



Article CO₂ Adsorption Properties of Amine-Modified Zeolites Synthesized Using Different Types of Solid Waste

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Abstract: In this study, organic amines were used to modify zeolite NaA and analcime synthesized using fly ash and iron tailing slag as raw materials, respectively, and the adsorption properties of the modified zeolites toward CO₂ were determined. We found that when tetraethylenepentamine (TEPA) was used, the modified zeolite NaA and analcime had the highest nitrogen content. The adsorption capacity of the modified zeolite NaA for CO₂ was 4.02 mmol/g and that of the modified analcime was 1.16 mmol/g when the adsorption temperature was 70 °C and the CO₂ flow rate was 50 mL/min. According to the adsorption isotherm, kinetic, and thermodynamic model fitting, the adsorption surface of the modified zeolite was not uniform, and the CO₂ adsorption of the modified zeolites was classified as chemical adsorption. In a mixed atmosphere of 15% CO₂/85% N₂, the dynamic selection coefficients of the modified zeolites had good selectivity for CO₂. After five cycles, the adsorption efficiencies of the modified zeolite NaA and modified analcime for CO₂ were 92.8% and 89%, respectively. Therefore, the two amine-modified zeolites showed good recycling performance.

Keywords: fly ash; iron tailing slag; amine-modified zeolites; CO2

1. Introduction

In the past few decades, the greenhouse effect and climate change have been mainly caused by excessive anthropogenic CO_2 emissions [1]. Moreover, the consumption of fossil fuels in industrial production will continue to increase CO_2 emissions in the coming decades. In the context of achieving carbon emissions reductions, CO_2 capture technology has attracted widespread attention [2]. Currently, ammonia-containing solvents are commonly used to capture CO_2 , such as ammonia solutions [3], amino acid solutions [4], and organic amine solutions [5]. However, ammonia-containing solvents degrade and generate the organic acids to corrode equipment and it is difficult to achieve regeneration after capturing CO_2 [6]. Studies have found that these disadvantages in capturing CO_2 can be avoided using solid adsorbents [7].

Among solid CO_2 adsorbents, zeolite is a cost-effective option for CO_2 capture. Zeolite is a silicon aluminate crystal, and the main chemical elements of industrial solid waste fly ash and iron tailing slag are silicon and aluminum; thus, it could be used as a cheap raw material to synthesize zeolite. Behin et al. [8] successfully synthesized LTA zeolite using fly ash in a simple alkali melting method with microwave heating. Lin et al. [9] successfully prepared SBA-16 mesoporous zeolite with a polyoxyethylene polyoxyel ether block copolymer (F127) as a surfactant using tailing slag. Therefore, different types of zeolites can be synthesized using fly ash and iron tailings as raw materials.

As an adsorbent of CO₂, zeolite has been widely used in carbon capture. Zeolite shows good performance in decarbonization from natural gas [10] and biogas [11], and it has a



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Copyright: © 2023 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). carbon capture ability [12] because the zeolite surface has sufficient alkaline sites, which are beneficial for the adsorption of acidic CO_2 [13]. Moreover, the electric field of zeolite can attract the quadrupole moment of the CO_2 molecule [14]. The adsorption properties of zeolite toward CO_2 can be further improved by modification. For example, Cai et al. [15] grafted Y zeolite with ethylenediamine and found that the modified zeolite showed high renewability during CO_2 adsorption. However, the use of solid waste as a raw material to synthesize zeolites with high adsorption, high selectivity and good regeneration for CO_2 is limited in the literature reports. Thus, it is necessary to further study the synthesis of adsorbents with high CO_2 adsorption performance using solid waste as a raw material, providing a new method for the functional utilization of solid waste.

Therefore, in this study, fly ash and iron tailing slag were used as raw materials to synthesize zeolite NaA and analcime on the basis of their Si and Al content, respectively, and the synthesized zeolites were modified with organic amines. Furthermore, the adsorption capacity, selectivity and regeneration performance of the modified zeolites for CO_2 were further studied. The study provides a new idea for the realization of the resource utilization of solid waste and a new cheap material for CO_2 capture.

2. Materials and Methods

2.1. Materials

The fly ash used in this study came from Erdos, Inner Mongolia, China; the iron tailing slag came from the Anshan Mining Group, China; and the diatomite came from Fengsheng Mining, China. The reagents used included sodium hydroxide, concentrated nitric acid, sodium aluminate, tetrapropyl ammonium bromide, triethylamine, 3-aminopropyltriethoxysilane (APTES) and tetraethylenepentamine (TEPA), all of which were of analytically pure grade, purchased from the Beijing Chemical Company (Beijing, China) and the Tianjin Yongda Chemical Company (Tianjin, China).

