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Role of Seawater Desalination in the Management of an Integrated Water and 100% Renewable Energy Based Power Sector in Saudi Arabia

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Abstract: This work presents a pathway for Saudi Arabia to transition from the 2015 power structure to a 100% renewable energy-based system by 2050 and investigates the benefits of integrating the power sector with the growing desalination sector. Saudi Arabia can achieve 100% renewable energy power system by 2040 while meeting increasing water demand through seawater reverse osmosis (SWRO) and multiple effect distillation (MED) desalination plants. The dominating renewable energy sources are PV single-axis tracking and wind power plants with 243 GW and 83 GW, respectively. The levelised cost of electricity (LCOE) of the 2040 system is 49 €/MWh and decreases to 41 €/MWh by 2050. Corresponding levelised cost of water (LCOW) is found to be 0.8 €/m³ and 0.6 €/m³. PV single-axis tracking dominates the power sector. By 2050 solar PV accounts for 79% of total electricity generation. Battery storage accounts for 41% of total electricity demand. In the integrated scenario, due to flexibility provided by SWRO plants, there is a reduced demand for battery storage and power-to-gas (PtG) plants as well as a reduction in curtailment. Thus, the annual levelised costs of the integrated scenario is found to be 1–3% less than the non-integrated scenario.

Keywords: 100% renewable energy; Saudi Arabia; energy transition; desalination; solar PV; wind energy; sector integration

1. Introduction

The Kingdom of Saudi Arabia (KSA) is the largest country in the Arabian Peninsula and is the 13th largest in the world. As of 2015, the Kingdom had a population of approximately 31,540,000—the highest among the Gulf Cooperation Council (GCC) countries [1,2]. Located between the Persian Gulf and the Red Sea, Saudi Arabia is also one of the largest arid countries without any permanent rivers or lakes. While the global average renewable water resource per capita per year is 6000 m³, Saudi Arabia has only 84.8 m³/(capita·a) [3]. In spite of the water scarcity, Saudi Arabia has the third highest water consumption per capita at 250 L/(capita·d) [3]. This is only behind the United States and Canada. The country's water demand is expected to increase by 56% by 2035. Meanwhile, at the current rate of water withdrawal, ground water aquifers are expected to provide potable water only for the next 10–30 years [4].

To augment the fresh water resources, Saudi Arabia relies on seawater desalination, particularly to meet the municipal and industrial water demands. In 2010, 58% of the country's total water demand was met through non-renewable ground water resources, 33.5% by surface water and renewable ground water, 6% by desalinated water and 2.2% by waste water reuse [5]. In 2014, desalinated water is estimated to have met 60% of KSA's municipal water demand [6]. By the end of 2015, Saudi Arabia accounted for 15% of the global installed desalination capacity [5]. With the diminishing of fresh water resources, seawater desalination is expected to play a pivotal role in meeting Saudi Arabia's future

water demands. However, desalination is an energy intensive process compared to traditional water treatment methods. Saudi Arabia is reported to use 25% of the domestic oil and gas production in desalination plants and the share is expected to increase to 50% by 2030 [7]. A report by General Electric (GE) suggests that Saudi Arabia requires 300,000 barrels of oil per day for the desalination plants on the country's Eastern and Western coasts [8].

Saudi Arabia has 1/5th of the world's proven oil reserves and is the largest producer and exporter of petroleum products [9]. In addition, KSA is the 9th largest exporter of natural gas [9]. Saudi Arabia's economy is based on oil revenues and during the time period 2010–2013, oil revenues contributed up to 91% of the country's national income [10]. This is reflected in the recent low oil prices and the resulting slower growth of the Saudi economy. Al Bassam [10] explains that although the government has had plans to diversify the economy and decouple economic growth from oil, there has in fact been an increase in dependence on oil revenues over the last few years. In addition to the low oil prices, growing concern is the share of local fossil fuel reserves, driven by increasing income and population, being used to meet the country's energy demand. According to the King Abdullah City for Atomic and Renewable Energy (KACARE) [11], the country's demand for fossil fuels is expected to grow from 3.8 million barrels of oil equivalent in 2010 to 8.3 million barrels of oil equivalent in 2028. Moser et al. [12] suggests that at the current rate of consumption, Saudi Arabia could become an oil importer by 2030. By 2015, Saudi Arabia's power plants capacities were almost equally separated into oil-based thermal power plants and gas-based power plants [13].

