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# N<sub>2</sub>O Decomposition over Cu–Zn/γ–Al<sub>2</sub>O<sub>3</sub> Catalysts

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**Abstract:**  $\text{Cu-Zn}/\gamma - \text{Al}_2\text{O}_3$  catalysts were prepared by the impregnation method. Catalytic activity was evaluated for N<sub>2</sub>O decomposition in a fixed bed reactor. The fresh and used catalysts were characterized by several techniques such as BET surface area, X-ray diffraction (XRD), and scanning electron microscopy (SEM). The  $\text{Cu-Zn}/\gamma - \text{Al}_2\text{O}_3$  catalysts exhibit high activity and stability for N<sub>2</sub>O decomposition in mixtures simulating real gas from adipic acid production, containing N<sub>2</sub>O, O<sub>2</sub>, NO, CO<sub>2</sub>, and CO. Over the  $\text{Cu-Zn}/\gamma - \text{Al}_2\text{O}_3$  catalysts, 100% of N<sub>2</sub>O conversion was obtained at about 601 °C at a gas hourly space velocity (GHSV) of 7200 h<sup>-1</sup>.  $\text{Cu-Zn}/\gamma - \text{Al}_2\text{O}_3$  catalysts also exhibited considerably good durability, and no obvious activity loss was observed in the 100 h stability test. The  $\text{Cu-Zn}/\gamma - \text{Al}_2\text{O}_3$  catalysts are promising for the abatement of this powerful greenhouse gas in the chemical industry, particularly in adipic acid production.

 $\textbf{Keywords:} \ N_2O\text{-}decomposition; \ Cu-Zn/\gamma-Al_2O_3 \ catalysts; \ greenhouse \ gases; \ real \ industrial \ conditions$ 

## 1. Introduction

Environmental issues such as global warming and ozone layer depletion are now of universal concern. Nitrous oxide (N<sub>2</sub>O) has attracted a great attention as the third most significant anthropogenic greenhouse gas and the largest stratospheric ozone depleting substance [1-5]. N<sub>2</sub>O has a lifetime of 114-130 years under atmospheric conditions, and the global warming potential (GWP) of nitrous oxide is about 310 times of carbon dioxide ( $CO_2$ ) [6]. The emission of  $N_2O$  comes from both natural sources and human contributions. Anthropogenic sources, adipic acid production, nitric acid manufacturing, fuel and biomass combustion, and vehicle emissions are considered significant [7]. Therefore, development of efficient technologies for effective N<sub>2</sub>O removal has become an emerging issue. A number of methods can potentially be employed to remove N2O emissions, such as thermal decomposition, selective catalytic reduction with hydrocarbons (HC-SCR), adsorption, and direct catalytic decomposition into O<sub>2</sub> and N<sub>2</sub> [8]. Among various types of abatement technologies, direct catalytic decomposition of  $N_2O$  ( $N_2O \rightarrow N_2 + 1/2O_2$ ) is a relatively simple and cost-effective way to remove N<sub>2</sub>O from industrial tail gases, and becomes one of the most attracting methods. A large number of catalysts, such as supported noble metals, pure and mixed oxides, and zeolite-based catalysts have been evaluated for N<sub>2</sub>O decomposition reaction [9–21]. Among them, noble metal-based catalysts exhibit satisfactory activity at intermediate temperatures [22,23]. However, their high cost represents an important obstacle towards practical applications. Furthermore, their catalytic efficiency is notably hindered by the presence of O2, NO, and CO, which usually coexist in an exhaust gas stream. Copper-based materials have a great advantage because of their low cost and excellent catalytic performance. However, its thermal stability is not the best, at more than 500 °C. One problem that Catalysts **2016**, *6*, 200

still exists in many cases is the deactivation of the catalyst, so it is necessary to replace the catalyst. Therefore, attempts have been made to provide a catalyst for decomposition  $N_2O$ , and the catalyst has a thermal stability at high temperature. The study of  $N_2O$  catalytic decomposition is mainly focusing on the low temperature catalyst. However, the development of the catalyst should always be consistent with the special characteristics of the pollutant's source, and is not limited by the low temperature catalytic performance [24]. It is an object of the present research to provide a catalyst for  $N_2O$  catalytic decomposition, which is thermally stable at elevated temperatures.