2.2. Instruments

X-ray fluorescence spectrometry (XRF-1800, Shimadzu Corporation, Kyoto, Japan) was used to analyze the chemical compositions of the raw materials. An X-ray diffractometer (XRD, Ultima IV, Rigaku Corporation, Tokyo, Japan) was used to analyze the diffraction patterns of the synthetic materials. A field emission electron microscope (SEM, SU8010, Hitachi Ltd., Tokyo, Japan) and energy-dispersive spectrometer (SEM-EDS, Oxford Instruments Company, Oxford, UK) were used to observe the surface morphologies and microstructural characteristics of zeolites and analyze the elements. A surface area and pore analyzer (ASAP 2460, Micromeritics Instrument Corporation, Norcross, GA, USA) was used to measure the N₂ adsorption-desorption isotherms before and after adsorbent modification. The N content of the modified zeolite was measured by EA (UNICUBE, Elemental Analysis Systems Co., Ltd., Hanau, Germany). Fourier transform infrared spectroscopy (FTIR, Nicolet iS5, Thermo Fisher Company, Waltham, MA, USA) was used to measure the changes in the functional groups of adsorbents before and after modification. The adsorption of CO_2 by the modified zeolites was measured by a thermogravimetric analyzer (TG-209, Neichi Scientific Instrument Trading (Shanghai) Co., Ltd., Shanghai, China). Before being measured by the above instruments, all samples were ground and passed through a 200-mesh sieve, and then dried in a drying oven at 80 °C for 8 h.

2.3. Sample Preparation

2.3.1. Zeolite Synthesis

The zeolite NaA was synthesized using the hydrothermal method from fly ash as the raw material. The synthesis steps were described in detail in our previous study [16]. First, fly ash, diatomite, NaOH and Na₂CO₃, according to the ratio of 9.1:0.9:16:1, were mixed and fused; then, the mixture was aged, crystallized, filtrated, washed and dried to obtain the zeolite NaA.

The analcime was synthesized using the hydrothermal method from iron tailing slag. First, the optimal parameters for the activation of iron tailing slag were determined in batch experiments (Figure S1), The analysis shows that the material with good activation effect is obtained [17,18]. Then, the optimal liquid–solid ratio, pH of the crystallization solution, aging time, crystallization temperature and crystallization time for analcime synthesis were determined by batch experiments (Figures S2–S6). According to the optimal parameters, the iron tailing slag and NaOH were mixed according to the mass ratio of 1:1, and then roasted in a muffle furnace at 850 °C for 2 h to activate the iron tailing slag. Then, 8.8 g activated iron tailing slag, 0.275 g NaAlO₂, 1.25 g TPABr and 51.95 mL deionized water were mixed, stirred for 2 h, aged for 5 h, transferred to a high-pressure reactor and crystallized in an

2.3.2. Amine-Modified Zeolite Synthesis

First, the synthesized zeolite NaA and analcime were dried and ground through a 200-mesh sieve; then, 1 g zeolite was added into three organic amine ethanol solutions with different mass fractions (25%, 40%, 50%, 60%); the mixtures were stirred for a certain time (3, 5, 6, 8 h), centrifuged, washed, filtered and dried overnight at 80 °C to obtain the amine-modified zeolites.

oven at 180 °C for 72 h. After washing and filtering, the analcime was obtained.

2.4. CO₂ Adsorption Experiments

The adsorption isotherms of CO₂ adsorbed by zeolites before and after modification were determined using ASAP 2460. The CO₂ adsorption test of the modified zeolites was carried out on TG-209. Before CO₂ adsorption, 50 mg samples were placed in an alumina crucible and activated at 150 °C in pure He gas for 30 min (50 mL/min) to remove adsorbed substances (H₂O, CO₂). Then, CO₂ was absorbed at different temperatures (30, 50, 70, 90 °C) and gas flow rates (50, 70, 125 mL/min) for 30 min. The amount of CO₂ adsorption was determined by the change in the mass of the adsorbent.

The adsorption selectivity of the amine-modified zeolites was tested on a BSD-MAB device (Bester Instrument Technology Co., Ltd., Beijing, China). Prior to the test, 1 g sample was filled into the penetrating column with a length of 66 mm and purged and activated for 1 h at 200 °C with a 10 mL/min He airstream. After activation, the penetrating column was removed from the activation furnace and placed in a water bath at 25 °C for cooling, until the temperature and mass spectrum signal were stable. Ensure that the gas entering the penetrating column is independent of each other, and start distributing gas after the signal is stable. MFC was used to control the flow rate of CO₂ at 1.5 mL/min and N₂ at 8.5 mL/min. From the beginning of the test, the gas signals of each component were detected and recorded by the mass spectrometer, and the penetration curve was drawn.

The reuse of the amine-modified zeolites was realized by the adsorption–desorption process. During the CO_2 adsorption process, the airflow was switched from CO_2 to He (50 mL/min), and the temperature was set at 150 °C for 30 min of desorption. The cycle experiment was completed through five adsorption–desorption processes.

