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Assessment of the Impact of Geomagnetic Disturbances on Korean Electric Power Systems

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Abstract: Geomagnetic disturbances have the potential to impact the operation of electric power systems, and thus the assessment of their impacts is required as the first step for secure power system operations. While the effects of the disturbances have been observed primarily at higher latitudes, geomagnetic problems are also observed at mid and low latitude locations, in particular including neighboring countries to Korea such as China and Japan. This paper deals with the assessment of impact of geomagnetic disturbances on Korean electric power systems. For the assessment, the geoelectric fields induced by the geomagnetic disturbances are calculated using geomagnetic data measured over the past 20 years in order to quantify the strength of geomagnetic events in Korea. Then, the geomagnetic currents on the grid driven by the geoelectric fields are computed. Finally, the increased reactive power absorption in high voltage transformers is analyzed and accordingly the change of system voltage magnitudes is identified to evaluate whether the system maintains the voltage stability. The systematic study concludes that during a strong geomagnetic disturbance, the Korean electric power system satisfies the associated standards in the U.S. and maintains system stability.

Keywords: geomagnetic disturbances; transformer half-cycle saturation; geoelectric field; geomagnetic induced currents; reactive absorption; system voltage levels; Korean electric power system

1. Introduction

It has been a growing concern that geomagnetic disturbances (GMDs) have the potential to impact on the operation of electric power systems [1–3]. GMDs occur when particles discharged from the sun during solar storms cause intensive variation in the Earth’s magnetic field. Through Faraday’s law of induction, the changing magnetic field creates the geoelectric field at Earth’s surface and in the ground, which in turn generates geomagnetically induced currents (GIC) to flow along transmission lines and through transformer neutral-groundings. When these quasi-direct current (DC) GIC currents, typically in the order of 0.1 Hz to 0.001 Hz, flow into a transformer winding, the operating point is shifted and the transformer cores become saturated. This is known as half-cycle saturation. As a consequence, the transformer suffers hot spot heating, produces harmonics, and absorbs more reactive power losses.

Many problems and even blackouts of power systems due to GIC have been reported in [4–6]. The most well-known example in North America is the collapse of the Hydro-Quebec system with the occurrence of 1.7 V/km geoelectric field in March 1989. More than six million people remained without power for nine hours. Another representative GIC event, also referred to as the Halloween

storm, caused a blackout in the south of Sweden at the end of October 2003. About 50,000 customers were left without electricity during the blackout that lasted for about an hour.

Two primary risks to the bulk power system from GMDs are noted by the North American Electric Reliability Council (NERC) [4]. The first one is the potential damage of bulk power system assets, typically associated with the high voltage transformers. The second is the loss of reactive power support, which may lead to voltage instability and power system collapse. The potential impacts of GMDs, in particular focusing on the voltage instability, can be assessed with following three steps: (1) calculation of the geoelectric field; (2) computation of GIC over the network; and (3) calculation of reactive power losses in transformers and evaluation of voltage collapse.

NERC TPL-007-1 standard (Transmission system planned performance for geomagnetic disturbance events) has been approved in September 2016 in order to ensure safe and reliable operation of the interconnected power systems from GMDs. All the electric power utilities in the U.S. are required to assess the vulnerability of their transmission systems to GMDs. If the results of the vulnerability assessment do not satisfy the requirements, corrective actions should be developed to mitigate their impacts and to manage system reliability. More details about the standard, including procedures, requirements and implementation timeline can be found in [7].

It was commonly understood that the effects of GIC are primarily experienced in higher geomagnetic latitude regions such as North America and North Europe. However, recent work has established that GIC problems are also observed at low and equatorially locations. While these locations are exposed to the greatly reduced intensity, the disturbances can persist for very long periods of time [8]. For example, the loss of 14 large 400 kV transformers have been reported in South Africa during the 2003 geomagnetic storm over 29–31 October [9]. Furthermore, power systems in southern Japan and China neighboring to Korea experienced widespread GIC flows [10–12]. No accidents associated with GMDs have been reported in Korea. However, considering these circumstances, the importance of the vulnerability assessment of Korean power systems to GMDs has been increasing.

