



Article Optimization of Component Sizing for a Fuel Cell-Powered Truck to Minimize Ownership Cost

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Abstract: In this study, we consider fuel cell-powered electric trucks (FCETs) as an alternative to conventional medium- and heavy-duty vehicles. FCETs use a battery combined with onboard hydrogen storage for energy storage. The additional battery provides regenerative braking and better fuel economy, but it will also increase the initial cost of the vehicle. Heavier reliance on stored hydrogen might be cheaper initially, but operational costs will be higher because hydrogen is more expensive than electricity. Achieving the right tradeoff between these power and energy choices is necessary to reduce the ownership cost of the vehicle. This paper develops an optimum component sizing algorithm for FCETs. The truck vehicle model was developed in Autonomie, a platform for modelling vehicle energy consumption and performance. The algorithm optimizes component sizes to minimize overall ownership cost, while ensuring that the FCET matches or exceeds the performance and cargo capacity of a conventional vehicle. Class 4 delivery truck and class 8 linehaul trucks are shown as examples. We estimate the ownership cost for various hydrogen costs, powertrain components, ownership periods, and annual vehicle miles travelled.

Keywords: fuel cell powered vehicle; medium- and heavy-duty trucks; component sizing; ownership cost; optimization

1. Introduction

Automotive powertrains are being electrified to achieve lower emissions and higher fuel efficiency. Along with battery-powered trucks, fuel cell-powered electric trucks (FCETs) are a promising candidate to replace conventional vehicles [1]. Researches done in California have shown feasibility of this technology for certain types of medium- and heavy-duty trucks [2]. Interest in FCETs for medium-duty vocational trucks such as parcel or package delivery has increased. United Parcel Service (UPS) has unveiled its first prototype for a fuel cell-powered van, and FedEx Express has started delivery using FCETs, which in this case are fuel cell range extenders (FCRExs). FCRExs rely primarily on a battery for power and energy, and they carry a fuel cell to extend the range of the battery pack [3]. The range extender enables the vehicle to cover longer distances that would be difficult with the battery pack alone. In addition, the battery is also used as a buffer for high power and for collecting regenerative energy like a hybrid electric vehicle.

A great deal of work has been done on fuel cell electric vehicle (FCEV) control strategies to improve overall fuel efficiency. In [4], the authors proposed control strategies ruled by fuel cell power. Hames et al. [5] compared different control strategies. However, hybrid powertrains with two or more power sources should optimize powertrain component sizes before developing their energy management control strategy. Fuel efficiency and vehicle performance are always dependent on the sizes of vehicle components. Moreover, improper component sizes can increase vehicle cost, which

makes the vehicle unattractive for the consumer to purchase. It is important to define the component system. Fauvel et al. [6] and Kim et al. [7] proposed and validated component sizing processes for hybrid electric vehicle (HEV) powertrain configurations. Marcinkoski et al. [8] optimized component sizes to replace diesel trucks with FCETs while ensuring equivalent performance. Bendjedia et al. [9] presented a methodology to size the energy storage system for different batteries by considering weight, cost, and battery volume. Unlike the presented rule-based sizing processes, Lee [10] proposed a sizing process to minimize fuel consumption with an optimization algorithm to search for an optimum value. It is called POUNDERS (practical optimization using no derivatives for sums of squares), and was developed by Argonne National Laboratory [11]. Using this process, we focused on vehicle ownership costs, including the cost of fuel consumption. Eren et al. [12] sized FCEVs based on, but they did not consider costs that occur when a vehicle is purchased and is being used.

Consumers want to know how much a vehicle will cost throughout the period of ownership; knowing this will help them decide which vehicle to purchase because they know how much money they need to own, purchase, sustain, and operate each vehicle. Total cost of ownership (TCO) is all costs for these. TCO has been used for the estimation of market penetration and the market forecasting [13]. Some researchers have attempted to quantify this cost. The TCO varies in the definition. Mock et al. [14] specify a measure of relevant ownership cost (RCO). Simeu et al. [15] and Rousseau et al. [16] analyzed energy consumption and the costs of plug-in electric vehicles using RCO.