2.5. Crystallinity Calculation

The relative intensity ratio (*RIR*) is one of the best tools to quantify X-ray diffraction data [19]. The *RIR* value is calculated as in Equation (1) [20].

$$RIR_{i,s} = \left(\frac{X_s}{X_i}\right) \left(\frac{I_{(hkl)i}}{I_{(hkl)'_s}}\right) \left(\frac{I_{(hkl)'_s}^{rel}}{I_{(hkl)i}^{rel}}\right)$$
(1)

where *X* is the mass fraction of the sample; *I* is the intensity of the characteristic reflection; I^{rel} is the relative intensity of the characteristic reflection; subscript _i indicates the tested sample; and subscript _s indicates the interior standard phase of the software.

In this study, the relative strength ratio (*RIR*) analysis function of the MDI JADE software was used to quantitatively calculate the XRD phase.

2.6. Model and Calculation

To study the adsorption characteristics and mechanism of CO₂ adsorption of the amine-modified zeolites, an isothermal adsorption model, adsorption kinetics model and thermodynamic model were used to fit the experimental data.

Adsorption isotherm models mainly include the Langmuir model [21], Freundlich model [22] and Toth model [23]. The Langmuir model holds that in the process of adsorption of the gas phase by the solid phase, the gas molecule is simultaneously adsorbed and desorbed on the solid surface and finally reaches a dynamic adsorption equilibrium [24]. The Langmir model is given by Equation (2).

$$q_e = \frac{K_L q_m p}{1 + K_L q} \tag{2}$$

where K_L is the equilibrium constant of the Langmuir model; q_m is the saturation adsorption amount, mmol/g; p is the equilibrium adsorption pressure, kPa; q_e is the equilibrium adsorption capacity, mmol/g.

The Freundlich isotherm model is represented by Equation (3) [25].

q

$$e = Kp^{1/n} \tag{3}$$

where *K* is the equilibrium constant of the Freundlich model; *n* is a constant that depends on the adsorption temperature; q_e is the equilibrium adsorption capacity, mmol/g; *p* is the equilibrium adsorption pressure, kPa.

The Toth model is an extension of the Langmuir model. Different from the Langmuir model, the Toth model is more suitable for the adsorption of non-uniform surfaces. The Toth model is a three-parameter isothermal adsorption model obtained after introducing the non-uniform parameter n on the basis of the Langmuir model [26]. The Toth isotherm model is given by Equation (4).

$$q_e = \frac{q_m bp}{\left[1 + (bp)^n\right]^{\frac{1}{n}}}$$
(4)

where q_e is the equilibrium adsorption capacity, mmol/g; q_m is the saturation adsorption amount, mmol/g; *b* is the equilibrium constant of the Langmuir model; *p* is the equilibrium adsorption pressure, kPa; *n* is a constant related to the degree of uneven adsorption on the surface of the adsorbent.

The pseudo-first-order kinetic model, pseudo-second-order kinetic model and Avrami kinetic model were used to fit the CO_2 adsorption kinetics of the amine-modified zeolites. The pseudo-first-order model considers that the adsorbate adsorption rate of an adsorbent is linearly related to the difference between the equilibrium adsorption capacity of the adsorbent and the adsorption capacity at a certain time [27], which can be expressed as in Equation (5):

$$\frac{\partial q_t}{\partial t} = k_1 (q_e - q_t) \tag{5}$$

where q_t is the adsorption amount at time t, mmol/g; q_e is the equilibrium adsorption capacity, mmol/g; k_1 is a quasi-first-order rate constant, min⁻¹.

The pseudo-second order kinetic model assumes that the reaction rate is proportional to the volume fraction of the two reactants, and chemisorption is described as the main control step and rate-limiting step of the adsorption process [28,29], which is expressed as in Equation (6):

$$\frac{\partial q_t}{\partial t} = k_2 (q_e - q_t)^2 \tag{6}$$

where q_t is the adsorption amount at time t, mmol/g; q_e is the equilibrium adsorption capacity, mmol/g; k_2 is a quasi-second-order rate constant, min⁻¹.

The Avrami dynamic model is a semi-empirical model based on particle nucleation theory, and it has been successfully used to describe the adsorption process of CO_2 by PE-MCM-41 and carbon nanotubes [30]. The expression of the Avrami dynamic model is given by Equation (7):

$$q_t = q_e \left[1 - e^{-(k_A t)^{n_A}} \right] \tag{7}$$

where q_t is the adsorption amount at time t, mmol/g; q_e is the equilibrium adsorption capacity, mmol/g; k_A is the Avrami rate constant, min⁻¹; n_A is the series of Avrami equations.

To accurately calculate the relevant data of the adsorption thermodynamic characteristics of amine-modified zeolites, the study obtained the expression of the adsorption isotherm through the Freundlich–Langmuir equation [31], which can be expressed as

$$V = \frac{abp^c}{1+bp^c} \tag{8}$$

where *V* is the adsorption amount, cm^3/g ; *p* is the pressure, bar; *a* is the saturation adsorption capacity, cm^3/g ; *b* is the Langmuir constant; *c* is a constant.

