic Development Zone WWPT in Nanjing, China. The sludge was stored in the freezer at -20 °C until use. In order to strengthen the hydrolysis step, the sludge was pretreated using alkaline method before the anaerobic fermentation [24]. In brief, the pH of sludge was adjusted to 12 using 4 M of sodium hydroxide, and then the sludge was stirred at 80 rpm for 6 h. After pretreatment, the pH of sludge was adjusted to 7 using 4 M of hydrochloric acid for anaerobic digestion. The characteristics of WAS and alkaline-pretreated sludge (APS) are compared in Table 1.

Table 1. The Characteristics of WAS and APS. WAS: waste-activated sludge; APS: alkaline-pretreated sludge; TCOD: total chemical oxygen demand; SCOD; soluble chemical oxygen demand; TS; total solids; VS: volatile solids; TSS: total suspended solids; and VSS: volatile suspended solids.

Parameters	Units	WAS	APS
TCOD	mg/L	$31,253 \pm 4107$	$30,854 \pm 4494$
SCOD	mg/L	121 ± 25	721 ± 28
TS	g/L	33.6 ± 4.9	32.9 ± 4.2
VS	g/L	20.7 ± 2.7	20.3 ± 2.4
TSS	g/L	32.4 ± 4.3	31.5 ± 3.9
VSS	g/L	19.8 ± 2.1	19.2 ± 1.8
pH	/	7.16 ± 0.11	7.06 ± 0.04
Total Fe	mg/L	31.2 ± 0.97	31.2 ± 0.94
Soluble Fe	mg/L	8.7 ± 0.15	9.4 ± 0.16
Soluble Sulphide	mg/L	34.7 ± 1.5	43.9 ± 1.8
SO_4^{2-}	mg/L	3.4 ± 0.18	5.5 ± 0.22
Total Elemental sulphur	mg/L	279.6 ± 13.1	279.6 ± 11.8

Inoculated anaerobic microorganisms were at the concentration of total solids (TS) = 34.7 g/L (volatile solids (VS) = 24.1 g/L), which were collected from the expanded granular sludge bed (EGSB) treating the distillery wastewater in Jiangsu Yanghe Brewery Joint-Stock Co., Ltd. (Suqian, China). Prior to use, the inocula were starved for 1 week and incubated at $35 \degree$ C.

RSI was used for addition of ferro-oxidative material for this study. The RSI tailings (approximately 10 mm \times 10 mm \times 0.3 mm) used in this study were obtained from a machine processing factory workshop. RSI was be covered by a layer of rust on inner ZVI surface which was mainly consisted of different iron oxides (Fe₂O₃, Fe₃O₄, FeO, FeOOH). The surface rust accounts for about 17.1% \pm 2.4% of the RSI weight. The inner part of RSI is elemental iron (zero-valent iron, ZVI). It was soaked in 0.1 M of NaOH solution for 24 h to remove oil residue and then washed with deionized water.

2.2. Semi-Continuous Microaerobic Digestion

In the previous study, we have examined the effects of varying concentrations of RSI additions (i.e., 0, 1, 5, 10, 20, 30 g/L) on anaerobic digestion performance from WAS, and obtained the optimal dosage of 20 g-RSI/L. The anaerobic digester with RSI dosage of 20 g/L is the RSI-loaded anaerobic digester in this study. The RSI was added to the reactor only at the beginning of the experiment. At the end of every period, the residual RSI was removed by using a magnet and replaced by new RSI for the next period.

To investigate the effects of a limited oxygen supply on SOB in a RSI-loaded anaerobic digester's performance and desulfurization, lab-scale bioreactors were operated with a working volume of 4 L and a headspace of 0.5 L under varying oxygen dosages and the optimal dosage of RSI as determined above over a span of 210 days. Digestion was performed in the mesophilic range (35 \pm 1 °C) with a hydraulic retention time (HRT) of approximately 20 days. The volumetric organic loading rate of the reactors was 1.54 kg_{COD}/m³·day. To increase the amount of hydrogen sulphide produced during digestion, sodium sulphate was added to the feed at a concentration of 2 g/L. The bioreactor was fed with WAS through a peristaltic pump on a semi-continuous basis, with feeding and discharge once a day (200 mL). The reactor was mixed with biogas recirculation provided by a miniature electroadcompressor (1 L/min). Oxygen was supplied with a 820 Top-Trak mass flow controller (Sierra Instruments, Sierra, CA, USA) from an oxygen cylinder. The oxygen was introduced into the headspace of the reactor once a day. The study was divided into seven operational periods with systematically increased dosages of oxygen. According to the relationship 5.0 NL_{oxygen}/Nm³ biogas and the biogas production in P2 to determine the dosage of oxygen (about $0.6-12.0 \text{ NL}_{oxygen}/\text{Nm}^3$ biogas). The first period (P1) represented a control, without RSI added in the absence of oxygen to establish performance of conventional anaerobic digestion of WAS, as determined by chemical oxygen demand (COD) removal and methane yield. The second period (P2) investigated the effect of addition of the optimally determined rusty scrap iron (RSI) concentration on anaerobic digestion performance in comparison to P1. The five additional periods (i.e., P3–P7) were carried out to evaluate the effect of the varying dosages of oxygen supply on the RSI-loaded anaerobic digester's performance and desulfurization in this system. Table 2 summarizes the experimental arrangement of the study, and a lab-scale bioreactor diagram is shown in Figure 1. Reactor contents were sampled every day and conserved at 4 °C. Biogas generated was collected in a 5 L Tedlar gas bag (CEL Scientific, Santa Fe Springs, CA, USA). Considering the amount of biogas yet to be treated, a biogas residence time (BRT) of more than 7 h would be maintained, which was sufficient to obtain an efficient hydrogen sulphide removal in a microaerobic reactor [25]. The biogas residence time is a value that reflects mean residence time of produced biogas in the headspace of the reactor which could be calculated by the following equation:

$$BRT = 24 \times V_{headspace} / ABPR$$

where *BRT* is biogas residence time; $V_{\text{headspace}}$ is the headspace volume of reactor (0.5 L in this study); and *ABPR* is average biogas production rate (L/day).

