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Influence of Li₂O Incrementation on Mechanical and Gamma-Ray Shielding Characteristics of a TeO₂-As₂O₃-B₂O₃ Glass System

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Abstract: According to the Makishema–Mackenzie model assumption, the dissociation energy and packing density for a quaternary TeO₂-As₂O₃-B₂O₃-Li₂O glass system were evaluated. The dissociation energy rose from 67.07 to 71.85 kJ/cm³, whereas the packing factor decreased from 16.55 to 15.21 cm³/mol associated with the replacement of TeO₂ by LiO₂ compounds. Thus, as a result, the elastic moduli (longitudinal, shear, Young, and bulk) were enhanced by increasing the LiO₂ insertion. Based on the estimated elastic moduli, mechanical properties such as the Poisson ratio, microhardness, longitudinal velocity, shear velocity, and softening temperature were evaluated for the investigated glass samples. In order to evaluate the studied glasses' gamma-ray shield capacity, the MCNP-5 code, as well as a theoretical Phy-X/PSD program, were applied. The best shielding capacity was achieved for the glass system containing 25 mol% of TeO₂, while the lowest ability was obtained for the glass sample with a TeO₂ concentration of 5 mol%. Furthermore, a correlation between the studied glasses' microhardness and linear attenuation coefficient was performed versus the LiO₂ concentration to select the glass sample which possesses a suitable mechanical and shielding capacity.

Keywords: mechanical properties; shielding properties; elastic moduli; Monte Carlo simulation



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1. Introduction

The field of radiation physics concerns the development of protective materials that are used to absorb radiation. These radiation shields are defined as any material used to attenuate photons, and are typically placed between the radiation source and the worker or patient. These shields are becoming increasingly more necessary as more fields begin using radiation on a daily basis [1–5]. Fields such as medicine, food conservation, and agriculture all rely upon radiation to fully function. Despite the benefits of radiation present across various fields of work, high-energy particles or ionizing radiation can be extremely harmful to the human body if underexposed for a long time. Some side effects of radiation exposure may include acute radiation syndrome, cutaneous radiation injuries, and cancer development. Radiation shields work to minimize these effects and protect humans that may come into contact with ionizing radiation [6–9].

When selecting a radiation shield for a specific application, several characteristics of how the radiation is being used must be known to utilize the best possible material.

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For example, concrete is commonly used against X-rays and neutrons, and is ideal for lining the walls of rooms. These properties make concretes suitable for lining the walls of nuclear reactors, for instance, but their lack of mobility and tendency to crack makes them unideal for other applications [10,11]. Other materials that have been used as radiation shields include alloys, composites, construction materials (such as granite and marble), and glass [12–16].

Glasses offer advantageous properties over other radiation shields because, in addition to their excellent shielding ability, they are transparent, are simple to manufacture, and can have a wide range of possible compositions. The structural, chemical, and shielding features of glasses can be changed by doping metal oxides and heavy metal oxides (HMOs) into the glass system. Metal oxides and HMOs act differently on the glass matrix, depending on their characteristics. There exist three different kinds of oxides: network formers, network modifiers, and intermediates [17–19].

Borate is commonly used as a glass former and is found in most commercial glasses. Borate can easily modify its coordination with three of four oxygen units to provide a strong and adjustable structural composition. This change increases its chemical and thermal resistance by creating non-bridging oxygens (NBOs). Additionally, borate glasses have a low viscosity, high chemical durability, high visible light transparency, low cost, and good mechanical stability. Despite the abilities of borate, it has a low density, which is undesirable by itself. Other metal oxides and HMOs are added to borate glasses to improve their density [20,21].

Tellurite, or TeO_2 , is a glass intermediate with a high dielectric constant, a good electrical conductivity, transparency in visible and infrared light, and good solubility of rare-earth ions. Tellurite glasses can be used as planar waveguides and optical amplifiers in optical applications, but have also been used in radiation shielding applications. Tellurite has a high density and atomic number, making it a HMO [22,23]. Due to tellurite being an intermediate, it does not form a stable glass system by itself due to its weak connectivity. By pairing TeO_2 with oxides, such as B_2O_3 , its stability can be increased. Borotellurite glasses have high stability and transparency and are used in fiber-optic communication systems and nonlinear optical devices.

In order to assess the capability of a medium to become a radiation shield, several parameters must be calculated and analyzed. These parameters are typically calculated experimentally, but simulations are often used to validate the obtained data. Simulations also offer the ability to test samples before spending the time and cost fabricating them, and if they demonstrate potential, they can then be experimentally examined. Simulations have also proven to be extremely reliable in correctly assessing the shielding ability of a sample across a wide range of energies [24,25].

The novelty of the present study lies in the application of the Makishima–Mackenzie (M–M) model to predict the elastic and mechanical characteristics of As_2O_3 - B_2O_3 - Li_2O -based tellurite glasses. Moreover, the radiation shielding properties of the mentioned glasses were evaluated using the Monte Carlo simulation method. Additionally, the accumulation of photons in air and inside the investigated glasses was calculated via the Phy-X/PSD program.

2. Materials and Methods

2.1. Mechanical Properties

The mechanical features (Poisson ratio, microhardness, fractal bond conductivity, and longitudinal and shear velocities), as well as elastic moduli (EM) (Young, shear, longitudinal, and bulk), were investigated for five glass samples reported by [26]. The mentioned glass system contained $\text{TeO}_2\text{-As}_2\text{O}_3\text{-B}_2\text{O}_3\text{-Li}_2\text{O}$ in composition. Based on the foundations approved by Makishema and Mackenzie [27,28], the EM were computed. The dissociation

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energy (G_t) is a measure for the heat of formations (enthalpy) required to fabricated the glass system. The following equation describes it.

$$Gt\left(\frac{kJ}{cm^3}\right) = \sum X_i G_i \tag{1}$$

 X_i is fractional by mol of the constating compounds. The packing density is an essential factor related to the oxide and metal ionic radius R_o and R_M . The V_t is evaluated using Equation (2), where V_i is the packing factor of the constituting compounds.

$$Vt = \left(\frac{\rho}{MW}\right) \times \sum X_i V_i \tag{2}$$

The previously calculated values for G_t and V_t were used to compute Young (E), shear (K), longitudinal (L), and bulk (B) modules, as presented in Equations (3)–(6). In addition, some mechanical properties based on that derived from the EM were evaluated in Equations (7)–(9), such as the Poisson ratio (σ), the microhardness (H), softening temperature (T_s), and fractal bond connectivity (d) [29].

$$E = 2 V_t G (3)$$

$$B = 1.2 V_t E \tag{4}$$

$$S = \frac{3EB}{(9B - E)} \tag{5}$$

$$L = B + \frac{3}{4} S \tag{6}$$

$$\sigma = 0.5 - \frac{1}{72} V_t \tag{7}$$

$$H = \frac{(1 - 2\sigma)}{6(1 + \sigma)} \tag{8}$$

$$T_{s} = \frac{M_{W}}{\left(\rho_{glass} \times C\right)} \times V_{s}^{2} \tag{9}$$

2.2. Gamma-Ray Simulation and Theoretical Calculations

The present study's second aim is to report the radiation protection capacity for the investigated TABLi samples. In order to achieve the desired target, the MCNP-5 [30] and a theoretical calculation program named Phy-X/PSD [31] were used to evaluate the protection ability. Both previous programs used the chemical compositions and densities of the investigated glasses to evaluate the shielding factors. On the other hand, there are differences in the nuclear libraries, which used to extract the interaction cross-sections. The MCNP-5 used ENDF/B-VI.8 as a primary source, but the Phy-X/PSD used only the NIST database. The geometry used in the MCNP-5 simulation was illustrated in Figure 1 and discussed in detail in many publications [32–34]. Additionally, the investigated glasses' chemical compositions were given in Table 1.