Then, the Clausius–Clapeyron Equation (9) was used to fit the single adsorption isotherm of CO_2 at different adsorption temperatures, and the equivalent adsorption heat was obtained [32].

$$Q = RT_1 T_2 ln \frac{P_2 / P_1}{T_2 - T_1}$$
(9)

where *Q* is the equal heat of adsorption, J/mol; R is the gas constant, 8.314 J/mol; T_1 and T_2 are the measured adsorption temperatures, K; P_1/P_2 is the adsorption pressure corresponding to the same adsorption amount on the measured isotherm of the sample at the above two adsorption temperatures, bar.

3. Results and Discussion

3.1. Synthesis of Amine-Modified Zeolites

3.1.1. Different Types of Zeolites

The chemical components of the fly ash and iron tailing slag were determined by XRF (Table 1). The content of Al_2O_3 in the fly ash was high and was close to that of SiO_2 , so the fly ash was used to synthesize the zeolite NaA with a similar Si/Al ratio. The content of SiO_2 in the iron tailing slag was high, so the slag was used to synthesize the high-Si analcime.

Table 1. Chemical compositions of raw materials.

Chemical Composition (w%)	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	LOI	Other
Fly ash	41.18	45.19	2.68	2.90	2.70	5.35
Iron tailing slag	76.98	1.83	13.32	1.44	1.6	4.83
Diatomite	89.06	2.59	1.25	0.38	2.76	3.96

In the XRD pattern, the characteristic peaks of the sample synthesized using fly ash at 7.183°, 10.165°, 12.458°, 14.394°, 20.411° and 22.851° all corresponded to the characteristic peaks of zeolite NaA (PDF#39-0222) (Figure 1a), indicating that zeolite NaA had been successfully synthesized using fly ash. In addition, the characteristic peaks of the sample synthesized using iron tailing slag at 15.197°, 18.261°, 24.235°, 25.936°, 33.245° and 35.791° corresponded to the standard peaks of analcime (PDF#99-0007) (Figure 1b), which showed that analcime had been successfully synthesized using tailing slag. According to *RIR* calculation, the crystallinity of zeolite NaA reached 83.61% and that of analcime was 84.62%.





Figure 1. XRD patterns of zeolite NaA (**a**) and analcime (**b**) synthesized using fly ash and iron tailing slag, respectively.

The synthesized zeolite NaA had a typical uniform cubic structure (Figure 2a,b). The element ratio of O:Si:Al:Na of the synthesized zeolite was approximately 4:1:1:1 according to the EDS element analysis (Figure 2c), which was consistent with the element ratio of zeolite NaA (Na₉₆Al₉₆Si₉₆O₃₈₄·216H₂O), and it further proved that zeolite NaA had been synthesized. The synthesized analcime was a granular block (Figure 2d,e). From the EDS element analysis (Figure 2f), the element ratio of O, Si, Al and Na in the analcime was approximately 7:2:1:1, which was similar to the typical element ratio of analcime (Na₉₆Al₉₆Si₉₆O₃₈₄·216H₂O), and this further proved that the synthesized product was analcime.



Figure 2. SEM and elemental analysis of zeolite NaA (a-c) and analcime (d-f).

3.1.2. Amine-Modified Zeolite

The type and mass fraction of organic amines and the stirring time directly affected the amine-carrying amount of zeolite. TEPA, triethylamine and APTES were used to modify the zeolites, respectively. It was found that the N content of the two types of modified zeolites prepared with TEPA was significantly higher than that of the other two amines, and with the increase in the mass fraction of organic amines, the N-carrying amount of the modified zeolites also increased. When the mass fraction of TEPA increased to 60%, the N content of the modified zeolite NaA and analcime reached the highest level (Figure 3a,b). In addition, when the stirring time increased from 3 to 6 h, the N content of the modified zeolites increased, but it remained unchanged with a further increase in the stirring time



(Figure 3c,d). Therefore, when the mass fraction of 60% TEPA was used and the stirring time was 6 h, the N content of the modified zeolite NaA was 5.81% and that of the modified analcime was 4.71%.

Figure 3. Effects of TEPA, triethylamine, APTES and their mass fractions on the nitrogen content of modified zeolite NaA (**a**) and analcime (**b**), and the effect of the stirring time on the nitrogen content of modified zeolite NaA (**c**) and analcime (**d**).

The SEM images of the zeolite NaA and analcime modified by TEPA had no obvious change compared with those of the original zeolites (Figure 4), which showed that the crystal structures of the zeolites had not been damaged by TEPA modification. The N element was evenly distributed on the surfaces of the two modified zeolites. EDS analysis showed that the N content of the modified zeolite NaA was 6.99% and that of the modified analcime was 5.56%. Surface scanning and EDS analysis further proved that TEPA was successfully loaded on the zeolites.