In this paper, Korean electric power grids have been studied with the presence of GMD. The assessment has been completed following the NERC TPL-007-1 standard. For the assessment, the geoelectric field is calculated using measured geomagnetic data in order to quantify the strength of geomagnetic events in the past 20 years. Then, GIC flows are analyzed by developing the DC equivalent circuit of Korean power systems. The amounts of increased reactive power absorption in high voltage transformers are evaluated, and the change of system voltages is then identified by incorporating the additional reactive power demands into alternating current (AC) power flow analysis.

This paper is organized as follows. Section 2 presents a brief analytic basis to model the GICs and assess the effects. In Section 3, the calculation of geoelectric fields using measured geomagnetic data is presented. Section 4 illustrates the evaluation of GMD impact on the Korean electrical power grid, including the computation of increased reactive power losses in all transformers, and the change in voltage levels. Finally, the conclusion is made in Section 5.

2. Procedure of Assessing the GMD Impact

This section describes the theoretical basis used to model GICs and the risk assessment procedure for GMD impacts on power systems.

2.1. Calculation of Induced Geoelectric Field

There are a number of methods used to calculate the induced geoelectric fields from the variation of geomagnetic fields [13]. These methods differ from simplifications of the complex phenomena in that the currents in the ionosphere or magnetosphere are functions of time and space, and the earth's conductivity distribution is required. The simplest and the most appropriate method is to use the plane wave theory requiring magnetic field measurements and one-dimensional (1-D) layered earth conductivity model. Equations (1) and (2) show the relationship between the geomagnetic field, earth surface impedance, and the geoelectric field.

$$E_x(\omega) = Z(\omega)H_y(\omega) \quad (1)$$

$$E_y(\omega) = -Z(\omega)H_x(\omega) \quad (2)$$

where $E_x(\omega)$: Northward geoelectric field (V/m); $E_y(\omega)$: Eastward geoelectric field (V/m); $H_x(\omega)$: Northward geomagnetic field intensity (A/m); $H_y(\omega)$: Eastward geomagnetic field intensity (A/m); $Z(\omega)$: Earth surface impedance (Ω).

As shown in (1) and (2), the electric fields can be calculated with frequency domain techniques. Time series of magnetic data are transformed into the frequency domain using a fast Fourier transform (FFT) and multiplied with the function of Earth's surface impedance. Then the result is converted to the time series of electric field values by the use of the inverse FFT.

The earth surface impedance depends on the earth conductivity structure below the power system. The conductivity (σ) is varied with depth (d), represented with a 1-D layered, laterally uniform model as shown in Figure 1.



Figure 1. One-dimensional (1-D) layered earth conductivity model reproduced with permission from [4], NERC, 2012.

The earth surface impedance can be obtained with following Equations (3)–(6) [14].

$$k_n = \sqrt{j\omega\mu_0\sigma} \quad (3)$$

$$r_n = \frac{1 - k_n \frac{Z_{n+1}}{j\omega\mu_0}}{1 + k_n \frac{Z_{n+1}}{j\omega\mu_0}} \quad (4)$$

$$Z_n = j\omega\mu_0 \frac{1 - r_n e^{-2k_n d_n}}{k_n (1 - r_n e^{-2k_n d_n})} \quad (5)$$

For the bottom layer, the surface impedance is:

$$Z_n = \frac{j\omega\mu_0}{k_n} \quad (6)$$

where: ω : Angular frequency (rad/s); μ_0 : Permeability of free space; σ_n : Conductivity of layer n ($1/\Omega \cdot m$); r_n : Thickness of layer n (m).

2.2. Calculation of GIC

The presence of geoelectric field on a power grid is equivalent to modeling a set of voltage source in the transmission lines. The value of voltage magnitude is the integral of the electric field along the line shown in Equation (7):

$$V_{AB} = \int_A^B \vec{E} \cdot d\vec{l} \quad (7)$$

Assuming the geoelectric fields are uniform over the power system network, Equation (7) can be simplified to (8) with the path independence of the integral:

$$V_{AB} = L_{AB}(E_x \sin \theta + E_y \cos \theta) \quad (8)$$

where L_{AB} is the distance between the nodes A and B , and θ is the angle between the line connecting the nodes and the y -axis.

Because GIC flows have much lower frequency than 1 Hz, a DC treatment is reasonable. Thus, the GIC calculation can be done by reducing the AC power network to its DC equivalent. GIC flows are then determined by solving the DC network equation shown in (9):

$$\bar{I} = \bar{G}\bar{V} \quad (9)$$

where \bar{G} is a symmetric matrix with real conductance values, and the voltage vector, \bar{V} .