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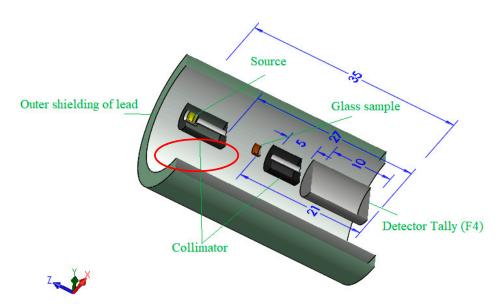


Figure 1. The Monte Carlo MCNP 3D simulation geometry is used in the present work.

Table 1. The chemical composition of the investigated glass samples.

		Composit	ion (wt%)		Density	MW	Vm	
	As_2O_3	B_2O_3	Li ₂ O	TeO ₂	(g/cm ³)	(g/mol)	(cm ³ /mol)	
TABLi5	19.217	40.574	1.451	38.757	3.71	102.95	27.72	
TABLi10	20.510	43.303	3.098	33.090	3.61	96.46	26.73	
TABLi15	21.988	46.424	4.982	26.607	3.50	89.98	25.72	
TABLi20	23.696	50.030	7.158	19.116	3.37	83.49	24.77	
TABLi25	25.692	54.244	9.701	10.363	3.19	77.01	24.14	

3. Results and Discussion

3.1. Mechanical Properties

The selected TABLi samples have a density (ρ , g/cm³) that decreased linearly from 3.714 to 3.190 g/cm³, as shown in Figure 2. The decrease in the glass density is related to the compactness of the glass materials, which is predicted through the distribution density for boron, D (B), and distribution density for Li, D (Li). The D (B) and D (Li) were calculated and showed in Table 2, where both D (B) and D (Li) increased with an increasing Li₂O concentration in the glass network. Thus, the density of the samples decreased. Table 2 also showed that the boron-boron separation, r (B-B), lithium-lithium separation, r (Li-Li), and tellurium-tellurium separation, r (Te-Te), decreased with an increasing Li₂O concentration in the glass network. This can be ascribed to the replacement of Te ions with a higher ionic radius ($R_{Te} = 2.22 \text{ Å}$) by a smaller Pauli ionic radius ($R_{Li} = 0.56 \text{ Å}$) for Li ions. Moreover, both the molecular weight (MW, g/mol) and molar volume (V_{M} , cm³/mol) follow the ρ trend, where they decreased from 102.949 to 77.005 g/mol and from 27.719 to 24.140, for Mw and V_{M} , respectively.

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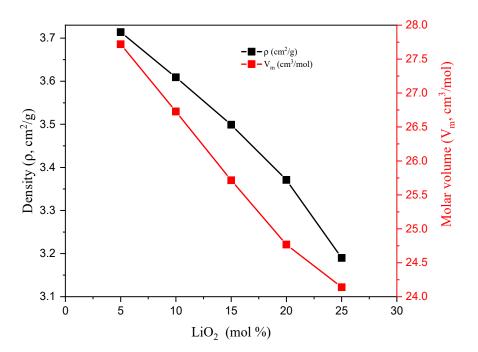


Figure 2. Variation in the density and molar volume versus the LiO₂ concentration.

Table 2. Some mecl	nanical pro	perties for	the glasses	under study.

TABLi5	TABLi10	TABLi15	TABLi20	TABLi25
0.60	0.61	0.62	0.63	0.63
5177.61	5362.85	5568.19	5792.38	6022.41
2917.22	3005.14	3101.19	3207.99	3330.88
2.20	2.16	2.12	2.08	2.07
2.56	2.53	2.49	2.46	2.44
2.82	2.77	2.71	2.65	2.61
2.79	2.77	2.73	2.70	2.67
	0.60 5177.61 2917.22 2.20 2.56 2.82	0.60 0.61 5177.61 5362.85 2917.22 3005.14 2.20 2.16 2.56 2.53 2.82 2.77	0.60 0.61 0.62 5177.61 5362.85 5568.19 2917.22 3005.14 3101.19 2.20 2.16 2.12 2.56 2.53 2.49 2.82 2.77 2.71	0.60 0.61 0.62 0.63 5177.61 5362.85 5568.19 5792.38 2917.22 3005.14 3101.19 3207.99 2.20 2.16 2.12 2.08 2.56 2.53 2.49 2.46 2.82 2.77 2.71 2.65

In order to compute the elastic moduli (EM), Young (Y), shear (K), bulk (B), and longitudinal (L), the Makishima–Mackenzie (M–M) model assumptions were applied. Thus, both the investigated TABLi glasses' dissociation energy (G_t) and backing factor (V_i) were calculated. The G_t values were increased by replacing the TeO₂ with Li₂O compounds. This is attributed to the heat of formation (enthalpy, ΔH_f) of constituting compounds, where it is -561.2 kJ/mol for Li₂O and -270.3 kJ/mol for TeO₂. On the other hand, the glasses' packing factor (V_i, cm³/mol) was computed for the TABLi glasses with the help of the values of the ionic radius of Te, B, As, Li, and O. Figure 3 displays a reverse relationship between the V_i and Li₂O concentration. The Vi values decreased from 16.55 to 15.215 cm³/mol, increasing TeO₂ substitution by Li₂O. This can be attributed to the replacement of Te ions with a higher ionic radius (R_{Te} = 2.22 Å) by Li ions with a smaller Pauli ionic radius (R_{Li} = 0.56 Å).

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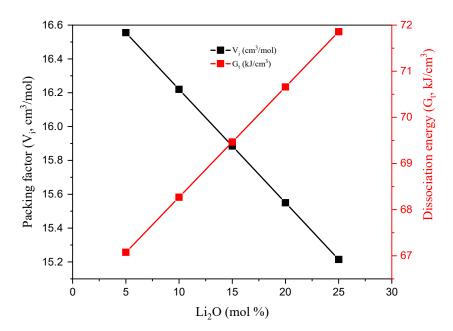


Figure 3. The investigated glasses' dissociation energy and packing factor versus the Li₂O concentration.

The TABLi glasses' packing density (V_t) was reported based on the predicted V_i values. V_t 's calculated values were 0.567 to 0.630, raising the ratio of Li ions in the glass network.

The elastic moduli (Y, K, B, and L) were reported for the investigated samples. Clearly, Y's modulus decreased by increasing the V_i values. But it is enhanced by increasing the G_t of the TABLi glasses, as shown in Figure 4. This is due to the substitution of weak Ti-O bonds by strong Li-O bonds. Additionally, Y's values enhanced from 80.120 to 90.579 GPa by raising the Li₂O between 5 and 25 mol%, respectively. The other moduli K, B, and L's values follow the same trend as Y when the Li₂O increases between 5 and 25 mol%.

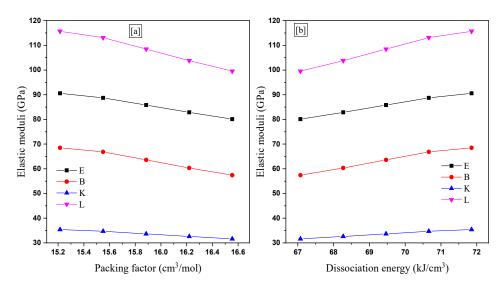


Figure 4. The elastic moduli (Y, B, K, and L) versus (a) packing factor and (b) dissociation energy.

