

Review

## Micromachined Thermal Flow Sensors—A Review

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**Abstract:** Microfabrication has greatly matured and proliferated in use amongst many disciplines. There has been great interest in micromachined flow sensors due to the benefits of miniaturization: low cost, small device footprint, low power consumption, greater sensitivity, integration with on-chip circuitry, *etc.* This paper reviews the theory of thermal flow sensing and the different configurations and operation modes available. Material properties relevant to micromachined thermal flow sensing and selection criteria are also presented. Finally, recent applications of micromachined thermal flow sensors are presented. Detailed tables of the reviewed devices are included.

**Keywords:** MEMS; thermal flow sensors; TCR; anemometry; thermoresistive; thermoelectric; thermoelectronic; frequency analog; gas flow; fluid flow

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### 1. Introduction

Micromachined flow sensors have great utility in a number of diverse applications requiring monitoring of gas [1] or fluid flow including flow cytometry [2], cleanroom environmental monitoring [3], wind [4], gas chromatography [5], wall shear stress [6], and viscosity measurements [7]. These sensors complement technologies such as microfluidic channels, valves, pumps, and heaters that are assembled together to create so-called lab on a chip (LOC) devices or micro total analysis systems ( $\mu$ TAS). As such, there has been great interest in their development in the microelectromechanical systems (MEMS) community since the first micromachined thermal flow sensor in 1974 [8–10].

Micromachined flow sensors can be classified as either thermal or non-thermal. Here, we focus on thermal flow sensors, which have been investigated extensively for their simple structure and implementation; a review of recent work is presented. Micromachining technology is amenable to creating microheaters and thermal sensors with no moving parts required, thus simplifying fabrication and operational design requirements. Another reason for the large interest in thermal flow sensors is the advantages gained through miniaturization: low power consumption, higher sensitivity to low flow rates, and ease of use with different modes of operation. In addition, thermal flow sensors can also detect thermal properties of fluids such thermal conductivity and thermal diffusivity when configured properly [11].

## 2. Theory

Thermal flow sensors rely on the ability of fluid flows to affect thermal phenomenon by way of heat transfer that, in turn, is transduced into a varying electrical signal capturing the sensor response to flow change. Ideally, sensors are thermally isolated so only heat transfer due to flow can occur. Other heat transfer pathways such as through substrate or electrical leads result in thermal losses that degrade sensor performance and should be minimized in the device design. Proper thermal flow sensor response is dependent upon a constant fluid temperature; temperature compensation must be implemented if fluid temperature will drift.

### 2.1. Thermal Flow Sensing Configurations

There are three forms of thermal flow sensing: hot-wire and hot-film, calorimetric, and time-of-flight [9].

#### 2.1.1. Hot-Wire and Hot-Film

Hot-wire and hot-film sensors operate by heat transfer from a heated element to a surrounding cooler fluid (Figure 1). The term hot-wire implies the use of a resistive wire sensor element within the fluid flow whereas hot-film implies the use of a thin film resistive sensor that acts as the element placed adjacent to the flow. Regardless of their differences in form, both hot-wire and hot-film sensors share the same physical sensing principle. The sensing element is heated and subjected to fluid flow. As fluid flow past the element increases, convective heat loss increases from the heated element. The relationship between increasing fluid flow and forced convective cooling of the element can be determined and used as a baseline calibration for sensing applications. Appropriately selected sensor materials will experience a change in electrical resistance based upon change in temperature; thus heat transfer rate can be transduced into an electrical signal that changes with respect to fluid flow.

King's Law describes heat transfer from a cylinder of infinite length in terms of the resulting voltage difference and is useful for hot-wire anemometry characterization [12]. The constants are a complex combination of fluid thermal conductivity properties and flow geometry and should be found empirically.

$$\Delta V(v) = a + bv^n \quad (1)$$

where:  $\Delta V$  = flow induced voltage difference;  
 $v$  = velocity;  
 $a, b, n$  = constants.

For typical thermal flow sensor materials (Table 1), the resistance relationship to temperature is given by:

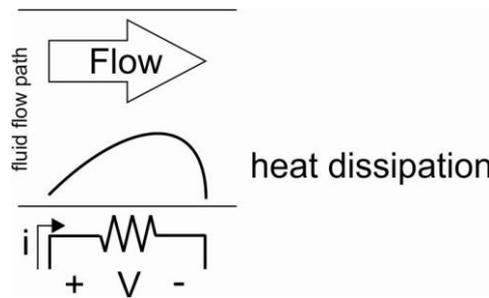
$$R(T) = R(T_0)[1 + \alpha(T - T_0)] \tag{2}$$

where  $R(T)$  is the resistance at temperature  $T$  and  $\alpha$  is the temperature coefficient of resistivity (TCR). TCR can be determined experimentally by:

$$a_R = \frac{R(T) - R(T_0)}{R(T_0)} = \alpha(T - T_0) \text{ or } \frac{\Delta R}{R} = \alpha \Delta T \tag{3}$$

in which  $a_R$  is the resistance overheat ratio and determined by measuring the change in resistance of the sensing material at two different temperatures.

**Figure 1.** Illustration showing concept of hot wire anemometry. The resistor serves as a heater and sensing element. Resistance value is dependent on temperature.



**Table 1.** Relevant electrical and thermal properties of thermal flow sensor materials [11].

Material	Resistivity, $\rho$ ( $\Omega \cdot m$ ) at 20 °C	TCR, $\alpha$ ( $10^{-4}/K$ )
Aluminum	$2.69 \times 10^{-8}$	42.0
Copper	$1.67 \times 10^{-8}$	43.0
Gold	$2.30 \times 10^{-8}$	39.0
Iron	$9.71 \times 10^{-8}$	65.1
Nickel	$6.84 \times 10^{-8}$	68.1
Palladium	$10.8 \times 10^{-8}$	37.7
Platinum	$10.6 \times 10^{-8}$	39.2
Silver	$1.63 \times 10^{-8}$	41.0
Tungsten	$5.50 \times 10^{-8}$	46.0
Polysilicon	$4 \times 10^{-6}$ [13]– $1 \times 10^1$ [14–16]	–250–10 [14,15]

The electrical and thermal properties of polysilicon are dopant dependent, which diffuse primarily across grain boundaries [13]. Conduction within a grain is similar to that of single crystal silicon with a positive TCR while conduction across grain boundaries exhibits negative TCR due to thermionic emission dominance [17]. Thus, the thermal and electrical properties of polysilicon can be tuned from a combination of grain size distribution, dopant concentration and type [13,15,17–19].