2.3. Calculation of Reactive Power Losses

Once the GIC flows have been calculated, transformer reactive power losses associated with the GICs are determined. These reactive power losses vary linearly with terminal voltage and the amount of the GIC, and also depend on transformer configuration affecting K_r in (10) [15]. The losses are represented with (10) [16].

$$Q_{GIC,r} = K_r V_{pu,r} I_{GIC,r} \quad (10)$$

where $Q_{GIC,r}$ is the GIC-related reactive power loss for the transformer r in Mvar, K_r is a transformer specific constant with Mvars/amp, $V_{pu,r}$ is the per unit AC terminal voltage for the transformer, and $I_{GIC,r}$ is the-per phase GIC through neutral in transformer r .

3. Calculation of the Electric Field Using Measured Data

3.1. Magnetometer Data Acquisition

In Korea, since 1996, magnetometer data have been collected at four observatories including Icheon, Jeju, Gangneung, and Yongin. These data have been provided online by Korea Space Weather Center [17]. The magnetic fields were recorded with a 1 min resolution on average. These time series data are used to calculate the geoelectric field.

3.2. 1-D-Layered Earth Conductivity Model in Korea

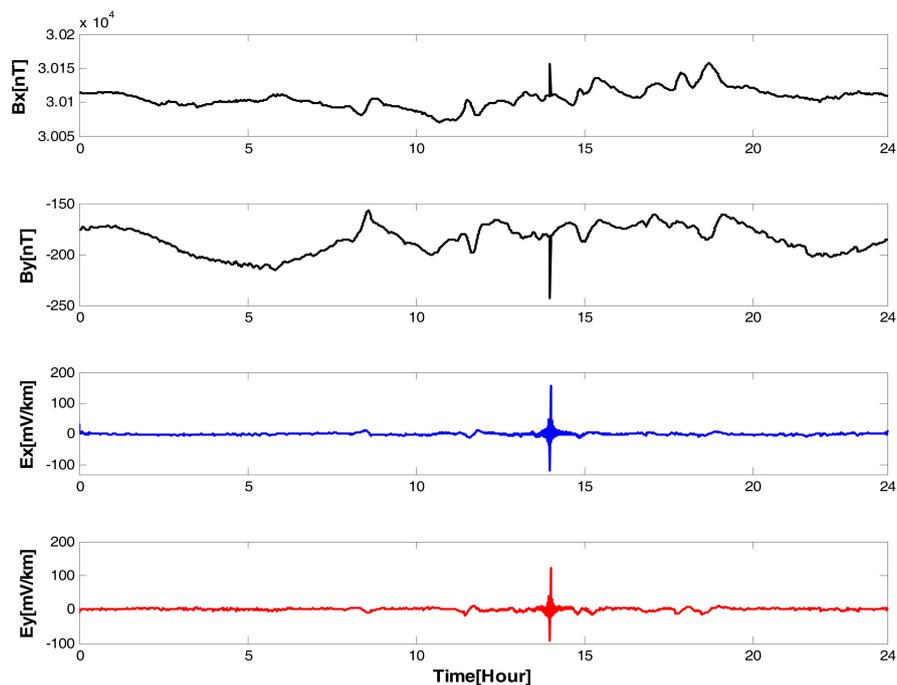
For the geoelectric field calculation, the required subsurface information was obtained from [18], where 1-D conductivity structure in the Korean peninsula was presented using the magnetotelluric method. [18] examined the conductivity with depth at seven different locations and minor differences exist among the conductivity value. For simplification of the study, the averaged value of each layer was used. In addition, the geoelectric field computation requires data with depths of hundreds of kilometers because of the quasi-DC nature of the field [4]. However, only four layers with depths of up to 100 km were revealed in [18]. For the additional information, the IP-4 model in [19] has been added, and the developed 1-D layered conductivity model is presented in Table 1.

Table 1. Developed 1-D layered earth conductivity model in Korea for the geoelectric field calculation.