The hardness (GPa) is considered an important parameter for shielding materials such as concretes and bricks, but in the case of small-scale materials, such as glass, the term microhardness (H, GPa) is applied. It is used to describe the load which the material can stand over without deformations. The TABLi glasses' microhardness presented in Figure 5 was enhanced from 4.900 to 5.199 GPa by increasing the Li₂O in the content. This can contribute to the increase in compactness of the material and decrease the r (B-B),

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r (Li-Li), and r (Te-Te) by increasing the Li ions in the glass network (Table 2). The Poisson ratio (σ) describes the expansion ratio of the investigated TABLi glasses in the direction vertical to the loader direction. Figure 5 showed that the σ values also increase from 0.267 to 0.280 with the replacement of TeO₂ with Li₂O content.

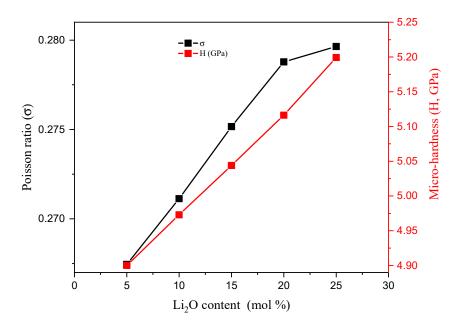


Figure 5. Variation in the Poisson ratio and microhardness for the fabricated TABLi glasses as a function of the Li_2O insertion ratio.

Softening temperature (T_g , °C) was reported for the TABLi glasses based on the EM predicted previously (see Figure 6). It is clear that the T_g 's values increased from 464.9 to 525.8 °C. The increase detected in T_g values is due to the replacement of T_g with a lower melting point (MP) by a higher (i.e., T_g), where the T_g 0 °C and T_g 1 °C.

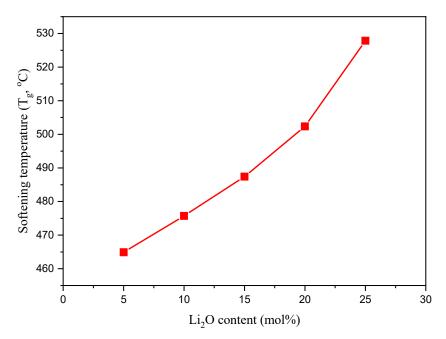


Figure 6. Variation in the softening temperature (T_g) versus the Ti₂O insertion ratio.

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The fractal bond conductivity (d) for the investigated glass samples decreased from 2.20 to 2.06. This means that the d values are close to two. Thus, the investigated glasses possess a two-dimensional layer structure network.

3.2. Shielding Properties

The glass understudy's effectiveness in resisting gamma quanta depends on the efficiency of the glass material in absorbing and attenuating incident gamma radiation. Therefore, essential shielding parameters such as radiation protection efficiency (RPE), linear attenuation (LAC), and mean free path (MFP) need to be studied. Awareness of these factors' performances makes it reasonable to assess the protection efficiency of and the suitable applications for utilizing the glasses to resist radiation. Figures 7-12 illustrate the data of simulated radiation shielding parameters computed via the MCNP-5 simulation code. It can be perceived in Figure 7 that the RPE results are influenced by the applied gamma photons' energy. The increment of the applied gamma energy leads to the decrement of the RPE values for the examined glasses. The following inferences can be interpreted from the examination of the reduction in the gamma radiation intensity with the variation of gamma energies. At low energies (0.0221-0.088 MeV), the investigated glasses appear to be effective at opposing incoming gamma radiation, with RPE values of approximately 100% for all investigated glasses. At the same time, the RPE values diminish with an increase in the gamma radiation intensity from 0.284 to 2.51 MeV based on the Li₂O concentration in the selected samples. The RPE values of the glasses with a high concentration of Li₂O (25% mol) have not exceeded 31% in the case of high gamma-quanta energy of 2.51 MeV. Thus, the obtained data for all investigated glasses illustrate that the glasses doped with 5% of Li₂O content are the preferable glasses that can be applied in the different radiation shielding implementations.

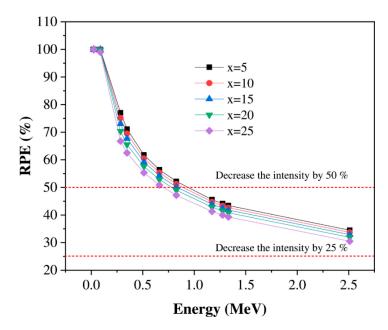


Figure 7. Variation in the investigated glasses' radiation protection efficiency (RPE) versus the photon energy.

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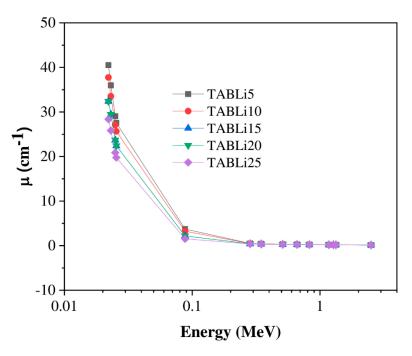


Figure 8. The studied glasses' linear attenuation coefficient vs the energy.

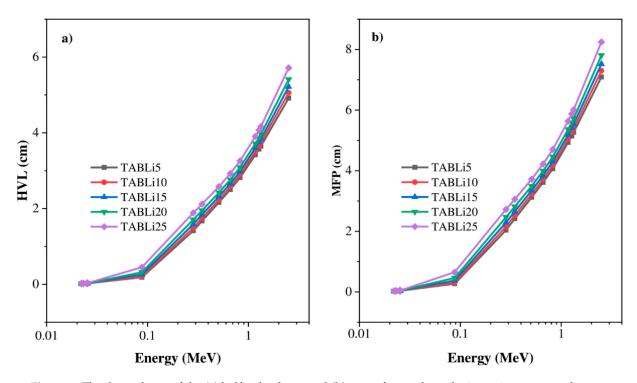


Figure 9. The dependence of the (a) half-value layer and (b) mean free path on the incoming gamma photons.

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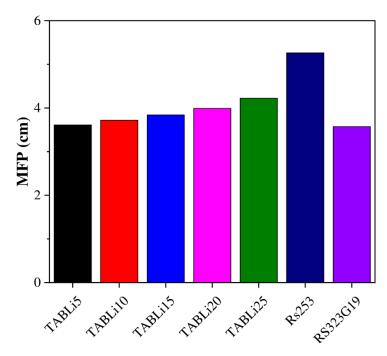


Figure 10. Comparison between the MFP of the studied glasses with some known commercial glasses (RS253 and RS323-G19).

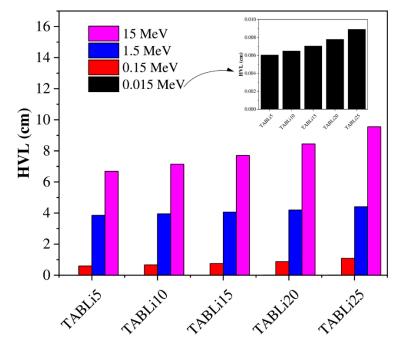


Figure 11. Variation of the investigated glasses' half-value layer versus LiO_2 concentration.

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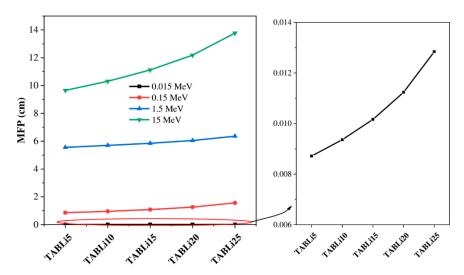


Figure 12. Variation of the investigated glasses' mean free path versus LiO₂ concentration.

