



Article Analysis of the Influence of Polarization Measurement Errors on the Parameter and Characteristics Measurement of the Fully Polarized Entomological Radar

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Abstract: Measuring the orientation, mass and body length of migratory insects through entomological radar is crucial for early warnings of migratory pests. The fully polarized entomological radar is an efficient device for observing migratory insects by calculating insect parameters through the scattering matrix obtained from the target. However, the measured target scattering matrix will be affected by system polarization measurement errors, leading to errors in insect parameter calculation, while the related analysis is currently relatively limited. Therefore, the scattering matrix measurement process is modeled, followed by an analysis of the effects of different errors on orientation, mass and body length estimation. The influence of polarization measurement errors, the measurement errors of insect orientation, mass and body length will vary with insect orientation in specific patterns, and the distribution of measured insect parameters will be drastically distorted compared to the true parameter distribution. In addition, polarization measurement errors could seriously disrupt the reciprocity and bilateral symmetry of the measured insect scattering matrix. These analyses and conclusions provide a good basis for eliminating the effects of polarization measurement.

Keywords: entomological radar; polarization measurement errors; insect parameter estimation; polarization scattering characteristics

1. Introduction

In order to search for suitable resources, address climate change, avoid competitive pressures and breed offspring, a large number of insects migrate across global ecosystems and transmit a large amount of material, energy and viruses between different regions [1–3]. The vast numbers of migratory insects not only influence natural ecosystems but are also closely related to human production and life. Migratory pests lead to a significant reduction in food production every year [4]. In order to study the migration patterns of insects and pest warning, the migration routes, biomass, and species of migratory insects have been studied by a multitude of researchers [5–7].

Insect orientation is the active flight direction of insects and an important parameter for studying insect migration routes. Insect mass can be used to calculate the biomass of migratory insects, and can also be used together with body length to identify insect species. Thus, it is important to accurately obtain parameters such as the orientation, mass and body length of insects.



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Copyright: © 2024 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). Entomological radar can measure the orientation, mass and body length [8,9] of insects through insect echoes and is an important tool for researchers to study migratory insects. As a newly developed entomological radar in recent years, the fully polarized entomological radar has the advantages of a high measurement efficiency and high signal-to-noise ratio (SNR) [10]. The fully polarized entomological radar simultaneously transmits two polarized and waveform orthogonal signals, and obtains the target scattering matrix (SM) through the received H and V polarization echoes [11,12]. The SM contains all the information of the target under the current radar perspective, which can be used to calculate the orientation, mass and body length of insects [13–16].

However, nonideal factors in the system could lead to estimation errors in parameters such as insect orientation, mass and body length. The main factors contributing to the distortion of the measured SM of targets are the imbalance present in the antenna and signal transmission links, cross-crosstalk between the antenna H and V channels [17] and antenna pattern modulation [18]. These nonideal factors in this article are collectively referred to as polarization measurement errors. These polarization measurement errors could cause distortion of transmission signals, leading to distortion of the measured SM of insects. The insect parameters calculated from the distorted SM might also deviate from the true insect parameters. In addition, polarization measurement errors can also influence the scattering characteristics of the measured insect SM, such as reducing the degree of reciprocity and bilateral symmetry of measured insect SMs.

Although insect parameter estimation and insect scattering characteristics could be severely affected by polarization measurement errors in practical situations, there is currently very little analysis on the influence of polarization measurement errors on insect parameter estimation and the characteristics of the measured insect SM. In this paper, the influence of various polarization measurement errors on insect parameter calculation is analyzed through theoretical derivation and simulation. The influence of polarization measurement errors on the distribution of insect orientation, mass and body length are also analyzed. Polarization measurement errors are related to components such as radar antennas and transmission links. Therefore, when designing the radar system, it is necessary to obtain the range of polarization measurement errors through the mapping relationship between insect parameter calculation errors and polarization measurement errors and to select appropriate radar components based on the range of polarization measurement errors. However, it is time-consuming to obtain the mapping relationship between insect parameter calculation errors and polarization measurement errors through extensive simulation. The relevant analysis provides the mapping relationship between polarization measurement errors and insect parameter calculation errors in the form of formulas, thus avoiding the complex simulation.

The influence of various polarization measurement errors on insect scattering characteristics, and the disruption of insect reciprocity and bilateral symmetry, is also analyzed through theoretical derivation and simulation. For radar with fixed polarization measurement errors, it is usually possible to measure the known SM calibrators and calculate the polarization measurement error using the calibrator SM and the measured SM. Then, using the calculated polarization measurement error to compensate for other targets, the accurate target SM can be obtained. During the operation of the radar, it is necessary to re-measure the calibrator and calculate the polarization measurement error at regular intervals, which is very cumbersome. Relevant analysis presents that it is possible to calculate polarization measurement errors by utilizing the influence of polarization measurement errors on target reciprocity and bilateral symmetry, thus avoiding complex calibrator measurements.

The influence of polarization measurement errors is further validated on an X band fully polarized entomological radar and a Ku band fully polarized entomological radar, respectively.

This paper is organized as follows. The polarization measurement model is introduced in Section 2. The influence of polarization measurement errors to the estimation of insect orientation, the estimation of insect mass and body length and the characteristics of the measured insect SM are analyzed in Sections 3–5. In Section 6, the influence of polarization measurement errors on insect orientation, mass and body length measurements, as well as the influence of polarization measurement errors on the reciprocity and bilateral symmetry of the measured SM, are discussed. And methods to solve polarization measurement errors are also discussed. In Section 7, conclusions are given.

2. Polarization Measurement Errors Model

The signal transmitted through the RF links, antenna and free space to the target can be represented as [19]:

$$\boldsymbol{E}_{target} = \frac{e^{-j2\pi r/\lambda}}{r} \begin{bmatrix} 1 & C_2 \\ C_1 & 1 \end{bmatrix} \begin{bmatrix} T_h & 0 \\ 0 & T_v \end{bmatrix} \boldsymbol{E}_{transmitter}$$
(1)

where $E_{transmitter}$ is a 2 × 1 vector, representing the polarization state of the generated signal. T_h and T_v represents the imbalance in the antenna and RF links during the transmission process. C_1 and C_2 are the cross-talks between the H and V channels in the antenna, with $|C_1| \ll 1$ and $|C_2| \ll 1$. r is the distance from the target to the radar. λ is the carrier wavelength. E_{target} is also a 2 × 1 vector, representing the polarization state of the signal at the target. The received signal could be expressed as

$$\boldsymbol{E}_{receiver} = g \frac{e^{-j2\pi r/\lambda}}{r} \begin{bmatrix} R_h & 0\\ 0 & R_v \end{bmatrix} \begin{bmatrix} 1 & C_1\\ C_2 & 1 \end{bmatrix} \begin{bmatrix} s_{hh} & s_{hv}\\ s_{vh} & s_{vv} \end{bmatrix} \boldsymbol{E}_{target}$$
(2)

where $s_{ij}(i, j = h, v)$ is the element of the SM and represents the ability of the target to convert a *j*-polarized signal into an *i*-polarized signal. R_h and R_v represent the imbalance in the antenna and RF links during the receiving process. g < 1 is the echo attenuation caused by antenna pattern modulation. $E_{receiver}$ is a 2 × 1 vector, representing the polarization state of the received signal.