Layer Number (<i>i</i>)	Depth (<i>d_i</i>) (km)	Conductivity (σ_i) (1/Ω·m)
1	0.43	1/1152
2	16.6	1/12660
3	87.96	1/1077
4	150	1/209
5	160	1/50
6	110	1/20
7	150	1/5.62
8	230	1/1.58

3.3. Result of Calculated Geoelectric Field

The method to calculate the geoelectric field with the magnetometer data was implemented using Matlab. Figure 2 shows the calculated geoelectric fields, E_x (Northward) and E_y (Eastward) with the data at the Icheon observatory on 19 October 2003. The abrupt change of the magnetic fields, nearly 50 nT in B_x and 60 nT in B_y led to the sudden increase of the geoelectric fields, 157 mV/km in E_x and 121 mV/km in E_y . Geoelectric fields at four stations in the years from 1996 to 2016 were also obtained. Much missing data existed in the magnetometer data, and some data that looked incorrect were not included in the calculation. The maximum of E_x and E_y during a day over the past twenty years was presented in Figure 3. The largest amplitude of the geoelectric field was 107.9 mV/km of E_x and 591.4 mV/km of E_y at the Icheon station on 24 December 2001.

**Figure 2.** Calculated geoelectric fields on 19 October 2003 at the Icheon observatory.

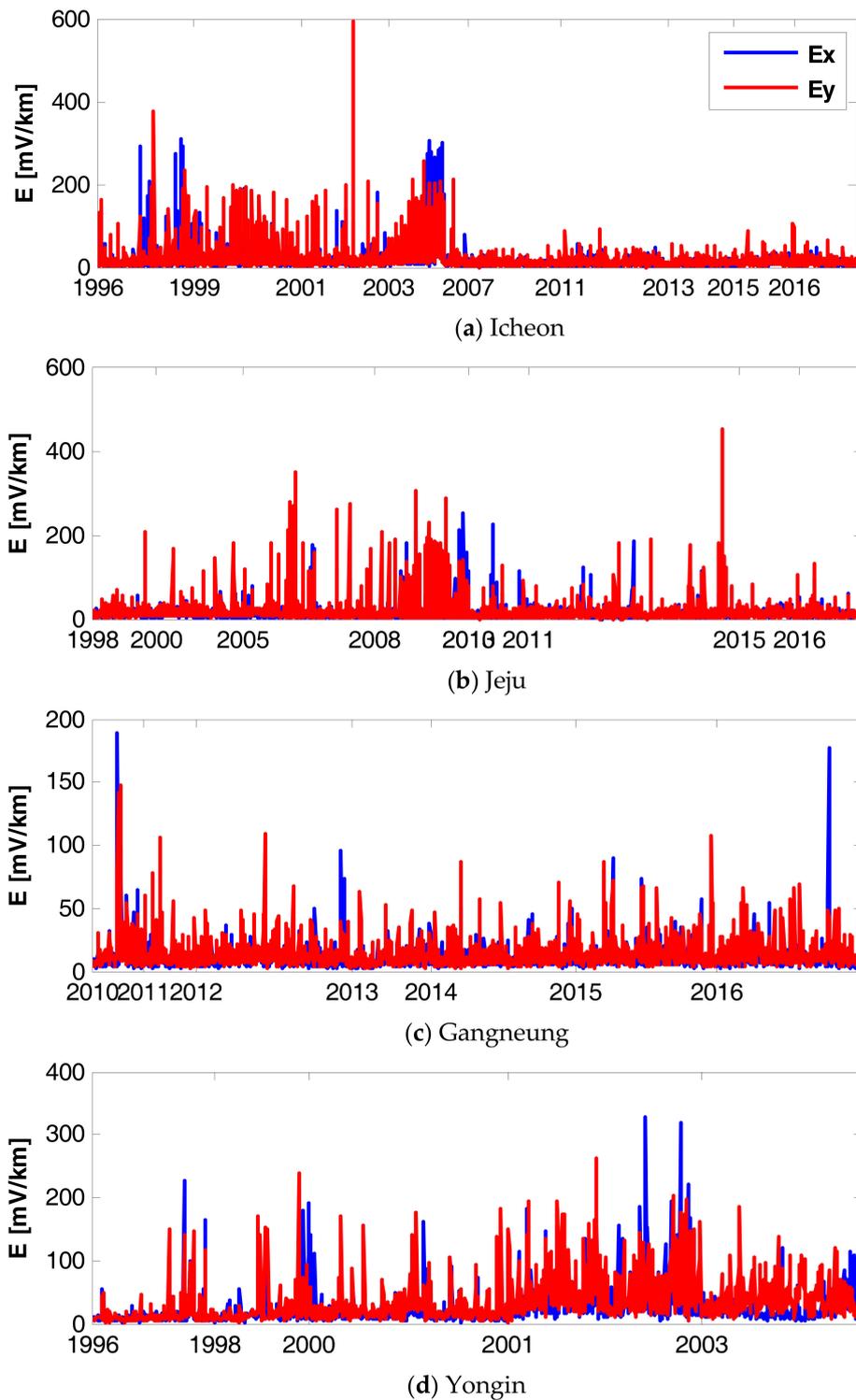


Figure 3. Daily maximum of geoelectric field (*Ex*: Blue, *Ey*: Red).

4. Assessment of GMD Impact on Korean Power Systems

4.1. NERC TPL-007 Vulnerability Assessment

NERC vulnerability assessment is based on a benchmark GMD event, on which the maximum geoelectric field strength of 8 V/km is defined at a reference location (geomagnetic latitude of 60 degrees). The benchmark case is associated with the most severe GMD event, which occurred once

every 100 years. A new draft of TPL-007-1 expected to be approved includes the local enhancement of the geoelectric field amplitude of up to 12 V/km. The intensity of GMD varies depending on latitude-based geomagnetic location, and thus the scaling factor is allowed in TPL-007. Table 2 presents the geomagnetic scaling factor. In addition, TPL-007 requires the preparation of a corrective action plan in order to mitigate the effect of GMD on power systems if the maximum transformer GIC is over 75 A per phase with the benchmark event.

Table 2. Geomagnetic field scaling factors [20].

Geomagnetic Latitude (Degrees)	Scaling Factor
≤40	0.1
45	0.2
50	0.3
57	0.7
59	0.9
≥60	1

4.2. Simulation with Korean Power Systems

The assessment was made with a practical Korean power system representing the peak loading in 2016. Overall system information is presented in Table 3. As presented in Section 3.3, the most severe GMD that happened in Korea during the past 20 years might generate a geoelectric field amplitude of about 0.6 V/km. In this vulnerability study, a 12 V/km strength with consideration of the latitude scaling was applied uniformly over the entire Korean power system. Geomagnetic latitude in South Korea is less than 30 degrees, and thus the geomagnetic scaling (0.1) was multiplied by the benchmark amplitude of 12 V/km, effectively 1.2 V/km.