Among the essential parameters of shielding properties is the linear attenuation coefficient (μ), which is used to display the ability of glass material to resist and absorb gamma quanta. Here in the present investigation, the μ is varied between low and high values depending on two parameters: the intensity of gamma-quanta energy and the concentration of dopant (Li₂O) in the studied glass material. The simulated μ values are deduced from the interaction of the gamma-quanta intensity (I) with the glass material at the known thickness (x), and represented in the following formula: ($\mu = \frac{1}{x} \ln \frac{I}{I_0}$). The data of μ depends on the interaction type of gamma quanta, and are explained as follows and plotted in Figure 8: the first interaction is a photoelectric effect (PE) which is achieved in the low gamma-quanta energy range (0.0221–0.088 MeV), and the μ data have appeared with the maximum values.

Successively, the increment of gamma-quanta energy above 0.1 MeV leads to a drop in the μ data as a result of the new interaction, namely Compton scattering (CS). Compton scattering is preponderant, and the inverse relation between CS cross-section and quanta energy was detected where $\sigma_{CS} \propto E^{-1}$ [35].

The μ data are manifested with the maximum values at the low applied gamma-quanta energy (0.0221 MeV). It was reduced from 40.5 to 28.3 cm $^{-1}$ for 5% mol and 25% mol of Li₂O content in the investigated glasses. In contrast, the μ data are observed with the minimum values at the highest applied gamma-quanta energy, 2.51 MeV, where it varies in decrement from 0.14 to 0.12 cm $^{-1}$ for 5% mol and 25% mol of Li₂O content, respectively.

Furthermore, the μ data impacted the insertion of Li₂O concentration in the studied glasses. At stationary gamma-quanta energy, the μ data are diminished with the addition of Li₂O content from 5 mol% to 25 mol% due to the molecular weight decrease from 102.95 to 77.01 g/mol for 5 mol% and 25 mol% of Li₂O content. Therefore, the effective atomic number (Z_{eff}) decreases. The maximum data of μ lessened in-between 40.5 and 0.14 cm $^{-1}$ for the studied glasses with 5 mol% content of Li₂O. The minimum data varied in decrement 8.89–0.03 cm $^{-1}$ and established at the examined glasses with 25 mol% content of Li₂O. Finally, the replacement of TeO₂ content with Li₂O content procures the decrement of μ data due to the direct proportionality between the cross-section of CS and the effective atomic number where σ_{CS} α Z_{eff} .

Agreement was detected between the obtained μ data with the kinds in the literature concerned with various types of tellurite glasses [36–38].

The other parameter is the mass attenuation coefficient (μ/ρ), which was computed via the MCNP-5 code based on the density of the investigated glasses, and compared with the theoretical data of μ/ρ , which was detected by Phy-X/PSD. The difference Δ (%)

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between the simulated and theoretical data was estimated by the next formula [39] and presented in Table 3:

$$\Delta (\%) = \frac{\left[\left(\frac{\mu}{\rho} \right)_{\text{MCNP}} - \left(\frac{\mu}{\rho} \right)_{\text{Phy-X/PSD}} \right]}{\left(\frac{\mu}{\rho} \right)_{\text{MCNP}}} \times 100$$
 (10)

The difference Δ (%) observed did not exceed 10% between all investigated TABLi glasses.

The HVL and the MFP are the radiation protection factors used to minimize the applied gamma-quanta energy to a half and display the distance between successive interactions. Contrarily, the μ data of simulated HVL are observed to rise with the applied gamma-quanta energy and the addition of Li₂O concentration in the TABLi glasses, as shown in Figure 9. The following formulas are applied to estimate the HVL and MFP:

$$HVL (cm) = \frac{\ln 2}{\mu} \& MFP (cm) = \frac{1}{\mu}$$
 (11)

The results presented in Figure 9 illustrate that an increment in the concentration of Li₂O in the glasses' structure and the creation of supplementary absorption bands assist in the reality that for dopant Li₂O contents of 5–25 mol% in the investigated glasses, the HVL and MFP diminish by 1.5 times. The difference revealed that the insertion of Li₂O could significantly decrease the thickness of the investigated glasses, without losing efficiency and minimizing the costs of production. The HVL data that reached the maximum values at the high gamma-quanta energy of 2.51 MeV ranged from 4.9 to 5.7 cm for TABLi5 and TABLi25, respectively, as well as the MFP data, which varied in an increase of 7.1 and 8.2 for TABLi5 and TABLi25, respectively. Furthermore, the investigated glasses' low HVL and MFP data are detected at the low applied gamma-quanta energy (0.0221 MeV). Moreover, the glasses' understudy with the lower content of Li₂O (5 mol%) is considered better than glasses with a high content of Li₂O. Consequently, it can be used in radiation protection applications. Based on the MFP data, the present glasses are compared with the commercial glasses RS253 and RS323-G19 [40] and plotted in Figure 10. The comparison displayed that the MFP values of studied glasses are lower than RS253 and comparable with the synthetic glasses RS323-G19. This means the examined glasses are suitable for application in the radiation protection fields, especially the glasses with 5% mol of Li₂O content (TABLi5) since the mean voyaged distance between two photo interactions is small.

Figures 11 and 12 depict the injection of $\rm Li_2O$ concentration in the tellurite glasses that impacted the HVL and MFP data. The Phy-x/PD computer program was employed to theoretically estimate the HVL and MFP data of the synthetic glasses. It is plain in Figures 11 and 12 that the TABLi5 glasses have the lowest data of HVL and MFP while the TABLi25 glasses have the highest data at all chosen gamma-quanta energies (0.015, 0.15, 1.5, and 15 MeV), and this agrees with their simulated data.

Furthermore, the Phy-x/PD was employed to compute radiation protection items, including glasses' effective atomic number ($Z_{\rm eff}$), equivalent atomic number ($Z_{\rm eq}$), as well as the accumulation factors, those being exposure buildup factors (EBF) and energy absorption buildup factor (EABF). Figures 13–18 depicted the acquired data, which were then addressed in the lines below.

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Table 3. The mass attenuation coefficient of the chosen glasses.