FCEVs use two different energy sources: a battery pack and a hydrogen tank. Properly sizing the fuel cell and the battery can reduce the overall cost of the vehicle while sustaining vehicle performance. The objective of component sizing is to help minimize the overall ownership cost of the FCEV. This paper seeks the optimal component size to minimize RCO for fuel cell hybrid vehicles. We use FCEV models developed in Autonomie and an optimization algorithm from POUNDERS to simulate and optimize a medium- and heavy-duty trucks. The paper is organized as follows. In Section 2, we review rules based on design assumptions from an earlier study. In Section 3, we propose a sizing process based on the cost of ownership and on performance. Sections 4 and 5 describe case studies for a class 4 delivery van and a class 8 linehaul truck, respectively. We analyzed how the sizing result that minimizes the ownership cost changes when some assumptions change. Finally, Section 6 provides a conclusion.

2. Rule-Based Design Process Assumptions

Here we review rule-based design logic from a prior study [8] for fuel cell-powered trucks. In the U.S. Department of Energy, all vehicles are classified based on the gross vehicle weight rating (GVWR), ranging from class 1 to class 8 [17]. We focus on a class 4 delivery van and a class 8 linehaul truck as shown in Table 1 for conventional vehicle simulations. Control algorithms and component sizes determine whether the vehicles are charge-sustaining or range-extended hybrids. There are two powertrain architectures. One is a battery-powered electric vehicle with a fuel cell range extender, called a FCREx. The other is a fuel cell-dominant system with a battery for peak acceleration events, which is known as a fuel cell hybrid electric vehicle (FCHEV). In FCRExs, the electric machine is sized to match baseline vehicle performance. The fuel cell meets the demands of continuous loads. The battery can assist on a road with a 6% grade for 18 km and is sized to drive 50% of daily driving range in electric vehicle (EV) mode, using only electric power. The hydrogen storage is sized to extend this range. The electric range assumption may not be optimum in this case, but it serves as the FCREx baseline for this analysis.

I	Properties		Class 8 Linehaul Truck	
Summary	Daily driving range Baseline power	321.9 km 149 kW	643.7 km 336 kW	
	Cargo mass	2395 kg	19,908 kg	
	Cruising speed	112.7 km/h	96.6 km/h	
Performance	6% grade speed	66.0 km/h	49.9 km/h	
	0–48 km/h accel. time	8.0 s	17.1 s	
	0–97 km/h accel. time	34.2 s	61.1 s	

Table 1. Conventional vehicle simulations.

Likewise, FCHEVs are also evaluated for performance. Fuel cells are sized to meet continuous loads for cruise and grade. The electric machine is sized for performance. The battery is sized for both performance and regenerative braking. Hydrogen storage is sized to satisfy daily driving requirements. We see that this sizing approach results in fuel cell-powered trucks that can match or outperform conventional vehicles, with no sacrifices in payload. More information is found in [8]. One limitation of this study was that it did not consider the cost of building or operating the truck. In this paper, we propose an optimum sizing process for fuel cell-powered trucks that will minimize ownership cost while ensuring that performance goals are met.

3. Sizing Process Based on Cost of Ownership and Performance

3.1. Optimization Algorithm for Sizing Components

We used Autonomie to simulate the vehicle performance of a fuel cell-powered truck. Autonomie is a vehicle system simulation tool for the energy consumption and performance [18]. We optimized its onboard hydrogen storage and battery pack size to minimize the ownership costs. This ensures that all performance requirements are met within a 2% tolerance. Figure 1 shows a sizing process. Input variables to be optimized are hydrogen tank, battery capacity, and fuel cell power. When the three input variables change, the vehicle model developed performs the three-vehicle performance test while checking their constraints. Through the optimization process, the input parameters are modified using previous results. Then the feedback process runs until the algorithm finds the optimal value for the objective. It will find the tradeoff relationship between hydrogen storage and battery power. We propose optimization problem as follows:

$$\min_{i} \{ rco(r_i) : l_i \le r_i \le u_i, \, c_j(r_i) \le 0, \, i, \, j = 1, \, 2, \, 3 \}, \tag{1}$$

where *rco* is the RCO. It is minimized over r_i whose range is from lower limit l_i to upper limit u_i . The value of c_j represents the vehicle performance constraints. The subscript *i* represents different components and the *j* represents additional performance constraints.



