

# GNSS/Acoustics seafloor positioning simulations using a multi-observations least square inversion: Supplementary Material

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## 1 General Formulation of a Least Square Inversion

We have a  $n$  number of observations  $l$ , and we want to determine  $p$  unknown physical quantities  $x$ . We have  $n > p$ . We also have a function  $F$  with several variables.

$$F : \begin{array}{ccc} \mathbb{R}^p & \longrightarrow & \mathbb{R}^n \\ (x_1, \dots, x_p) & \longmapsto & F(x_1, \dots, x_p) = (l_1, \dots, l_n) \end{array} \quad (1)$$

The exact values  $(\hat{x}_1, \hat{x}_2, \dots, \hat{x}_p)$  of  $(x_1, x_2, \dots, x_p)$  are inherently inaccessible because the observations are tainted with errors. Thus, we try to estimate values close to  $(\hat{x}_1, \hat{x}_2, \dots, \hat{x}_p)$ . We introduce the notion of residuals  $v$ , which is the difference between the actual observations  $l_i$  (called *stochastic model*) and the theoretical values  $\lambda_i$  obtained by the model based on the estimated parameters  $\hat{x}_i$  (called *functional model*) (Sillard, 2001). So that:

We have :

$$\forall i \in \llbracket 1, n \rrbracket \quad v_i = l_i - f(\hat{x}_1, \dots, \hat{x}_p) = l_i - \lambda_i \quad (2)$$

Then, we impose a condition on the residuals : we want the quadratic sum of the latter  $\sum_i^n v^2$  to be minimal. It is called the **least squares condition** (Legendre, 1805; Gauss, 1809).

We call  $\mathbf{L}$  the vector of the actual observations (length  $n$ ):

$$\mathbf{L} = \begin{bmatrix} l_1 \\ l_2 \\ \vdots \\ l_n \end{bmatrix} \quad (3)$$

We call  $\mathbf{X}$  the vector of the unknown parameters to estimate ( $p$  length):

$$\mathbf{X} = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_p \end{bmatrix} \quad (4)$$

And we call  $\mathbf{V}$  is the vector of the residuals associated with each observation at the end of the inversion (length  $n$ ):

$$\mathbf{V} = \begin{bmatrix} v_1 \\ v_2 \\ \vdots \\ v_n \end{bmatrix} \quad (5)$$

The problem must be linearized near a solution close enough to  $(\hat{x}_1, \hat{x}_2, \dots, \hat{x}_p)$ : this solution is called the *solution a priori* and write it  $\mathbf{X}_0 = (x_{0,1}, x_{0,2}, \dots, x_{0,p})$ . To do this, we introduce the matrix of *partial derivatives* or *Jacobian*  $\mathbf{J}$  of the function  $F$ , of size  $(n, p)$  :

$$\mathbf{J}_F(\mathbf{X}) = \begin{bmatrix} \frac{df_1}{dx_1} & \dots & \frac{df_1}{dx_p} \\ \vdots & \ddots & \vdots \\ \frac{df_n}{dx_1} & \dots & \frac{df_n}{dx_p} \end{bmatrix} \quad (6)$$

And we call  $\mathbf{A}$  the matrix of partial derivatives *in the neighborhood* of  $\mathbf{X}_0$ , also called *design matrix*.

We have  $\mathbf{A} = \mathbf{J}_F(\mathbf{X}_0)$

We call  $\mathbf{\Lambda}$  the vector of modeled observations associated with *a priori* values such as:

$$F(\mathbf{X}_0) = \mathbf{\Lambda} = \begin{bmatrix} \lambda_1 \\ \lambda_2 \\ \vdots \\ \lambda_n \end{bmatrix} \quad (7)$$

We set  $\mathbf{B}$  the vector of the differences between the actual observations  $l_i$  and the modeled observations associated with the *a priori* values  $\lambda_i$ . We have  $\mathbf{B} = \mathbf{L} - \mathbf{\Lambda}$ .