Economic reforms have been discussed in the past but it is only recently that reforms have been discussed with haste. A report in the Guardian [14] suggests that swift actions were triggered by the 100 billion \in deficit the Saudi government incurred in 2015. Consequently, in April 2016, King Salman bin Abdulaziz presented details of the Saudi vision 2030 plan and heralded a Saudi future without oil [14]. A key component of the new vision is the growth of Saudi Arabia's renewable energy sector for both power and water desalination. It is planned to have 9.5 GW of renewable capacity by 2023, as an initial stage to meet the country's increasing energy demands [15]. According to a recent article [16], the Saudi Energy Minister has discussed the Kingdom's visions to push installed renewable energy (RE) capacities higher to 10 GW by 2023.

In spite of the country's wealth of solar and wind resources, Saudi Arabia had only 83 MW of renewable power plants, all solar photovoltaic installations, by early 2015 [13]. Figure 1 presents the total installed capacities, by the beginning of 2015, in Saudi Arabia and illustrates the almost complete reliance on oil and gas in the current power sector [13]. The country lies within the sunbelt region of the world and the average population weighted global horizontal irradiation is estimated to be 2158 kWh/($m^2 \cdot a$) [17,18]. According to Yamada [19], the potential for solar energy in Saudi Arabia is finally being acknowledged with the Saudi government referring to solar energy as 'yellow oil'. The recent bids for 300 MW of solar PV in Saudi Arabia is set to end with an electricity production cost as low as 1.78 USD cents/kWh—the lowest bid to date [20]. With 7 out of the 8 bids placed for the 300 MW installation being less than 3 USD cents/kWh, the new threshold for large scale projects in the MENA region is being discussed to be as little as 3 USD cents/kWh [21]. Further to these developments, the Saudi Public Investment Fund together with the SoftBank Vision Fund, has confirmed the construction of a 3 GW solar and storage project in 2018 [22]. This would enable to meet one-third of Saudi Arabia's renewable energy capacity of 9.5 GW by 2023.

Table 1 illustrates the energy consumption of the most prevalent desalination technologies in Saudi Arabia [23]. In the past, Saudi Arabia has relied on thermal desalination technologies. However, due to the lower energy consumption and improvement in technology, reverse osmosis is expected to dominate the Saudi market in the future [5].

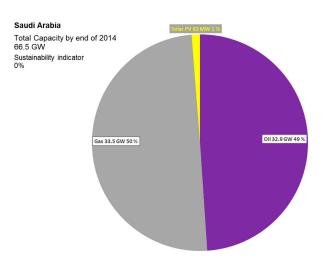


Figure 1. Total Installed Capacities by the beginning of 2015 in Saudi Arabia [13].

Desalination Technology	Electrical Energy Consumption (kWh _e /m ³)	Thermal Energy Consumption (kWh _{th} /m ³)
Seawater Reverse Osmosis (SWRO)	4.0	-
Multi Stage Flash (MSF)	2.5-5.0	85
Multiple Effect Distillation (MED)	2.0–2.5	65

 Table 1. Average energy consumption of prevalent seawater desalination technologies in the KSA [23].

In Caldera et al. [24], it was shown that the global water demand of 2030 can be met by seawater reverse osmosis (SWRO) plants powered by 100% hybrid renewable energy power plants at a cost level competitive with that of fossil powered SWRO plants today. This system eliminates the reliance of SWRO desalination plants on non-renewable fossil fuels and concerns about greenhouse gas emissions. Meanwhile, reflecting the Saudi government's vision of high renewable energy capacities, there is recent literature that discusses the 100% renewable energy transition of different countries and regions [25–32], as well as detailed visualization of respective electricity systems [33].

In this paper, motivated by the growing demand for seawater desalination in Saudi Arabia and transition towards 100% renewable energy power systems, we pose the following research question: What are the impacts on Saudi Arabia's electricity and water production costs when the seawater desalination demand is integrated into the country's 100% renewable energy (RE)-based power sector? The energy transition pathway, for Saudi Arabia, from the current fossil-based power system to a 100% RE-based system is first found. Then, the seawater desalination demand is integrated into the power and water sectors. The excess heat present in the energy system is utilized for the thermal desalination plants during the transition

In addition, the transition accounts for the non-energetic industrial gas demand of Saudi Arabia. During the transition, the non-energy demand for natural gas by the Saudi industry is increasingly met through synthetic natural gas production (SNG). Power to gas plants (PtG) are used to produce SNG from renewable electricity generation [34,35] and integrated into the power system. During the production of the SNG, there may be excess heat produced that can contribute to the operation of thermal desalination plants.