The complete signal reception process can be represented as

$$E_{receiver} = g \frac{e^{-j4\pi r/\lambda}}{r^2} \begin{bmatrix} R_h & 0\\ 0 & R_v \end{bmatrix} \begin{bmatrix} 1 & C_1\\ C_2 & 1 \end{bmatrix} \begin{bmatrix} s_{hh} & s_{hv}\\ s_{vh} & s_{vv} \end{bmatrix} \begin{bmatrix} 1 & C_2\\ C_1 & 1 \end{bmatrix} \begin{bmatrix} T_h & 0\\ 0 & T_v \end{bmatrix} E_{transmitter}$$
(3)

Defining

$$G = gR_h T_h \frac{e^{-j4\pi r/\lambda}}{r^2} \tag{4}$$

$$a_1 = R_v / R_h \tag{5}$$

$$u_2 = T_v / T_h \tag{6}$$

G, a_1 , a_2 , C_1 and C_2 are polarization measurement errors, which could influence the received signal and the measurement of insect parameters. Ideally or after precise calibration of the radar, $a_1 = a_2 = 1$ and $C_1 = C_2 = 0$, but this is not the case for actual systems. Usually for entomological radar, the distance of insects can be measured, and r could be compensated. R_h and T_h are also calibratable, so g is usually the main factor affecting insect parameters' measurement. Thus, in the following, G is assumed to be less than 1, as g.

a

Equation (3) could be re-expressed as

$$E_{receiver} = GRCSC^{T}TE_{transmitter}$$
⁽⁷⁾

where

$$\mathbf{R} = \begin{bmatrix} 1 & 0\\ 0 & a_1 \end{bmatrix} \tag{8}$$

$$\mathbf{C} = \begin{bmatrix} 1 & C_1 \\ C_2 & 1 \end{bmatrix} \tag{9}$$

$$\mathbf{T} = \begin{bmatrix} 1 & 0\\ 0 & a_2 \end{bmatrix} \tag{10}$$

$$\mathbf{S} = \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix}$$
(11)

and the superscript T represents the transpose of the matrix.

By Equation (7), it can be seen that the target measured SM in the presence of systematic polarization measurement errors can be expressed as

$$\mathbf{S}^{m} = \begin{bmatrix} s_{hh}^{m} & s_{hv}^{m} \\ s_{vh}^{m} & s_{vv}^{m} \end{bmatrix} = \mathbf{R}\mathbf{C}\mathbf{S}\mathbf{C}^{\mathsf{T}}\mathbf{T}$$
(12)

In the following, the influence of polarization measurement errors on calculating the insect orientation, mass, body length, degree of reciprocity and degree of bilateral symmetry through S^m is presented.

3. The Influence of Polarization Measurement Errors on Orientation Measurement

System polarization measurement errors could lead to estimation errors in insect orientation, resulting in severe distortion of the final insect orientation distribution. In the following, the insect orientation calculation method is first introduced and the influence of polarization measurement errors on insect orientation calculation is theoretically analyzed. Then, the influence of polarization measurement errors on individual insect orientation measurement and statistical distribution of insect orientation is analyzed through simulation. Finally, the influence of polarization measurement errors on insect orientation distribution statistics is demonstrated through measurement results of two fully polarized radars.

3.1. The Calculation Method of Insect Orientation

When the insect body axis is parallel to H-polarization, the SM can be expressed as [18]

$$\mathbf{S}_{\theta=0} = \begin{bmatrix} \sqrt{\sigma_{hh}} & 0\\ 0 & e^{j\phi}\sqrt{\sigma_{vv}} \end{bmatrix}$$
(13)

where σ_{hh} and σ_{vv} are the RCS of the HH and VV channels, respectively, and ϕ is the phase difference between the HH channel and VV channel. The insect SM for an arbitrary angle could be expressed as

$$\mathbf{S}_{\theta} = \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix} = \mathbf{R}_{\theta} \mathbf{S}_{\theta=0} (\mathbf{R}_{\theta})^{\mathbf{T}}$$
(14)

where $\theta \in (-\pi/2, \pi/2]$ denotes the angle of the insect's orientation deviation from H-polarization and **R**_{θ} is the rotation matrix:

$$\mathbf{R}_{\theta} = \begin{bmatrix} \cos\theta & -\sin\theta\\ \sin\theta & \cos\theta \end{bmatrix}$$
(15)

By constraining the target cross channel to be minimized after rotating the S_{θ} by a certain angle, the expression for the insect orientation could be obtained [18]:

$$\hat{\theta}_0 = \frac{1}{2} \arctan\left(\frac{s_{hv} + s_{vh}}{s_{hh} - s_{vv}}\right) \qquad \hat{\theta}_0 \in \left(-\frac{\pi}{4}, \frac{\pi}{4}\right) \tag{16}$$

For bilateral symmetry targets, $\hat{\theta}_0$ is real. Due to the influence of noise, the imaginary part of $\hat{\theta}_0$ may not be 0 and the calculated orientation can be consistent with the actual orientation by filtering out the imaginary part of $\hat{\theta}_0$:

$$\hat{\theta}_1 = \frac{1}{2} \operatorname{real}(\arctan(\frac{s_{hv} + s_{vh}}{s_{hh} - s_{vv}})) \qquad \hat{\theta}_1 \in (-\frac{\pi}{4}, \frac{\pi}{4})$$
(17)

where real(•) represents taking the real part of the complex. It could be seen that the range of $\hat{\theta}_1$ is smaller than that of θ . The ambiguity of $\hat{\theta}_1$ could be solved by the relative phase of SM eigenvalues [20] or a classifier based on more features [18]. The final calculated orientation of insect could be expressed as

$$\hat{\theta} = \mathrm{SA}(\frac{1}{2}real(\arctan(\frac{s_{hv} + s_{vh}}{s_{hh} - s_{vv}}))) \qquad \hat{\theta} \in (-\frac{\pi}{2}, \frac{\pi}{2}]$$
(18)

where SA(•) represents the function to expand the orientation to the range of $(-\pi/2, \pi/2]$. A more detailed introduction to insect orientation calculation could be found by referring to [17,19].