Period	P1	P2	P3	P4	P5	P6	P 7
Condition	An ^a	An	Ma ^b	Ma	Ma	Ma	Ma
Day	1-30	31-60	61–90	91-120	121-150	151-180	181-210
Duration (day)	30	30	30	30	30	30	30
RSI dosages (g/L)	0	20	20	20	20	20	20
ABPR (mL/day)	937	1671	1645	1592	1644	1591	1197
O_2 supply (mL)	0	0	1	5	10	15	20
O ₂ /biogas ^c	0	0	0.61	3.14	6.08	9.43	16.71
BRT (h)	12.8	7.1	7.2	7.5	7.2	7.5	10.0

Table 2. Experimental parameters and results during semi-continuous anaerobic and microaerobic digestion of activated sludge supplemented with RSI over seven periods of operation associated with stepwise increases in oxygen concentration. RSI: rusty scrap iron; *ABPR*: Average biogas production rate; and *BRT*: biogas residence time.

^a An: anaerobic; ^b Ma: microaerobic; ^c O₂/biogas: ratio of supply of oxygen to biogas produced from anaerobic digestion at standard condition, (NL_{oxygen}/Nm³ biogas).



Figure 1. Lab-scale bioreactor diagram for the semicontinuous anaerobic and microaerobic digestion of activated sludge supplemented with rusty scrap iron (RSI).

2.3. Analysis

Prior to daily sampling, pH and ORP values were quantified by a HQ30d meter (HACH, Loveland, CO, USA) equipped with a standard electrode (PHC101, HACH) and a standard electrode (MTC101, HACH), respectively. TS, VS, total suspended solids (TSS), volatile suspended solids (VSS), total chemical oxygen demand (TCOD) and soluble chemical oxygen demand (SCOD) were measured according to the standard methods [26]. For analysis of the soluble fraction, the samples were centrifuged at 8000 rpm for 10 min and then the supernatant was passed through a 0.45 mm nitrocellulose filter.

Fe(II) and Fe(T) [Fe(II) + Fe(III)] were examined according to standard methods [26]. Samples for Fe(II) analysis were acidified by 0.1 M HCl and measured immediately to minimize its oxidation. Aqueous concentrations were determined after filtering water samples through 0.22 um glass-fiber filter papers (Gelman A/E, Ann Arbor, MI, USA).

Sulphate and thiosulphate were measured by high performance liquid chromatography (HPLC) according to the method described by van der Zee et al. [18]. Total sulfide in the effluent was analyzed by the potentiometric titration method (Leici PHS-3C, Shanghai, China), which included H_2S , HS^- , and S^{2-} . The sulphur content in the sludge was estimated from an elemental analysis of sulphur. Samples were dried at 95 °C, cooled and analysed in a SC32 oven (LECO, Joseph, UT, USA). Analysis was carried out by combustion of the samples at 1350 °C, as a result, the sulphur was completely oxidized to SO_2 and evaluated in the detection cell. The sulphur estimation was the result of subtracting the content of the other analyzed sulphur species (sulphate, thiosulphate) of the sample from the total sulphur content.

Biogas composition (CH₄, CO₂, H₂S, and O₂) was measured daily using a portable biogas analyzer (Biogas 5000, Geotech, Denver, CO, USA). The gas bag was emptied at the end of each working day, with biogas accumulated over 24 h, with biogas samples taken for analysis at the beginning of the following day. The volume was measured by displacement of water then converted to standard temperature and pressure (STP).

2.4. DNA Extraction, Amplification by Polymerase Chain Reaction, Denaturing Gradient Gel Electrophoresis and Sequencing

In this study, in order to evaluate how the presence of RSI and O_2 affected the microbial community, three samples were collected on the last day of P1, P2 and P6 and stored at -20 °C. The genomic DNA of the samples were extracted using an extraction kit (Bioteke Corporation, Beijing, China) according to the manufacturer's instructions. A primer combination of 341F (5'-CCTACGGGAGGCAGCAG-3') and 907R (5'-CCGTCAATTCCTTTGAGTTT-3') was used to selectively amplify the 16S rRNA sequences of bacteria [27]. Another primer combination of 787F (5'-ATTAGA TACCCTGGTAGTCC-3') and 1059R (5'-GGACTACCAGGGTATCTAAT-3') was used to selectively amplify the 16S rRNA sequences of archaea [28]. A 40 base pair GC clamp was added to the forward primer at the 5'-end to improve detection of the sequence variation in DNA fragments by subsequent denaturing gradient gel electrophoresis (DGGE) [27]. The 16S rDNA fragment was amplified using a polymerase chain reaction (PCR) thermal cycler Dice (BioRad Laboratories, Inc., Hercules, CA, USA) with a touchdown PCR method [29]. The PCR products obtained were applied in the DGGE analysis using a BioRad Dcode system (BioRad Laboratories, Inc.). A DGGE gel of 6% polyacrylamide with a linear denaturing gradient ranging from 30% to 60% (100% denaturing gradient contains 7 M urea and 40% formamide) was applied. Electrophoresis was conducted at a constant voltage of 180 V in 1 \times TAE (tris-acetate-edta) buffer and 60 °C for 6 h. The gels were then stained with SYBR Gold (Dalian TaKaRa, Dalian, China) in $1 \times TAE$ buffer for 40 min, after which the UV transillumination image of the gel was photographed using the Gel Doc 2000 System (BioRad Laboratories, Inc.).