A high absolute TCR is desired for a thermal sensing material since sensitivity to temperature change is proportional to a material's TCR. However, consideration of resistivity is also required since it is the resistance change that is being detected; a higher nominal resistance will increase sensitivity. Ease of material microfabrication processing needs to be balanced with TCR and resistivity considerations as well. Finally, consideration of how the sensor will be packaged and used will affect material selection. Sensors exposed to fluids may experience corrosion and low power may be required for use with volatile gases.

Of the commonly used materials for thermal flow sensors, platinum is worth highlighting; while this material does not possess the highest TCR its proven biocompatible property has made it a popular choice for biomedical flow sensing applications. Platinum is corrosion resistant, operates in high temperature range, compatible with standard micromachining techniques and used in many implantable devices [20–25].

Hot-wire and hot-film sensors are first characterized by imposing a known fluid flow and measuring the resulting resistance or voltage change of the sensors. It is important to note that the fluids used to characterize these sensors should be the same fluids used in measurements since the thermal conductive properties of the fluid are integral to the transduction mechanism. Fluids with similar thermal conductive properties may be substituted as well.

Six operational modes are possible with hot-wire and hot-film sensors by controlling the either the heater power or temperature and observing the heater temperature, power, or temperature difference resulting from fluid flow [9]. Constant heater power mode involves imposing a constant current bias on the heating element and monitoring the change in resistance or voltage due to flow. Constant temperature mode requires feedback circuitry that monitors and holds constant the sensor temperature; the increase in power required to maintain temperature under higher flow rates is monitored. While more complex in implementation, constant temperature mode can deliver better sensor resolution and frequency response [11].

One method of utilizing hot-wire and hot-film sensors is with a Wheatstone bridge. A single resistor can serve as both heater and sensor by placing it in a quarter-bridge configuration, where it acts as one of four resistors in a Wheatstone bridge [26]. A current source provides a current thereby heating the resistor. The Wheatstone bridge output is constantly monitored with a multimeter and any imbalance due to flow induced sensor electrical resistance change is measured.

### 2.1.2. Calorimetric

Calorimetric sensing involves at least one thermal sensor upstream and downstream the heating element that detect the thermal profile around the heater due to fluid flow. Thermal flow asymmetry due to fluid flow direction can be detected and thus this method allows for velocity measurements as opposed to flow (Figure 2).

For example, a simple one-dimensional model of a calorimetric sensor on silicon substrate heater temperature is [27]:

$$T_h = \frac{P}{k_F w_h \left( \frac{l_h}{\delta} + \sqrt{4k + \frac{v\delta^2}{4a^2}} \right)} \quad (4)$$

where:  $T_h$  = heater temperature for constant heat power;  
 $P$  = heat power;  
 $k_F$  = thermal conductivity of fluid;  
 $w_h$  = heater width;  
 $l_h$  = heater length;  
 $\delta$  = boundary layer thickness;  
 $v$  = average flow velocity;  
 $a$  = thermal diffusivity of fluid;  
 $k = \frac{1}{2} + \frac{k_{Si}t_d}{k_F\delta}$  dimensionless factor;  
 $k_{Si}$  = thermal conductivity of silicon substrate;  
 $t_d$  = diaphragm thickness.

The temperature difference between temperature sensors is given by:

$$\Delta T = T_h [e^{\gamma_2 l_d} - e^{\gamma_1 l_u}] \tag{5}$$

where:  $\Delta T$  = temperature difference;

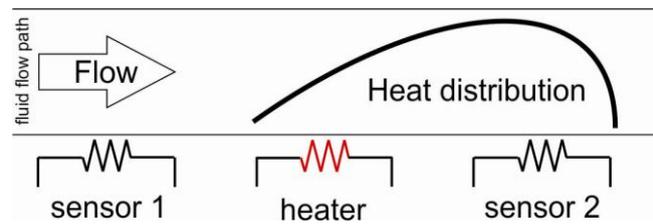
$$\gamma_{1,2} = \frac{v \pm \sqrt{v^2 + 16a^2K/\delta^2}}{4aK};$$

$l_u$  = distance to upstream sensor;

$l_d$  = distance to downstream sensor.

Characterization with the fluid to be measured is required since the unique thermal conductivity properties of the fluid are essential to correct transduction of velocity to electrical signal.

**Figure 2.** Illustration of calorimetric sensing concept.



### 2.1.3. Time-of-Flight

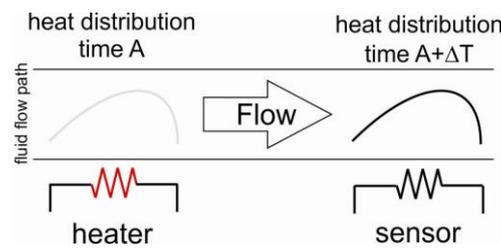
In time-of-flight sensing, the transit time of a thermal pulse is tracked to extract flow rate information. At least one heater and one downstream thermal sensor are required. A short thermal pulse is transferred from the heater to the surrounding fluid flow. Ideally, the heater is thermally isolated from the substrate to eliminate interference from thermal conduction effects. The downstream thermal flow sensor detects the thermal pulse (Figure 3).