Table 3. Information of the Korean power system for study.

Type	Numbers	MW	Mvar
Generators	411	83,652.2	19,450.1
Loads	1328	82,427.7	27,572.7
Switched Shunts	573	0	15,091.3
Buses	2250	-	-
Transformers	687	-	-
Branches	2329	-	-

The assessment was performed with the PowerWorld simulator providing the calculation of GIC flows over the network and additional reactive power losses in transformers [21]. The PowerWorld simulator also offers analysis on how the system voltages are changed with the additional reactive power demands caused by GIC flows.

To create a DC equivalent circuit required for GIC calculation, geographic location information including latitude and longitude at all system buses and substations were entered into the simulator. One ohm of substation grounding resistance is assumed according to the substation design criterion at Korea Electric Power Corporation. All the transformer neutral resistances were ignored and accordingly, the larger GICs are expected. Associated with Kr coefficient, transformer classification was made on the basis that 765 kV and 345 kV is single-phase (three separate cores) and the autotransformer and 154 kV is with a 3-phase, 5-legged transformer.

With the geoelectric field amplitude (1.2 V/km) and a northern direction (0 degree), GIC flows were analyzed in terms of DC voltage and DC current on transmission lines, and transformer neutral currents and its reactive power losses. The induced DC voltages on transmission lines are presented in Figure 4. Various levels of DC voltages appeared because of their dependence on the length as well as on the placement of a transmission line. The largest DC voltage in absolute value was 111.85 V on

93.36 km transmission line, making angles of 183.33 degrees with respect to the northern direction. Figure 5 shows the GIC amp per phase in absolute value on transmission lines. A maximum value of 185.58 A was found. GIC neutral currents of transformers are shown in Figure 6. The maximum GIC neutral current per phase flowed through one of the generator step up (GSU) transformers at a nuclear power plant, of which the value was 51.13 A. It should be noted that this GIC amplitude was smaller than 75 A, the allowable maximum value of the NERC guideline. The additional reactive power demands of transformers were also investigated. The largest reactive losses were identified with a 765 kV transformer and its value was 37.16 Mvar.