Selected DGGE bands were excised and re-amplified by PCR with the aforementioned primers without the GC clamp. The PCR products were sequenced at TaKaRa Biotechnology Co. Ltd., (Dalian, China). The obtained sequences were then compared to the reference microorganisms in the GenBank database using the BLAST (Basic Local Alignment Search Tool) program.

3. Results and Discussion

3.1. Sludge Digestion System with Rusty Scrap Iron Amendments during Semi-Continuous Anaerobic and Microaerobic Digestion

3.1.1. The Variation of pH and Oxidation-Reduction Potential

To investigate the effects of the limited oxygen supply to the RSI anaerobic system on steady-state performance in this study, the variation of pH and ORP were characterized during semi-continuous digestion experiments (Figure 2). During P1, which involved neither addition RSI nor supply O_2 , the pH decreased from near neutral values to 6.33 over the initial 3 days (Figure 2). This can be attributed to the build-up of VFAs during APS digestion because methanogens grow more slowly than acidogens in the degradative process [30]. Afterwards, pH increased slightly, fluctuating from 6.5 to 6.8 over the remainder of P1. During P2, the RSI (20 g/L) was added into reactor. As expected, the pH in the reactor quickly returned to 7.0 and remained in the near-optimal pH range (6.8–7.2) [31], due to the previously described mechanism of pH regulation through corrosion process. On the 61st day (period P3), 1 mL pure O_2 was introduced into the reactor headspace, and as shown in Figure 2, the pH was maintained at ideal levels (6.8–7.2)., with similar effects observed at P4, P5 and P6. Supplying limited O_2 could have increased the chemical corrosion of ZVI, as the common consensus is that the principal site of cathodic oxygen reduction, (Equation (6)), and anodic metal dissolution according to Equation (7) occurs close to RSI edges [32]:

$$O_2 + 2H_2O + 4e^- \rightarrow 4OH^- \tag{6}$$

$$Fe(s) \to Fe^{2+}(aq) + 2e^{-}$$
 (7)



 $2H_2O + 4Fe^{2+} (aq) + O_2 \rightarrow 4Fe^{3+} (aq) + 4OH^- (aq)$ (8)

Figure 2. Variation of pH (\blacksquare) and oxidation-reduction potential (ORP, \blacktriangle) under anaerobic and microaerobic conditions during semi-continuous digestion of activated sludge supplemented with RSI (error bars represent standard deviation, *n* = 3).

When Fe(III) enters liquid phase it will rapidly be converted into Fe(II) by iron-reducing bacteria (IRB) [33,34]. By looking at the fast Fe(III) reduction at the time, two possible reasons could be proposed for the observed pH stabilization: (1) the electrons generated during the degradation of the sludge organics were, to a large extent, utilized for Fe(III) reduction, decreasing the amount of electrons flowing to the intermediates to form fermentation end products, mainly in the form of VFAs; (2) much of the resultant VFAs from the sludge digestion were consumed as the electron donors for Fe(III) reduction. In both the above ways, the supplemented RSI acted as an electron sink to alleviate the accumulation of reducing equivalents for VFAs formation, thus preventing the pH from decreasing. However, slight pH drops were observed in P7, mainly fluctuating from 6.6 to 6.9. This can be ascribed to excess oxygen because the system reductive environment was destroyed, which restrained the methanogens activity but did not inhibit acidogenic facultative anaerobes [35].

In the first stage (P1), reactor ORP generally ranged from -410 to -350 mV, which is suitable for anaerobic digestion normal operation. Because of the rapid dissolution of iron oxide and release of ferric ions, the ORP level in P2 was noticeably higher than in P1 in the first two day (Figure 2) and which consequently decreased to a lower lever (about $-450 \sim -500$ mV), which should be attributed to the reducing ability of inner ZVI. Previous research indicated that ORP in anaerobic environment can be decreased by as much as 100 mV through addition of ZVI [36]. In P3, micro-oxygenation (1 mL O₂) was started (Table 3), and a slight increase in ORP was observed, fluctuating from -450 to -480 mV. The ORP is a measure of the redox potential and is sensitive to the presence of O₂ in an aqueous solution. In the remaining four stages (P4, P5, P6 and P7), the system ORP increased with stepwise increasing O_2 dosage with fluctuations of -410 to -440 mV, -350 to -400 mV, -300 to -340 mV and -200 to -230 mV, respectively. With respect to P4–P6, although the system ORP levels were increased from -440to -300 mV, any negative impact on methanogenic activity was non-existent. Instead of decreasing, the average COD removal and average methane yield increased slightly (Table 3). This is consistent with the fact that ZVI created a favorable environment for the growth of methanogens by lowering the ORP (-270 to -370 mV) and increasing the buffer capacity of the system [37]. In comparison, in P7, excess oxygen disrupted the system reductive environment that is necessary for methanogens growth, followed by the reduction of average COD removal and average methane yield (Table 3).