The time between heat pulse generation and downstream detection is determined by several factors: the thermal conductivity and diffusivity of the fluid, heater-sensor distance ratio, and average flow velocity. Approximating the heater as a line source, the thermal distribution of the pulse as a function of distance and time can be described as [27]:

$$T(x, t) = \frac{q_0}{4\pi kt} e^{\left[-\frac{(x-vt)^2}{4at}\right]} \tag{6}$$

where  $T$  = temperature distribution at time  $t$ ;  
 $x$  = distance from heater;  
 $t$  = time;  
 $q_0$  = pulse signal input strength;  
 $k$  = thermal conductivity of fluid;  
 $v$  = average flow velocity;  
 $a$  = thermal diffusivity.

**Figure 3.** Illustration showing concept of time-of-flight sensing.



Flow velocity is calculated from the time and distance between heater and sensor,  $d_{hs}$ :

$$v = \frac{d_{hs}}{t} \tag{7}$$

Thermal diffusion in addition to forced convection is dominant in microflow and so needs to be taken into account. Thus, the time is given by:

$$\tau = \frac{-2a + \sqrt{4a^2 + v^2 d_{hs}^2}}{v^2} \text{ for } v \neq 0 \tag{8}$$

$$\tau = \frac{d_{hs}^2}{4a} \text{ for } v = 0 \tag{9}$$

As before, characterization with the fluid to be measured by imposing a known flow rate is required since fluid heat transfer properties determine relationship between detected signal and flow.

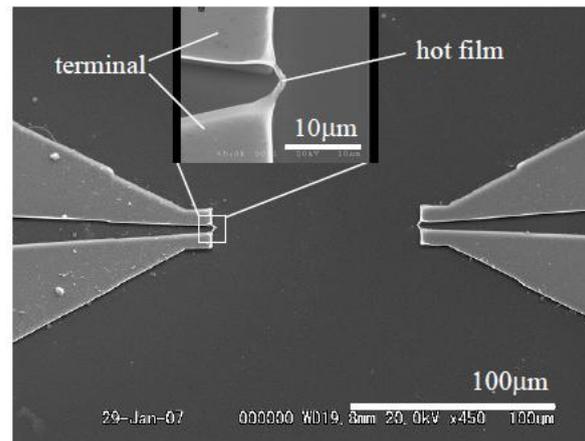
## 2.2. Thermal Flow Sensing Transduction Principles

Micromachined thermal flow sensors can be categorized into different types depending on their physical transduction method and materials [9]. Thermoresistive sensors utilize resistive elements for thermal sensing. Thermoelectric sensors detect thermal changes using thermopiles. In contrast, diode and transistor elements are used in thermoelectric sensing. Changes in resonant frequency within mechanical structures due to temperature change induced stress are utilized for frequency analog sensors.

### 2.2.1. Thermoresistive/Thermoanemometers

Thermoresistive or thermoanemometer sensors work by heat transfer away from a resistive element that is heated. As the resistor cools, the corresponding change in voltage or current can be calibrated to fluid flow. Resistors can also be used as thermal sensors without heating; the change in fluid temperature is also detected as a change in resistance, which alters the voltage or current flowing through it. These are by far the most popular types of micromachined flow sensors due to the ease of fabrication and operation (typical example in Figure 4).

**Figure 4.** Micromachined Pt resistor used for thermoresistive flow sensing [28].



2.2.2. Thermoelectric

Thermopiles, made up of several connected thermocouples, are used as the sensing element and operated in conjunction with a heater element for thermoelectric sensing. The fabrication of such sensors is more complicated since less conventional materials are utilized for fabrication of thermopiles but CMOS (complementary metal oxide semiconductor) compatible processing is possible (Table 2). The Seebeck effect of thermopiles enables higher sensitivity and unbiased output voltage with no offset or drift [29,30].

**Table 2.** Seebeck coefficients and thermal conductance of thermoelectric materials [31,32].

Material	Seebeck coefficient (µV/K) at 0 °C	Thermal conductance (W/K·m)
Aluminum	-1.7 <sup>1</sup>	237
Chromium	18.8	
Gold	1.79	318
Copper	1.70	
Platinum	-4.45	
Nickel	-18.0	90
Bismuth	-79 <sup>1</sup>	
Antimony	43 <sup>2</sup>	
p-type silicon	300–1,000 <sup>1</sup>	149
n-type silicon	-500–-200 <sup>1</sup>	

<sup>1</sup> At 27 °C. <sup>2</sup> Averaged over 0 to 100 °C.

The output voltage of a thermocouple is given by:

$$V_{ab} = \alpha_{ab} \Delta T_{hot-cold} = (\alpha_a - \alpha_b)(T_{hot} - T_{cold}) \tag{10}$$

- where:  $\alpha_a$  = Seebeck coefficient of material *a*;
- $\alpha_b$  = Seebeck coefficient of material *b*;
- $\alpha_{ab}$  = Seebeck coefficient of thermocouple;
- $T_{hot}$  = Hot junction temperature;
- $T_{cold}$  = Cold junction temperature;
- $\Delta T_{hot-cold}$  = Temperature difference between hot and cold junction.

Thermopiles are constructed with thermocouples in series and so the output voltage due to temperature change is summed and increased over that of a single thermocouple. However, thermal conduction between hot and cold junctions and Johnson noise increases with increasing number of thermocouples, thereby degrading sensor performance. For increased sensitivity, high thermal isolation is desired in order to maximize temperature difference between hot and cold junctions. Thus, optimization of thermocouple number per thermopile should be taken into consideration.

Semiconductor thermopiles are more sensitive than metal thermopiles because of their higher Seebeck coefficients that are tuned with dopant type and concentration. Thermopiles can be any combination of materials and a figure of merit [31,33] for material combination optimization can be used to predict thermopile performance. Thermopiles fabricated from polysilicon and metals are commonly used in thermoelectric flow sensing.

### 2.2.3. Thermoelectronic

Transistors and diodes are used as thermal sensing elements in thermoelectronic sensors. The I–V relationship for a p-n junction is [34]:

$$I = I_r(e^{V/nV_T} - 1) \quad (11)$$

where:  $I$  = Current;

$I_r$  = Reverse saturation current;

$V$  = Voltage;

$n$  = Ideality factor; 2 for Si and 1 for Ge;

$V_T$  = Volt equivalent of temperature.