3.2. Theoretical Analysis on the Orientation Calculation Error

According to Equations (12) and (14), in the presence of polarization measurement errors, the SM of insects at an arbitrary angle could be expressed as

$$\mathbf{S}_{\theta}^{m} = \begin{bmatrix} s_{hh}^{m} & s_{hv}^{m} \\ s_{vh}^{m} & s_{vv}^{m} \end{bmatrix} = G\mathbf{R}\mathbf{C}\mathbf{R}_{\theta}\mathbf{S}_{\theta=0}(\mathbf{R}_{\theta})^{\mathsf{T}}\mathbf{C}^{\mathsf{T}}\mathbf{T}$$
(19)

Based on the measured SM \mathbf{S}_{θ}^{m} of insects, the $\hat{\theta}_{0}$ calculated by Equation (16) can be expressed as

$$\hat{\theta}_0^m = \frac{1}{2} \arctan(\frac{s_{vh}^m + s_{hv}^m}{s_{vv}^m - s_{hh}^m})$$
(20)

Obviously, *G* will not affect the calculation of $\hat{\theta}_0^m$. The first-order Taylor expansion of Equation (20) at $a_1 = 1$, $a_2 = 1$, $C_1 = 0$ and $C_2 = 0$ can be expressed as

$$\hat{\theta}_{0}^{m} = \hat{\theta}_{0}^{m} \Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0} + (a_{1}-1)\frac{\partial\hat{\theta}_{0}^{m}}{\partial a_{1}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0} + (a_{2}-1)\frac{\partial\hat{\theta}_{0}^{m}}{\partial a_{2}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0} + C_{1}\frac{\partial\hat{\theta}_{0}^{m}}{\partial C_{1}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0} + C_{2}\frac{\partial\hat{\theta}_{0}^{m}}{\partial C_{2}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0} + o^{n}$$

$$(21)$$

where o^n is the error term.

By substituting Equations (19) and (20) into Equation (21) and simplifying them, we could obtain

$$\hat{\theta}_{0}^{m} = \hat{\theta}_{0} + \frac{1}{4}(a_{1} + a_{2} - 2) \frac{(\sigma_{hh} - e^{j\varphi}\sigma_{vv})}{(e^{j\phi}\sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}})^{2}} \sin 2\theta + \frac{1}{2}(C_{1} + C_{2}) \frac{\sigma_{hh} - e^{j2\phi}\sigma_{vv}}{(e^{j\phi}\sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}})^{2}} \cos 2\theta + \frac{1}{2}(C_{2} - C_{1}) + o^{n}$$
(22)

Assuming that the polarization measurement errors could not affect the process of resolving ambiguity (as can be seen from subsequent analysis, the SA(•) function only fails when the polarization measurement errors are huge). The final measured insect orientation $\hat{\theta}^m$ could be obtained by filtering out the imaginary part of $\hat{\theta}^m_0$ and resolving the ambiguity:

$$\hat{\theta}^m = \hat{\theta} + \Delta \hat{\theta}'_{\max} \sin 2\theta + \Delta \hat{\theta}''_{\max} \cos 2\theta + \frac{1}{2} \operatorname{real}(C_2 - C_1) + o^n$$
(23)

where

$$\Delta \hat{\theta}'_{\max} = \frac{1}{4} \operatorname{real}[(a_1 + a_2 - 2) \frac{(\sigma_{hh} - e^{j\phi}\sigma_{vv})}{(e^{j\phi}\sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}})^2}]$$
(24)

$$\Delta \hat{\theta}_{\max}^{\prime\prime} = \frac{1}{2} \operatorname{real}[(C_1 + C_2) \frac{\sigma_{hh} - e^{j2\phi} \sigma_{vv}}{\left(e^{j\phi} \sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}}\right)^2}]$$
(25)

It can be seen that the orientation measurement error of insects is not only related to a_1 , a_2 , C_1 and C_2 , but also to the σ_{hh} , σ_{vv} , ϕ and θ of the insects. a_1 and a_2 bring error terms that vary in the form of $\sin(2\theta)$ with the orientation of the insect. C_1 and C_2 not only bring

error terms that vary in the form of $cos(2\theta)$ with the orientation of the insect, but also lead to a constant error term related to the difference between C_1 and C_2 .

Equation (23) could also be expressed as

$$\hat{\theta}^m = \theta + \Delta \hat{\theta}_{\max} \sin(2(\theta + \varphi_u)) + \frac{1}{2} \operatorname{real}(C_2 - C_1) + o^n$$
(26)

where

$$\Delta\hat{\theta}_{\max} = \sqrt{\left(\Delta\hat{\theta}'_{\max}\right)^2 + \left(\Delta\hat{\theta}''_{\max}\right)^2} \tag{27}$$

$$\varphi_{u} = \frac{1}{2} \arctan(\frac{\Delta \hat{\theta}_{\max}''}{\Delta \hat{\theta}_{\max}'})$$
(28)

The orientation estimation error due to polarization measurement errors could be expressed as

$$\hat{\theta}_{error} = \Delta \hat{\theta}_{\max} \sin(2(\theta + \varphi_u)) + \frac{1}{2} \operatorname{real}(C_2 - C_1)$$
⁽²⁹⁾

It can be seen that the orientation estimation error of insects consists of two parts: a trigonometric variation with orientation and a constant error term. If $real(C_2 - C_1) > 0$, when the insect angle is $0.25\pi + k\pi - \varphi_u$, the maximum orientation estimation error of the insect is $\Delta \hat{\theta}_{max} + 0.5real(C_2 - C_1)$; if $real(C_2 - C_1) < 0$, when the insect angle is $0.75\pi + k\pi - \varphi_u$, the maximum orientation estimation error of the insect angle is $-\Delta \hat{\theta}_{max} + 0.5real(C_2 - C_1)$.

3.3. Simulation on Individual Measurement Error and Orientation Distribution Distortion

In order to verify the accuracy of Equation (29) about the insect orientation estimation errors, simulations are conducted on the pests *Helicoverpa armigera*, *Mythimna separata* and *Agrotis ipsilon*. The SM of these pests comes from the dataset introduced in [20], and SMs in the Ku band are chosen. Through Equation (14), the SMs of insects with different orientations can be obtained. Then, the measured target SMs are obtained by Equation (12), and the polarization measurement errors are presented in Table 1. The orientation of insects is calculated using Equation (18) through these measured target SMs, and the orientation estimation error is recorded.

Table 1. Polarization measurement errors in simulation.

Simulation Label	<i>a</i> ₁	<i>a</i> ₂	<i>C</i> ₁	<i>C</i> ₂	G
1	1.1	1.1	0	0	1
2	$e^{j\pi/32}$	$e^{j\pi/32}$	0	0	1
3	1	1	$0.01 e^{j\pi/32}$	0	1
4	$1.01 e^{j\pi/64}$	$1.01 e^{j\pi/64}$	$0.01 e^{j\pi/64}$	$0.01 e^{j\pi/64}$	1
5	$1.5e^{j\pi/8}$	1.5	0	0	1
6	1	1	$0.1e^{j\pi/4}$	$0.1e^{-j\pi/2}$	1
7	$1.5e^{j\pi/8}$	$1.5e^{j\pi/8}$	$0.1e^{-j\pi/2}$	$0.1e^{-j\pi/2}$	1
8	$1.5e^{j\pi/8}$	1	$0.1e^{-j\pi/2}$	0	1
9	0	0	0	0	0.7
10	$1.01e^{j\pi/64}$	$1.01e^{j\pi/64}$	$0.01 e^{j\pi/64}$	$0.01 e^{j\pi/64}$	0.7

Taylor's first-order and second-order expansions are also used to calculate insect orientation estimation errors.

The orientation estimation error of the first to fourth systems are illustrated in Figure 1. It can be seen that the orientation estimation error of insects calculated through first-order Taylor expansion and second-order Taylor expansion is relatively close to the estimation error obtained through simulation. This indicates that the estimation errors of insect orientation calculated through Equation (29) obtained by first-order Taylor expansion are accurate enough to describe the estimation error of insect orientation.