							Mass Attenu	ation Coeffi	cient (cm²/	(g)						
Energy		TABLi5			TABLi10			TABLi15			TABLi20			TABLi25		
(MeV)	MCNP-5	Phy- X/PSD	Δ (%)	MCNP-5	Phy- X/PSD	Δ (%)	MCNP-5	Phy- X/PSD	Δ (%)	MCNP-5	Phy- X/PSD	Δ (%)	MCNP-5	Phy- X/PSD	Δ (%)	
0.015		30.89			29.60			28.12			26.41			24.41		
0.022	10.91	10.92	-0.07	10.46	10.46	-0.05	9.95	9.95	-0.02	9.61	9.35	2.67	8.89	8.65	2.71	
0.023	9.69	9.69	-0.04	9.29	9.29	-0.01	8.83	8.83	0.03	8.73	8.30	4.94	8.10	7.68	5.18	
0.025	7.82	7.84	-0.18	7.50	7.51	-0.15	7.13	7.14	-0.10	7.02	6.71	4.42	6.54	6.21	4.99	
0.026	7.41	7.43	-0.23	7.11	7.12	-0.20	6.76	6.77	-0.15	6.65	6.37	4.26	6.19	5.89	4.88	
0.030		4.82			4.62			4.39			4.12			3.82		
0.050		4.19			3.71			3.17			2.54			1.80		
0.080		1.25			1.12			0.96			0.79			0.59		
0.088	0.95	0.98	-4.20	0.90	0.88	1.37	0.76	0.77	-0.58	0.64	0.64	1.26	0.48	0.48	0.45	
0.100		0.73			0.66			0.58			0.48			0.37		
0.150		0.31			0.29			0.26			0.23			0.20		
0.284	0.13	0.13	-0.33	0.13	0.13	-0.32	0.12	0.13	-0.30	0.12	0.12	-0.28	0.12	0.12	-0.25	
0.300		0.13			0.12			0.12			0.12			0.11		
0.347	0.11	0.11	-0.18	0.11	0.11	-0.17	0.11	0.11	-0.16	0.11	0.11	-0.15	0.10	0.10	-0.13	
0.500		0.09			0.09			0.09			0.09			0.09		
0.511	0.09	0.09	-0.18	0.09	0.09	-0.17	0.09	0.09	-0.16	0.08	0.08	-0.14	0.08	0.08	-0.12	
0.662	0.07	0.07	-0.22	0.07	0.07	-0.21	0.07	0.07	-0.19	0.07	0.07	-0.18	0.07	0.07	-0.16	
0.800		0.07			0.07			0.07			0.07			0.07		
0.826	0.07	0.07	-0.19	0.07	0.07	-0.18	0.07	0.07	-0.17	0.07	0.07	-0.16	0.07	0.07	-0.14	
1		0.06			0.06			0.06			0.06			0.06		
1.173	0.05	0.06	-0.90	0.05	0.06	-0.83	0.06	0.06	-0.75	0.06	0.06	-0.66	0.06	0.06	-0.55	
1.275	0.05	0.05	-0.76	0.05	0.05	-0.70	0.05	0.05	-0.63	0.05	0.05	-0.55	0.05	0.05	-0.46	
1.333	0.05	0.05	-0.72	0.05	0.05	-0.66	0.05	0.05	-0.59	0.05	0.05	-0.52	0.05	0.05	-0.43	
1.5		0.05			0.05			0.05			0.05			0.05		
2.506	0.04	0.04	-0.45	0.04	0.04	-0.43	0.04	0.04	-0.40	0.04	0.04	-0.37	0.04	0.04	-0.34	
3		0.04			0.04			0.04			0.04			0.04		
5		0.03			0.03			0.03			0.03			0.03		
8		0.03			0.03			0.03			0.03			0.02		
10		0.03			0.03			0.03			0.02			0.02		
15		0.03			0.03			0.03			0.02			0.02		

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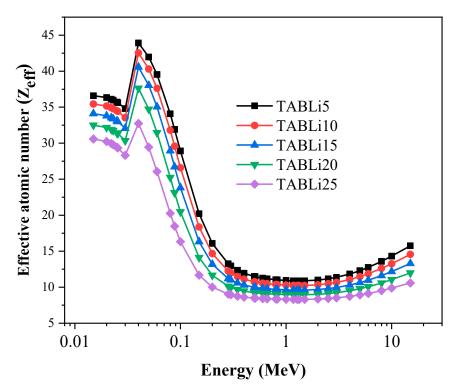


Figure 13. Variation of the studied glasses' effective atomic number (Z_{eff}) versus the gamma photon energy.

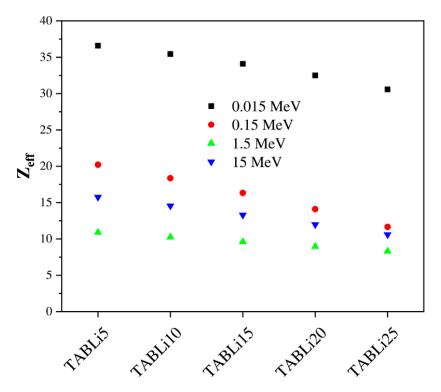


Figure 14. The dependence of the studied glasses' effective atomic number (Z_{eff}) on the LiO_2 concentration.

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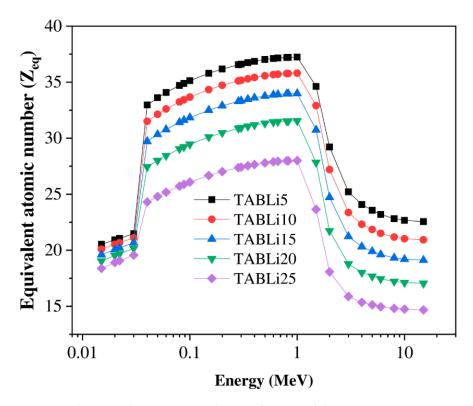


Figure 15. The equivalent atomic number as a function of the energy.

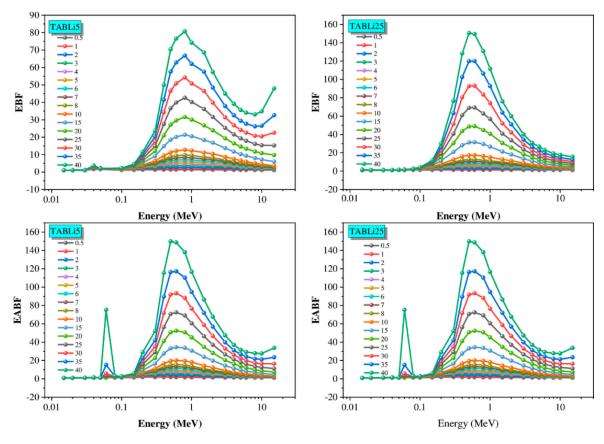


Figure 16. The buildup factors versus the energy.

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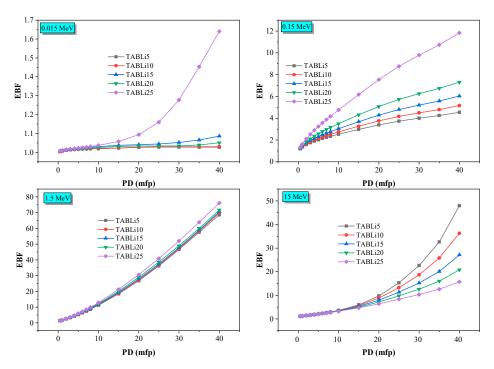


Figure 17. The exposure buildup factor (EBF) dependent on the penetration depth values (PD) at some fixed energies.

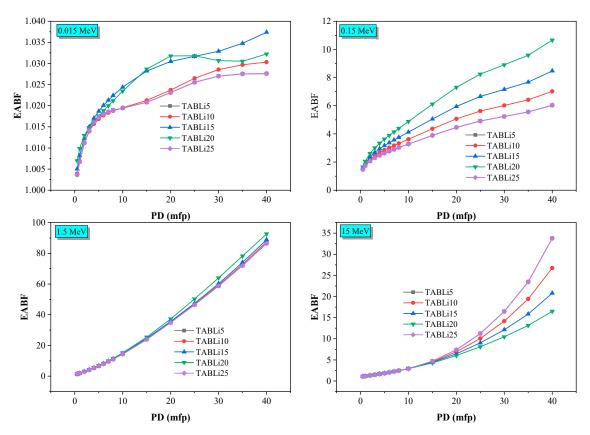


Figure 18. The EABF dependent on the penetration depth values (PD) at some fixed energies.

Figure 13 reveals the effective atomic number ($Z_{\rm eff}$) data that are designated to investigate the capacity of the synthetic glasses for serving in the implementations of gamma shielding. The data of $Z_{\rm eff}$ are changed with the gamma-quanta energy (0.015–15 MeV)

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and the Li_2O concentration (5–25 mol%) in the examined TABLi glasses. The Z_{eff} data are influenced by the gamma quanta interaction with the glass material. For low gamma-quanta energy range (0.015–0.1 MeV), the photoelectric effect (PE) interactions are dominant, and the maximum Z_{eff} data seem to be where Z^4 varied. After that, the Z_{eff} data diminished when the gamma-quanta energy increased. However, unpredicted peaks are observed at gamma-quanta energy 0.0318 MeV [41].