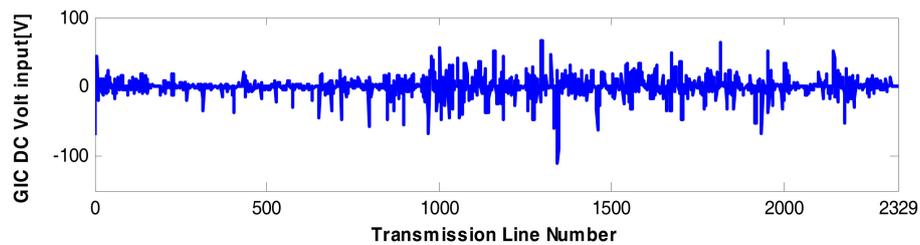


Figure 4. Geomagnetically induced currents (GIC) direct current (DC) volts on the Transmission Line.

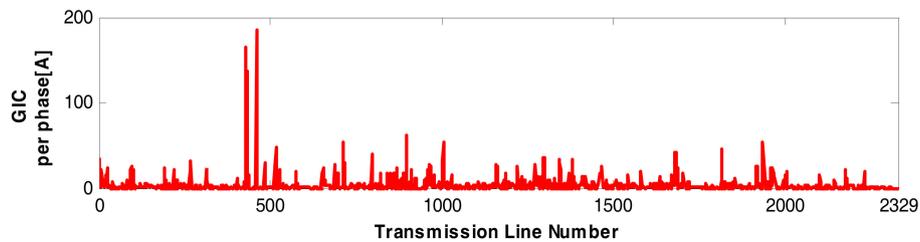


Figure 5. GIC per phase (in absolute value) on the Transmission Line.

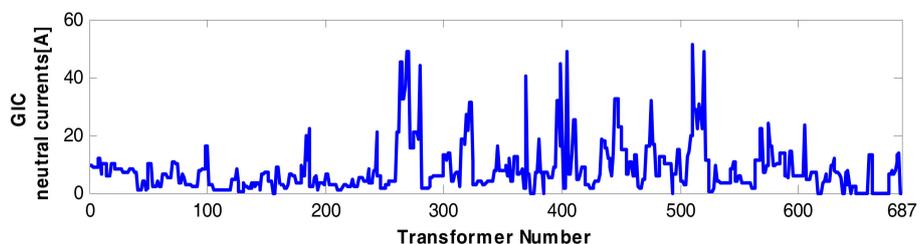


Figure 6. Transformer neutral currents (in absolute value).

Total sum of reactive losses absorbed at all the system transformers is given in Table 4. Maximum and minimum values were obtained by considering the variation of the geoelectric field direction. The amount of maximum losses was 1145.5 Mvar when the geoelectric field had an orientation of 114 degrees. The minimum value was 883.6 Mvar with a direction of 26 degrees. For the purpose of comparison, when the amplitude of geoelectric field was increased to 6 V/km (effectively the same as 60 V/km at the reference location), reactive power losses are accordingly increased by about five times as shown in Table 4.

The additional reactive power consumptions lead to the change of system voltage levels. The change was analyzed, taking account both reactive power losses from the event, with 1.2 and 6 V/km in Table 4.

Table 4. Additional Mvar losses at transformers with 1.2 V/km geomagnetic disturbances (GMD) in a Korean power system.

E-Field Direction (Degrees)	Mvar Losses with 1.2 V/km	Mvar Losses with 6 V/km	Remark
0	961.4	4807.1	-
114	1145.5	5727.4	Maximum
26	883.6	4417.7	Minimum

The simulation results are provided with the contour plot in Figure 7. The plot shows the difference in bus voltage magnitude between before and after the GMD impacts. The addition of reactive power losses (961.4 Mvar) resulted from the 1.2 V/km strength led to a voltage variation between 0.023 p.u. and -0.007 p.u. As shown in the Figure 7, the changes were very small over the system. This is because an additional 961.4 Mvar in losses are not big enough compared to the total reactive power generation of 19,450 Mvar. It was interesting to find the voltage increase, as represented with red color in the contour plot. The cause of the increase was due to switched shunt devices providing the reactive power supports to maintain a specified voltage level at the bus. The largest support was 55.04 Mvar, which increases the voltage level by 0.023 p.u. Figure 7 also shows the voltage profiles with the 6 V/km geoelectric field. Compared to the change from 1.2 V/km amplitude, most areas experienced a change in system voltage, especially a decrease, ranging from 0.018 p.u. to -0.015 p.u. A violent storm, with the amplitude of 60 V/km at the reference location, would not bring about a voltage collapse in a Korean power system.