Lastly, we introduce the notion of weight, which indicates the quality of the observations, and allows to homogenize them if they are of different nature: each observation  $b_i$  is associated to a standard deviation  $\varsigma_i$  quantifying its accuracy. The more accurate the measurement, the lower the standard deviation. We then define for each  $\varsigma_i$  weight  $\pi_i$  such that  $\pi_i = \frac{1}{\varsigma_i^2}$ . The more reliable the measurement, the greater the

weight. The associated matrix called *weights* is a diagonal matrix <sup>1</sup>, such as :

$$\mathbf{P} = \begin{bmatrix} \frac{1}{\varsigma_1^2} & 0 & \dots & 0 \\ 0 & \frac{1}{\varsigma_2^2} & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ 0 & \dots & 0 & \frac{1}{\varsigma_n^2} \end{bmatrix} = \begin{bmatrix} \pi_1 & 0 & \dots & 0 \\ 0 & \pi_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ 0 & \dots & 0 & \pi_n \end{bmatrix} = \begin{bmatrix} \frac{1}{\varsigma_1^2} & 0 & \dots & 0 \\ 0 & \frac{1}{\varsigma_2^2} & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ 0 & \dots & 0 & \frac{1}{\varsigma_n^2} \end{bmatrix} \quad (8)$$

If the weight matrix is considered, the least squares condition becomes:

$$\sum_i^n \frac{v_i^2}{\sigma_i^2} = \mathbf{V}^t \mathbf{P} \mathbf{V} \text{ minimal} \quad (9)$$

And the optimal solution in the least squares sense  $\hat{\mathbf{X}} = \mathbf{X}_0 + \delta\mathbf{X}$ , where  $\delta\mathbf{X}$  is the correction to make to the *a priori* initial estimate, is estimated by the following system:

$$\begin{cases} \mathbf{A}\delta\mathbf{X} + \mathbf{V} = \mathbf{B} \\ \mathbf{V}^t \mathbf{P} \mathbf{V} \text{ minimal} \end{cases} \quad (10)$$

If we call the matrix  $\mathbf{N} = \mathbf{A}^t \mathbf{P} \mathbf{A}$  the *normal matrix*, the correction  $\delta\mathbf{X}$  is obtained by solving the *normal equation*:

$$\mathbf{N}\delta\mathbf{X} = \mathbf{A}^t \mathbf{P} \mathbf{B} \quad (11)$$

Which gives :

$$\boxed{\delta\mathbf{X} = \mathbf{N}^{-1} \mathbf{A}^t \mathbf{P} \mathbf{B}} \quad (12)$$

The residues are obtained as follows:

$$\hat{\mathbf{V}} = \mathbf{B} - \mathbf{A}\hat{\mathbf{X}} = \mathbf{L} - f(\hat{\mathbf{X}}) \quad (13)$$

Following an iterative process, the new estimate  $\hat{\mathbf{X}}$  becomes the new *a priori*  $\mathbf{X}_0$  in the next inversion step. We have, at the  $k$ -th iteration of the inversion:

$$\hat{\mathbf{X}}_k = \mathbf{X}_{0,k+1} \quad (14)$$

We stop the iterations when the convergence criterion is fulfilled, *i.e.* when  $\|\delta\mathbf{X}_k\| < \kappa$  (where  $\kappa$  is a predetermined threshold).

## 1.1 About the observation function

The function  $F$  is an *ad hoc* multivariate function of  $\mathbb{R}^p \rightarrow \mathbb{R}^n$ , specific to each problem. It can be separated into  $n$  *observation equations*  $f_i$ .

For each observation  $l_i$ , we have the associated functional model:

$$\lambda_i = f_i(x_1, \dots, x_p, \mathbf{\Omega}_{l_i}) \quad (15)$$

where  $\mathbf{\Omega}$  is a set of additional observations.

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<sup>1</sup>in the simplified case where the uncorrelated observations are assumed

We can then define  $F$ :

$$F(x_1, \dots, x_p) = \begin{cases} f_1(x_1, \dots, x_p, \boldsymbol{\Omega}_{l_1}) & = \lambda_1 \\ \vdots & \\ f_n(x_1, \dots, x_p, \boldsymbol{\Omega}_{l_n}) & = \lambda_n \end{cases} \quad (16)$$

We call the function  $F$ , common to all observations, the *observation function*.