Then, the Compton scattering interactions are begun to possess gamma-quanta energy in the range of above 0.1 MeV, and the data of $Z_{\rm eff}$ are observed gradually in decrement where it altered with the atomic number (Z). The increase in gamma-quanta energy at high values leads to pair production, which varied with Z^2 [42]. Additionally, the $Z_{\rm eff}$ data reduced, as illustrated in Figure 14.

Figure 15 offers the equivalent atomic number (Z_{eq}) at various gamma photon energy. It is estimated according to the values of μ/ρ in addition to the atomic numbers of elements (Z1 and Z2) related to the ratios R1 and R2 as well as the ratio for the examined glasses at stationary gamma-quanta energy. Thus, Z_{eq} is estimated by the following formula $(Z_{eq} = \frac{Z1~(\log R2 - \log R) + Z2~(\log R - \log R1)}{\log R2 - \log R1}).$

It can be noticed that the Z_{eq} data increased with the increment of gamma-quanta energy up to 1 MeV. The maximum values of Z_{eq} are founded in the CS region (energy > 1 MeV). The maximum data of Z_{eq} are 37.23 and 28.01 for TABLi5 and TABLi25, respectively, while the minimum data are 22.56 and 14.68 for TABLi5 and TABLi25, respectively.

The total flux of gamma quanta in the studied glass material can be determined by utilizing two main buildup and accumulation factors: the EBF and the EABF. The alteration of EBF and EABF data with the gamma-quanta energy for the TABLi5 and TABLi25 glasses is plotted in Figure 16. The EBF and EABF data are computed according to the Z_{eq} values and the approximation of G-P fitting [43,44]. For instance, the Z_{eq} data and the five factors of GP fitting are presented in Table 4 for TABLi5 and TABLi25 glasses, respectively.

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Table 4 The CP titting narameters for t	ne TAT Bib sample at various	gamma energies
Table 4. The GP fitting parameters for t	ic 17 LDIS sample at various	gamma cricigics.

E (MeV)	7			EBF		EABF					
	Z_{eq}	a	b	с	d	Xk	a	b	с	d	Xk
0.015	20.53	-0.04	1.01	0.69	0.15	6.89	-0.02	1.01	0.68	0.14	9.31
0.02	20.93	0.26	1.02	0.39	-0.18	10.98	0.26	1.02	0.35	-0.20	12.47
0.03	21.49	0.22	1.05	0.37	-0.17	16.39	0.24	1.05	0.35	-0.16	14.46
0.04	32.96	0.19	2.04	0.33	-0.07	17.54	0.17	1.19	0.37	-0.20	24.68
0.05	33.61	0.02	1.88	0.23	-0.06	12.52	0.08	1.20	0.23	-0.04	11.06
0.06	34.08	0.61	1.67	0.21	-0.14	15.27	0.49	1.21	0.20	-0.17	14.70
0.08	34.71	0.47	1.42	0.25	-0.18	14.18	0.39	1.27	0.24	-0.17	14.22
0.1	35.13	0.23	1.22	0.40	-0.13	13.82	0.23	1.28	0.39	-0.13	16.50
0.15	35.79	0.14	1.36	0.57	-0.08	14.23	0.25	1.74	0.39	-0.15	13.85
0.2	36.17	0.12	1.56	0.64	-0.07	14.02	0.24	2.41	0.45	-0.16	13.80
0.3	36.61	0.05	1.69	0.84	-0.03	13.76	0.11	2.59	0.69	-0.08	13.59
0.4	36.85	0.02	1.78	0.98	-0.03	13.22	0.07	2.72	0.84	-0.07	13.30
0.5	37.02	0.00	1.82	1.05	-0.02	12.83	0.04	2.67	0.94	-0.05	13.10
0.6	37.11	-0.01	1.83	1.09	-0.02	12.13	0.02	2.59	0.99	-0.04	12.75
0.8	37.20	-0.02	1.82	1.12	-0.01	11.73	0.01	2.43	1.05	-0.03	12.06
1	37.23	-0.02	1.79	1.13	-0.01	11.49	0.00	2.29	1.07	-0.02	11.46
1.5	34.62	-0.03	1.68	1.17	0.01	12.99	-0.02	1.95	1.12	-0.01	10.71
2	29.21	-0.02	1.69	1.12	0.00	8.97	-0.02	1.84	1.11	-0.01	9.56
3	25.22	-0.01	1.63	1.06	-0.01	12.14	0.00	1.68	1.04	-0.02	12.39
4	24.08	0.01	1.56	1.02	-0.02	12.67	0.01	1.57	0.99	-0.03	13.43
5	23.57	0.01	1.49	1.00	-0.02	13.15	0.02	1.48	0.97	-0.04	14.30
6	23.20	0.02	1.45	0.97	-0.03	13.29	0.03	1.41	0.96	-0.04	13.75
8	22.82	0.03	1.36	0.96	-0.04	13.59	0.03	1.31	0.95	-0.04	13.19
10	22.67	0.04	1.31	0.94	-0.05	13.78	0.04	1.26	0.93	-0.05	14.08
15	22.56	0.05	1.21	0.93	-0.06	14.12	0.04	1.16	0.96	-0.04	14.54

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Figure 16 exhibits the variety of EBF and EABF data with the gamma-quanta energy up to 15 MeV. The EBF and EABF data seem to have their minimum values in the low gamma-quanta energy zone. This is due to the gamma photons passing through the studied glass material linked with the PE phenomena. In this region, the sharp peaks of both factors are reported around the quanta energy (0.0318 MeV). The increment of quanta energy leads to the increase in the accumulation of gamma photons inside the material, where the CS process is significant. The drop photons interacted with and penetrated the studied glass thickness while the rest of the photons are scattered to induce multiple interactions. In the CS region, the EBF and EABF data reach their maximum values. After that, it can be seen that the both factors began to decrease when the gamma-quanta energy had high values thanks to the third interaction as represented in the PP. (Mahmoud et al., 2020; YS. Rammah et al., 2020).

Furthermore, Figures 17 and 18 show that the EBF and EABF data impacted the penetration depth, which changes from 0.5 to 40 mfp at four specified gamma-quanta energies of 0.015, 0.15, 1.5, and 15 MeV, as well as the chemical composition of TABLi glasses.

Figures 17 and 18 manifested the exchange of EBF and EABF data with the penetration depth (PD) at identified gamma-quanta energy (0.015, 0.15, 1.5, and 15 MeV) prominently. The photon accumulation inside the glass material is associated with the distance that photons will travel as well as the time spent inside the investigated material. The low EBF and EABF data are identified at the short traveling distance (0.5 mfp), while the highest data was achieved at the long traveling distance (40 mfp). Moreover, the alteration of $\rm Li_2O$ within the examined glass material was due to the elevation of EBF and EABF.

Figure 19 showed the variation of the LAC and the microhardness (H) versus the Li₂O concentration. The LAC of the investigated samples diminished while the H values enhanced by increasing the Li₂O substitution ratio. The glass sample with Li₂O content of 5 mol% (TABLi5) has the highest LAC (LAC = 0.276 cm $^{-1}$) at energy 0.662 MeV, but the microhardness of the mentioned sample is relatively low (H = 4.900 GPa). In contrast, the sample with Li₂O content of 25 mol% (TABLi25) has the lowest LAC value (LAC = 0.236 cm $^{-1}$), but it has the highest H value (H = 5.199 GPa). Thus, the correlation showed in Figure 19 is used to predict which sample has both LAC and H suitable values. According to this relation, the sample with a suitable LAC and H contains around 16 mol% of Li₂O concentration. The microhardness of this glass (i.e., containing 16 mol% of Li₂O) is around 4.055 GPa, and the LAC is about 2.585 cm $^{-1}$.