Parameter	P1	P2	P3	P4	P5	P6	P7
COD in (mg/L)	31,253	31,253	31,253	31,253	31,253	31,253	31,253
Average COD out (mg/L)	19,314	13,314	13,658	14,314	13,908	14,126	17,189
Average COD removal (%)	38.2	57.4	56.3	54.2	55.5	54.8	45.0
VS in (g/L)	20.3	20.3	20.3	20.3	20.3	20.3	20.3
Average VS out (g/L)	12.7	8.9	8.9	9.5	9.5	9.4	11.1
Average VS removal (%)	37.6	56.4	56.1	54.2	54.2	53.5	45.3
Average Methane Yield (mL/g COD)	218.76	306.00	300.59	298.54	298.90	301.13	261.39
Average Methane Yield (mL/gVSfed)	342.3	484.6	465.3	457.2	465.7	486.4	406.8
Average H_2S concentration (ppmv)	12504	1933	776	484	234	75	68
Average O_2 concentration (ppmv)	/ a	/	158	759	1230	2083	8438
Average CH_4 concentration (ppmv)	557,964	656,972	642,738	634,655	630,789	648,816	614,308
Average CO ₂ concentration (ppmv)	419,672	332,948	346,459	356,842	356,129	341,027	372,648

Table 3. Reactor performance during semi-continuous anaerobic and microaerobic digestion of activated sludge supplemented with RSI over seven periods of operation associated with stepwise increases in oxygen concentration.

^a: undetectable.

3.1.2. The Anaerobic and Microaerobic Digestion Performance

The variation of daily COD removal and daily methane yield for entire duration of the semi-continuous digestion are illustrated in Figure 3. The variation trend of COD removal is similar to methane yield. It is possible that methane production is the predominant way of COD removal in anaerobic digestion systems with low hydrogen production. The COD removal and methane yield in P1 (neither RSI supplementation nor O_2 supply), which were considered data for the baseline period, were 38.2% and 218.75 mL/g COD on average (Table 3). After RSI supplementation in P2 COD removal and CH₄ yield increased noticeably in the initial four days, with subsequent fluctuation within a narrow range. A 1.50-fold increase in average COD removal and a 1.41-fold increase in average methane yield were achieved compared with P1. This is attributed to the reduction of the Fe(III) oxides on the RSI surface, which promoted microbial hydrolysis-acidification of complex matter, providing more organic matter for methanogenesis [1]. In addition, a previous study has suggested that RSI could enhance decomposition of propionate and created further improvements on the propionate conversion [29]. While propionate could not be utilized directly by methanogens, its biotransformation products could, ultimately enhancing methane yield. In P3-P6 (i.e., stepwise increase in oxygen concentration), the COD removal and the methane yield were almost equal to that of P2 (Figure 3), which fluctuated in small scope arising from the variability of feeding composition.



Figure 3. Daily COD removal (\blacksquare) and daily methane yield (\blacktriangledown) under anaerobic and microaerobic conditions during the digestion of sludge (error bars represent standard deviation, *n* = 3).

The COD removal during P2–P6 was on average 57.4%, 56.3%, 54.2%, 55.5% and 54.8%, respectively. And P2–P6 achieved average methane yields of 306.00, 300.59, 298.54, 298.90 and 301.13 mL/g COD, respectively. In P7, the COD removal and methane yield declined simultaneously due to system reductive environment destruction (Figure 2). As noted above, these results are consistent with those reported in literature, even on an industrial scale, it has been broadly demonstrated that the presence of limited amounts (not exceeding 15 mL in this study) of O_2 in digesters does not negatively affect digestion performance [38,39].

3.1.3. H₂S and O₂ Concentration in Biogas

The H₂S content in biogas produced in P1 (under anaerobic conditions) had a larger fluctuation range (Figure 4) and was on average 12504 ppmv (Table 2). In P2, RSI supplementation could drastically reduce the H₂S content in biogas to achieve an average of 1933 ppmv, representing an overwhelming 84.5% reduction compared with P1. The result shows that RSI addition had a positive effect on both H₂S control in biogas production. The commonly accepted mechanism of electron transfer from RSI to microorganisms is via microbial corrosion and surface oxidation of RSI. RSI was initially observed to be covered by a layer of rust on inner ZVI surface, and this rust consisted of different iron oxides (Fe₂O₃, Fe₃O₄, FeO, FeOOH) [40]. These oxides are understood to react with H⁺ (corrosion process), inducing the release of Fe(II) and Fe(III). When Fe(III) enters the liquid phase it is rapidly converted into Fe(II) by IRB [33,34]. Under anaerobic conditions, inner ZVI is oxidized to Fe(II), producing cathodic hydrogen (H₂/[H]) via Equation (9) [41]. The corrosion process of iron oxide and ZVI exerts a beneficial effect on pH control for the digestion system. Subsequently, the produced Fe(II) by IRB can precipitate with sulfide by forming FeS (Equation (10)), which is the proposed mechanism through which RSI addition reduces H₂S concentrations in biogas:

$$Fe^{0} + 2H_{2}O \rightarrow Fe^{2+} + H_{2} + 2OH^{-} \Delta G^{0'} = -5.02 \text{ kJ/mol}$$
 (9)

$$\mathrm{Fe}^{2+} + \mathrm{S}^{2-} \to \mathrm{FeS} \tag{10}$$



Figure 4. Hydrogen sulphide (\blacklozenge) and oxygen (\blacktriangledown) concentrations under anaerobic and microaerobic conditions during semi-continuous digestion of activated sludge supplemented with RSI (error bars represent standard deviation, *n* = 3).