## 1.2 Constraints from the Helmert Method

In our case, some additional information links the unknowns to one another. Thus, it is necessary to augment the system with additional equations. We use the constraining method described by the German geodesist Friedrich Helmert (Helmert, 1872). It allows to set some unknowns with predefined values, or to specify some relations linking the unknowns to one another.

It aims to “surround” the normal matrix  $\mathbf{N}$  with a matrix  $\mathbf{C}$  representing the constraints on the parameters (Ghilani, 2011):

$$\begin{bmatrix} \mathbf{N} & \mathbf{C}^t \\ \mathbf{C} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \delta\mathbf{X} \\ \boldsymbol{\Gamma} \end{bmatrix} = \begin{bmatrix} \mathbf{A}^t\mathbf{P}\mathbf{B} \\ \boldsymbol{\Phi} \end{bmatrix} \quad (17)$$

If there are  $q$  constraint equations,  $\mathbf{C}$  is a  $q \times p$ -sized matrix that describes the relationships between  $p$  parameters, and  $\boldsymbol{\Phi}$  is a vector of length  $q$  where the constraints values are stored.  $\boldsymbol{\Gamma}$  denotes the vector of Lagrange multipliers, estimated in addition to  $\delta\mathbf{X}$ .

This new normal equation is solved in the same way as the classical version, by inverting the augmented normal matrix.

## 2 Generic design matrix definition

If  $n_R$  transponders are used, the associated design matrix  $\mathbf{A}_{SMA}$  is block-diagonal, of size  $(n_\tau \cdot n_R, 3n_R)$ , in the ideal case where each transponder has responded to  $n_\tau$  pings sent from the surface. In a more realistic case, its size is  $(\sum_{i=1}^{n_R} n_{\tau, R_i}, 3n_R)$  where we have a number  $n_{\tau, R_i}$  of pings for each receiver  $R_i$

$$\mathbf{A}_{SMA} = \begin{bmatrix} \mathbf{A}_{SMA, R_1} & 0 & \cdots & 0 \\ 0 & \mathbf{A}_{SMA, R_2} & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & \mathbf{A}_{SMA, R_{n_R}} \end{bmatrix} \quad (18)$$

with :

$$\mathbf{A}_{SMA, R_i} = \begin{bmatrix} \frac{df_{SMA, \tau_1}}{dx_{R_i}} & \frac{df_{SMA, \tau_1}}{dy_{R_i}} & \frac{df_{SMA, \tau_1}}{dz_{R_i}} \\ \frac{df_{SMA, \tau_2}}{dx_{R_i}} & \frac{df_{SMA, \tau_2}}{dy_{R_i}} & \frac{df_{SMA, \tau_2}}{dz_{R_i}} \\ \vdots & \vdots & \vdots \\ \frac{df_{SMA, \tau_{n_\tau}}}{dx_{R_i}} & \frac{df_{SMA, \tau_{n_\tau}}}{dy_{R_i}} & \frac{df_{SMA, \tau_{n_\tau}}}{dz_{R_i}} \end{bmatrix} \quad (19)$$

$f_{SMA, \tau_i}$  is the observation function associated to a two-way travel time  $\tau_i$  as defined in relation 2 of the main article. It can be differentiated numerically using a method described in Abramowitz and Stegun

(1965) or Burden and Faires (1998) for instance. In our study, we implemented the *three-point midpoint formula*.

To each acoustic observation, a weight  $\pi_{\tau,i}$  is associated, to complete the weight matrix  $\mathbf{P}_{SMA}$ .