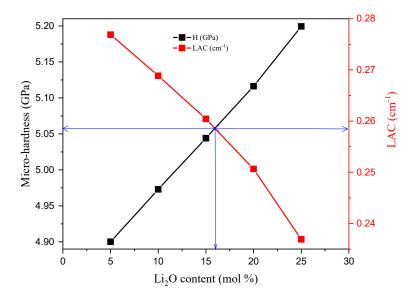


Figure 19. Relationship between the microhardness and the linear attenuation coefficient (LAC) for the various investigated samples.

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4. Conclusions

The microhardness and softening temperature, elastic moduli and Poisson ratio were calculated based on the M–M model. The microhardness and Poisson ratio were enhanced by the replacement of the TeO₂ by the Li₂O. The H values increased from 4.90 to 5.20 GPa, and σ values rose from 0.267 to 0.280, raising the Li₂O concentration between 5 and 25 mol%, respectively. The elastic Young, shear, longitudinal, and bulk modules were enhanced by increasing the Li ions in the glass network. Also, the shielding characteristics showed that the LAC was diminished with the replacement of Te by Li ions in the glass network. The LAC decreased from 30–90 to 24.40 cm⁻¹ at 0.015 MeV when the Li₂O concentration increased between 5 and 25 mol%, respectively. The HVLand MFP values increased by raising the Li₂O concentration in the glass network. Additionally, the accumulation of photons in air EBF and inside the glass layers (EABF) was increased by increasing the Li₂O concentration.

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References

- 1. Sayyed, M.I.; Al-Hadeethi, Y.; AlShammari, M.M.; Ahmed, M.; Al-Heniti, S.H.; Rammah, Y.S. Physical, optical and gamma radiation shielding competence of newly boro-tellurite based glasses: TeO₂–B₂O₃–ZnO–Li₂O₃–Bi₂O₃. *Ceram. Int.* **2020**, 47, 611–618. [CrossRef]
- 2. Abdel Wahab, E.A.; Koubisy, M.S.I.; Sayyed, M.I.; Mahmoud, K.A.; Zatsepin, A.F.; Makhlouf, S.A.; Shaaban, K.S. Novel borosilicate glass system: Na₂B₄O₇-SiO₂-MnO₂: Synthesis, average electronics polarizability, optical basicity, and gamma-ray shielding features. *J. Non-Cryst. Solids* **2021**, *553*, 120509. [CrossRef]
- 3. Dong, M.; Xue, X.; Yang, H.; Liu, D.; Wang, C.; Li, Z. A novel comprehensive utilization of vanadium slag: As gamma ray shielding material. *J. Hazard. Mater.* **2016**, *318*, 751–757. [CrossRef] [PubMed]
- 4. Obaid, S.S.; Sayyed, M.I.; Gaikwad, D.K.; Pawar, P.P. Attenuation coefficients and exposure buildup factor of some rocks for gamma ray shielding applications. *Radiat. Phys. Chem.* **2018**, *148*, 86–94. [CrossRef]
- 5. Dong, M.; Xue, X.; Yang, H.; Li, Z. Highly cost-effective shielding composite made from vanadium slag and boron-rich slag and its properties. *Radiat. Phys. Chem.* **2017**, *141*, 239–244. [CrossRef]
- 6. Sayyed, M.I.; Mhareb, Y.M.H.A.; Alajerami, S.M.; Mahmoud, K.A.; Imheidat, M.A.; Alshahri, F.; Alqahtani, M.; Al-Abdullah, T. Optical and radiation shielding features for a new series of borate glass samples. *Optik* **2021**, 239, 166790. [CrossRef]
- 7. Chanthima, N.; Kaewkhao, J.; Limkitjaroenporn, P.; Tuscharoen, S.; Kothan, S.; Tungjai, M.; Kaewjaeng, S.; Sarachai, S.; Limsuwan, P. Development of BaO–ZnO–B₂O₃ glasses as a radiation shielding material. *Radiat. Phys. Chem.* **2017**, *137*, 72–77. [CrossRef]
- 8. Yasmin, S.; Barua, B.S.; Khandaker, M.U.; Chowdhury, F.U.Z.; Rashid, M.A.; Bradley, D.A.; Olatunji, M.A.; Kamal, M. Studies of ionizing radiation shielding effectiveness of silica-based commercial glasses used in Bangladeshi dwellings. *Results Phys.* **2018**, *9*, 541–549. [CrossRef]
- Kaewjaeng, S.; Kothan, S.; Chaiphaksa, W.; Chanthima, N.; Rajaramakrishna, R.; Kim, H.J.; Kaewkhao, J. High transparency La₂O₃-CaO-B₂O₃-SiO₂ glass for diagnosis x-rays shielding material application. *Radiat. Phys. Chem.* 2019, 160, 41–47. [CrossRef]
- 10. Gökçe, H.S.; Yalçınkaya, Ç.; Tuyan, M. Optimization of reactive powder concrete by means of barite aggregate for both neutrons and gamma rays. *Constr. Build. Mater.* **2018**, *189*, 470–477. [CrossRef]
- 11. Şensoy, A.T.; Gökçe, H.S. Simulation and optimization of gamma-ray linear attenuation coefficients of barite concrete shields. *Constr. Build. Mater.* **2020**, 253, 119218. [CrossRef]

Materials **2021**, 14, 4060 20 of 21

12. Sayyed, M.I.; Jecong, J.F.M.; Hila, F.C.; Balderas, C.V.; Alhuthali, A.M.S.; Guillermo, N.R.D.; Al-Hadeethi, Y. Radiation shielding characteristics of selected ceramics using the EPICS2017 library. *Ceram. Int.* **2021**, *47*, 13181–13186. [CrossRef]