Thus, the results will present an optimal transition path for Saudi Arabia to manage the country's future electricity, water and gas demands through a 100% RE system.

2. Methodology

2.1. Overview

The key objective of our work is to understand the role that seawater desalination can play in the optimal transition of Saudi Arabia's 2015 power sector a 100% renewable energy power sector by 2050. The approach that was taken to answer this research question can be summarized as follows:

- 1. The energy transition from the current (as of the beginning of 2015) fossil-based power system in KSA to a 100% renewable energy-based power system by 2050, in 5 year time steps, is found. After 2015, there are no new fossil powered thermal plants allowed in order to achieve the target of a 100% RE-based power system. The existing fossil-based power systems are phased out based on their lifetimes. The increase in total electricity demand and population over the years is accounted for. The optimal mix of renewable power systems to replace the phased out fossil power systems are found and the resulting system's levelised cost of electricity (LCOE) is found for every time step.
- 2. The non-energy industrial gas demand of Saudi Arabia, from 2015 to 2050 is found and integrated into the power system. Figure 6 presents the projected growth in the industrial gas demand in Saudi Arabia. To attain a 100% renewable energy future, our work assumes that over time the industrial gas demand is met from synthetic natural gas (SNG). This can be achieved through power-to-gas plants (PtG) that comprise of two processes already used in industry: electrolysis and methanation [34,35]. PtG plants convert renewable electricity to renewable methane that can be stored in the existing gas infrastructure and used as conventional natural gas or for the industry.
- 3. Seawater desalination demand in KSA from 2015 to 2050 is determined and the corresponding desalination capacities integrated into the system. After 2015, the model is allowed to only install SWRO plants. This is based on the increasing dominance of the technology in the Saudi Arabian desalination market. MED plants are considered due to the low thermal consumption and lower electricity demand than SWRO [23,36]. The heat from the power system is used to meet the thermal demand of MED plants. Multi stage flash (MSF) desalination capacities that were online up to 2015 are included and phased out based on the lifetimes. MSF stand alone plants are excluded due to the relatively higher thermal consumption compared to MED plants [23,36]. In addition, MED and MSF cogeneration plants are excluded due to the requirement for fossil powered thermal power plants [37]. According to a Water Desalination Report [38], the Ras Al Khair IWPP plant, the largest desalination plant in the world, is expected to be the last new MSF plant in KSA.
- 4. The energy transition for KSA from the 2015 fossil-based power system to the 100% renewable energy-based power system by 2050 is found with the gas sector and seawater desalination integrated. Ultimately, the total cost of the power, gas and water sectors are compared to determine the impacts of integrated seawater desalination in the energy system.

For the design and analysis of the energy transition, the energy model, used and further developed at LUT, is used [29,39–41]. The LUT Energy System Transition model is based on the linear optimization method with interior point optimization, and is designed in an hourly temporal and $0.45^{\circ} \times 0.45^{\circ}$ spatial resolution. The energy model allows for the design of local, national, regional or global energy systems. It is composed of all relevant power generation and storage technologies, respective installed capacities and different operation modes of these technologies. A key feature of the model is its flexibility and expandability besides the hourly resolution for a full real year.

The sections that follow present an overview of the technical and financial assumptions of the energy model, the power plants and seawater desalination plants. The data assumed for the time period from 2015–2050 are presented.

2.2. Model Overview

A key requirement of the LUT Energy Systems model is to match the power generation and demand for every hour of the applied year. The hourly modeling enables a more accurate system description including synergy effects of different system components for power system balance [29]. The aim of the system optimization is to minimize the total annual cost of the installed capacities of the different technologies, cost of energy generation and generation ramping. The full description of the model, its input data including RE resources and technical assumptions can be found in Bogdanov and Breyer [29] and Barbosa et al. [39].

The three main components of the energy model can be listed as:

- Technologies for the conversion of RE into electricity;
- Energy storage technologies;
- Energy sector bridging technologies enable the coupling of different electricity demand sectors. This provides further flexibility to the complete energy system, bringing down the overall system cost.

Aghahosseini et al. [40] describe the various components of the LUT Energy System model and how the model determines the optimal 100% renewable energy mix for Iran for the year 2030.