The current research study is focused on the abatement of nitrous oxide from adipic acid production facilities. The real conditions of the plant (i.e., in the presence of CO, CO<sub>2</sub>, and O<sub>2</sub> and at a high N<sub>2</sub>O concentration) are very important to enlighten differences in terms of activity and stability; the latter is a crucial point for the decomposition of a highly concentrated N<sub>2</sub>O stream. Thus, the goal of the present work was to test a Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalyst for N<sub>2</sub>O decomposition in a model atmosphere from adipic acid production. The catalyst was characterized before and after the catalytic tests in order to identify potential changes in the physico-chemical properties and how these changes could affect the catalyst performance. The stability of Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalysts for long term use in high temperatures was also investigated.

## 2. Experimental Section

## 2.1. Catalyst Preparation

The Cu–Zn-based catalysts supported on  $\gamma$ –Al $_2O_3$  (Changling Catalyst Factory) were prepared via an impregnation method. Before impregnation,  $\gamma$ –Al $_2O_3$  was calcined at 450 °C for 4 h under an air atmosphere. In a typical impregnation process, Cu(NO $_3$ ) $_2$ ·3H $_2$ O (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, A.C.S. grade) and Zn(NO $_3$ ) $_2$ ·6H $_2$ O (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, A.C.S. grade) were dissolved in distilled water with a Cu/Zn molar ratio of 1:7. Ni(NO $_3$ ) $_2$ ·6H $_2$ O (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China, A.C.S. grade) was also added to the distilled water. The amounts of Ni(NO $_3$ ) $_2$ ·6H $_2$ O used for precursors of metal promoter were 3% of CuO and ZnO total mass. A certain amount of  $\gamma$ –Al $_2$ O $_3$  was added into the solution and kept at ambient temperature for 4 h. Then, excess water was evaporated at 90 °C on a hot plate. The slurry was oven dried at 120 °C for 10 h and calcined in air flow at 800 °C for 4 h. This prepared catalyst was denoted as Cu–Zn/ $\gamma$ –Al $_2$ O $_3$ .

## 2.2. Catalysts Characterization

BET surface area, pore volume and pore diameter of the catalysts were analyzed by  $N_2$  adsorption at  $-196\,^{\circ}\text{C}$  using a Micrometrics ASAP 2020 instrument (ASAP2020, Micromeritics, Micromeritics Instrument Corporation, Norcross, GA, USA). XRD patterns of the catalysts were obtained by an X-ray diffractometer (XRD-7000, Shimadzu, Shimadzu Corporation, Kyoto, Japan) in with Cu K $\alpha$  radiation. The  $2\theta$  range was kept between 10 and 80 degrees with a scan speed of  $6^{\circ}\cdot \text{min}^{-1}$ . Measurements of the surface morphology and composition of catalyst were performed using scanning electron microscopy (SEM) with associated energy-dispersive X-ray spectroscopy (EDS) (Quanta 400F, FEI Company, Hillsboro, OR, USA).