Figure 4. SEM image (**a**), N element surface scanning (**b**) and EDS element characteristic peak distribution map (**c**) of amine-modified zeolite NaA, and SEM image (**d**), N element surface scanning (**e**) and EDS element characteristic peak distribution map (**f**) of amine-modified analcime.

The infrared spectra of the zeolite NaA before and after modification showed that, compared with zeolite NaA, the amine-modified zeolite NaA contained all the characteristic absorption peaks of origin zeolite [33,34]. C-N bond bending vibration existed at 1320 cm⁻¹ and C-H bond bending vibration existed at the band around 1480 cm⁻¹. The peak at 1580 cm⁻¹ was caused by the bending vibration of the N-H bond, and the peak at 2840 cm^{-1} was attributed to the asymmetric bending vibration of the C-H bond of the TEPA methyl group. The peak at 2950 cm⁻¹ was caused by symmetric flexural vibrations of the C-H bond of the TEPA methyl group (Figure 5a). Similarly, the modified analcime contained all the characteristic absorption peaks of analcime [35,36], and new peaks were formed at 1317 cm⁻¹, 1482 cm⁻¹, 1667 cm^{-1} , 2850 cm⁻¹ and 2950 cm⁻¹ [37]. C-N bond bending vibration existed at 1317 cm⁻¹, and C-H bond bending vibration existed at 1482 cm⁻¹. The peak at 1667 cm⁻¹ was caused by the bending vibration of the N-H bond, and the absorption peak at 2850 $\rm cm^{-1}$ was attributed to the asymmetric bending vibration of the C-H bond of the TEPA methyl group. The peak at 2950 cm⁻¹ was caused by symmetric flexural vibrations of the C-H bond of the TEPA methyl group (Figure 5b). Therefore, the infrared spectral analysis also proved that TEPA was successfully loaded on the zeolite NaA and analcime.



Figure 5. Infrared spectra of zeolite NaA (a) and analcime (b) before and after modification.

3.2. Pore Size Characteristics

Both zeolites showed type IV isotherms and H3 hysteresis loops before and after modification (Figure 6). Zeolite NaA before and after modification had obvious adsorption behavior at low pressure; thus, there were more micropores in both zeolite NaA and the modified zeolite NaA (Figure 6a,b). The H3 hysteresis rings before and after the modification of zeolite NaA had no obvious adsorption platform, indicating that the adsorbents had a secondary pore structure formed by particle accumulation [38–40], and the H3 hysteresis rings of the modified zeolite NaA were smaller than those of the original zeolite, which might have been due to the partial pore blocking by TEPA. The adsorption behavior of analcime before and after modification was minor at low pressure, indicating that the zeolites contained fewer micropores, and the main pore size was mesoporous (Figure 6c,d). The H3 hysteresis loops of the modified analcime were mainly caused by mesoporous pores in the zeolite, and the changes in the H3 hysteresis loops of analcime before and after modified analcime with TEPA.

The S_{BET} of zeolites before and after modification was obtained according to the N₂ adsorption–desorption curve. The S_{BET} and the cumulative area of the zeolite NaA were greater than those of analcime because the pore structure of zeolite NaA was microporous, while the pore structure of analcime was mainly mesoporous (Table 2 and Figure 6). The specific surface area of the modified zeolite decreased slightly, which might have been due to some of the zeolite pores being blocked by TEPA [41].



Figure 6. N₂ adsorption–desorption curves and pore size distribution before and after modification of zeolite NaA (**a**,**b**) and analcime (**c**,**d**).

Table 2. BET specific surface area, t-top surface area and total pore volume of zeolites before and after modification.

Sample	S_{BET} (m ² /g)	S _{t-top} (m ² /g)	V _{total} (m ³ /g)
Zeolite NaA	31.25	6.15	0.059
Analcime	22.05	6.27	0.070
Modified zeolite NaA	23.42	3.49	0.066
Modified analcime	21.56	4.93	0.071

3.3. CO₂ Adsorption

3.3.1. Adsorption Capacities of Zeolite and Modified Zeolite

After amine modification, the CO₂ adsorption capacity of the two types of modified zeolites increased compared with that of the original zeolites (Figure 7a,b), indicating that amine modification could effectively improve the CO₂ adsorption capacity. The CO₂ adsorption capacity of zeolite NaA before and after modification was greater than that of analcime and modified analcime. Before modification, because the Na⁺ ion in the zeolite had a higher electric field than the proton, and CO₂ had large polarization and a large electric quadrupole moment, it was easily adsorbed by the ion–quadrupole interaction with cations located in the zeolites [42,43]. The Na⁺ ion content of zeolite NaA (Na₉₆Al₉₆ Si₉₆O₃₈₄·216H₂O) was significantly higher than that of analcime (Na₁₆Al₁₆ Si₃₂O₉₆·16H₂O), and the specific surface area of zeolite NaA was also higher than that of analcime. Therefore, zeolite NaA could provide more adsorption sites to capture CO₂ than analcime. After modification, TEPA was successfully loaded on the zeolites, and the loaded amino groups could react with CO₂ to produce carbamate [44]. Because zeolite NaA had a high specific surface area and could carry more TEPA (Figure 3), the CO₂ adsorption capacity of the modified zeolite NaA was greater than that of the modified analcime.