For Saudi Arabia, the model described by Aghahosseini et al. [40] was modified with the addition of thermal desalination technologies as another desalination technologies and a subsequent energy transition, i.e., the system setup found for one period had been adjusted by the capacities being beyond their technical lifetime as a starting value for incremental optimization for the new period. Figure 2 illustrates the modified energy model. For the energy transition, the model determines the optimal combination of the components that meets the electricity demand of every hour for the time period from 2015 to 2050, in 5 year time steps.

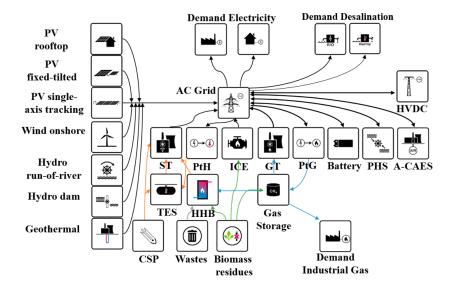


Figure 2. Block diagram of the LUT Energy Systems model used for Saudi Arabia.

2.3. Power Plant Capacities—Technical and Financial Assumptions

The average rate of increase in electricity demand in KSA is 6% and as of 2015, for a total population of 32,540,000, the total electricity consumption of the country was 289 TWh [42,43]. To determine the future energy system, the forecasted total energy demand numbers are required. The International Energy Agency assumes a compound annual growth rate of 2.7% for the Middle East [44]. This growth rate was applied to Saudi Arabia to project the future electricity consumption, as presented in Table 2. Figure 3 illustrates the hourly load profile for Saudi Arabia assumed for

2015 [42,43]. As expected, during the summer period of May to September, the highest loads occur. For the subsequent time periods, the load profile presented is varied depending on the total electricity consumption for the period. The capacity factor on the right y-axis indicates the percentage of the maximum load that is being required for a given point in time.

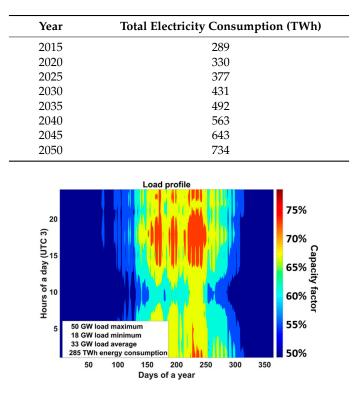


Table 2. Variation in the electrical energy consumption of Saudi Arabia from 2015 up to 2050 [44].

Figure 3. Aggregated load curve for the year 2015 for Saudi Arabia.

The model takes the 2015 installed power plant capacities, presented in Figure 1, corresponding lifetimes, total electrical energy demand, and optimizes the mix of renewable energy plants needed to be installed to achieve a 100% renewable energy power system by 2050. The optimization for each time period is carried out on basis of assumed costs and technological status of the renewable energy technologies. In the integrated scenario, the RE plants are optimized to also cater for the energy demands of the desalination and gas sectors.

The capital expenditures (capex), operational expenditures (opex) and efficiency variations of all the power sector components, from 2015 up to 2050, assumed in the model are presented in Appendix A (Tables A1 and A3). Figure 4 is a visual representation of the capex numbers. A learning curve approach based on several references, is used to identify the variation in capex for the different components. The references for the different components are presented in the Appendix A (Table A1).

The capex and opex numbers generally refer to a kW of electrical power. For the case of water electrolysis the capex and opex numbers refer to a kW of hydrogen thermal combustion energy, and for CO_2 direct air capture, methanation and gas storage to a kW of methane thermal combustion energy. The financial assumptions for storage systems refer to a kWh of electricity, and gas storage refers to a thermal kWh of methane at the lower heating value. Weighted average cost of capital (WACC) is set to 7% for all years. The technical assumptions concerning power to energy ratios for storage technologies, and efficiency numbers for generation and storage technologies are provided in the Appendix A (Tables A1 and A2).