Figure 1. Sizing process with vehicle simulation and POUNDERS (practical optimization using no derivatives for sums of squares).

We used the optimization algorithm for components as the POUNDERS. The POUNDERS is a derivative-free optimization to seek local solutions to a potentially multimodal problem, which is a bound-constrained augmented Lagrangian problem [10]:

$$\min_{r_i} \Big\{ h(r,s) = rco(r) - \sum_{j \in J} \lambda_j \big(c_j(r) + s_j \big) + \frac{\mu}{2} \sum_{j \in J} \big(c_j(r) + s_j \big)^2 : s \ge 0; \, 0 \le r \le u \Big\},$$
(2)

where *h* is a cost function value, *s* represents slack variables, λ_j is an estimate of Lagrangian multipliers, and μ is the penalty parameter for the constraints. If the constraints are not satisfied, the slack variables increase the cost function value, *h*.

The optimization process is conducted based on Autonomie including the POUNDERS, which developed using MATLAB/Simulink. We update the component cost estimate depending on the component sizes, and define the cost function, performance tests and constraints, as explained further in more detail. The cost is calculated by running the performance tests for each vehicle according to the powertrain components. Because the vehicle weight is different and the component performances change themselves, different powertrain components can affect the vehicle performances through the optimization process. Although the algorithm is one objective optimization, it is difficult to optimize powertrain component sizes to minimize the cost, while ensuring the performance. In this study, the process iterates more 31 times, sufficient to find an optimal value.

3.2. Relevant Cost of Ownership

RCO is the net present cost to own and operate the vehicle. It includes the investment cost with the purchase price and any fees, taxes, and incentive or disincentives. It also includes all operating costs, maintenance costs, and a resale or residual value. The following equation is a way to calculate the RCO. For more detail, see reference [16]:

$$rco = cost_{inv} + cost_{vv} = energy + cost_{vv} = maint + cost_{vv} = batt replace - cost_{residual},$$
(3)

where $cost_{inv}$ is total investment cost for purchase, initial registration, home electric vehicle service equipment, and vehicle incentive. The $cost_{pv_energy}$ value is the present value energy cost while considering vehicle fuel efficiency and the current costs of fossil fuel and hydrogen. The $cost_{pv_maint}$ is the present value of maintenance costs, repairs, and so on. The $cost_{pv_batt_replace}$ is the present cost of battery replacement. The $cost_{residual}$ is the residual value of function with initial cost, the vehicle's annual vehicle miles travelled (VMT), and a discount rate. Purchase price and fuel (or energy) costs are the primary variables for RCO. All other factors are either constants or a function of the purchase price.

We assume that the depreciation is 5%, and vehicle life is 15 years. We assume that the ownership period is 5 years but the actual value will depend on class and vocation. The Federal Highway Administration states that the average delivery truck travels an average of 21,108 km annually [19]. We assume that VMT is 22,531 km for class 4. However, class 8 drives more, so we assume 160,934 km per year.

To calculate the energy cost, we assume that the fuel price is \$3 per gallon and the hydrogen price is \$4 or \$12 per gasoline gallon equivalent (gge). We estimate the manufacturing cost based on component costs, which is based on 2017 FCTO/VTO Benefit Analysis Assumptions [20]. The purchase price is set at 1.5 times the cost of manufacturing. Battery cost is estimated using energy and power, which is \$243 per kilowatt-hour (kWh) and \$20 per watt (W). The fuel cell system is calculated using simplified cost calculations based on the peak efficiency of the stack and weight ratio for the tank. The values are based on the assumptions used for the Fiscal Year 2016 fuel cell technology analysis [21]. The cost of the fuel cell tank is estimated to be \$595 per kilogram of usable hydrogen at a 4.4% storage weight ratio. We estimate that the cost of the fuel cell system is \$50.69 per kilowatt (kW) at 59.5% efficiency.

Component size also affects vehicle weight, which affects specific power. We assume that the specific power of the fuel cell system is 659 W/kg [22,23]. Motor specific power is 1.9 kW per kilogram (kW/kg), based on U.S. Department of Energy (DOE) estimates [24].