Figure 7. Adsorption capacity of zeolite NaA (a) and analcime (b) before and after amine modification.

Before and after modification, the adsorption capacity of CO_2 in the zeolites increased with the pressure. The zeolite NaA before and after modification had more micropores, so the adsorption capacity of CO_2 increased gradually with the pressure increase. However, the analcime before and after modification was more mesoporous, so CO_2 could quickly enter the zeolites, and the adsorption capacity increased linearly with the pressure increase at 0–0.1 bar, and then tended toward adsorption saturation. Therefore, compared with the microporous zeolite, the mesoporous zeolite was more conducive to CO_2 diffusion.

Therefore, the amine-modified zeolite NaA synthesized from fly ash had a higher CO_2 adsorption capacity than the amine-modified analcime synthesized from iron tailing slag because it could carry more TEPA and introduced more amino groups. However, due to the microporous structure of the amine-modified zeolite NaA, its adsorption rate for CO_2 was lower than that of the amine-modified analcime with mesopores.

3.3.2. Influence of Temperature and Flow Rate

As the adsorption temperature increased from 30 °C to 70 °C, the CO₂ adsorption capacity of the modified zeolite NaA increased from 2.906 mmol/g to 4.022 mmol/g, and that of the modified analcime increased from 0.935 mmol/g to 1.160 mmol/g (Figure 8a,c). These might be due to the increasing temperature, which led to the intense thermal motion of CO₂, accelerated the CO₂ diffusion in the modified zeolite and increased the effective collisions between CO₂ molecules and adsorption sites on the modified zeolite. However, when the adsorption temperature further increased from 70 °C to 90 °C, the adsorption capacity of the two types of amine-modified zeolites decreased, mainly because the reaction between the amino group loaded on the zeolites and CO₂ was reversible and the higher temperature increasing (from 30 °C to 70 °C), the amino group carried on the zeolites could react with the CO₂ and increase the adsorption capacity, but, when the temperature further increase the adsorption capacity of the amine-modified zeolite for CO₂.

$$2RNH_2 + CO_2 \leftrightarrow RNHCOONHR \tag{10}$$

At 70 °C, when the CO₂ flow rate increased from 50 mL/min to 125 mL/min, the CO₂ adsorption capacity of the two types of amine-modified zeolites decreased slightly (Figure 8b,d). The adsorption capacity of the amine-modified zeolite NaA decreased from 4.02 mmol/g to 3.22 mmol/g, and that of the amine-modified analcime decreased from 1.16 mmol/g to 0.93 mmol/g. Therefore, the larger the gas flow velocity of CO₂, the smaller the adsorption capacity of the two types of amine-modified zeolites for CO₂, the smaller the gas flow velocity of CO₂ and the larger the adsorption capacity of CO₂, which is consistent with other research conclusions [46,47].



Figure 8. CO_2 adsorption at different temperatures for amine-modified zeolite NaA (a) and aminemodified analcime (b) and at different gas flow rates for amine-modified zeolite NaA (c) and amine modified analcime (d).

Therefore, although our study only separately investigated the effects of the temperature and flow rate on CO₂ adsorption by amine-modified zeolites, based on the above analysis, we could conclude that with the increase in the temperature (30 °C to 70 °C) and CO₂ flow rate, the CO₂ adsorption capacity of the amine-modified zeolites would gradually increase before adsorption saturation, while, with a further increase in the temperature (70 °C to 90 °C) and flow rate, the adsorption capacity of the amine-modified zeolites for CO₂ might decrease due to the beginning of the reverse reaction.

3.3.3. Adsorption Models

To study the adsorption characteristics and mechanism of CO₂ adsorption of the amine-modified zeolites, an isothermal adsorption model, adsorption kinetics model and thermodynamic model were used to fit the experimental data.

At 0–0.5 bar, the CO₂ adsorption capacities of the two types of modified zeolites increased rapidly; then, with the pressure increase, the adsorption capacities gradually declined and reached the maximum saturated adsorption capacity (Figure 9). After fitting (Table 3), based on R^2 , the Toth model was more suitable to describe the actual situation of CO₂ adsorption by the modified zeolites. Specifically, the adsorption surfaces of the two amine-modified zeolites were not uniform, which might have been because the amine groups were not evenly distributed on the modified zeolite surface after the zeolites were loaded with TEPA. Although the fitting R^2 of the Freundlich model was lower than that of the Toth model, it was higher than that of the Langmuir model. Thus, the CO₂ adsorption of the two modified zeolites might have multiple layers of adsorption, which might be because the amine loaded on the zeolite surface and the covered Na⁺ ions in the zeolite could simultaneously adsorb CO₂ molecules.