Microaerobic conditions were applied in the following 5 periods (P3–P7) and gradually the O_2 concentration was increased stepwise (Table 2). The result showed that the content of H_2S in biogas was decreased with increasing of O_2 dose, and, but naturally the O_2 content in the resulting biogas

was higher. Specifically, from P3 to P7, the average H_2S concentration in biogas was 776, 484, 234, 75 and 68 ppmv, respectively, while O_2 concentrations were on average 158, 759, 1230, 2083 and 8438 ppmv, respectively. It is worth noting that at even the highest micro-oxygenation level (P7), the surplus O_2 content greatly increased by 305.1% compared with P6, while the biogas H_2S content was almost equal to that in P6, indicating diminishing returns past this concentration. The considerable increase in biogas O_2 concentration also accompanied by a decrease of methane production in P7 and decreased O_2 consumption. Regarding the biogas H_2S content, it hardly changed in comparison to P6, which could be related to two possibilities: (1) the biogas desulphurization took place predominantly in the gas-liquid interface [42]. Although sufficient O_2 was supplied, it is hard to accommodate excessive SOB in this limited space due to the unavailability of H_2S ; (2) the precision of the gas analyzer to detect H_2S could be also be limited at lower values. In P6, the average methane yield increased by 37.65% comparing with P1. What's more, the H_2S removal efficiency in biogas decreased by 99.40% in this case, and a concentration below 100 ppmv was reached, guaranteeing levels adequate for combined heat and power (CHP) (100–300 ppmv), which represents a major use of biogas, thus avoiding high costs associated with desulfurization.

3.2. Sulfur Balance

Microaeration had a significant and rapid effect on the sulfur distribution in reactor, as did RSI supplementation. All sulfur species (i.e., H_2S , S^{2-} , HS^- , S^0 , $S_2O_3^{2-}$, SO_4^{2-}) exist in three states: solid, liquid and gas. The mass of all relevant species were measured and are summarized in Table 4, while Figure 5 shows species distribution before and after the experiment.

Phase Sulfur Species		P1	P2	P3	P4	P5	P6	P 7
S-sulfur compounds in waste sludge	55.9	41.8	38.3	33.8	33.1	31.4	32.5	37.1
S-iron sulphide	/	2.2	41.7	45.1	51.2	58.9	55.1	51.1
S ⁰	/	/	/	26.9	32.7	37.2	42.4	30.1
S-Total sulfide (S^{2-}, HS^{-}, H_2S)	8.3	78.6	53.8	26.6	20.1	15.9	11.2	7.6
S-Sulphide oxidation products $(S_2O_3^{2-}, SO_4^{2-})$	90.5	4.7	5.1	4.9	5.4	4.8	5.7	23.9
S in gaseous phase (mg) S-H ₂ S		16.7	4.6	1.8	1.1	0.6	0.3	0.2
Total Elemental Sulphur (mg)		144	143.5	139.1	143.6	148.8	3 147.2	150
	Sulfur SpeciesS-sulfur compounds in waste sludgeS-iron sulphide S^0 S-Total sulfide (S^{2-}, HS^-, H_2S) S-Sulphide oxidation products $(S_2O_3^{2-}, SO_4^{2-})$ S-H_2SSulphur (mg)	Sulfur SpeciesFeedS-sulfur compounds in waste sludge 55.9 S-iron sulphide/S^0/S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S) 8.3 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 S-H ₂ S/Sulphur (mg) 154.7	Sulfur Species Feed P1 S-sulfur compounds in waste sludge 55.9 41.8 S-iron sulphide / 2.2 S^0 / / S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S) 8.3 78.6 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 4.7 S-H ₂ S / 16.7 Sulphur (mg) 154.7 144	Sulfur SpeciesFeedP1P2S-sulfur compounds in waste sludge 55.9 41.8 38.3 S-iron sulphide/2.2 41.7 S ⁰ ///S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S) 8.3 78.6 53.8 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 4.7 5.1 S-H ₂ S/16.7 4.6 Sulphur (mg)154.7144143.5	Sulfur SpeciesFeedP1P2P3S-sulfur compounds in waste sludge 55.9 41.8 38.3 33.8 S-iron sulphide/ 2.2 41.7 45.1 S^0 ///26.9S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S) 8.3 78.6 53.8 26.6 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 4.7 5.1 4.9 S-H ₂ S/ 16.7 4.6 1.8 Sulphur (mg) 154.7 144 143.5 139.1	Sulfur SpeciesFeedP1P2P3P4S-sulfur compounds in waste sludge 55.9 41.8 38.3 33.8 33.1 S-iron sulphide/ 2.2 41.7 45.1 51.2 S^0 ///26.9 32.7 S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S) 8.3 78.6 53.8 26.6 20.1 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 4.7 5.1 4.9 5.4 S-H ₂ S/ 16.7 4.6 1.8 1.1 Sulphur (mg) 154.7 144 143.5 139.1 143.6	Sulfur SpeciesFeedP1P2P3P4P5S-sulfur compounds in waste sludge 55.9 41.8 38.3 33.8 33.1 31.4 S-iron sulphide/2.2 41.7 45.1 51.2 58.9 S ⁰ ///26.9 32.7 37.2 S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S)8.378.6 53.8 26.6 20.1 15.9 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻) 90.5 4.7 5.1 4.9 5.4 4.8 Sulphur (mg) 154.7 144 143.5 139.1 143.6 148.8	Sulfur SpeciesFeedP1P2P3P4P5P6S-sulfur compounds in waste sludge 55.9 41.8 38.3 33.8 33.1 31.4 32.5 S-iron sulphide/ 2.2 41.7 45.1 51.2 58.9 55.1 S ⁰ ///26.9 32.7 37.2 42.4 S-Total sulfide (S ²⁻ , HS ⁻ , H ₂ S)8.378.6 53.8 26.6 20.1 15.9 11.2 S-Sulphide oxidation products (S ₂ O ₃ ²⁻ , SO ₄ ²⁻)90.5 4.7 5.1 4.9 5.4 4.8 5.7 S-H ₂ S/16.7 4.6 1.81.1 0.6 0.3 Sulphur (mg)154.7144143.5139.1143.6148.8147.2

Table 4. The mass distribution of sulfur compounds (mg) in the system before and after semicontinuous anaerobic and microaerobic digestion of activated sludge supplemented with RSI over seven periods of operation associated with stepwise increases in oxygen concentration.