#### 2.3. Activity Tests

The catalytic tests in the decomposition of  $N_2O$  were performed in a fixed-bed quartz reactor of 10 mm internal diameter containing 0.8 g of catalyst. Two protocols were applied for catalytic evaluation. The reactant gas mixture (12 vol %  $N_2O$ , 16.8 vol %  $O_2$ ,  $N_2$  balance) was fed to the reactor. The total flow rate was 120 mL·min<sup>-1</sup>, which could be converted to a gas hourly space velocity (GHSV) of 7200 h<sup>-1</sup>. The  $N_2O$  conversion performance was evaluated in a temperature range of 300–620 °C at a 2 °C/min rate. The composition of outlet gases was analyzed using an on-line gas SP-3420 gas chromatograph (GC) equipped with a thermal conductivity detector (TCD). Figure 1 shows the

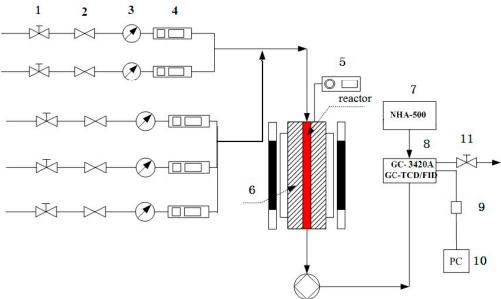
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schematic of the proposed experimental set-up. The  $N_2O$  conversion was determined according to the following equation:

 $X_{N_2O}(\%) = \frac{(C_{N_2O_{in}} - C_{N_2O_{out}})}{C_{N_2O_{in}}} \times 100$ 

where  $X_{\rm N2O}$  was the percent conversion of N<sub>2</sub>O;  $C_{\rm N2Oin}$  and  $C_{\rm N2Oout}$  were concentrations of N<sub>2</sub>O (ppm) in the inlet and outlet, respectively.

The catalytic performance was also evaluated in a gas mixture (12 vol %  $N_2O$ , 16.8 vol %  $O_2$ , 2.02 vol %  $CO_2$ , 696 ppm CO, 134 ppm  $NO_2$ , 211 ppm NO,  $N_2$  balance). The composition simulates real waste gas from adipic acid production. A long-term stability test was done at 601 °C where  $GHSV = 7200 \ h^{-1}$ .



1.cut-off valve 2.pressure reducing valve 3. pressure gage 4.flowmeter 5. temperature controller

6.heating furnace 7.Nitrogen,hydrogen and air integrated machine 8.gas chromatography

9.chromatographic workstation 10. computer 11.vent valve

Figure 1. Schematic of the experimental set-up.

#### 3. Results and Discussion

## 3.1. Effect of Cu–Zn Loading Amount on N<sub>2</sub>O Decomposition

In order to investigate the effect of Cu–Zn loading amount for  $N_2O$  decomposition, several Cu–Zn/ $\gamma$ –Al $_2O_3$  catalysts with different Cu–Zn loading amounts were prepared. The feed stream consisted of 7 vol %  $N_2O$ , 2 vol %  $O_2$ , and balanced  $N_2$ . Figure 2 shows the effect of the Cu–Zn loading amount on the decomposition of  $N_2O$  as a function of temperature. As shown in Figure 1, below 450 °C, the catalytic activity increased progressively with the increase in Cu–Zn loading amount in the range of 30–45 wt %. Above 450 °C, the catalytic activity increased with the increase in Cu–Zn loading amount, and the catalytic activity then decreased when the Cu–Zn loading amount increased to 45 wt %. The effect of the Cu–Zn loading amount on catalytic activity was more significant above 450 °C. This result may suggest that a suitable Cu–Zn loading amount is 35–40 wt %. The 35 wt % Cu–Zn loading catalyst shows  $T_{50}$  (the temperatures of 50% conversion) at 480 °C. Hence, this 35 wt % Cu–Zn loading amount was considered optimum for  $N_2O$  decomposition, and further studies were carried out using this catalyst.

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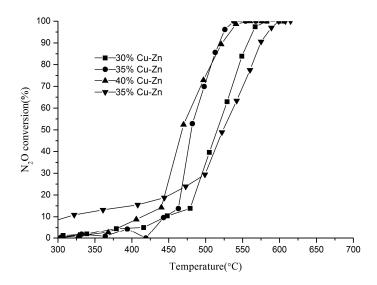


Figure 2. The effect of the Cu–Zn loading amount on the decomposition of N<sub>2</sub>O.