In the case where  $I$  is constant across the junction:

$$\frac{dV}{dT} = \frac{V - (V_g + mnV_T)}{T} \quad (12)$$

where:  $m = 1.5$  for Si and 2 for Ge;

$V_g$  = Forbidden-gap energy.

Empirically, it has been found that at room temperature (300 K) for both Si and Ge:

$$\frac{dV}{dT} \approx -2.5 \text{ mV/K}$$

for maintaining a constant current across the p-n junction. In practice, King's Law [35] can be used to characterize the effect of flow on diode or transistor signal output.

Thermoelectronic sensors are compatible with CMOS fabrication. Thus, integrated circuits for signal processing and amplification can be included on the same device without separate packaging.

### 2.2.4. Frequency Analog

Thermal sensing is realized by the use of mechanical structures such as cantilevers or surface acoustic wave (SAW) oscillators in frequency analog sensors. The resonant frequency of the structure changes in response to temperature change due to mechanical stress, described by the equations below [36].

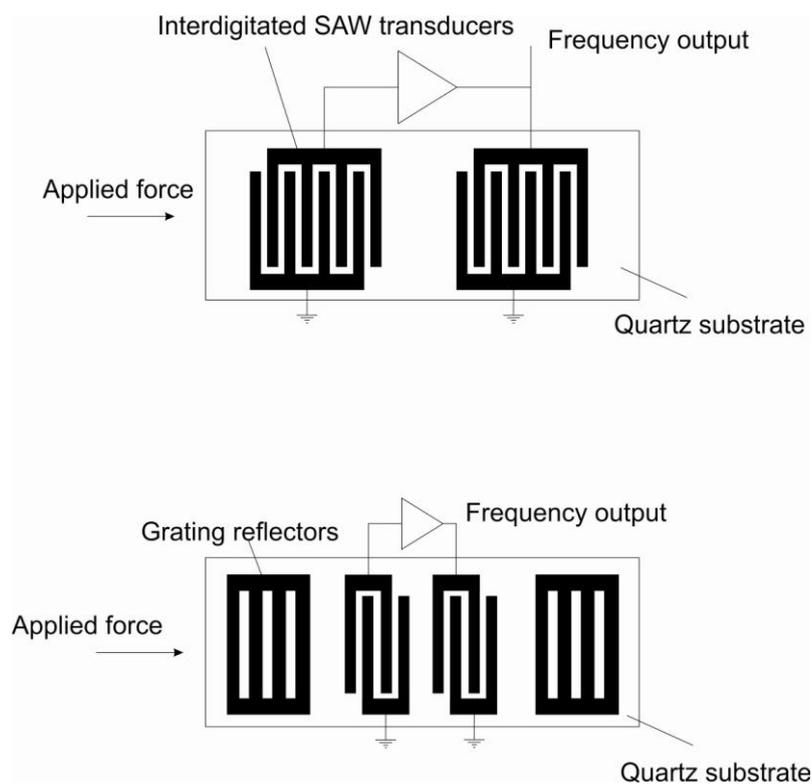
$$\frac{\Delta f}{f_0} = \alpha \Delta T_s \tag{13}$$

where:  $\alpha$  = temperature coefficient of frequency (TCF) of a SAW device

$T_s$  = change in temperature due to an incremental change in flow rate.

The resonant frequency is monitored and used to transduce flow rate in configurations analogous to calorimetric [37], time-of-flight [37], and hot-film [36,38] thermal flow sensors (Figure 5). Fabrication processes for resonant mechanical structures is well established, utilizing standard photolithographic techniques. While thermoresistive devices rely on constant power draw to induce heating, capacitive sensing options [39] for SAW based sensing result in comparatively reduced power draw.

**Figure 5.** Frequency analog device, analogous modes of operation [37].



However, fabrication of SAW transducers requires less common piezoelectric materials, thus limiting integration with CMOS devices and placing potential constraints on the intended operating environment.

### 3. Recent Applications of Micro-Thermal Flow Sensors

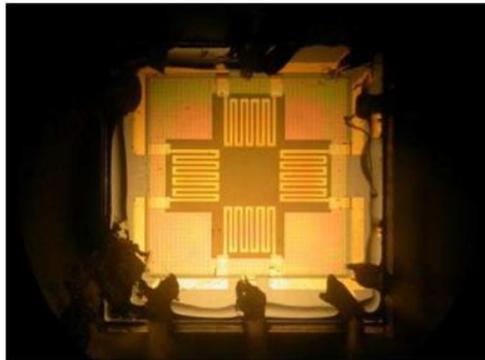
#### 3.1. Thermoresistive

Nickel resistors have been used for flow sensing due to their high TCR (Figure 6) [40,41]. Kaanta *et al.* used Cr/Ni resistors over a suspended silicon nitride membrane to create an array of flow sensors for micro-gas chromatography systems [5]. Sensing flow at multiple points through an array of sensors allows for tracking of an analyte plug as it passes through the system [42].