/: not detected.

Before anaerobic and microaerobic digestion, the sulfur species in the digester included organic sulfur-containing compounds in the waste sludge and added sulfate. The dissolved sulfur compounds obtained from the waste sludge were mainly sulfate and sulfide, while the thiosulfate were negligible. After anaerobic/microaerobic digestion, six major streams of sulfur species in the digester were identified: (1) sulfur compounds in waste sludge; (2) iron sulphide precipitation; (3) elemental sulfur S⁰ (deposition in the headspace of the reactors); (4) sulfide in liquid phase; (5) sulphide oxidation products ($S_2O_3^{2-}$, SO_4^{2-}); and (6) sulfur in biogas (as hydrogen sulfide).



Figure 5. Calculated sulfur balance during semicontinuous anaerobic and microaerobic digestion of activated sludge supplemented with RSI over seven periods of operation associated with stepwise increases in oxygen concentration: (1) sulfur compounds in waste sludge; (2) iron sulphide precipitation; (3) elemental sulfur S⁰; (4) sulfide in liquid phase; (5) sulphide oxidation products; and (6) sulfur in biogas.

The solid form of sulphur in this system mainly consisted of sulfur compounds in waste sludge, precipitated iron sulphide and elemental sulfur S^0 (deposition in the headspace of the reactors). It can be seen that after anaerobic and microaerobic digestion, the amount of sulfur compounds in sludge decreased across all the periods, which resulted from the biological reduction of both sulfate and organic sulfur compounds by SRB. In P1, sulfur compounds in sludge decreased by 25.29%, while percent reduction of more than 40% was achieved in the later periods. Combining RSI with O₂ can enhance cell lysis, which released more organic sulfur compounds which can be reduced to sulfide by SRB [43–45]. Only 1.44% of the sulfur dosed was present in the solid phase of the iron sulphide precipitation in P1, while over 26% was in P2 due to the addition of RSI. Starting from P3, supply of micro-oxygen promoted the generation of Fe(II) and Fe(III), which further increased the mass of iron sulphide precipitate, which ranged from 45 to 60 mg. In addition, oxygen can also directly to react with sulphide as an electron acceptor. Furthermore, sulfide was transformed into elemental sulfur through SOB activity as an electron donor. In P3 through P6, 26.94%, 32.70%, 37.24% and 42.39% of the sulfur dosed was transformed into elemental sulfur, respectively, while in P7 a 30.07% reduction was achieved. The possible reason could be that excess oxygen was supplied, leading to part of sulphide being oxidized to thiosulfate or sulphate [46].

The dissolved forms of sulphur in this system are mainly sulfide (S^{2-} , HS^- , H_2S) and sulphide oxidation products ($S_2O_3^{2-}$, SO_4^{2-}). The sulfide detected in the liquid from P1 to P7 accounted for 50.82%, 34.81%, 17.18%, 13.02%, 10.30%, 7.25% and 4.89% of the sulfur dosed, respectively. Thus, the addition of RSI into the reactor decreased not only the concentration of hydrogen sulfide in biogas, but also the concentration of sulfide in the liquid, and combining limited amounts of O_2 with RSI achieved this more effectively. During the first six periods, only negligible amounts (stabilized at around 5 mg) of sulphide oxidation products ($S_2O_3^{2-}$, SO_4^{2-}), were found in the liquid. Díaz et al. [47] discovered that sulphate was found to be easily accessible for sulphate-reducing microorganisms, while organic sulphur in the form of proteins, or cell constituents, was only partly reduced, and a large portion left the bioreactor unchanged. However in P7, the amounts of sulphide oxidation products significantly improved to 23.97 mg. Indeed, the optimum ORP for methane reducing bacteria is below –230 mV while an ORP value above –280 mV is inhibitory to sulphate reducing bacteria [48,49]. In P7, the reactor ORP already exceeded the value (Figure 2).

The gaseous form of sulphur in this system was mainly H₂S. The digester was fed with 154.69 mg/day of sulphur, 10.82% was found in biogas during P1, while only 2.99% of sulfur was detected in biogas during P2 resulting from addition of RSI (Fe²⁺ + S²⁻ \rightarrow FeS). Starting from P3, O₂ was added into the reactor to enhance the biogas desulphurization. A fraction of O₂ acting electron acceptor directly reacting with sulphides, and another fraction of O₂ corroded iron producing Fe(II) and Fe(III), which then also reacted with sulphide. Of all sulphur dosed into reactor, 2.99%, 1.18%, 0.71%, 0.36%, 0.21% and 0.11% was found in biogas respectively for P3, P4, P5, P6 and P7.

The outputs of sulphur accounted for 93.12%, 92.76%, 89.95%, 92.84%, 96.21%, 95.19% and 96.93% of inputs, respectively. This 'lost' sulphur, comparing inputs and outputs, was not analysed in this research. There are several possible explanations for this lack of sulphur in the balance. Firstly, sulphur emission in the biogas may not be limited to H₂S but other possible S-containing gaseous forms emitted in the biogas but were not taken into account in our balance. These include dimethyl sulphide, carbon disulphide, mercaptans, etc. Secondly, total sulphur determination may have been biased by the high total dissolved sulphide content, which could have volatilized during the drying procedure before elemental analysis [50].