#### 3.2. Characterization of the Catalyst

The XRD patterns of the fresh and used Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalysts are shown in Figure 3. In the PDF#44-0706 card of CuO, the characteristic diffraction peaks of  $2\theta$  values are at  $38.472^{\circ}$ ,  $35.244^{\circ}$ , and  $48.589^{\circ}$ . In the PDF#36-1451 card of ZnO, the characteristic diffraction peaks of  $2\theta$  values are at  $31.769^{\circ}$ ,  $36.252^{\circ}$ ,  $47.538^{\circ}$ ,  $56.602^{\circ}$ , and  $66.378^{\circ}$  However, for the XRD patterns of Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub>, the sharp diffraction peaks were at  $2\theta = 31.35^{\circ}$ ,  $36.88^{\circ}$ ,  $45.30^{\circ}$ ,  $55.57^{\circ}$ ,  $59.26^{\circ}$ , and  $65.59^{\circ}$ . They were somewhat different from the PDF card of CuO and ZnO. These peaks should be attributed to characteristic diffraction peaks of Cu–Zn composite metal oxides. The detected phase is similar to the spinel phase. The crystal particle sizes of fresh and used catalysts were 6.92 nm and 7.01 nm, respectively. From the XRD spectra, it was found that the diffractograms of the fresh and used catalysts were identical, and no structural changes appeared due to working in real conditions.

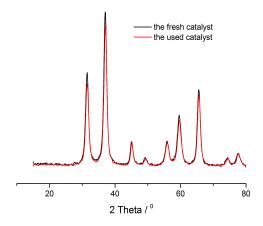


Figure 3. X-ray diffractograms of the fresh catalyst and used catalyst.

The BET textural characteristics of the fresh and used catalyst are reported in Table 1. The surface area of the pure support  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> was also measured as 597 m<sup>2</sup>/g. Incorporation of Cu–Zn into the alumina support resulted in a slight decrease in surface area. As observed, the surface areas obtained before and after the catalytic tests are not notably changed, indicating that the catalyst has good structural stability. It is also observed that the used catalyst show a lower pore diameter than the fresh catalysts. However, the pore volume is lower in the case of the fresh catalyst compared to the used catalyst. This may be due to the formation of fine pores.

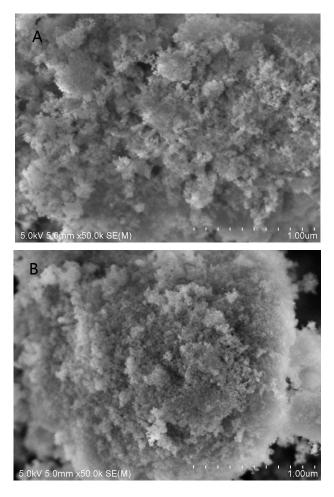
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	Catalyst	BET Area ( $m^2 \cdot g^{-1}$ )	Pore Diameter (nm)	Pore Volume (cm <sup>3</sup> ⋅g <sup>-1</sup> )			
	fresh	506	6.36	0.8038			
	used	564	6.10	0.8562			
	$\gamma$ -Al <sub>2</sub> O <sub>3</sub>	597	7.16	1.0704			

**Table 1.** Textural characteristics of the fresh and used catalyst.

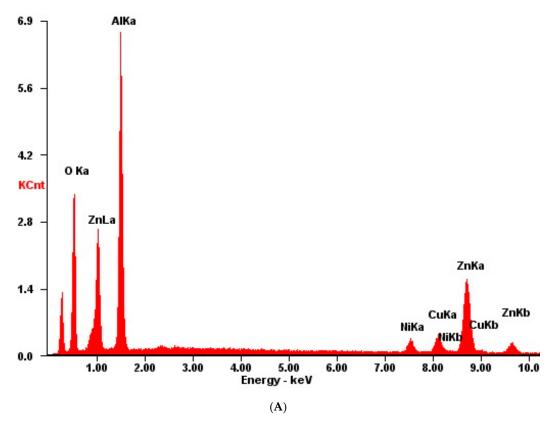
Figure 4 shows the surface morphology of the fresh and used catalyst. The surface of the catalyst is cabbage shape and very rough. Its microstructure appears a spongy morphology. The components are evenly distributed on the carrier surface. There was no obvious change in the surface morphology of the fresh and used catalyst.