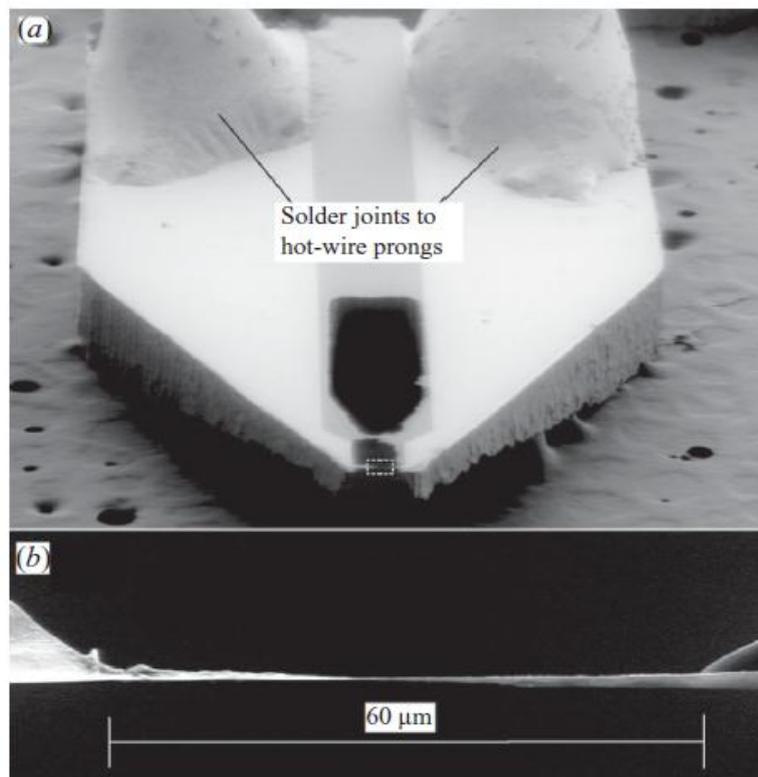
Polysilicon has been investigated as a thermal flow sensor material [43]. Soundararajan *et al.* used phosphorous doped polysilicon resistors as heaters in hot-wire mode on a silicon nitride diaphragm.

Constant temperature mode was utilized and sensor characterization took place within a PDMS microchannel [44]. Wu *et al.* used boron-doped polysilicon as heaters embedded into silicon nitride walls of a microchannel. Low flow rates of 10 nL/min were detected due to increased TCR of polysilicon due to boron doping [45].

**Figure 6.** Nickel resistors arranged in bridge formation for air flow sensing on  $\text{Si}_3\text{N}_4$  membrane for thermal isolation [41].



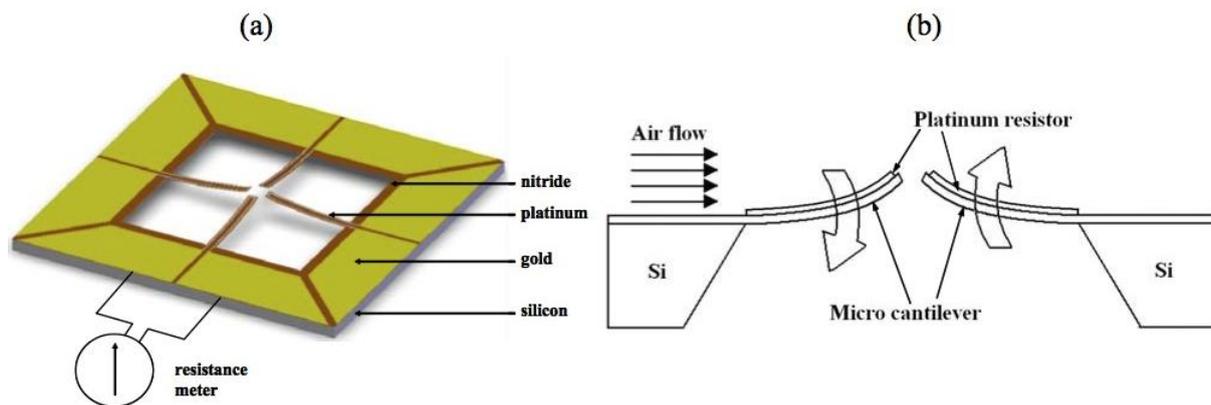
**Figure 7.** Pt nanoscale suspended wire for hot-wire thermal flow sensing [46].



Platinum (Pt) resistors have been extensively used in thermal flow sensing (Table 3). Bailey *et al.* fabricated a nanoscale Pt hot-wire that measured  $100 \text{ nm} \times 2 \text{ μm} \times 60 \text{ μm}$  (Figure 7). The small dimensions led to better spatial and frequency responses compared to traditional anemometers [46]. Ito *et al.* added carbon nanotubes to Pt resistors to enhance heat transfer due to flow, thereby increasing sensor sensitivity [28]. Meng *et al.* used an array of Pt resistors and were able to compare hot-film, calorimetric, and time-of-flight sensor response on the same device. Multiple modes of operation

extended the range of the device with constant temperature mode giving a better response over constant current [47]. Later, arrays of Pt resistors were used for neurotransmitter delivery [26,48]. Berthet *et al.* utilized time-of-flight through Pt sensors suspended in between microchannels created by the bonding of two etched Pyrex wafers [49]. Pt sensors were placed over suspended silicon nitride membranes for increased thermal isolation [50–52]. Even better thermal isolation can be obtained by creating a vacuum sealed cavity underneath the membrane while temperature is sensed above as used by Liu *et al.* and Hsiai *et al.* [53,54]. SU-8 can also be used for thermal isolation of Pt resistors due to its low thermal conductivity of 0.2 W/mK [55,56].

**Figure 8.** Diagram of flow device with integrated thermoresistors for thermal flow sensing and cantilevers for dual mode flow sensing; flow speed is thermally sensed and flow direction is physically sensed by cantilever deflection [57].



Wind sensors have been created with thermoresistive technology [58]. Dom ínguez *et al.* created a wind sensor for use in Martian atmosphere on a space probe. Pyrex structures were used to maximize thermal isolation to increase sensor sensitivity since Martian pressure is very low (6 mbar) which impedes heat convection compared to normal atmosphere [59]. 3-dimensional MEMS structures have been used for wind sensing [60]. Ma *et al.* implemented a temperature compensation scheme through a RTD to compensate for temperature variations in air as it flowed over their device. Interestingly, piezoresistors on cantilevers were integrated into the device for flow sensing through physical transduction as well (Figure 8) [57].