3.3. Optimization Conditions and Vehicle Performance Requirements

There are three performance requirements by checking the car's driving range with all provided energy, an acceleration time, and a final vehicle speed on a specific grade. The car's range should be higher than 241 km on Air Resources Board (ARB) Transient cycle used by the U.S. Environmental Protection Agency (EPA) for class 4 vehicles. Likewise, the driving range for class 8 linehaul truck is 483 km at EPA's 105 km/h rating because the truck drives more highway over long distances. Next, the acceleration time includes the period from stationary to 97 km/h; this may be lower than 34 s for class 4 and 64 s for class 8. In the grade speed test, the vehicle runs on a road with a 6% grade; the end speed should be 66 km/h and 48 km/h for class 4 and class 8, respectively, which is an approximation for the Davis Dam test [25].

4. Case Study 1: Optimizing a Class 4 Delivery Van

4.1. Fuel Cell Range Extenders

The first type of truck we decided to target is a medium-duty or class 4 pickup or delivery van. It has a cargo mass of 2800 kg, just like the conventional baseline. As mentioned above, FCREx is battery-dominant and similar to a series hybrid electric vehicle that uses a fuel cell instead of an internal combustion engine. Figure 2 shows the configuration of the FCEV in Autonomie. This fuel cell connects to the battery for charging. As the battery becomes fully charged, an electric motor runs the vehicle using electrical energy. When it runs on the electrical energy and uses hydrogen with the fuel cell system while its battery sustains a certain charge state, this is called charge sustaining mode. FCRExs often use power from both the battery and the fuel cell when they need the large amounts of wheel power demanded for energy management control strategies. Table 2 shows vehicle

specifications. We do not expect much change in fuel cell power or motor power, because the vehicle should still meet all performance requirements.



Figure 2. Configuration of fuel cell electric vehicle (FCEV) in Autonomie.

Medium Duty	Vehicle Mass	Frontal Area	Drag Coefficient	Electric Motor	Fuel Cell Power	Battery Type	Battery Energy	On Board H ₂ Storage
Class 4	7317 kg	7.50 m ²	0.70	211 kW	100 kW	Li-ion	59 kWh	4 kg
Class 8	41,723 kg	10 m ²	0.55	870 kW	340 kW	Li-ion	770 kWh	46.4 kg

Table 2. Vehicle specifications of a class 4 van and class 8 line haul truck.

Above all, the optimization technique needs to be verified against parameter sweeps for the test cases. For example, there are class 4 FCREx optimization results. The optimization is 4 times faster than parameter sweeps and yields better results. Figure 3a,b show feasible points for grade and range tests, respectively. Figure 3c shows sums the feasible ranges of Figure 3a,b. The right square magnified shows the related results. Blue circles are feasible points and red crosses are surrounding points. Red and blue stars are the estimated and POUNDERS results, respectively. Squares are POUNDERS tracking points. Each number next to a point is an RCO value. Some variables do not coincide exactly with the optimal value because the POUNDERS results can be one of the local optimums. We found the estimated optimal value by using the minimum value from the fixed grid data, which can reveal the optimal point because of low resolution, 7 by 7. The lowest RCO is located on the left side and bottom of Figure 3c. Therefore, the bottom left values within the feasible section are optimal, closer to the POUNDERS result. If the resolution for the estimated results rise to explore more points the current estimate did not identify, the new optimal point may be closer to the POUNDERS result. POUNDER



Figure 3. Feasible values of (**a**) range and (**b**) grade for 100 kW of fuel cell power, and (**c**) relevant ownership cost (RCO) results for the estimate and POUNDERS.

Optimized FCRExs have component size that are similar to FCHEVs, as shown in Figure 4. The FCREx can have the same hydrogen tank as FCHEV, but the different driving strategies of both vehicles increase the FCREx battery to achieve the same performance as FCHEV. Table 3 summaries optimization results and compares them with rule-based component sizes. There is tradeoff between fuel mass and battery capacity. The optimized vehicle has lower battery capacity and higher hydrogen mass. Some performance results are lower than those for the rule-based sizing, but they still meet performance requirements. The 0–97 km/h acceleration time increases, but it is still better than that of the conventional vehicle. Grade speed drops, because the battery is no longer assisting the fuel cell during grades. The total vehicle mass remains largely unchanged, although there is a small reduction of 76 kg. These results are independent of fuel cell cost, because fuel cell power remains the same in both cases. In this case, 100 kW of power is necessary to cruise at highway speeds. Therefore, the fuel cell cell cannot be further downsized.