Figure 9. Isothermal adsorption model fitting of amine-modified zeolite NaA (**a**) and amine-modified analcime (**b**).

Model	Parameters	Amine-Modified Zeolite NaA	Amine-Modified Analcime
Langmuir	K_L	0.5316	0.2665
	q_m	3.49367	0.94045
	R^2	0.95779	0.93827
	п	5.22179	4.71687
Freundlich	Κ	3.60377	1.03886
	R^2	0.96163	0.9717
	b	0.5316	0.2665
Toth	q_m	3.72373	1.08952
	n	0.3546	0.64811
	R^2	0.99982	0.99687

Table 3. Parameters of the isothermal adsorption model.

The adsorption capacity of CO_2 of the amine-modified zeolites increased rapidly with time during the initial stage of 0–10 min and reached more than 90% of the final equilibrium adsorption capacity, and then the adsorption slowed down in the following time period until the equilibrium adsorption capacity was reached (Figure 10). Through fitting, it was found that the two types of amine-modified zeolites were more consistent with the pseudo-second-order kinetic models, and the CO_2 equilibrium adsorption capacities calculated by the models were close to the experimental data (Table 4), which indicated that chemisorption was the limiting step of CO_2 adsorption for the amine-modified zeolites. In addition, the k_2 of the amine-modified analcime was higher than that of the amine-modified zeolite NaA, indicating that the adsorption rate of amine-modified analcime was higher than that of the modified zeolite NaA. It was again proven that the pore size affects the diffusion and adsorption rate of CO_2 in zeolites.



Figure 10. Adsorption kinetic model fitting of amine-modified zeolite NaA (**a**) and amine-modified analcime (**b**).

Model	Parameters	Amine-Modified Zeolite NaA	Amine-Modified Analcime
	<i>q</i> e	3.78415	1.00618
Pseudo-first-order	\dot{k}_1	0.27969	0.30286
	R^2	0.96298	0.9765
Pseudo-second-order	9e	4.28071	1.24011
	\dot{k}_2	0.09013	0.34727
	R^2	0.9955	0.99933
Avrami	9e	4.09004	1.14787
	k_A	0.2412	0.29075
	n_A	0.62283	0.71288
	R^2	0.99279	0.99805

Table 4. Kinetic parameters of CO₂ adsorption by amine-modified zeolites.

3.3.4. Thermodynamic Analysis

Figure 11 shows the Freundlich–Langmuir fitting results of amine-modified zeolite NaA and amine-modified analcime at 60 °C, and Table 4 shows the Freundlich–Langmuir fitting results of the two types of amine-modified zeolites. The fitting curve of the Freundlich–Langmuir equation has high similarity to the experimental adsorption data (Figure 11), and the fitting R^2 values are all above 0.99 (Table 5), which approximately predicts the adsorption trend.



Figure 11. Freundlich–Langmuir fitting curve of CO₂ isotherm of amine-modified zeolite NaA (**a**) and amine-modified analcime (**b**).

Table 5. Fitting results of Freundlich–Langmuir equation.

	а	b	С	R^2
Amine-modified zeolite NaA	115.6443	2.50932	0.88896	0.99993
Amine-modified analcime	29.21022	3.18114	0.45374	0.99454

The adsorption heat of the amine-modified zeolite NaA ranged from 60 to 70 kJ/mol, while that of the amine-modified analcime ranged from 38 to 50 kJ/mol (Figure 12). Because the adsorption heat of physical adsorption ranges from 0 to 40 kJ/mol, the CO_2 adsorption achieved by the two types of amine-modified zeolites was mainly in the form of chemisorption.

Therefore, based on the above model fitting, after carrying TEPA, the modified zeolite removed CO_2 mainly through the reaction between the amine group and CO_2 [48]. In addition, the Na⁺ ion in the modified zeolite also could adsorb CO_2 molecules via ion–quadrupole interaction. Since zeolite NaA could carry more amine groups and contained more Na⁺ ions than analcime, the adsorption capacity of the modified zeolite NaA for CO_2

was higher than that of modified analcime. Thus, after amine modification, the zeolite synthesized using solid waste had excellent adsorption capacity for CO_2 compared to other amine-modified adsorbents and zeolites (Table 6).



Figure 12. Relationship between CO_2 adsorption heat and adsorption capacity of amine-modified zeolite NaA (**a**) and amine-modified analcime (**b**).

Adsorbent	Adsorption Capacity (mmol/g)	References
Amine-modified porous carbon materials	3.34	[41]
Ethylenediamine-modified zeolite HY	1.76	[49]
TEPA-modified zeolite ZSM-5	1.80	[50]
Zeolite NaX	3.2	[33]
TEPA-modified zeolite NaA	4.02	This study
TEPA-modified analcime	1.16	This study

Table 6. Comparison of the adsorption capacities of different adsorbents for CO₂.