Polymer substrates have been used to create flexible sensors that can be placed on curved surfaces [61–63]. Ahrens *et al.* created sensors for sensing possible leakage in piston systems using a polymer substrate. Flow pulsations of 1,200 Hz were detected and sensors could withstand high pressures of up to 100 bar [64,65]. Li *et al.* fabricated flow and glucose sensors on Kapton tape which were then rolled and fitted into catheters for eventual use in measuring blood flow. Different concentrations of glucose dissolved into PBS were used for characterization to mimic *in vivo* changes in blood viscosity and sensor performance was found to differ by less than 1.07% at the tested flow rate range, with compensation for drift [66–68]. Yu *et al.* created a flexible sensor on Parylene C polymer substrate for use in measuring rabbit arterial blood flow. The sensor was packaged to an electrically conductive catheter and inserted into the arterial walls of live rabbits where dynamic pulsatile blood flow was measured. Rabbit blood was used for benchtop characterization of the sensor through a PDMS flow channel before *in vivo* implantation [69–75].

**Table 3.** Thermoresistive flow sensor feature comparison.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Ni Si <sub>3</sub> N <sub>4</sub>	Calorimetric	N <sub>2</sub> gas		40 mV/SLM	0–20sccm up to 8 SLM		N. Sabat é[40]
Ni Si <sub>3</sub> N <sub>4</sub>	Hot-film Calorimetric	Air	<1%		0–20 m/s	50 mW	Adamec [41]
Pt CNT for enhanced heat transfer	Hot-wire	N <sub>2</sub> gas			0–3 m/s		Ito [28]
Ti/Pt Parylene	Hot-film	DI H <sub>2</sub> O	250 nL/min		0–1 µL/min		Kuo [26]
W/Ti/Pt Parylene	Hot-film Calorimetric Time-of-flight	DI H <sub>2</sub> O	0.5 µL/min	25.1–3.92 × 10 <sup>4</sup> µV/(µL/min)	0–400 µL/min	3.3–23.5 mW	Meng [47]
Si Si <sub>3</sub> N <sub>4</sub>	Calorimetric	Water N <sub>2</sub> gas			0–10 mL/min	600 mW	Nguyen [43]
Pt Pyrex	Time-of-flight	Hexadecane IPA			10–10,000 µL/min	3.3 W	Berthet [49]
Polysilicon Si <sub>3</sub> N <sub>4</sub>	Hot-film	Air			0–30 m/s		Liu [54]
Pt Si <sub>3</sub> N <sub>4</sub>	Calorimetric	Air	Heater power dependent	Heater power dependent	0–4 m/s	2–20 mW	Fürjes [50]
Pt Pyrex	Hot-film	CO <sub>2</sub> gas	0.3 m/s		0–20 m/s	14 mW	Domnguez [59]
Au Polyimide	Hot-film	N <sub>2</sub> gas Water	10 mL/min 10 µL/min		0–200 mL/min 3–167 µL/min		Ahrens [64]
Au Polyimide	Hot-film	Oil			0–90 L/min		Ahrens [65]
Pt Au Si <sub>3</sub> N <sub>4</sub>	Calorimetric	Air			0–32 m/s		Ma [57]

Table 3. Cont.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Ti/Pt Ceramic	Calorimetric	Air	0.3 m/s		0–8 m/s	100 mW	Shen [58]
Ti/Au Kapton	Hot-film	Glucose/PBS (0–60%)		3.06 mV/(mL/min)	0–10 mL/min	<5 mW	Li [66]
Ti/Au Cu Parylene	Hot-film	Glucose/DI H <sub>2</sub> O	5 mL/ 100 gram-min	1.467 mV/mL/ 100 gram-min	0–160 mL/ 100 gram-min		Li [67]
Ti/Pt Si <sub>3</sub> N <sub>4</sub>	Hot-film	Air		CV 2V: 0.01433 mA (m/s) <sup>-1/2</sup> CV 4V: 0.04593 mA (m/s) <sup>-1/2</sup> CC 12.96mA: 7.98 mV (m/s) <sup>-1/2</sup> CC 23.08mA: 27.35 mV (m/s) <sup>-1/2</sup>	0–11 m/s	CV 2V: 14.56 mW CV 4V: 50.83 mW CC 12.96mA: 45.10 mW CC 23.08 mA: 157.61 mW	Hung [51]
Cr/Pt/Ni/Pt Polyimide	Hot-wire	Air	Heater power dependent	Heater power dependent	Heater power dependent	Heater power dependent	Chen [60]
Cr/Au Polyimide	Hot-film	N <sub>2</sub> gas			0–6 m/s		Tan [61,62]
Cr/Ni/Pt Polyimide	Hot-film	Air	0.1 m/s		0–15 m/s	30 mW	Liu [63]
Pt	Hot-wire	Air			7–40 m/s		Bailey [46]
Cr/Ni Si <sub>3</sub> N <sub>4</sub>	Hot-wire	N <sub>2</sub> gas	0.002 m/s		0–1.6 m/s		Kaanta [42]
Polysilicon Si <sub>3</sub> N <sub>4</sub>	Hot-wire				0.2–0.5 mL/min		Soundararajan [44]
Polysilicon Silicon dioxide and Si <sub>3</sub> N <sub>4</sub>	Hot-wire	Cell medium					Hsiai [53]

Table 3. Cont.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Ti/Pt Parylene	Hot-film	Rabbit blood	Non-linear	0.35 mV/(dynes/cm <sup>2</sup> )			Yu [70–71]
Polysilicon Si <sub>3</sub> N <sub>4</sub>	Hot-film	DI H <sub>2</sub> O	10 nL/min	3.6–361.2 μV/(nL/min)	0–650 nL/min	140 μW	Wu [45]
Germanium Chromium heater	Calorimetric	DI H <sub>2</sub> O	100 nL/h		0–90 μL/h	1 mW	Ernst [76]
Germanium Si <sub>3</sub> N <sub>4</sub> SiO <sub>x</sub>	Calorimetric	Air	<1 cm/s	12.99–232.77 V/W/(m/s)	0–5 m/s	0.25–5.8 mW	Cubukcu [77]
Ti/Pt SU-8	Hot-wire Calorimetric	N <sub>2</sub> gas		3.76 mΩ/(m/s)	0–10 SLPM		Kaltsas [55]
Ti/Pt SU-8	Calorimetric	DI H <sub>2</sub> O IPA	40 nL/min	485 μV/( μL/min)	0–6 μL/min	0–20 mW	Vilares [56]
Pt Silicon-rich silicon nitride	Calorimetric	Water	0.2 μL/min	218 μV/( μL/min)	0–2 μL/min	1.9 mW	Dijkstra [52]