Figure 1. The influence of polarization measurement errors on insect orientation estimation. (a-c): the first system in Table 1 is used; (d-f): the second system in Table 1 is used; (g-i): the third system in Table 1 is used; (j-i): the fourth system in Table 1 is used.

The C_1 and C_2 are zero in the first and second system, and a_1 and a_2 cause orientation estimation errors. Thus, the orientation estimation errors in Figure 1a–f vary in the form of $sin(2\theta)$ with the orientation of the insect. The minimum estimation error for insect orientation is at 0, 90°, 180° and 270°. The a_1 and a_2 are 1 in the third system, and C_1 and C_2 cause orientation estimation errors. Thus, the orientation estimation errors in Figure 1g–i vary in the form of $cos(2\theta)$ with the orientation of the insect. Due to the difference between C_1 and C_2 , the orientation estimation error is also affected by the constant error term, as presented in Equation (29). The a_1 and a_2 are not 1, and C_1 and C_2 are not 0 in the fourth system. Thus, the estimation errors of insect orientation vary approximately in the form of a regular trigonometric function with respect to insect orientation.

The orientation estimation error calculated by simulation of the fifth to eighth systems are illustrated in Figure 2. The orientation estimation error approaches 90° in some cases, indicating that insect orientation solution ambiguity errors occur, although the insect orientation solution ambiguity errors usually occur only in partial orientation intervals. It can be seen that compared with the first four systems, the polarization measurement errors of the fifth to eighth systems are more severe, which is the condition for the occurrence of ambiguity resolution errors.



Figure 2. The influence of polarization measurement errors on solving the orientation ambiguity.

In order to analyze the influence of polarization measurement errors on orientation distribution, simulations are conducted on all insects in the dataset, and the SM in the Ku band are chosen. The SMs of insects with different orientations are obtained through Equation (14), and the orientations of insects are evenly distributed in the range of $0-360^{\circ}$, as presented in Figure 3.



Figure 3. Insect orientation distribution without the influence of polarization measurement errors.

The simulation results of insect orientation distribution are presented in Figure 4. In Figure 4a,b, the measured insect orientations cluster in the direction of H or V polarization. This is due to the fact that the orientation estimation error is smaller at insect orientations of 0, $\pi/2$, π and $3\pi/4$, whereas the more the insect's orientation deviates from these angles, the greater the orientation estimation errors. It can be seen that a_1 and a_2 are the reasons that cause insects to converge towards the H and V polarization direction. In Figure 4c, the measured insect orientations cluster in direction, deviating from H and V polarization. This is due to the fact that for errors of the $\cos(2\theta)$ form, the larger insect orientation estimation estimation error term due

to the difference between C_1 and C_2 , the final insect orientation will be biased towards the $\pi/4 + 0.5\text{real}(C_2 - C_1)$ or $-\pi/4 + 0.5\text{real}(C_2 - C_1)$. For the more general case, the insect orientation will be biased to $-\varphi_u + 0.5\text{real}(C_2 - C_1)$ or $-\varphi_u + \pi/2 + 0.5\text{real}(C_2 - C_1)$. These analyses are consistent with Equation (29). For cases with huge polarization measurement errors, as presented in Figure 4e–h, the insect orientation will be more clustered or deviated towards H and V polarization.



Figure 4. The influence of polarization measurement errors on the distribution of insect orientation.

3.4. Analysis of Radar Measurement Data

In order to verify the effect of polarization measurement errors on the insect orientation estimation in the real system, the orientation distribution of the insect target is recorded based on a Ku band entomological radar and an X band entomological radar, as presented in Figure 5. The Ku band entomological radar has been introduced in [10] and [21]. The X band radar adopts the same waveform and operating mode as the Ku band radar, and system parameters of the X band entomological radar are presented in Table 2.



Figure 5. The Ku band fully polarized entomological radar (**a**) and X band fully polarized entomological radar (**b**).

Parameters	Values	Parameters	Values	
Frequency/wavelength	$10 \mathrm{GHz}/3 \mathrm{cm}$	Pulse width	1 µs	
Beam width	1.5°	Waveform	Stepped-frequency chirp	
Pulse repetition frequency	40 kHz	Stepped number	40	
Range resolution	~0.2 m	Detection range	150–2000 m	

Table 2. System parameters of the X band entomological radar.

The Ku band radar recorded the orientation of the measured targets in the air on the evening of 2 September 2020, during the time period from 17:00 to 23:00 Beijing time. The X band radar recorded the orientation of the measured targets in the air throughout the day of 13 October 2023. The SM of the measured targets has not been calibrated, and the orientation distributions of all targets are presented in Figure 6. In Figure 6, 0 represents the H polarization direction, 90° represents the V polarization direction.



Figure 6. The orientation distribution obtained from Ku band and X band radar.

It can be seen that the clustering degree of measured insect orientation is relatively high. For the Ku band radar, most of the measured orientation of the targets tend to cluster towards the V polarization direction, while a small portion of the measured orientations tend to cluster towards the H polarization direction. For the X band radar, most measured orientations of the target cluster towards the H polarization direction, while a small portion of the measured orientations cluster towards the V polarization direction or other directions. On the one hand, the convergence of insect orientation towards the H and V polarization directions indicates that a_1 and a_2 are the main polarization measurement errors affecting insect orientation calculation; Conversely, these distributions demonstrate the necessity of polarization for accurately obtaining polarization information of the fully polarized radar.

4. The Influence of Polarization Measurement Errors on Mass and Body Length Measurement

System polarization measurement errors could lead to estimation errors in insect mass and body length, resulting in severe distortion of the measured insect mass and body length distribution. In the following, the insect mass and body length calculation methods are first introduced, and the influence of polarization measurement errors on the calculation of SM eigenvalues, which is closely related to estimators for insect mass and body length, are theoretically derived. Then, the influence of polarization measurement errors on individual insect mass and body length calculations and the statistical distribution of insect mass and body length are analyzed through simulation. Finally, the influence of polarization measurement errors on the insect mass and body length distribution is demonstrated through the measurement results of two fully polarized radars.

4.1. The Calculation Method of Insect Mass and Body Length

For the fully polarized entomological radar, different types of estimators can be calculated through target SMs, and the target mass or body length can be calculated using the constructed mapping from these estimators to the target mass or body length [9,14].

From Equations (13) and (14), it can be seen that $\sqrt{\sigma_{hh}}$ and $\sqrt{\sigma_{vv}}e^{j\phi}$ are the eigenvalues of \mathbf{S}_{θ} . Most of the estimators could be calculated by $\sqrt{\sigma_{hh}}$ and $\sqrt{\sigma_{vv}}e^{j\phi}$; for example v, which is mostly used in the fully polarized entomological radar [15]:

v

$$=\sigma_{vv}$$
 (30)

The eigenvalues of S_{θ} could be expressed as

$$\lambda_1 = \frac{1}{2}(s_{hh} + s_{vv} - \sqrt{(s_{hh} - s_{vv})^2 + 4s_{hv}s_{vh}})$$
(31)

$$\lambda_2 = \frac{1}{2}(s_{hh} + s_{vv} + \sqrt{(s_{hh} - s_{vv})^2 + 4s_{hv}s_{vh}})$$
(32)

For some insects, λ_1 corresponds to $\sqrt{\sigma_{hh}}$ and λ_2 corresponds to $\sqrt{\sigma_{vv}}e^{j\phi}$, while for other insects, λ_1 corresponds to $\sqrt{\sigma_{vv}}e^{j\phi}$ and λ_2 corresponds to $\sqrt{\sigma_{hh}}$ [20]. This is also the same for v, which might be calculated by one of λ_1 or λ_2 .