### 3 Baseline length observations

Starting from the observation function 15 of the main article, we have the following derivatives :

$$\frac{df_D(\mathbf{X}_{R_A}, \mathbf{X}_{R_B})}{d\mathbf{X}_{R_A}} = \left[ \frac{x_{R_A} - x_{R_B}}{D_{AB}}, \frac{y_{R_A} - y_{R_B}}{D_{AB}}, \frac{z_{R_A} - z_{R_B}}{D_{AB}} \right] \quad (20)$$

et

$$\frac{df_D(\mathbf{X}_{R_A}, \mathbf{X}_{R_B})}{d\mathbf{X}_{R_B}} = \left[ \frac{x_{R_B} - x_{R_A}}{D_{AB}}, \frac{y_{R_B} - y_{R_A}}{D_{AB}}, \frac{z_{R_B} - z_{R_A}}{D_{AB}} \right] \quad (21)$$

The observation vector  $\mathbf{L}$  is enhanced so as :

$$\mathbf{L} = \begin{bmatrix} \mathbf{L}_{SMA} \\ \mathbf{L}_D \end{bmatrix} = \begin{bmatrix} \tau_1 \\ \vdots \\ \tau_{n_\tau} \\ D_{12} \\ \vdots \\ D_{ij} \\ \vdots \\ D_{n_R-1, n_R} \end{bmatrix} \quad (22)$$

And the design matrix is also enhanced :

$$\mathbf{A} = \begin{bmatrix} \mathbf{A}_{SMA} \\ \mathbf{A}_D \end{bmatrix} \quad (23)$$

where  $\mathbf{A}_{SMA}$  is the design matrix defined in the main article section 2.3, and  $\mathbf{A}_D$  the design matrix of baseline length measurements, of size  $(n_D, 3n_R)$ .

We have (with  $n = n_R$ ):

$$D = \begin{bmatrix} \frac{x_{R_1} - x_{R_2}}{D_{12}} & \frac{y_{R_1} - y_{R_2}}{D_{12}} & \frac{z_{R_1} - z_{R_2}}{D_{12}} & \frac{x_{R_2} - x_{R_1}}{D_{21}} & \frac{y_{R_2} - y_{R_1}}{D_{21}} & \frac{z_{R_2} - z_{R_1}}{D_{21}} & 0 & \dots 0 \dots & 0 \\ \vdots & \vdots \\ 0 \dots & \frac{x_{R_i} - x_{R_j}}{D_{ij}} & \frac{y_{R_i} - y_{R_j}}{D_{ij}} & \frac{z_{R_i} - z_{R_j}}{D_{ij}} & \dots 0 \dots & \frac{x_{R_j} - x_{R_i}}{D_{ji}} & \frac{x_{R_j} - x_{R_i}}{D_{ji}} & \frac{x_{R_j} - x_{R_i}}{D_{ji}} & \dots 0 \\ \vdots & \vdots \\ 0 & \dots 0 \dots & 0 & \frac{x_{R_{n-1}} - x_{R_n}}{D_{n-1, n}} & \frac{y_{R_{n-1}} - y_{R_n}}{D_{n-1, n}} & \frac{z_{R_{n-1}} - z_{R_n}}{D_{n-1, n}} & \frac{x_{R_n} - x_{R_{n-1}}}{D_{n, n-1}} & \frac{x_{R_n} - x_{R_{n-1}}}{D_{n, n-1}} & \frac{x_{R_n} - x_{R_{n-1}}}{D_{n, n-1}} \end{bmatrix} \quad (24)$$

Or, in a simplified form :

$$\mathbf{A}_D = \begin{bmatrix} \mathbf{A}_{D_{12}} & \mathbf{A}_{D_{21}} & 0 & \cdots 0 \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 \cdots & \mathbf{A}_{D_{ij}} & \cdots 0 \cdots & \mathbf{A}_{D_{ji}} & \cdots 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 0 & \cdots 0 \cdots & 0 & \mathbf{A}_{D_{n-1,n}} & \mathbf{A}_{D_{n,n-1}} \end{bmatrix} \quad (25)$$

With :

$$\mathbf{A}_{D_{ij}} = \begin{bmatrix} \frac{x_{R_i} - x_{R_j}}{D_{ij}} & \frac{y_{R_i} - y_{R_j}}{D_{ij}} & \frac{z_{R_i} - z_{R_j}}{D_{ij}} \end{bmatrix} \quad (26)$$

It is also necessary to add weights  $\pi_{D,i}$  corresponding to the lengths of baselines in the corresponding matrix  $P$ , since we add observations of different nature to the problem.