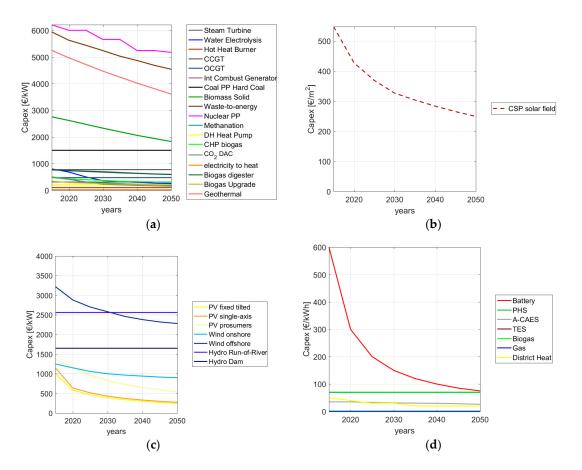


Figure 4. Variation in capex of power system components (**a**), CSP solar field (**b**), RE components (**c**) and storage components (**d**) assumed in the model.

To determine the capacities of the different renewable energy power plant components, it is necessary to understand the local resources available. The solar irradiation components and wind speed data, in a $0.45^{\circ} \times 0.45^{\circ}$ spatial and hourly temporarily resolution, is obtained from the NASA [45,46] and reprocessed by the German Aerospace Center [29]. The wind speed data is provided for a height of 50 m. In the LUT Energy Systems model, due to higher performance, ENERCON 3 MW wind turbines (E-101, Enercon, Aurich, Germany), with a hub height of 150 m, are used [29]. The wind speed data from the German Aerospace Center is converted to the relevant wind speed at 150 m using the logarithmic wind shear law [29]. The approach discussed by Aghahosseini et al. [40] is used to identify the biomass and geothermal potential available in KSA. Table 3 presents the biomass and geothermal potential results for KSA and it is assumed that these are the amounts available for every time period from 2015 to 2050.

Table 3. Estimation of biomass potentials and geothermal energy potential for Saudi Arabia from 2015–2050.

Solid Waste	Solid Biomass	Biogas Sources	Geothermal Potential
(TWh _{th} /a)	(TWh _{th} /a)	(TWh _{th} /a)	(TWh _{th} /a)
1.92	4.14	1.97	57.53

Feed-in full load hours (FLH) for Saudi Arabia is also computed, as described in Bogdanov and Breyer [29], on the basis of the $0.45^{\circ} \times 0.45^{\circ}$ spatially resolved data. The average FLH for CSP solar field, PV optimally tilted, PV single-axis tracking and wind power plants in Saudi Arabia are presented in Table 4. The average full load hours represent the number of hours in a year with the equivalent

maximum generation for the annually obtained yield, which is identical to the capacity factor derived by the average full load hours divided by 8760, the numbers of all hours in a year. Wind energy has the highest FLH, followed by PV single-axis tracking, CSP solar field and PV optimally tilted. Figure 5 presents the aggregated profiles of CSP solar field, wind energy power generation, solar PV generation (optimally tilted and single-axis tracking). The profiles represent the weighted average of the RE resource available as a percentage of the total respective RE resource potential of the country.

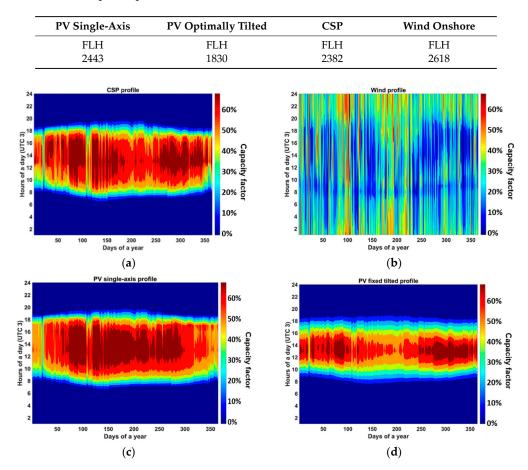


Table 4. Average full load hours (FLH) for CSP solar field, PV optimally tilted, PV single-axis tracking and wind onshore power plants in Saudi Arabia.

Figure 5. Aggregated feed in profiles in KSA for CSP solar fields (**a**), wind power plants (**b**), single-axis tracking PV (**c**) and optimally tilted PV (**d**).

The model specifies the upper limits and lower limits for the renewable energy power plant capacities. Lower limits are the installed capacities of renewable energy plants by 2015. For Saudi Arabia this is only 81.6 MW of solar PV plants as listed in Table 5. In periods after 2015, the lower limit is set to the capacity of the previous period adjusted by the capacities reached the end of their technical lifetime. The upper limits are calculated according to Bogdanov and Breyer [29] and the relevant results for KSA are listed in Table 6. For solid biomass residues, biogas and waste-to-energy plants it is assumed, due to energy efficiency reasons, that the available and specified amount of the fuel is used during the year.