Figure 4. Summary of optimized hydrogen tank and battery pack for class 4 fuel cell vehicles; the #1 case assumes a hydrogen cost of \$4/gge (gasoline gallon equivalent) and #2 assumes a hydrogen cost of \$12/gge.

Vehicle Type	Fuel Mass	Battery Capacity	Fuel Cell Power	RCO	Acc. Time	Range	Grade Speed
FCREx rule-based	4.0 kg	58.7 kWh	100.0 kW	\$79 <i>,</i> 588	17.3 s	237.2 km	74.7 km/h
FCREx optimized	6.2 kg	3.6 kWh	101.5 kW	\$60,586	21.9 s	241.4 km	64.2 km/h
Difference	55.0%	-93.9%	1.5%	-23.9%	26.6%	1.8%	-14.0%

Table 3. Comparison between the rule-based and optimized results. FCREx: fuel cell range extenders.

In addition, the optimum solution changes as hydrogen cost increases. We assume \$12 per gge of hydrogen, not \$4 per gge. Table 4 shows the optimized results, comparing hydrogen costs of \$4 and \$12. We observe larger battery capacity and reduced hydrogen fuel use as hydrogen cost increases. Figure 5 shows the RCOs for different hydrogen costs. The manufacturing cost rises with a larger battery and the energy cost increases. The RCO increased by about \$20,000 because of the increased energy cost. The overall component design remains fuel cell dominant.

Table 4. Optimized results according to hydrogen price.

H ₂ Cost	Fuel Mass	Battery Capacity	Fuel Cell Power	RCO	Range
\$4	6.217 kg	3.649 kWh	101.5 kW	\$60,586	241.4 km
\$12	6.095 kg	4.447 kWh	101.2 kW	\$80,231	241.2 km
Difference	-2.0%	21.9%	-0.3%	33.4%	-0.1%





4.2. Fuel Cell Hybrid Electric Vehicles

For a class 4 truck, the FCHEV is optimized to minimize its RCO. When we optimize components, the fuel cell power increases more than that of an FCREx. Because an FCHEV battery has less specific energy than that an FCREx, an FCHEV has a smaller capacity but its mass is higher. Therefore, an FCHEV needs more fuel cell power to reach the same performance as an FCREx. Figure 4 summarizes the optimal fuel tank and battery pack for an FCHEV and an FCREx. Specifically, optimizing battery size for FCHEV is important. Using the rule-based process in Section 2, the battery is sized for maximum regenerative braking. This helps improve overall vehicle fuel economy. Otherwise, optimization to minimize RCO shows that a 38% smaller battery is a better choice. This results in higher fuel consumption and higher operating cost. A smaller battery pack reduces fuel economy in the vehicle optimized for ownership cost. Table 5 shows how battery pack size affects fuel economy. Figure 6a shows battery power operating points and the optimized reduced operating range. Figure 6b,c are motor power and fuel cell power, respectively. The optimized battery reduces regenerative braking torque. Motor size remains unchanged due to performance requirements. As mentioned above, in the rule-based results, the battery is sized to maximize regenerative braking. In the optimized design, however, only the RCO value is considered for component sizing. By optimizing FCHEV components, the fuel mass and battery capacity decrease and the fuel cell power increases while satisfying vehicle performances. Although both processes ensure the same performance, the optimized design reduces RCO. Optimization strikes the right balance between higher initial cost and

higher operating cost. A large battery results in higher initial cost but increases fuel economy through additional regenerative braking. A small battery results in higher operating costs but reduces initial cost because the smaller battery is less expensive.

FCHEV	Rule-Based	Optimized
Fuel economy gasoline equivalent	10.7 km/L	10.4 km/L
Percent regenerative braking at battery	74.1%	63.0%
Battery capacity	2.85 kWh	1.76 kWh

Table 5. Comparison of results for rule-based and optimized FCHEVs.



Figure 6. Simulation results for rule-based and optimized FCHEVs: (**a**) battery power operating points, (**b**) motor power, and (**c**) fuel cell power.