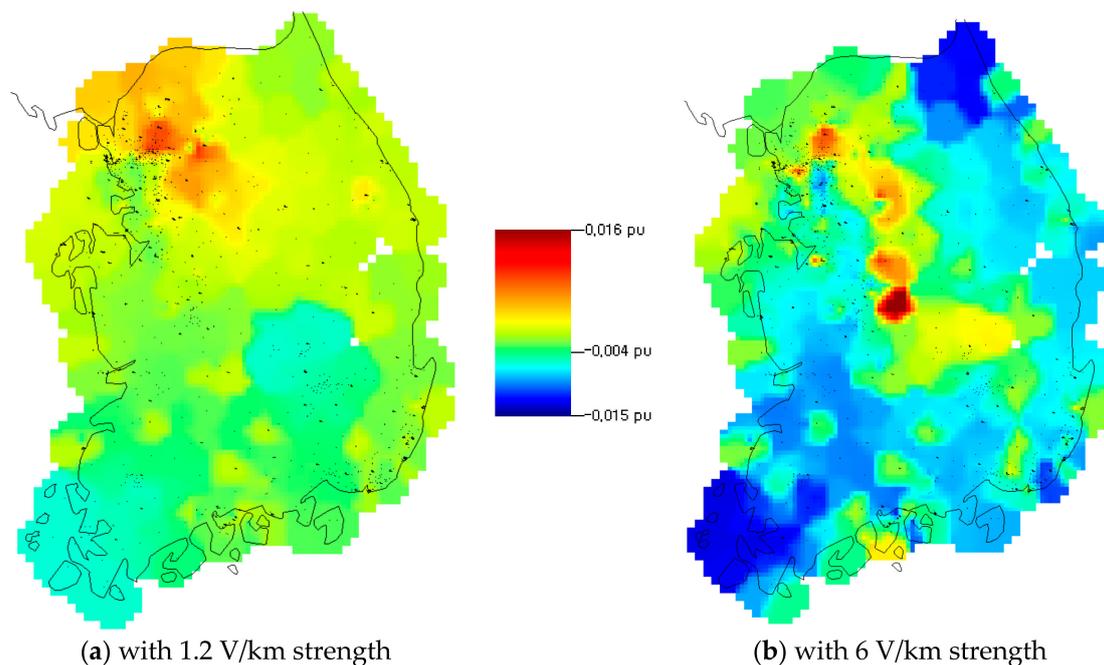


Figure 7. Contour plot of voltage differences before and after GMD.

5. Conclusions

The potential for GMDs to impact the operation of power systems has been a growing concern. Though representative events have occurred mostly in the higher-latitude regions, several failures have been reported at mid and lower latitude regions. Thus, careful considerations are required to monitor the GIC flows and analyze the impact on the bulk power system and if needed, mitigation plan should be prepared. This paper presents the vulnerability assessment of Korean electric power grid with the presence of GMDs. First, the amplitude of geoelectric field is calculated using the

magnetometer data. It is identified that the largest GMD producing the geoelectric field strength of 0.6 V/km occurred on 24 December 2001. Second, based on the benchmark event proposed by the NERC, DC voltages, and GIC currents on transmission lines, GIC neutral currents in transformers are obtained. When Korean power systems are exposed to 1.2 V/km geoelectric field, the maximum GIC neutral is estimated to be 51.13 A, which satisfies the NERC standard defining 75 A as the maximum allowable current. Reactive power losses and the change of voltage profiles are also studied. If a super-mega storm with 6 V/km in Korea (effectively same as 60 V/km at a reference location, latitude of 60 degrees) takes place, the Korean power system will not show big changes in voltage magnitudes and will maintain system voltage stability.

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