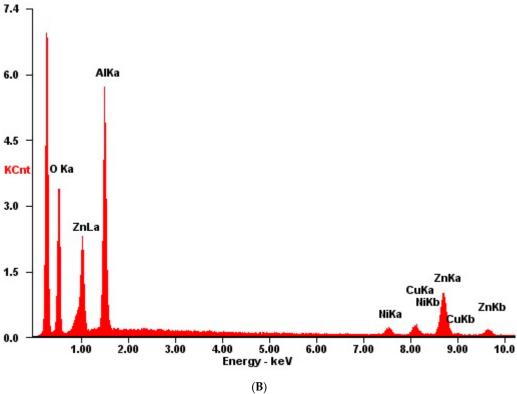
The EDS patterns of the fresh and used catalyst are given in Figure 5. It is observed clearly that the expected elements such as Cu, Zn, and Ni are involved in the surface of the catalyst confirmed by the EDS survey, and the atom ratio of Cu/Zn on the surface before the reaction is 5.36 from the EDS result. Moreover, the atom ratio of Cu/Zn on the surface after the reaction is 5.34, indicating that the content of Cu elements on the catalyst decreased after the reaction. Quantitative EDS analysis of Cu–Zn/ $\gamma$ –Al $_2$ O $_3$  catalysts are reported in Table 2. EDS analysis shows the content variation of the catalyst components during the reaction. Oxygen and aluminum were lost during the reaction, which led to an increase in Cu, Zn, and Ni.



**Figure 4.** SEM (scanning electron microscope) images of catalysts (**A**) the fresh catalyst and (**B**) the used catalyst.

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**Figure 5.** The EDS (energy dispersive spectroscopy)patterns of catalysts (**A**) the fresh catalyst and (**B**) the used catalyst.

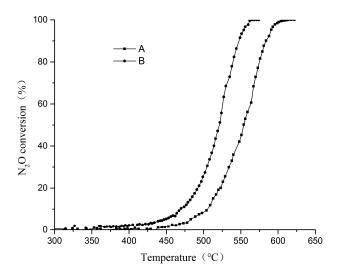
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Catalyst			wt %		
	0	Al	Ni	Cu	Zn
fresh	24.67	32.61	3.05	6.09	33.58
used	18.85	30.84	3.34	7.23	39.74

**Table 2.** Quantitative EDS analysis of Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalysts.

## 3.3. Catalytic Performance

 $N_2O$  decomposition studies were carried out on the Cu–Zn/ $\gamma$ –Al $_2O_3$  catalysts using Gas Mixture A (12% vol N $_2O$ , 16.8% vol O $_2$ , N $_2$  balance) and Gas Mixture B (12% vol N $_2O$ , 16.8% vol O $_2$ , 2.02% vol CO $_2$ , 696 ppm CO, 134 ppm NO $_2$ , 211 ppm NO, N $_2$  balance). The catalyst with 35 wt % Cu/Zn was used, unless otherwise stated. As shown in Figure 6, Cu–Zn/ $\gamma$ –Al $_2O_3$  catalysts are virtually not active below 400 °C, and they start to show some activities above 425 °C. Compared with Gas Mixture A, Gas Mixture B has more components, but the reaction temperature is lower, which is related to the reduction of CO and NO in Gas Mixture B. When N $_2O$  was totally converted (more than 99%), the reaction temperature of Gas Mixture B was 561 °C, which is 42 °C lower than Gas Mixture A. After the catalytic reaction, the main components of the mixed gas were O $_2$  and N $_2$ , so the catalyst could effectively eliminate N $_2O$ . The temperatures of 50% conversion ( $T_{50}$ ) were read out from the curves and are listed in Table 3.