Ernst *et al.* fabricated amorphous germanium on a silicon nitride membrane. Amorphous germanium was chosen for its high TCR (~2%/K) while chromium was used as a heater for its low TCR (0.214%/K) [76]. Cubukcu *et al.* also utilized amorphous germanium thermistors with TCR of  $358.1 \times 10^{-4}/K$  to achieve a sub-mW powered flow sensor that still possessed high flow sensing range up to 5 m/s [77].

### 3.2. Thermoelectric

Kaltsas *et al.* fabricated thermopiles from polysilicon and aluminum (Al). Thermopile hot contacts were placed close to the polysilicon heater while cold contacts were placed on the silicon substrate. A 40 μm porous silicon layer was used for thermal isolation on top of which the thermopile hot contacts and heater were fabricated [29,78–80].

Others have fabricated thermoelectric flow sensors using more conventional silicon nitride and oxide materials for thermal isolation (Figure 9) [81–83].

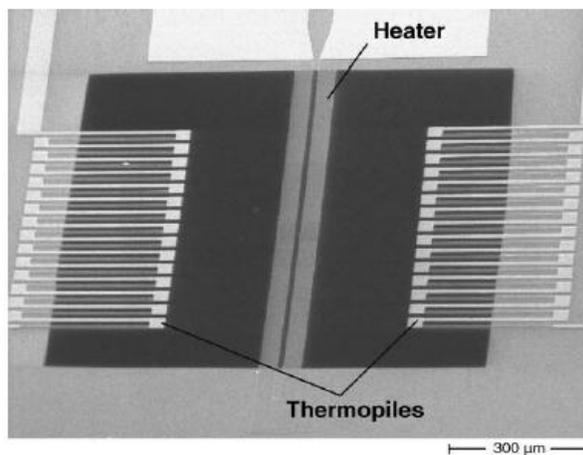
Bruschi *et al.* created thermopiles in a pseudo-calorimetric fashion over a silicon oxide membrane. Two thermally isolated heaters instead of one were used in between two thermopiles and thermal feedback maintained equal temperature between the two heaters under varying flow conditions [84–86].

In addition to silicon-based devices, thermopiles supported on polymers have been investigated for flow sensing applications in which a flexible substrate is desired (Table 4). Buchner *et al.* utilized a thin, flexible polyimide substrate to fabricate thermopiles and a heater in a calorimetric configuration [30,87].

**Table 4.** Thermoelectric flow sensor feature comparison.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Polysilicon/Al Porous Si	Calorimetric	N <sub>2</sub> gas	$4.1 \times 10^{-3}$ m/s	0.4 mV/(m/s)	0–0.4 m/s	67 mW	Kaltsas [29]
Polysilicon/Al Porous Si	Calorimetric	N <sub>2</sub> gas	~0.5 m/s	$175 \times 10^{-3}$ mV/(m/s) <sup>1/2</sup>	0–4 m/s		Kaltsas [78]
Polysilicon/Al Porous Si	Hot-wire Calorimetric	Not stated		0.95 mV/(m/s) <sup>1/2</sup>	0–6.67 m/s	100 mW for hot-wire	Kaltsas [79]
Polysilicon/ Ti-Tungsten	Calorimetric	Water IPA	0.2 μL/s	9.5 mV mm <sup>-1</sup> s	0–2 mm/s		Buchner [81]
Polysilicon/ Ti-Tungsten Polyimide	Calorimetric	Air		–0.12 mV/slm	10–100 slm		Buchner [30]
Polysilicon/Al	Calorimetric	N <sub>2</sub> gas			0–8 m/sec	15 mW	Laconte [82]
Polysilicon/Al Polysilicon heaters Silicon dioxide membrane	Pseudo- calorimetric	N <sub>2</sub> gas			0–200 sccm		Bruschi [84]
n-polysilicon/ p-polysilicon thermopile Polysilicon heater	Calorimetric	Air	0.002 sccm		0.9–8.4 m/s	4 mW	Bruschi [85]
Al/polysilicon Al heater Silicon-rich silicon nitride	Calorimetric	Water			0–500 nL/min	0.1–0.6 mW	Wiegerink [83]

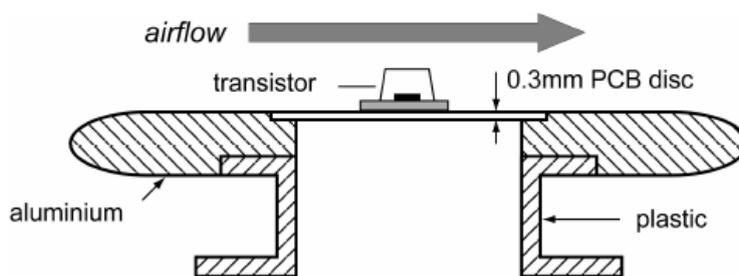
**Figure 9.** SEM image of thermopiles placed around a heater in a calorimetric configuration for thermoelectric flow sensing [81].



### 3.3. Thermoelectronic

Makinwa and Huijsing used standard CMOS processing to create wind sensor with a central diode that measured the temperature of the chip. On-chip comparators are used to control temperature differences. In addition, thermopiles are also used for thermal flow sensing in a thermoelectric manner [88–92]. Makinwa and Huijsing also investigated the use of a bipolar transistor in hot-wire mode for airflow measurement (Figure 10). A decrease in packaging was achieved by the transistor’s self-heating; obviating the need for separate heaters [93].