Table 5. Lower limits of installed capacities [MW] considered in this study for Saudi Arabia.

Country	Solar PV
KSA	81.6

Table 6. Upper limits on installable capacities in Saudi Arabia in units of GW_{th} for CSP and GW_{el} for all other technologies.

Country	Area (1000 km ²)	Solar CSP	Solar PV	Wind
KSA	446.5	19347	9673	722

Tables A1 and A2, in the Appendix A, provide detailed technical and financial assumptions, from 2015 to 2050, for the energy system components used in this research for Saudi Arabia.

2.4. Seawater Desalination Capacities—Technical and Financial Assumptions

Table 7 represents the total online capacities of seawater desalination in Saudi Arabia by 2015 [47].

Desalination Technology	Total Online Capacity (m ³ /day)
SWRO	2,736,238
MSF Stand Alone	1,519,777
MSF Cogeneration	2,727,021
MED Stand Alone	1,507,074
MED Cogeneration	975,371
Other technologies, including those that use brackish water	220,324

 Table 7. Online capacities of seawater desalination in Saudi Arabia by 2015.

The desalination capacity required for the time period from 2015–2050 is determined using the methodology described in Caldera et al. [24]. The approach is based on the water stress and the water demand values in Saudi Arabia for an optimistic future scenario. The desalination capacities are calculated assuming a 100% utilization of the available renewable water resource. The National Water Strategy (NWS) for Saudi Arabia outlines specific amounts of non-renewable water to be consumed from 2015 up to 2040, such that by 2040 there is 5 billion m³ of non-renewable water resource being withdrawn annually [48]. Therefore, the actual desalination demand also should take into account the usage of non-renewable water resources. For the model, the non-renewable water resource being withdrawn is deducted from the modelled desalination capacity to find the actual desalination capacity required. However, the non-renewable water resource numbers found in the NWS are based on a percentage of renewable water resource used. In the model, the desalination capacities are based on optimal use of the available renewable freshwater resource. As a result, the actual non-renewable water resource withdrawal decreases. This is ultimately used to find the actual desalination capacity required for the Kingdom of Saudi Arabia from 2015–2050. Table 8 represents the numbers and the final desalination capacities needed. In addition, the capacities online by 2015 are presented. This is less than the actual desalination demand in 2015. It has to be noted that other desalination technologies, such as brackish water reverse osmosis (BWRO), have been excluded from the present study. The desalination capacities in the following years are optimized by the model.

Table 8. Desalination capacities required to meet KSA's increasing total water demand.

	Unit	2015	2020	2025	2030	2035	2040	2045	2050
Population	mill	31.50	34.40	36.85	39.13	41.24	43.14	44.76	46.06
Total water demand	mill m ³ /day	65.4	68.5	75.6	81.0	88.6	96.7	105.0	112.6
Desalination demand based on [21]	mill m ³ /day	19.1	21.8	27.5	32.0	38.4	45.2	53.8	58.7
Final non-renewable water resource used	mill m ³ /day	8.9	7.9	5.8	3.9	6.2	8.5.	0	0
Actual desalination demand	mill m ³ /day	10.2	13.9	21.7	28.2	32.3	36.7	53.8	58.7
	In	stalled ca	pacities						
SWRO	mill m ³ /day	2.7							
MSF Stand Alone	mill m ³ /day	1.52							
MSF Cogeneration	mill m ³ /day	2.73							
MED Stand Alone	mill m ³ /day	1.57							
MED Cogeneration	mill m ³ /day	0.95							

From 2015 onwards, SWRO and MED stand alone desalination plants are optimized to meet the increasing desalination demand. The thermal energy required for the MED stand alone plants are provided through excess heat in the system. The excess heat may be generated from the gas turbines, internal combustion generators, municipal waste incinerators and power-to-gas units. Based on the availability of heat in the system and the cost of required heat generation, the model optimizes the water production from MED stand alone plants.