3.3.5. Selective Adsorption and Regeneration Properties

Adsorption selectivity is a key factor in the study of gas separation. Through the penetration curves of the two types of amine-modified zeolites in the 15% $CO_2/85\%$ N₂ mixed gas adsorption bed (Figure 13), we observed that, at the initial stage, the concentration of CO_2 in the tail gas at the end of the device was less than that of N₂, indicating that CO_2 was preferentially adsorbed at the initial stage. The penetration point of amine-modified zeolite NaA was 145.5 s, the dry point was 335.1 s, and the dynamic selection coefficient for CO_2 was 2.8942. The penetration point of amine-modified analcime was 48.5 s, the dry point was 128.0 s, and the dynamic selection coefficient for CO_2 was 2.9509. During CO_2/N_2 mixed gas flow through the amine-modified zeolite's adsorption column, CO_2 had the advantage of preferential adsorption in the competitive adsorption with N₂. Among them, amine-modified zeolite NaA had higher selectivity for CO_2 adsorption than amine-modified analcime.

The amine-modified zeolite NaA and amine-modified analcime were reused five times, respectively (Figure 14). The CO₂ adsorption–desorption capacity of the amine-modified zeolite NaA at the first and fifth times was 4.47/4.31 mmol/g and 4.15/4.01 mmol/g, respectively. The CO₂ adsorption capacity decreased by 0.32 mmol/g, the adsorption efficiency remained above 92.8%, and the desorption rate was above 95%, indicating that the amine-modified zeolite NaA had a good regeneration ability. The adsorption–desorption capacity of the amine-modified analcime at the first and fifth times was 1.16/1.09 mmol/g and 1.03/0.95 mmol/g, respectively. The CO₂ adsorption capacity decreased by 0.13 mmol/g, the adsorption efficiency remained above 89.0%, and the desorption rate was above 90%. This showed that the amine-modified analcime also had good reusability.



Figure 13. Penetration curves of CO_2/N_2 mixture on amine-modified zeolite NaA (**a**,**b**) and amine-modified analcime (**c**,**d**).



Figure 14. Reusability of amine-modified zeolite NaA (a) and amine-modified analcime (b).

4. Conclusions

In this study, according to the content of Si and Al, fly ash and iron tailing slag were used as raw materials to synthesize zeolite NaA with crystallinity of 83.61% and analcime with crystallinity of 84.62% via a simple alkali fusion hydrothermal method, respectively. Then, the synthesized zeolites were modified with triethylamine, APTES and TEPA. It was found that when 60 wt% TEPA ethanol solution was used and the stirring time was 6 h, the N capacity of zeolite NaA and analcime was high, and the N content of the modified zeolite NaA and analcime was 5.83% and 4.71%, respectively.

When the adsorption temperature was 70 °C and the CO_2 flow rate was 50 mL/min, the adsorption capacity of the modified zeolites for CO_2 was the best; that of the modified zeolite NaA reached 4.02 mmol/g and that of the modified analcime reached 1.16 mmol/g. Through adsorption isothermal model and kinetic adsorption model fitting, and thermodynamic calculation, we found that the adsorption surfaces of the two types of modified zeolites were not uniform, and the adsorption of modified zeolites for CO_2 was in the form of chemisorption. The two types of amine-modified zeolites had good adsorption selectivity for CO_2 in a mixed atmosphere of CO_2 and N_2 . The two types of amine-modified zeolites showed a good regeneration ability after five cycles of adsorption–desorption. In this study, fly ash and iron tailing slag were used to synthesize amine-modified zeolites to capture CO_2 , which not only provides a new method for the efficient utilization of solid waste but also offers a cheap adsorption material for CO_2 capture.

Supplementary Materials: The following supporting information can be downloaded at: https: //www.mdpi.com/article/10.3390/su151310144/s1, Figure S1: XRD patterns of iron tailing slag (a), and activation product under different conditions (b–d); Figure S2: Effect of liquid-solid ratio on analcime synthesis (pH 10.0, aging time 5 h, crystallization temperature 180 °C, crystallization time 72 h); Figure S3: Effect of pH of crystallization liquid on analcime synthesis (liquid-solid ratio 5: 1, aging time 5 h, crystallization temperature 180 °C, crystallization time 72 h); Figure S4: Effect of aging time on analcime synthesis (liquid-solid ratio 5: 1, pH 12.0, crystallization temperature 180 °C, crystallization time 72 h); Figure S5: Effect of crystallization temperature on analcime synthesis (liquidsolid ratio 5:1, pH 12.0, aging time 5 h, crystallization time 72 h); Figure S6: Effect of crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization time on analcime synthesis (liquid-solid ratio 5:1, pH 12.0, aging time 5 h, crystallization temperature 180 °C); Figure S7: Images of zeolite NaA before (a) and after amine modification (b), and analcime before (c) and after amine modification (d).

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