When the ownership period and hydrogen cost increase, the optimum solution also changes. Next we consider an ownership period of 10 years and a hydrogen cost of \$12 per gge. Table 6 summarizes the results for an FCHEV. Fuel economy increases in importance due to the higher cost of fuel, making a larger battery feasible. This gets closer to the battery size necessary to minimize fuel consumption. The optimization led to a 0.7% drop in fuel economy, reducing the RCO by about \$1,000. The optimum solution is sensitive to ownership periods and hydrogen cost assumptions. We compare both rule-based and optimized RCOs for class 4 trucks, as shown in Figure 7. Case #1 results when the ownership period is 5 years and the hydrogen cost is \$4/gge. Case #2 results when the ownership period is 10 years and the hydrogen cost is \$12/gge. All other assumptions remain the same. In this case, the optimized FCREx is cheaper than the optimized FCHEV by about \$800. When the hydrogen cost is \$4 over a 5-year ownership period, FCHEV and FCREx RCOs decrease by 1.8% and 24.2%, respectively. On the other hand, when the hydrogen cost is \$12 over a 10-year ownership period, FCHEV and FCREx RCOs decrease by 0.5% and 9.4%, respectively. Infrastructure cost is not considered in this analysis. There is no cost assigned to downtime associated with charging.

FCHEV	Rule-Based		Optimized #1	Optimized #2
Ownership period	5 years	10 years	5 years	10 years
H ₂ cost	\$4/gge \$12/gge		\$4/gge	\$12/gge
H_2 mass	6.60 kg		6.34 kg	6.10 kg
Battery capacity	2.9	kWh	1.8 kWh	2.35 kWh
Fuel economy gasoline equivalent	10.7]	km/L	10.4 km/L	10.6 km/L
RCO	\$62,486	\$118,588	\$61,364	\$117,969

Table 6. Summary of results for class 4 fuel cell hybrid electric vehicle (FCHEV) with various assumptions.

120,000 100,000 80,000 Cost [\$] 60.000 40,000 20,000 0 Vehicle Manufacturing Vehicle Purchas e Price Vehicle Residual Value Present Value of Fue RCO of Vehicle Conventional 33.364 50.045 13.973 15.717 57.024 FC HEV; rule-based #1 43,658 65,487 18,268 62,486 7,023 FC REx; rule-based #1 60,786 91,179 25,415 8,952 79,950 FC HEV; optimized #1 42,483 63,724 17,778 7,129 61,364 FC REx: optimized #1 41.832 62.747 17.506 10.110 60.586 118,588 » FC HEV: rule-based #2 43.658 65.487 7.501 35.989 FC REx; rule-based #2 60,786 91,179 10,435 28,187 130,199 = FC HEV; optimized #2 42,917 64,376 7,374 36,245 117,970 FC REx; optimized #2 43,023 64,534 7,392 117,988 36,161

Figure 7. Comparison of relevant cost of ownership (RCO) for class 4 delivery van.

5. Case Study 2: Optimizing a Class 8 Linehaul Truck

Likewise, for a class 4 delivery van, we apply the optimum sizing process to FCREx and FCHEV class 8 linehaul trucks. The truck requires 483 km of range, less than 64 s of acceleration time, and 48 km/h of grade speed. For a class 8 linehaul truck, we modify this assumption: its VMT is 160,934 km per year and the fuel cell cost is \$200 per kW. A class 8 linehaul truck usually operates on the highway, so we simulate it on an EPA 65 driving cycle. Vehicle specifications appear in Table 2. Its objective is also to minimize RCO.

When components are optimized, an FCHEV is cheaper than an FCREx. The optimized FCREx relies primarily on onboard hydrogen storage. Table 7 summarizes the results for a class 8 linehaul truck. Figure 8 compares hydrogen mass and battery capacity sizes for an FCHEV and an FCREx. Battery size decreases from 770 kWh to 24 kWh, and the vehicle runs mostly in charge sustaining mode. Arbitrarily sizing the battery power to supply half the daily driving is not optimum. Fuel cell power and hydrogen storage compensates for the reduction in battery size. The fuel cell power and hydrogen storage increase by 50 kW and 22 kg, respectively. FCHEV sizing remains largely unchanged from the rule-based approach. The result chose a slightly smaller fuel cell and battery. This is likely because the optimization utilized the 2% tolerance allowed in grade speed and acceleration.