The mapping of insect mass and body length calculated by v could be expressed as:

$$Mass = x_{10}\log^2(v) + x_{11}\log(v) + x_{12}$$
(33)

$$Length = x_{20}\log^2(v) + x_{21}\log(v) + x_{22}$$
(34)

where $x_{ij}(i = 1, 2; j = 0, 1, 2)$ are the coefficients calculated through the Microwave Anechoic Chamber dataset. In the following, the influence of polarization measurement errors on v is analyzed, but the relevant conclusions could also be applied to other estimators.

4.2. Analysis on the Scattering Matrix Eigenvalues Calculation Error

The eigenvalues of S^m_{θ} could be expressed as

$$\lambda_1^m = \frac{1}{2} (s_{hh}^m + s_{vv}^m - \sqrt{(s_{hh}^m - s_{vv}^m)^2 + 4s_{hv}^m s_{vh}^m})$$
(35)

$$\lambda_2^m = \frac{1}{2} (s_{hh}^m + s_{vv}^m + \sqrt{(s_{hh}^m - s_{vv}^m)^2 + 4s_{hv}^m s_{vh}^m})$$
(36)

The first-order Taylor expansion of Equation (35) at $a_1 = 1$, $a_2 = 1$, $C_1 = 0$, $C_2 = 0$ and G = 1 could be expressed as

$$\lambda_{1}^{m} = \lambda_{1}^{m} \Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + (a_{1}-1)\frac{\partial\lambda_{1}^{m}}{\partial a_{1}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + (a_{2}-1)\frac{\partial\lambda_{1}^{m}}{\partial a_{2}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + C_{1}\frac{\partial\lambda_{1}^{m}}{\partial C_{1}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + C_{2}\frac{\partial\lambda_{1}^{m}}{\partial C_{2}}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + G\frac{\partial\lambda_{1}^{m}}{\partial G}\Big|_{a_{1}=1,a_{2}=1,C_{1}=0,C_{2}=0,G=1} + o^{n}$$

$$(37)$$

By substituting Equations (19) and (35) into Equation (37) and simplifying them, we can obtain

$$\lambda_1^m = G\lambda_1 + \Delta\lambda_1' \sin 2\theta + \Delta\lambda_1'' \cos 2\theta + \Delta\lambda_1''' + o^n \tag{38}$$

where

$$\Delta\lambda_1' = \frac{1}{1} (e^{j\phi} \sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}}) [1 - \frac{2(\sqrt{\sigma_{hh}} + e^{j\phi} \sqrt{\sigma_{vv}})}{\sqrt{(\sqrt{\sigma_{hh}} - e^{j\phi} \sqrt{\sigma_{vv}})^2}}] (C_1 + C_2)$$
(39)

$$\Delta\lambda_1'' = \frac{1}{4} (e^{j\phi} \sqrt{\sigma_{vv}} - \sqrt{\sigma_{hh}}) [1 - \frac{2(\sqrt{\sigma_{hh}} + e^{j\phi} \sqrt{\sigma_{vv}})}{\sqrt{(\sqrt{\sigma_{hh}} - e^{j\phi} \sqrt{\sigma_{vv}})^2}}] (a_1 + a_2 - 2)$$
(40)

$$\Delta\lambda_{1}^{\prime\prime\prime} = (a_{1} + a_{2} - 2)\left\{\frac{1}{4}(\sqrt{\sigma_{hh}} + e^{j\phi}\sqrt{\sigma_{vv}})\left[1 - \frac{2(\sqrt{\sigma_{hh}} + e^{j\phi}\sqrt{\sigma_{vv}})}{\sqrt{(\sqrt{\sigma_{hh}} - e^{j\phi}\sqrt{\sigma_{vv}})^{2}}}\right] + \frac{2\sqrt{\sigma_{hh}}\sqrt{\sigma_{vv}}e^{j\phi}}{\sqrt{(\sqrt{\sigma_{hh}} - e^{j\phi}\sqrt{\sigma_{vv}})^{2}}}\right\}$$
(41)

It can be seen that λ_1^m is not only affected by a_1 , a_2 , C_1 and C_2 , but also by *G*. According to Equation (4), *G* is influenced by *r* and *g*, which are the target distance and the modulation of the antenna pattern on the echo intensity. The influence of *r* could be compensated by the measured target distance. And the influence of *g* could be compensated by the measured target angle and the antenna pattern for radar with monopulse measurement capability. However, for radars that do not use monopulse technology, the antenna pattern modulation might seriously affect *g*, thereby seriously affecting λ_1^m .

 C_1 and C_2 bring error terms that vary in the form of $sin(2\theta)$ with the orientation of the insect. a_1 and a_2 not only bring error terms that vary in the form of $cos(2\theta)$ with the orientation of the insect, but also lead to a constant error term related to the difference between a_1 and a_2 .

Equation (38) could also be expressed as

$$\lambda_1^m = G\lambda_1 + \Delta\lambda_1 \sin(2(\theta + \varphi_\lambda)) + \Delta\lambda_1^{\prime\prime\prime} + o^n \tag{42}$$

where

$$\Delta\lambda_1 = \sqrt{\left(\Delta\lambda_1'\right)^2 + \left(\Delta\lambda_1''\right)^2} \tag{43}$$

$$\varphi_k = \frac{1}{2} \arctan(\frac{\Delta \lambda_1''}{\Delta \lambda_1'}) \tag{44}$$

The λ_1^m calculation error due to polarization measurement errors could be defined as

$$\lambda_1^{error} = \left| (G\lambda_1 + \Delta\lambda_1 \sin(2(\theta + \varphi_\lambda)) + \Delta\lambda_1^{\prime\prime\prime}) / \lambda_1 \right|$$
(45)

In order to verify the accuracy of Equation (42) about the λ_1^m calculation errors, simulations are also conducted on *Helicoverpa armigera*, *Mythimna separata* and *Agrotis ipsilon*, and the SMs in the Ku band are chosen. Through Equation (14), the SMs of insects with different orientations can be obtained. Then, the first, third, ninth and tenth group of polarization measurement errors in Table 1 are used to obtain radar-measured target SMs. The λ_1^m of these insects is calculated using Equation (31) through these measured target SMs, and the λ_1^m calculation errors are recorded.

Taylor's first-order and second-order expansions are also used to obtain the calculation error of λ_1^m .

The λ_1^m calculation error are illustrated in Figure 7. It can be seen that the λ_1^m calculation error of insects calculated through first-order Taylor expansion and second-order Taylor expansion is relatively close to the λ_1^m calculation error obtained through simulation. This indicates that the estimation errors of λ_1^m calculated through Equation (42) obtained by first-order Taylor expansion is accurate enough to describe the λ_1^m calculation error.