3.3. The Possible Control Mechanism of H₂S in Biogas

Based on previous studies and the results obtained in this study, the possible control mechanism of H_2S in biogas by the couple of RSI with micro-oxygen can be proposed, as shown in Figure 6. These biotic/abiotic factors all eventually led to the observed decrease in biogas H_2S content. O_2 addition induced the microbial oxidation of sulphide by stimulating SOB and chemical corrosion of iron, which promoted the release of Fe(II) and Fe(III). They combined with sulphide and formed deposits of FeS and Fe₂S₃, which will decrease the sulphide concentration in the liquid. And part of oxygen was used as electron acceptor to oxidize sulphide existed in the liquid through the action of SOB. According to the law of gas solubility (Henry's Lay), the lowered sulphide concentration in the liquid would decrease the amount of H_2S coming out of the liquid. Of course, neither pathway excludes the other, such as the H_2S near the top of gas-liquid interface also can be oxidized through the action of SOB. This work builds solid support for the potential applicability of RSI for WAS digestion and provides an additional route for enhancing biogas desulphurization accompanied with micro-oxygen.



Figure 6. The possible desulfurization mechanisms by combination of RSI and micro-oxygen during digestion system.

3.4. DGGE Analysis of the Microbial Communities

Archaea and bacterial community structure after the anaerobic digestion was studied by the DGGE analysis of PCR amplified 16S rRNA gene fragments (Figure 7). Representative bands were selected from the DGGE gel for sequencing in order to identify the species presented in the digester and the results are shown in Table 5. A total of 11 and 19 discernible DGGE bands were respectively observed in the two DGGE profiles for archaea and bacteria.

In this study, the archaea species could be divided into two different classes: Methanomicrobia (band A1–A10), and Methanococci (band A11). This result revealed that Methanomicrobia species were the prevalent methanogens in the archaeal community. Most species were highly coupled with aceticlastic methanogens (band A8–A11) and hydrogenotrophic methanogens (band A1–A7). With RIS addition, the diversity of methanogens was enhanced, particularly hydrogenotrophic methanogens. Band A1, A4 and A5 detected in P2 and P6 only, were closely related to *Methanoculleus palmolei*, *Methanolinea tarda* and *Methanosarcina mazei*, hydrogenotrophic. [51]. Given the band intensity, the aceticlastic methanogens populations corresponding to band A8–A11 likely formed the dominant methanogen group in all periods. The band intensity of A8 and A11 were enhanced obviously (Figure 7). In P6, the diversity of methanogens didn't decreased in the reactor. Therefore, micro-oxygenation did not seem to cause a harmful impact on the archaeal diversity.



Figure 7. The DGGE profiles of archaea and bacterial 16S rRNA genes from the samples of digestion reactor in the last day of P1, P2 and P6. The gels with band were collected from the DGGE gel and labeled as bands A1–A11 (for archaea) and B1–B19 (for bacteria). The sequencing results of each band are shown in Table 5.

Bands B1 and B2 were most closely related to *Methylovirgula ligni* and *Methylocella silvestris*, respectively. These two species were known as facultative methanotrophs that could attenuate methane emissions [52]. Both microorganisms were found in P1, while only *Methylovirgula ligni* was found in P2 and P6, which indicated that addition of RSI could remove *Methylocella silvestris* to weak the consumption of methane biologically [5]. Some detected microorganisms are capable of degrading complex organic matters to form organic acid, i.e., bands B3 (Uncultured bacterium), B4 (*Sphingopyxis witflariensis*), B5 (*Novosphingobium indicum*), B6 (*Clostridium orbiscindens*), B7 (*Clostridium populeti*) and B8 (*Caloramator proteoclasticus*). Band B7 was an anaerobic cellulolytic microorganism and band B8 had strong ability to degrade proteins and amino acids [53]. These two microorganisms have been found in P2 and P6 indicating that iron can enhance the ability of cellulose and protein hydrolysis.

Hydrogen-producing bacteria and acetobacteria may play important roles in anaerobic fermentation since hydrogen and acetate can be directly utilized by methanogenesis [54]. Band 9 was closest to *Clostridium* species belonging to the H₂-producing bacteria, which had been found in the three periods. *Syntrophobacter fumaroxidans* (band 10) was enriched in the digester with the RSI (P2 and P6) which was capable of producing both hydrogen and formate by propionate oxidation. Band B11, B12 and B13 showed high sequence similarity to acetobacter *tropicalis*, *Roseomonas lacus* and *Sporomusa silvacetica*, respectively. *Acetobacter tropicalis* had been found in the three periods but the other two microorganisms were only generated in P2 and P6 indicating that the iron enhanced the diversity of acetobacteria in the digesters so as to increase acetate production.