- 13. Yasmin, S.; Rozaila, Z.S.; Faruque-Uz-Zaman, K.; Barua, B.S.; Rashid, M.A.; Bradley, D.A. The radiation shielding offered by the commercial glass installed in Bangladeshi dwellings. *Radiat. Eff. Defects Solids* **2018**, 173, 657–672. [CrossRef]
- 14. Kaky, K.M.; Sayyed, M.I.; Ati, A.A.; Mhareb, M.H.A.; Mahmoud, K.A.; Baki, S.O.; Mahdi, M.A. Germanate oxide impacts on the optical and gamma radiation shielding properties of TeO₂-ZnO-Li₂O glass system. *J. Non-Cryst. Solids* **2020**, *546*, 120272. [CrossRef]
- Almuqrin, A.H.; Sayyed, M.I. Radiation shielding characterizations and investigation of TeO₂–WO₃–Bi₂O₃ and TeO₂–WO₃–PbO glasses. Appl. Phys. A 2021, 127, 1–11. [CrossRef]
- 16. Sayyed, M.I.; Mahmoud, K.A.; Lacomme, E.; AlShammari, M.M.; Dwaikat, N.; Alajerami, Y.S.M.; Alqahtani, M.; El-bashir, B.O.; Mhareb, M.H.A. Development of a novel MoO₃-doped borate glass network for gamma-ray shielding applications. *Eur. Phys. J. Plus* **2021**, *136*, 1–16.
- 17. Mhareb, M.H.A. Physical, optical and shielding features of Li₂O–B₂O₃–MgO–Er₂O₃ glasses co-doped of Sm₂O₃. *Appl. Phys. A* **2020**, *126*, 1–8. [CrossRef]
- 18. Yasaka, P.; Pattanaboonmee, N.; Kim, H.J.; Limkitjaroenporn, P.; Kaewkhao, J. Gamma radiation shielding and optical properties measurements of zinc bismuth borate glasses. *Ann. Nucl. Energy* **2014**, *68*, 4–9. [CrossRef]
- Sayyed, M.I.; Mahmoud, K.A.; Tashlykov, O.L.; Khandaker, M.U.; Faruque, M.R.I. Enhancement of the shielding capability of soda-lime glasses with Sb₂O₃ dopant: A potential material for radiation safety in nuclear installations. *Appl. Sci.* 2021, 11, 326.
 [CrossRef]
- 20. Abouhaswa, A.S.; Sayyed, M.I.; Mahmoud, K.A.; Al-Hadeethi, Y. Direct influence of mercury oxide on structural, optical, and shielding properties of a new borate glass system. *Ceram. Int.* **2020**, *46*, 17978–17986. [CrossRef]
- 21. Alajerami, Y.S.; Drabold, D.; Mhareb, M.H.A.; Cimatu, K.L.A.; Chen, G.; Kurudirek, M. Radiation shielding properties of bismuth borate glasses doped with different concentrations of cadmium oxides. *Ceram. Int.* **2020**, *46*, 12718–12726. [CrossRef]
- 22. Sayyed, M.I. Bismuth modified shielding properties of zinc boro-tellurite glasses. J. Alloys Compd. 2016, 688, 111–117. [CrossRef]
- 23. Al-Hadeethi, Y.; Sayyed, M.I. A comprehensive study on the effect of TeO₂ on the radiation shielding properties of TeO₂–B₂O₃–Bi₂O₃–LiF–SrCl₂ glass system using Phy-X/PSD software. *Ceram. Int.* **2020**, *46*, 6136–6140. [CrossRef]
- 24. Aygün, B. High alloyed new stainless steel shielding material for gamma and fast neutron radiation. *Nucl. Eng. Technol.* **2020**, *52*, 647–653. [CrossRef]
- 25. El-Mallawany, R.; El-Agawany, F.I.; Al-Buriahi, M.S.; Muthuwong, C.; Novatski, A.; Rammah, Y.S. Optical properties and nuclear radiation shielding capacity of TeO₂-Li₂O-ZnO glasses. *Opt. Mater.* **2020**, *106*, 109988. [CrossRef]
- 26. Pujari, N.; Birampally, K.; Edukondalu, A.; Vardhani, C.P. Effect of Li₂O content on structural and optical properties of Li₂O-TeO₂-As₂O₃-B₂O₃ glasses. *J. Phys. Chem. Solids* **2021**, *148*, 109627. [CrossRef]
- 27. Makishima, A.; Mackenzie, J.D. Direct calculation of Young's moidulus of glass. J. Non-Cryst. Solids 1973, 12, 35–45. [CrossRef]
- 28. Makishima, A.; Mackenzie, J.D. Calculation of bulk modulus, shear modulus and Poisson's ratio of glass. *J. Non-Cryst. Solids* **1975**, *17*, 147–157. [CrossRef]
- 29. Yousef, E.S.; El-Adawy, A.; El-KheshKhan, N. Effect of rare earth (Pr₂O₃, Nd₂O₃, Sm₂O₃, Eu₂O₃, Gd₂O₃ and Er₂O₃) on the acoustic properties of glass belonging to bismuth-borate system. *Solid State Commun.* **2006**, *139*, 108–113. [CrossRef]
- 30. X-5 Monte Carlo Team. MCNP—A General Monte Carlo N-Particle Transport Code, Version 5. La-Ur-03-1987 II; Los Alamos National Laboratory: Los Alamos, NM, USA, 2003.
- 31. Erdem, Ş.; Özgür, F.; Bünyamin, A.; Sayyed, M.I.; Kurudirek, M. Phy-X/PSD: Development of a user friendly online software for calculation of parameters relevant to radiation shielding and dosimetry. *Radiat. Phys. Chem.* **2020**, *166*, 108496.
- 32. Kilic, G.; Ilik, E.; Mahmoud, K.A.; El-Agawany, F.I.; Alomairy, S.; Rammah, Y.S. The role of B₂O₃ on the structural, thermal, and radiation protection efficacy of vanadium phosphate glasses. *Appl. Phys. A* **2021**, *127*, 265. [CrossRef]
- 33. Al-Yousef, H.A.; Alotiby, M.; Hanfi, M.Y.; Alotaibi, B.M.; Mahmoud, K.A.; Sayyed, M.I.; Al-Hadeethi, Y. Effect of the Fe₂O₃ addition on the elastic and gamma-ray shielding features of bismuth sodium-borate glass system. *J. Mater. Sci. Mater. Electron.* **2021**, 32, 6942–6954. [CrossRef]
- 34. Alotaibi, B.M.; Abouhaswa, A.S.; Sayyed, M.I.; Mahmoud, K.A.; Al-Yousef, H.A.; Hila, F.C.; Al-Hadeethi, Y. Structural, optical, and gamma-ray shielding properties of a newly fabricated P₂O₅–B₂O₃–Bi₂O₃–Li₂O–ZrO₂ glass system. *Eur. Phys. J. Plus* **2021**, 136, 1–22.
- 35. Hehn, G. Principles of Radiation Shielding. Nucl. Technol. 1986, 74, 104–105. [CrossRef]
- 36. Süsoy Doğan, G. Lithium-boro-tellurite glasses with ZnO additive: Exposure Buildup Factors (EBF) and Nuclear Shielding Properties. Eur. J. Sci. Technol. 2020, 18, 531–544. [CrossRef]
- 37. Rammah, Y.S.; Al-Buriahi, M.S.; El-Agawany, F.I.; AbouDeif, Y.M.; Yousef, E.S. Investigation of mechanical features and gamma-ray shielding efficiency of ternary TeO₂-based glass systems containing Li₂O, Na₂O, K₂O, or ZnO. *Ceram. Int.* **2020**, *46*, 27561–27569. [CrossRef]
- 38. Kamislioglu, M.; Altunsoy Guclu, E.E.; Tekin, H.O. Comparative evaluation of nuclear radiation shielding properties of xTeO₂ + (100–x)Li₂O glass system. *Appl. Phys. A* **2020**, 126, 1–16. [CrossRef]
- 39. Singh, K.; Singh, S.; Dhaliwal, A.S.; Singh, G. Gamma radiation shielding analysis of lead-flyash concretes. *Appl. Radiat. Isot.* **2015**, 95, 174–179. [CrossRef]

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40. Singh, K.J.; Singh, N.; Kaundal, R.S.; Singh, K. Gamma-ray shielding and structural properties of PbO-SiO₂ glasses. *Nucl. Instrum. Methods Phys. Res. Sect. B Beam Interact. Mater. At.* **2008**, 266, 944–948. [CrossRef]

- 41. Hanfi, M.Y.; Sayyed, M.I.; Lacomme, E.; Akkurt, I.; Mahmoud, K.A. The influence of MgO on the radiation protection and mechanical properties of tellurite glasses. *Nucl. Eng. Technol.* **2021**, *35*, 2000–2010. [CrossRef]
- 42. Singh, V.P.; Badiger, N.M.; Kaewkhao, J. Radiation shielding competence of silicate and borate heavy metal oxide glasses: Comparative study. *J. Non-Cryst. Solids* **2014**, *404*, 167–173. [CrossRef]
- 43. Singh, V.P.; Badiger, N.M. Gamma ray and neutron shielding properties of some alloy materials. *Ann. Nucl. Energy* **2014**, *64*, 301–310. [CrossRef]
- 44. Matori, K.A.; Sayyed, M.I.; Sidek, H.A.A.; Zaid, M.H.M.; Singh, V.P. Comprehensive study on physical, elastic and shielding properties of lead zinc phosphate glasses. *J. Non-Cryst. Solids* **2017**, *457*, 97–103. [CrossRef]