The λ_1^m calculation errors in Figure 7a–c are the sum of the $\sin(2\theta)$ form error and the constant error, and the λ_1^m calculation errors in Figure 7d–f vary in the form of $\cos(2\theta)$, which is consistent with Equation (38). In the ninth system, only the modulation of the antenna pattern or *G* could influence the calculation of λ_1^m , and it could be seen that the λ_1^m calculation errors are a constant in Figure 7g–i. In addition, for cases where *G* is less than 1, λ_1^m will be smaller than λ_1 . As will be seen in the following, *G* will also lead to smaller measurement results of insect mass and body length.



Figure 7. The influence of polarization measurement errors on the calculation of λ_1^m . (**a**–**c**): the first system in Table 1 is used; (**d**–**f**): the third system in Table 1 is used; (**g**–**i**): the ninth system in Table 1 is used; (**j**–**i**): the tenth system in Table 1 is used.

The a_1 , a_2 and G are not 1, and C_1 and C_2 are not 0 in the tenth system. Thus, in Figure 7j–l, the estimation error of λ_1^m varies approximately in the form of the sum of a regular trigonometric function and a constant error with respect to insect orientation.

The influence of polarization measurement errors on λ_1^m is similar to that on λ_1^m and is not described in detail in this paper.

4.3. Simulation on Individual Measurement Error and Insect Parameter Distribution Distortion Equation (45) could also be expressed as

$$\log(|\lambda_1^m|) = \log(|\lambda_1|) + \log(|\lambda_1^{error}|)$$
(46)

where log is an abbreviation of log10. For the case where v could be calculated from λ_1 , the measured v could be expressed as

$$p^m = |\lambda_1^m|^2 \tag{47}$$

According to Equation (33), the measured mass of an insect could be expressed as

$$Mass^{m} = x_{10} \log^{2}(v^{m}) + x_{11} \log(v^{m}) + x_{12}$$

= Mass + Mass^{error} (48)

where *Mass*^{error} is the mass estimation error of an insect:

$$Mass^{error} = 4x_{10}\log^2(|\lambda_1^{error}|) + 8x_{10}\log(|\lambda_1|)\log(|\lambda_1^{error}|) + 2x_{11}\log(|\lambda_1^{error}|)$$
(49)

Equation (49) presents the relationship between the insect mass estimation error and the λ_1^m calculation error. In subsequent simulations, it can be seen that the influence of polarization measurement errors on λ_1^m calculation is similar to that on insect mass estimation.

Simulations are conducted on *Helicoverpa armigera*, *Mythimna separata* and *Agrotis ipsilon*, and the SMs in the Ku band are chosen. The curve of the insect mass estimation error with insect orientation is illustrated in Figure 8. It could be seen from Figure 8a that the estimation error of insect mass varies approximately in the form of the sum of a $cos(2\theta)$ function and a constant error with respect to insect orientation. And in Figure 8b, the estimation error of insect mass varies approximately in the form of $sin(2\theta)$. In Figure 8c, the measured mass is smaller than the actual mass, and the difference between the measured mass varies approximately in the estimation error of insect mass varies and the true mass is a constant. Figure 8d illustrates that the estimation error of insect mass varies approximately for a regular trigonometric function and a constant error with respect to insect orientation, for the case where the influences of all polarization measurement errors are present.



Figure 8. The influence of polarization measurement errors on the calculation of insect mass. (a): the first system in Table 1 is used; (b) the third system in Table 1 is used; (c): the ninth system in Table 1 is used; (d): the tenth system in Table 1 is used.

In order to analyze the influence of polarization measurement errors on the mass distribution of insects, the mass of each insect in Figure 8 is also recorded, and the distribution of insects is presented in Figure 9. The real mass of insects is marked with a red line. It can be seen from Figure 9a–f that due to the varying influence of a_1 , a_2 , C_1 and C_2 on



Figure 9. The influence of polarization measurement errors on the distribution of insect mass. (**a**–**c**): the first system in Table 1 is used; (**d**–**f**): the third system in Table 1 is used; (**g**–**i**): the ninth system in Table 1 is used; (**j**–**l**): the tenth system in Table 1 is used.

It is worth noting that in this paper, only the situation where the insect species are single and the orientation distribution is uniform is analyzed. In actual situations, the calculated insect mass distribution will be more complex.

Because the forms of calculating insect mass and body length are similar, the influence of polarization measurement errors on the mass are similar to that on the body length of insects and is not described in detail in this paper.

4.4. Analysis of Radar Measurement Data

The Ku and X band entomological radars introduced in Section 3 are used to measure insect mass, and data from the same time period are recorded. The SM of the measured targets has also not been calibrated, and the mass distributions of all targets are presented in Figure 10. Due to the fact that Ku band radar can only measure the mass of insects below 200 mg, Figure 10a only presents the distribution of insect mass below 200 mg. During the mass calculation process, the influence of *r* is compensated, but due to the lack of angle information of the target relative to the radar, the influence of *g* could not be compensated.





It can be seen from Figure 10 that the number of insects decreases with mass increases. In fact, for all statistical distribution results without compensating *g*, the number of larger insects (insect with mass larger than 100 mg) is always relatively small, which is seriously inconsistent with reality. According to the analysis above, only *g* could cause the measured mass of a large number of insects to be smaller. The flight trajectory of most measured insects does not pass through the center of the radar beam, which causes the measured mass of insects to be smaller than the real mass. Thus, the mass estimation error mainly depends on the flight trajectory and antenna pattern.

5. The Influence of Polarization Measurement Errors on the Characteristics of the Measured Scattering Matrix

The insect SMs measured by entomological radar often highly satisfy reciprocity and symmetry [17]. In this section, the polarization measurement errors are decomposed into the part that affects the reciprocity of the measured SM of the target and the part that affects the bilateral symmetry of the measured SM of the target. And the disruption of the reciprocity and symmetry of the insect's measured SM caused by polarization measurement errors is demonstrated through a simple method. Then, through simulation and data from two fully polarized radars, the influence of polarization measurement errors on the reciprocity and bilateral symmetry of the target's measured SM is analyzed.