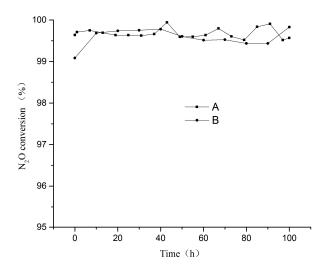
**Figure 6.** Conversion of  $N_2O$  over Cu–Zn/ $\gamma$ – $Al_2O_3$  catalysts. Reaction conditions: (A) 12% vol  $N_2O$ , 16.8% vol  $O_2$ ,  $N_2$  balance; GHSV (gas hourly space velocity) = 7200 h $^{-1}$ ; (B) 12% vol  $N_2O$ , 16.8% vol  $O_2$ , 2.02% vol  $CO_2$ , 696 ppm CO, 134 ppm  $NO_2$ , 211 ppm NO;  $N_2$  balance; GHSV = 7200 h $^{-1}$ .

**Table 3.** Temperatures of 10%, 50%, and 99% conversion of N<sub>2</sub>O ( $T_{10}$ ,  $T_{50}$ , and  $T_{99}$ ) over the Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalyst.

Gas Mixture A (°C)			Gas Mixture B (°C)		
T <sub>10</sub>	T <sub>50</sub>	T <sub>99</sub>	T <sub>10</sub>	T <sub>50</sub>	T <sub>99</sub>
505	553	603	470	521	561

Measuring the durability of catalysts is important in determining their practical feasibility. Figure 7 shows the catalytic stability of the Cu–Zn/ $\gamma$ –Al $_2$ O $_3$  catalyst for N $_2$ O decomposition. These tests were carried out at  $T=601\,^{\circ}$ C. In the model atmosphere (Gas Mixture A and Gas Mixture B), N $_2$ O conversion over the Cu–Zn/ $\gamma$ –Al $_2$ O $_3$  catalyst after reaction at  $T=601\,^{\circ}$ C for 100 h was maintained at 99%, indicating that the catalyst has high activity and stability.

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**Figure 7.** Stability test run of the Cu–Zn/ $\gamma$ –Al<sub>2</sub>O<sub>3</sub> catalysts at 601 °C for 100 h.

#### 4. Conclusions

In this study,  $\text{Cu-Zn/}\gamma\text{-Al}_2\text{O}_3$  catalysts were prepared by an impregnation method and characterized by means of SEM, XRD, and  $\text{N}_2$  adsorption–desorption techniques. Prepared catalysts were tested for  $\text{N}_2\text{O}$  catalytic decomposition. The results illustrate that the  $\text{Cu-Zn/}\gamma\text{-Al}_2\text{O}_3$  catalyst is quite effective for the catalytic decomposition of  $\text{N}_2\text{O}$  under model atmosphere.  $\text{N}_2\text{O}$  can be completely decomposed at 601 °C in oxygen atmosphere. In addition, the  $\text{Cu-Zn/Al}_2\text{O}_3$  catalyst exhibited appreciable activity even in the presence of CO and  $\text{NO}_2$ , which are commonly found in exhaust gases from adipic acid production. Good performance and no deactivation of the catalyst were confirmed by 100 h stability tests. This study serves only as an exploratory work on this catalyst system; detailed fundamental studies are underway.

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**Author Contributions:** Runhu Zhang and Chao Hua conceived and designed the experiments; Runhu Zhang performed the experiments; Bingshuai Wang and Chao Hua analyzed the data; Yan Jiang contributed reagents/materials/analysis tools; Runhu Zhang wrote the paper.

Conflicts of Interest: The authors declare no conflicts of interest.

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