**Figure 10.** A transistor is soldered to a PCB and packaged for wind sensing [93].



**Table 5.** Thermoelectronic flow sensor feature comparison.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Polysilicon heater Polysilicon/ Al Bipolar transistor Ceramic	Hot-wire	Air	0.5 m/s		0–30 m/s		Sun [35]
Al/Si PNP transistor Ceramic	Calorimetric Hot-wire	Air	±4%		2–18 m/s	0.4–1 W	Makinwa [89]
Bipolar transistor	Hot-wire	Air			0–15 m/s	50 mW	Makinwa [93]

Thermoelectronic flow sensors were also realized in ceramic substrates (Table 5). Sun *et al.* fabricated thermopiles, polysilicon heaters, and a bipolar transistor and packaged them on a thin

ceramic substrate. The sensor was exposed to flow through the underside of the ceramic substrate and heat transfer was aided by copper pillar bumps [35].

### 3.4. Frequency Analog

Conventional thermal flow sensors (operating in hot film mode) require calibration circuitry or external signal processing to maintain accuracy. The combination of a SAW transducer with a hot-wire sensing element provides the additional feedback information that eliminates the need for temperature calibration procedures [38].

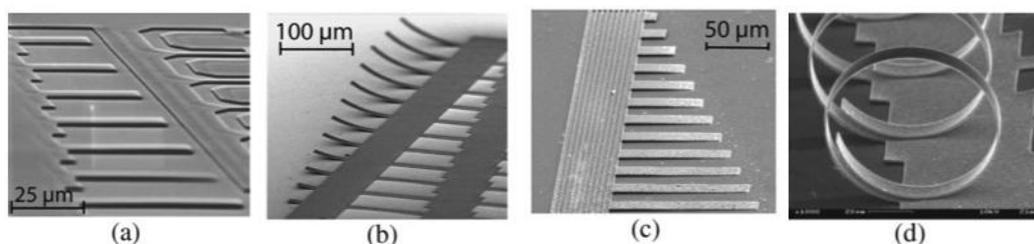
The typical SAW transducer device utilizes the effects of temperature on resonance frequency (Table 6). However, an ultra-high temperature stable device made of ST-X quartz was fabricated that operates without the need for calibration. Resonance frequency shifts were negligible in response to temperature, but fluid flow induced a pressure gradient across a SAW transducer, resulting in an observable phase shift [94].

**Table 6.** Frequency analog flow sensor feature comparison.

Material	Configuration	Gas/liquid	Resolution	Sensitivity	Range	Power Consumption	References
Tungsten, Aluminum oxide	Hot-wire	Air	3%				Kielbasa [38]
LiNbO <sub>3</sub> , Au, Cr	Time-of-flight	Liquid, refractive index from 1.33–1.35		0.1 °C/10 <sup>-5</sup> change in refractive index unit			Renaudin [95]
Si, SiO <sub>2</sub> , Si <sub>3</sub> N <sub>4</sub> , Al	Time-of-flight	Air		Increases with temperature, geometry dependent	0–20 m/s, geometry dependent		Iker [39]

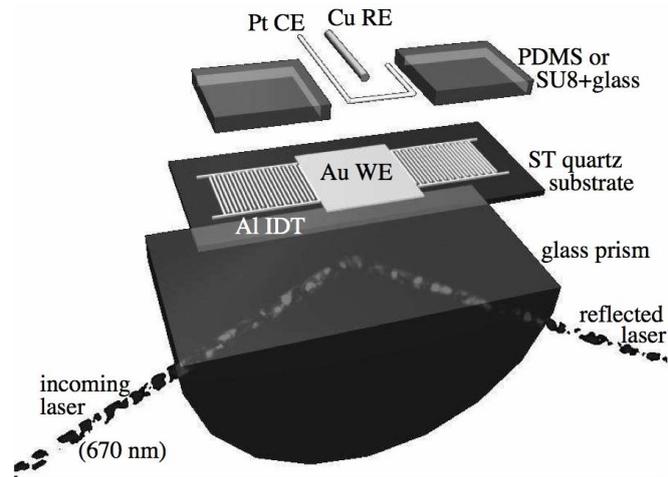
MEMS fabrication techniques have long been able to create three-dimensional microstructures, which enables geometries that may be fine-tuned (in terms of sensitivity and range) for thermal flow sensing (Figure 11). Self-assembling, interdigitated cantilever structures exhibit frequency changes in response to temperature, which is capacitively sensed [39].

**Figure 11.** 3D structures for frequency analog gas-flow sensing [39].



Surface Plasmon Resonance (SPR) devices have also been integrated with SAW transducers (Figure 12). The intended purpose is to use the SAW action to induce fluid flow and utilize SPR for sensing a target analyte. However, it was reported that the SAW action creates localized heating, which may be observed through SPR [95].

**Figure 12.** Integrated surface plasmon resonance (SPR) and surface acoustic waves (SAW) device [96].



### 3.5. Optical/SPR/Other

At the interface of specially selected materials, light couples to surface plasmons. This coupling is sensitive to changes in thickness, chemical species, and temperature, which manifests as a variation in reflectivity [95,96].

The resonance wavelength of an optical fiber Bragg grating will shift in response to temperature. Optical power heats up the grating, while fluid flow cools it. A pair of gratings were arranged to create a time-of-flight type sensor [97].

## 4. Conclusions

The current landscape of micromachined thermal flow sensors consists of the evolution of several established methodologies as well as the development and exploration of recent discoveries. Virtually any application can be addressed with the variety of materials, operation modes, transduction types (thermoresistive, thermoelectric, thermoelectronic, frequency analog), and configurations (hot-film, calorimetric, time-of-flight) that can be used to create flow sensors. The benefits of micromachined sensors are higher sensitivity to flow, ease of fabrication, and lack of moving parts as opposed to non-thermal flow sensing methods. Low cost micromachined thermal flow sensors will continue to mature and proliferate across many disciplines.

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