Band No.	Closest Relatives	Similarity (%)	Classification
A1	Methanoculleus palmolei (NR028253)	99	Methanomicrobia
A2	Methanosphaerula palustris (NR074167)	92	Methanomicrobia
A3	Methanoculleus marisnigri (NR074174)	98	Methanomicrobia
A4	Methanolinea tarda (NR028163)	97	Methanomicrobia
A5	Methanosarcina mazei (NR041956)	100	Methanomicrobia
A6	Methanoculleus bourgensis (NR042786)	98	Methanomicrobia
A7	Methanosarcina mazei (NR074221)	93	Methanomicrobia
A8	Methanosaeta concilii (NR102903)	99	Methanomicrobia
A9	Methanosarcina siciliae (NR104757)	99	Methanomicrobia
A10	Methanosarcina barkeri (NR025303)	97	Methanomicrobia
A11	Methanococcus aeolicus (NR029140)	93	Methanococci
B1	Methylovirgula ligni (NR044611)	98	Alphaproteobacteria
B2	Methylocella silvestris (NR074237)	98	Alphaproteobacteria
B3	Uncultured bacterium (JQ726674)	98	Alphaproteobacteria
B4	Sphingopyxis witflariensis (NR028010)	99	Alphaproteobacteria
B5	Novosphingobium indicum (NR044277)	99	Alphaproteobacteria
B6	Clostridium orbiscindens DSM 6740 (NR029356)	99	Clostridia
B7	Clostridium populeti (NR026103)	93	Clostridia
B8	Caloramator proteoclasticus (NR026265)	95	Clostridia
B9	Clostridium sp. (JQ670700)	94	Clostridia
B10	Syntrophobacter fumaroxidans (NR027598)	94	Deltaproteobacteria
B11	Acetobacter tropicalis (NR036881)	95	Alphaproteobacteria
B12	Roseomonas lacus (NR042318)	98	Alphaproteobacteria
B13	Sporomusa silvacetica (NR026378)	98	Alphaproteobacteria
B14	Geobacter bemidjiensis Bem (NR042769)	97	Deltaproteobacteria
B15	Acidimicrobium ferrooxidans (NR074390)	92	Acidimicrobidae
B16	Ferrimicrobium acidiphilum (NR041798)	93	Acidimicrobidae
B17	Uncultured Arcobacter sp. (HQ392839)	99	Epsilonproteobacteria
B18	Uncultured Epsilonproteobacterium (DQ295695)	99	Epsilonproteobacteria
B19	Uncultured Acinetobacter sp. (EU567041)	95	Gammaproteobacteria

Table 5. Phylogenetic affiliation of archaeal and bacterial 16S rRNA gene sequences retrieved from DGGE bands.

Band B14, only found in P6, showed high sequence similarity to *Geobacter bemidjiensis* Bem which had the ability to reduce Fe(III) and oxidize acetate and other multi-carbon organic substrates to carbon dioxide [55]. IRB was only found in the digester with RSI (P2 and P6), which further proved that RSI could enrich IRB to enhance degradation of complex substrates, which contributed higher sludge reduction. Band B15 and B16 showed high sequence similarity to *Acidimicrobium ferrooxidans* and *Ferrimicrobium acidiphilum*, respectively, which had the ability to oxidize Fe(II) [56]. Both of them were found in P6, while only band B16 was found in P2. It could be because O₂ supplementation improved the Fe(II) releasing rate and enhanced the diversity of Iron-Oxidizing Bacteria.

In this study, SOB microoganisms were only found in P6. The bands B17, B18 and B19 affiliated to the Epsilonproteobacteria class, Epsilonproteobacteria class and Gammaproteobacteria class were assigned to the Uncultured *Arcobacter* species, Uncultured *Epsilonproteobacterium* and Uncultured *Acinetobacter* species (Table 5), which are capable of oxidizing sulphide. Band B17 was found in the headspace of microaerobic digesters treating sewage sludge [57]. Band B18 was described by Kodama and Watanabe [58] as a chemolithoautotrophic SOB capable of oxidizing H₂S, S⁰ and S₂O₃^{2–} under microaerobic conditions. And band B19 was partially responsible for H₂S removal in the bioscrubber system developed by Potivichayanon et al. [59].

3.5. Economic Analysis

The economic assessment mainly included the consumption of RSI, sodium hydroxide, hydrochloric acid and oxygen in this study while the operational costs were not considered as they were the same for all the anaerobic digestion experiment. The consumption of additional materials as well as their price during the sixth period which was the optimal condition was shown in Table 6. It can be calculated that the total cost in sixth period is 0.11\$. Considering the average biogas production rate and average methane content in biogas (Tables 2 and 3), the increment of methane enhancement can be calculated as follows: $\Delta V(\text{mL CH}_4) = 1.591 \times 30 \times 64.9\% - 0.937 \times 30 \times 55.8\% = 15.29$ L. Currently, the market price of methane is about \$0.015/L. It meant that a profit of about \$0.23 could be obtained when the sludge digestion were operating under the optimal condition, more than two folds of its cost. Besides, the RSI added in each period could be reused in real applicability for about 10 periods which can further reduce the cost.

Consumption					Price						
RSI g/perio	Sodium Hydroxide d g/period	Hydrochloric Acid mL/period	Oxygen L/period	RSI \$/kg	Sodium Hydroxide \$/kg	Hydrochloric Acid \$/L	Oxygen \$/m ³				
8.4	7.2	17.8	0.45	1.6	20	20	57.7				

Table 6. The consumption and price of additional materials in the sixth period of sludge digestion.

Therefore, it is economical and applicable to employ RSI and micro-oxygen technology to enhance the methane production during sludge digestion which could simultaneously dispose the sludge and recover energy effectively.

4. Conclusions and Outlook

The combination of microaerobic desulphurization with RIS amendment during waste activated sludge digestion was investigated to develop a cost-effective and environment-friendly technology for H_2S removal and energy recovery. The optimal condition is combining a dosage of 20 g/L RSI with supply of 15 mL O₂ (9.43 NL_{oxygen}/Nm³ biogas) to the digestion system. In this case, the negative influence of micro-oxygen on digestion performance was found to be negligible. DGGE analysis revealed that the relatively high transfer rate of O₂ to the liquid maintained by biogas recirculation caused an apparent change in the structure and a considerable increase in the richness of the microbial communities in the long run. An average methane yield of 301.13 mL/g COD was reached and biogas H₂S content remained steady below 100 ppmv. Under optimal dosing conditions, H₂S content in

the biogas could fulfill the quality standards required for subsequent application of the produced biogas and obviating the need for any desulphurization processes. Next, relevant research on how to put the technique into practice in a large-scale digester for simultaneous controlling biogas H₂S concentration and improving digestion performance with low cost and high efficiency should be done. If this technology could be developed as a mature and widely used technology, it could be adopted to treat high sulfur-containing wastewater.

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