Table 7. Summary of	optimization resul	ts for a class 8 linehaul	truck driving 482.8 km.
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Vehicle Type	Fuel Mass	Battery Capacity	Fuel Cell Power	RCO	Acc. Time	Range	Grade Speed
FCHEV initial	60.0 kg	4.56 kWh	391.3 kW	\$848k	45.2 s	483.6 km	49.9 km/h
FCHEV optimized	60.2 kg	3.03 kWh	369.7 kW	\$836k	40.5 s	483.9 km	47.8 km/h
FCREx initial	43.0 kg	770 kWh	340.0 kW	\$1469k	30.6 s	482.8 km	51.5 km/h
FCREx optimized	65.3 kg	24.2 kWh	391.0 kW	\$904k	25.2 s	486.5 km	48.0 km/h



Figure 8. Summary of optimized hydrogen tank and battery pack for class 8 fuel cell vehicles.

The optimized FCREx has larger hydrogen tank than that of the optimized FCHEV. As the weight of the powertrain components increases, the optimization to satisfy the performances increases hydrogen tank as well as battery. The increased battery capacity increases the weight, and then the hydrogen tank also increases to cover longer distance.

The RCOs of class 8 linehaul trucks are compared in the rule-based technique and optimized as shown in Figure 9. A fuel cell-dominant hybrid is the most economical design choice for a class 8 linehaul fuel cell truck. The present value of costs is almost as high as the purchase price. This indicates that this design solution depends on VMT, energy cost, and duration of ownership. An FCHEV has the lower fuel cost in this case.



Figure 9. Comparison of relevant cost of ownership (RCO) for a class 8 linehaul truck.

For longer distance class 8 linehaul trucks, we changed the optimization objective to 644 km. We assume that the cost of hydrogen increases to \$12 per gge. Onboard hydrogen storage increases by optimizing components. Table 8 summarizes the results. Hydrogen storage increases by 20 kg for 161 km. It needs more fuel cell power to sustain both grade speed and acceleration performance. FCREx sizing increases fuel cell power by about 50 kW and FCHEV sizing also increases fuel cell power by 10 kW to compensate for the loss in battery power. EPA 65 may not offer many opportunities for regenerative braking either. The impact of battery size on fuel economy is not very prominent.

Vehicle Type	Fuel Mass	Battery Capacity	Fuel Cell Power	RCO	Acc. Time	Range	Grade Speed
FCHEV optimized	80.7 kg	3.02 kWh	377.6 kW	\$1565k	40.6 s	643.9 km	48.0 km/h
FCREx optimized	85.8 kg	17.5 kWh	440.0 kW	\$1683k	27.6 s	643.6 km	53.6 km/h

Table 8. Optimization results for a class 8 linehaul truck driving 643.7 km.

We add the RCO obtained by optimizing a class 8 linehaul truck for 644 km to Figures 7 and 8. In a longer-range case, a fuel cell–dominant hybrid is also the most economical design for a class 8 linehaul truck. Higher hydrogen costs result that the present value of total fuel costs is more than twice the vehicle purchase price.

6. Conclusions

The optimum component size for an FCREx depends on the cost of hydrogen and the powertrain components, the length of the ownership period, and VMT. Optimum component sizing for an FCHEV is less sensitive to these factors. The optimum design for an FCREx relies primarily on onboard hydrogen storage for energy. The proposed sizing process finds economically optimum design solutions for fuel cell vehicles while ensuring that there is no tradeoff in performance. For class 4 delivery trucks, optimized FCRExs and FCHEVs have comparable component sizes and RCO estimates. The FCREx ownership costs is slightly less than that of FCHEV by 1.3%. For a class 8 linehaul truck, the RCO of an FCHEV is 7.5% lower than that of an FCREx design. The energy cost may be equal to the initial cost. Therefore, a higher hydrogen cost could affect the solution. In this study, we do not consider the cost associated with infrastructure or downtime for charging. They need to be factored in later when comparing the RCOs of different powertrains. We expect that the proposed sizing process will use representative real-world cycles for sizing and cost estimates and for linking fuel cell cost to the power and operating conditions of load levels, duration, and so on.

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