5.1. The Influence of Polarization Measurement Errors on Reciprocity

The a_2 in Equation (12) could be decomposed into a_1 and a_c .

$$a_2 = a_1 a_c \tag{50}$$

And Equation (12) could be expressed as

$$\mathbf{S}^{m} = G \begin{bmatrix} 1 & 0 \\ 0 & a_{1} \end{bmatrix} \begin{bmatrix} 1 & C_{1} \\ C_{2} & 1 \end{bmatrix} \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix} \begin{bmatrix} 1 & C_{2} \\ C_{1} & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & a_{1} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & a_{c} \end{bmatrix}$$
(51)

Assuming $a_1 = 1$, $C_1 = 0$ and $C_2 = 0$, Equation (51) could be expressed as

S

$$\mathbf{S}^{m} = \begin{bmatrix} s_{hh}^{m} & s_{hv}^{m} \\ s_{vh}^{m} & s_{vv}^{m} \end{bmatrix} = G \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & a_{c} \end{bmatrix}$$
(52)

where

$$s_{hv}^m = a_c G s_{hv} \tag{53}$$

$$_{vh}^{m} = Gs_{vh} \tag{54}$$

According to [22,23], for the target that satisfy reciprocity, the off-diagonal elements of the SM are the same:

$$s_{hv} = s_{vh} \tag{55}$$

However, according to Equations (53) and (54), it can be seen that a_c could affect the reciprocity of the measured target SM. When the off-diagonal elements of **S** are 0 or a_c is 1, the **S**^{*m*} could satisfy reciprocity. While in other cases, **S**^{*m*} will no longer satisfy reciprocity. The operator **P** — could be used to calculate the degree of target reciprocity [16,22]:

The operator \mathbf{P}_{rec} could be used to calculate the degree of target reciprocity [16,22]:

$$\theta_{rec}(\mathbf{S}) = \arccos(\frac{\left\|\mathbf{P}_{rec} \,\vec{\mathbf{S}}\right\|}{\left\|\vec{\mathbf{S}}\right\|}), 0 \le \theta_{rec} \le \frac{\pi}{2}$$
(56)

where **S** is the target SM in the form of a 4 × 1 vector, and $\|\cdot\|$ represents the 2-norm of the vector. The θ_{rec} of the target ranges from 0 to $\pi/2$, and the smaller the value, the higher the degree of reciprocity of the target. In the absence of polarization measurement errors, the degree of insect reciprocity does not vary with orientation.

In the case of $a_c = 0.708e^{j\pi/4}$, $a_1 = 1$ and $C_1 = C_2 = 0$, the degree of reciprocity of *Helicoverpa armigera*, *Mythimna separata*, and *Agrotis ipsilon* varying with orientation is illustrated in Figure 11a. It can be seen that the θ_{rec} of target reciprocity varies with the orientation of the insect, and it is lowest at approximately 0, 90°, 180° and 270°, which means that the degree of reciprocity is the highest at these angles. This is because at these angles, the insect SM off-diagonal elements are close to 0, so the degree of target reciprocity is less affected by a_c .



Figure 11. The influence of polarization measurement errors to the characteristics of the measured SM. (a) Influence of a_c to reciprocity. (b) Influence of a_1 to bilateral symmetry. (c) Influence of C to bilateral symmetry.

5.2. The Influence of Polarization Measurement Errors on Bilateral Symmetry

According to [18], for the targets that satisfy bilateral symmetry, the $\hat{\theta}_0$ is real:

$$\hat{\theta}_0 = \frac{1}{2}\arctan(\frac{s_{hv} + s_{vh}}{s_{hh} - s_{vv}}) \qquad \hat{\theta}_0 \in \left(-\frac{\pi}{4}, \frac{\pi}{4}\right) \tag{57}$$

However, in the case of $a_c \neq 1$, $C_1 \neq 0$ or $C_2 \neq 0$, $\hat{\theta}_0$ might not be real. Assuming $a_c = 1$, $C_1 = 0$ and $C_2 = 0$, Equation (51) could be expressed as

$$\mathbf{S}^{m} = \begin{bmatrix} s_{hh}^{m} & s_{hv}^{m} \\ s_{vh}^{m} & s_{vv}^{m} \end{bmatrix} = G \begin{bmatrix} 1 & 0 \\ 0 & a_{1} \end{bmatrix} \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & a_{1} \end{bmatrix}$$
(58)

And under the influence of a_1 , by substituting the matrix elements in Equation (58) into Equation (57), $\hat{\theta}_0$ could be expressed as

$$\hat{\theta}_0^{m1} = \frac{1}{2} \arctan(\frac{s_{hv} + s_{vh}}{s_{hh}/a_1 - a_1 s_{vv}})$$
(59)

According to Equations (57) and (59), it can be seen that when the off-diagonal elements of **S** are 0 or a_1 is ± 1 , $\hat{\theta}_0^{m1}$ is real. While in other cases, $\hat{\theta}_0^{m1}$ will not remain real, and **S**^m will no longer satisfy bilateral symmetry.

The operator **D** could be used to calculated the degree of target bilateral symmetry [16,22]:

$$\theta_{sym}(\mathbf{S}) = \arccos\left(\left|\frac{(\mathbf{P}_{rec} \mathbf{\vec{S}}, \mathbf{D} \mathbf{P}_{rec} \mathbf{\vec{S}})}{||\mathbf{P}_{rec} \mathbf{\vec{S}}|| \cdot ||\mathbf{D} \mathbf{P}_{rec} \mathbf{\vec{S}}||}\right|\right), 0 \le \theta_{sym} \le \frac{\pi}{2}$$
(60)

where (\vec{a}, \vec{b}) represents the inner product of \vec{a} and \vec{b} . Similar to \mathbf{P}_{rec} , the θ_{sym} of the target ranges from 0 to $\pi/2$, and the smaller the value, the higher the degree of bilateral symmetry of the target. In the absence of polarization measurement errors, the degree of insect bilateral symmetry does not vary with orientation.

In the case of $a_c = 1$, $a_1 = 0.708e^{j\pi/4}$ and $C_1 = C_2 = 0$, the degree of bilateral symmetry of insects varying with orientation is illustrated in Figure 11b. It can be seen that the degree of target bilateral symmetry varies with the orientation of the insect, and it is highest at approximately 0, 90°, 180° and 270°. As introduced earlier, the insect SM off-diagonal elements are close to 0 at these angles, and the degree of target bilateral symmetry is not affected by a_1 when the off-diagonal elements of **S** are 0.

Assuming $a_1 = 1$ and $a_c = 1$ Equation (51) could be expressed as

$$\mathbf{S}^{m} = \begin{bmatrix} s_{hh}^{m} & s_{hv}^{m} \\ s_{vh}^{m} & s_{vv}^{m} \end{bmatrix} = G \begin{bmatrix} 1 & C_{1} \\ C_{2} & 1 \end{bmatrix} \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix} \begin{bmatrix} 1 & C_{2} \\ C_{1} & 1 \end{bmatrix}$$
(61)

And under the influence of C_1 and C_2 , by substituting the matrix elements in Equation (61) into Equation (57), $\hat{\theta}_0$ could be expressed as

$$\hat{\theta}_0^{m2} = \frac{1}{2} \arctan\left\{ \frac{2[C_2 s_{hh} + (C_1 C_2 + 1) s_{hv} + C_1 s_{vv}]}{(1 - C_2^2) s_{hh} + 2(C_1 - C_2) s_{hv} + (C_1^2 - 1) s_{vv}} \right\}$$
(62)

According to Equation (62) and Equation (57), for cases other than $C_1 = C_2 = 0$, $\hat{\theta}_0^{m^2}$ will not remain real, and S^m will no longer satisfy bilateral symmetry.

In the case of $a_c = 1$, $a_1 = 1$ and $C_1 = C_2 = 0.1e^{j\pi/4}$, the degree of bilateral symmetry of insects varying with orientation is illustrated in Figure 11c. The degree of target bilateral symmetry varies with the orientation of the insect, indicating that C_1 and C_2 could also influence the degree of symmetry of the insect's measured SM.