## 4 Direct estimation of the barycentrer coordinates

Relation 9 in the main article stipulates that :

$$\sum_{i=1}^{n_R} \Delta \mathbf{X}_{R_i} = 0 \quad (27)$$

meaning that the sum of the coordinate differences between all transponders must be equal to zero.

For  $n$  transponders on the seafloor, the vector of unknowns is :

$$\mathbf{X} = \begin{bmatrix} x_G \\ y_G \\ y_G \\ \Delta x_{R_1} \\ \Delta y_{R_1} \\ \Delta z_{R_1} \\ \vdots \\ \Delta x_{R_n} \\ \Delta y_{R_n} \\ \Delta z_{R_n} \end{bmatrix} \quad (28)$$

Since

$$\frac{df_{SMA,\tau}}{d\mathbf{X}_G} = \frac{df_{SMA,\tau}}{d\Delta \mathbf{X}_R} \quad (29)$$

by analogy with the relations 18 and 19, the design matrix  $\mathbf{A}_{SMA}$  takes the following form:

$$\mathbf{A}_{SMA} = \begin{bmatrix} \mathbf{A}_{SMA,R_1} & \mathbf{A}_{SMA,R_1} & 0 & \cdots & 0 \\ \mathbf{A}_{SMA,R_2} & 0 & \mathbf{A}_{SMA,R_2} & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \mathbf{A}_{SMA,R_{n_R}} & 0 & 0 & \cdots & \mathbf{A}_{SMA,R_{n_R}} \end{bmatrix} \quad (30)$$

Following the Helmert's method described in section 1.2 (equation 17), the matrix  $\mathbf{C}$  and the vector  $\Phi$  are respectively equal to :

$$\mathbf{C} = \begin{bmatrix} 0 & 0 & 0 & \cdots & 1 & 0 & 0 & \cdots \\ 0 & 0 & 0 & \cdots & 0 & 1 & 0 & \cdots \\ 0 & 0 & 0 & \cdots & 0 & 0 & 1 & \cdots \end{bmatrix} \quad (31)$$

$\underbrace{\hspace{10em}}_{n_R \text{ times}}$

$$\Phi = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad (32)$$

## 5 Estimation of a single depth

If we assume a single common depth for all seafloor transponders, then the vector of unknowns becomes :

$$\mathbf{X} = \begin{bmatrix} x_{R_1} \\ y_{R_1} \\ \vdots \\ x_{R_n} \\ y_{R_n} \\ \bar{z} \end{bmatrix} \quad (33)$$

The design matrix takes the following shape :

$$\mathbf{A}_{SMA} = \begin{bmatrix} \mathbf{A}_{SMA,R_1} & 0 & \cdots & 0 & \frac{df_{SMA,\tau_1}}{d\bar{z}} \\ 0 & \mathbf{A}_{SMA,R_2} & \cdots & 0 & \frac{df_{SMA,\tau_2}}{d\bar{z}} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & \mathbf{A}_{SMA,R_{n_R}} & \frac{df_{SMA,\tau_{n_R},R_{n_R}}}{d\bar{z}} \end{bmatrix} \quad (34)$$

In this case:

$$\mathbf{A}_{SMA,R_i} = \begin{bmatrix} \frac{df_{SMA,\tau_1}}{dx_{R_i}} & \frac{df_{SMA,\tau_1}}{dy_{R_i}} \\ \frac{df_{SMA,\tau_2}}{dx_{R_i}} & \frac{df_{SMA,\tau_2}}{dy_{R_i}} \\ \vdots & \vdots \\ \frac{df_{SMA,\tau_{n_R},R_i}}{dx_{R_i}} & \frac{df_{SMA,\tau_{n_R},R_i}}{dy_{R_i}} \end{bmatrix} \quad (35)$$