5.3. Analysis of Radar Measurement Data

The data measured by the Ku and X band entomological radars introduced in Section 3 are analyzed. The SM of targets has also not been calibrated, and the degree of reciprocity and bilateral symmetry of all targets are presented in Figures 12 and 13. The mean, maximum, median and variance of the degree of reciprocity and the degree of bilateral symmetry measured by these two radars are presented in Table 1.



Figure 12. The distribution of degree of reciprocity obtained from Ku band and X band radar. (a) insects measured by Ku band radar. (b) insects measured by X band radar.



Figure 13. The distribution of degree of bilateral symmetry obtained from Ku band and X band radar. (a) insects measured by Ku band radar. (b) insects measured by X band radar.

According to the introduction of the reciprocity and symmetry of insect targets in the dataset in [20], the degree of reciprocity and symmetry of insect targets is high. Table 3 also presents the mean, maximum, median and variance of the degree of reciprocity and bilateral symmetry measured in the Microwave Anechoic Chamber. It can be seen that in the Ku and X bands, the degree of reciprocity and bilateral symmetry measured by radar is much lower than that measured in a Microwave Anechoic Chamber.

Table 3. Comparison of scattering characteristics between insect SM dataset measured by MicrowaveAnechoic Chamber and target SMs measured by radars.

Degree of Reci- procity	Ku Band Dataset	Ku Band Radar	X Band Dataset	X Band Radar	Degree of Bilateral Symme- try	Ku Band Dataset	Ku Band Radar	X Band Dataset	X Band Radar
Mean	0.0470	0.1795	0.0442	0.2509	Mean	0.0133	0.1794	0.0280	0.1369
Maximum	0.1681	0.9310	0.2508	0.8929	Maximum	0.0384	0.7108	0.1210	0.6026
Median	0.0417	0.1689	0.0295	0.2238	Median	0.0112	0.1581	0.0224	0.1154
Variance	0.0434	0.6657	0.1012	1.3078	Variance	0.0049	0.9610	0.0309	0.6550

6. Discussion

Polarization measurement errors, including G, a_1 , a_2 , C_1 and C_2 , could lead to measurement errors in insect orientation, mass and body length, as well as disrupt the reciprocity and bilateral symmetry of the measured SM of insects. This paper first models the measurement process of the target SM, and then analyzes the influence of polarization measurement errors on the calculation of insect orientation, mass, body length and scattering charac-

teristics of insects through theoretical derivation, simulation and measured data from entomological radars.

 a_1 , a_2 , C_1 and C_2 lead to error terms in the measurement of insect orientation that vary in trigonometric form with insect orientation. C_1 and C_2 could also bring additional constant error terms. The method for calculating the insect orientation estimation error through polarization measurement errors is given in Equation (29). When calculating the orientation distribution of a large number of insects, a_1 and a_2 will lead the calculated insect orientation to cluster towards the H or V polarization direction, and C_1 and C_2 will lead the calculated insect orientation to deviate from the H or V polarization direction. The measured data from two fully polarized entomological radars indicate that most measured insect orientation cluster in the H or V polarization direction. Thus, a_1 and a_2 are the main factors affecting the measured insect orientation distribution in the actual system.

 a_1 , a_2 , C_1 and C_2 lead to error terms in the measurement of insect mass and body length that vary in trigonometric form with insect orientation. *G*, a_1 and a_2 could bring additional constant error terms. The method for calculating the insect mass estimation error through polarization measurement errors is given in Equations (42) and (49), and the estimation error calculation method of body length are similar. When calculating the mass distribution of a large number of insects, a_1 , a_2 , C_1 and C_2 will mainly lead the mass and body length distribution of insects to diverge, and *G* will always lead to a smaller measured mass and measured body length of all the insects. The measured data from two fully polarized entomological radars indicate that *G* or the modulation of the antenna pattern are the main factors affecting the measured insect mass and body length distribution in the actual system. Thus, in the distribution of measured insect mass, the number of small-mass insects is always abnormally high, and the number of large-mass insects is abnormally low.

 a_c , which is the ratio of a_2 and a_1 , could disrupt the reciprocity of the measured SM, and a_1 , C_1 and C_2 could disrupt the bilateral symmetry of the measured SM. The comparison between insect data measured by Microwave Anechoic Chamber and entomological radar indicates that the reciprocity and bilateral symmetry of insect targets are significantly reduced due to the influence of polarization measurement errors.

Usually, using a large amount of simulation to calculate the influence of polarization measurement errors on insect parameter measurement consumes a lot of time. The calculation methods for orientation estimation error, mass estimation error and body length estimation error could be quickly used to calculate estimation errors and guide the design of the system.

In addition, there are two methods to solve the polarization measurement errors of the system and improve the accuracy of insect parameter measurement. Antenna pattern modulation is the main reason for the smaller measurement results of insect mass and body length, and by designing estimators that are not affected by echo intensity, insect mass and body length can be estimated to avoid the influence of antenna pattern modulation. Although the two eigenvalues of the measured SM S_{θ}^m , λ_1^m and λ_2^m are both affected by *G* in the same way, the ratio of λ_1^m and λ_2^m is not affected by *G*. Thus, the amplitude and phase of this ratio have great potential as estimators for calculating insect mass and body length without being affected by *G*.

Another method is to measure the polarization measurement errors of the system and compensate for the measured SM to obtain the accurate target SM, which is also known as polarization calibration. The traditional polarization calibration method calculates polarization measurement errors by measuring multiple known SM targets. However, entomological radars are often deployed in the wild for a long time, making it difficult to measure targets with known SM. According to the analysis in Section 5, a_c could affect the reciprocity of the measured target SM, while a_1 , C_1 and C_2 could affect the bilateral symmetry of the measured target. It is possible to first collect a certain number of insect SMs, and then use \hat{a}_1 , \hat{a}_c , \hat{C}_1 and \hat{C}_2 to compensate the influence of a_1 , a_c , C_1 and C_2 to these measured SMs. The set of \hat{a}_1 , \hat{a}_c , \hat{C}_1 and \hat{C}_2 that maximizes the degree of reciprocity and degree of symmetry of these SMs is the accurate estimate of a_1 , a_c , C_1 and C_2 . The influence

of a_1 , a_c , C_1 and C_2 on target SMs could be obtained by compensating the measured SM with the estimates of a_1 , a_c , C_1 and C_2 .

7. Conclusions

In this paper, the influence of polarization measurement errors on the estimation of insect orientation, mass and body length and the calculation of reciprocity degree and bilateral symmetry degree are introduced. Polarization measurement errors can cause estimation errors in insect orientation, mass and body length to fluctuate with insect orientation, ultimately leading to the measured insect orientation clustering in certain directions, the estimates of mass and body length decreasing and the distribution of the measured insect mass and body length diverging. Polarization measurement errors could also reduce the degree of reciprocity and symmetry of the target measured SM.

In addition, the calculation methods for the orientation, mass and body length estimation errors of known SMs of insects are given. Methods used to solve polarization measurement errors are briefly introduced. In the future, these methods will be studied to thoroughly address the influence of polarization measurement errors.

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