MSF standalone plants are not installed after 2015. This is due to the higher thermal consumption compared to MED stand alone plants, as highlighted in Table 1. Similar to the MED stand alone plants, the already installed MSF standalone capacities utilize heat from the energy system. Mehzer et al. [49] explain the dependence of the MSF water production costs on the fuel cost. The water production cost has been reported to be 1 USD/m³ for an oil price of 20 USD/barrel and 4 USD/m³ for an unsubsidized oil price of 100 USD/barrel. As a result of technological improvements and lower energy consumption, Mehzer et al. [49] discuss the potential for MED to substitute MSF in future desalination markets. MED and MSF cogeneration plants online by 2015 are powered through natural gas, and depending on the cost effectiveness, the cogeneration plants are run to produce water and electricity. Gradually, the MSF desalination plants and MED cogeneration plants are decommissioned based on lifetime.

It has to be noted that there are other desalination technologies with smaller scale applications such as vapor compression and electro-dialysis [49,50]. There are more technologies being researched and developed such as forward osmosis and membrane distillation [46]. Gude and Nirmalakhandan [50,51] have developed a desalination technology that utilizes low grade heat, at about 60 °C, coupled with thermal energy storage, to produced potable water continuously. Meanwhile Inoue et al. [52] and Arnau et al. [53] present a means to desalinate and transport seawater using the difference in seawater and inland temperature. In this study, however, only the seawater desalination technologies that have the largest market shares and used in large scale applications are considered.

The technical and financial parameters of the desalination technologies from 2015–2050 are presented in the Appendix A (Table A2). Similarly, the capex, opex and energy consumption of the water transportation and water storage are presented. There is no variation in the latter numbers from the time period 2015 to 2050.

The future capex of the desalination technologies and the corresponding energy consumption was estimated as follows:

2.4.1. SWRO

- 1. Using the Global Water Intelligence (GWI) Desal Database, the average capex of plants of the capacity range of 10,000 m³/day up to 50,000 m³/day, contracted in all years from 1980–2015, was found [47]. It is assumed that all the plants to be built in Saudi Arabia in the future, would have a capacity of 50,000 m³/day or higher. Then, the methodology discussed by Loutatidou et al. [54] to determine the EPC costs for SWRO desalination plants up to 2030 was utilized. In our study, this methodology was used to estimate the capex costs for SWRO plants of a capacity 50,000 m³/day from 2020 up to 2050. The average capex value for 2015 was estimated from the GWI Desal Database.
- 2. Al Zahrani et al. [55] illustrate the energy consumption of SWRO plants with hydraulic turbines for seawater of different salinity levels. For 35 parts per million (ppm) salinity level, the energy consumption is approximately 3.1 kWh/m³. Assuming that the other processes such as seawater intake, pretreatment, post-treatment and brine discharge take 1 kWh/m³, the total energy consumption is 4.1 kWh/m³. This is in line with a presentation [56] on the desalination plants in Masdar, UAE, where energy consumption of SWRO plants is estimated at 4.5 kWh/m³. However, test plants built recently have an energy consumption of 3.3 kWh/m³. These low energy consumption trends are also observed in recently built large SWRO plants such as Ghlalilah, in the United Arab Emirates [57]. The total energy consumption of this plant is estimated to

be just under 3 kWh/m³ [57]. However, the larger scale plants built recently use a pressure exchanger as the energy recovery device (ERD). For the purpose of our work, it is assumed that, after 2015, all SWRO plants will utilize pressure exchangers. According to Al Zahrani [55], the energy consumption with a pressure exchanger is about 2.6 kWh/m³. Thus, by 2020, it is assumed that the total energy consumption of the plants will drop to 3.6 kWh/m³. This is feasible as there are currently large scale plants with similar or lower energy consumption values. Meanwhile, Elimelech et al. [58] present the optimal energy consumption of the SWRO plants from 1970–2008. It is shown that the decrease in energy consumption between 2004 and 2008 is 5%. From 2020 onwards, there is assumed to be about a 5% decrease in energy consumption every 5 years. Elimelech et al. [58] explain that the practical minimum energy consumption of a SWRO plant with a 50% recovery rate and seawater salinity of 35 ppm, is 1.56 kWh/m³. Assuming 1 kWh/m³ for the other processes, the total minimum energy consumption is about 2.56 kWh/m³. Thus, by 2050, a total energy consumption of 2.6 kWh/m³ is assumed.

2.4.2. MED

- 1. Reddy et al. [59] and Al-Mutaz et al. [60] discuss the advantages of MED with thermal vapor compression (TVC) over MED without vapor compression. For our model, it was assumed that the MED plants installed are MED-TVC plants due to the lower thermal energy consumption and the recent growth in MED-TVC installations. A report by Fichtner explains that MED-TVC plants are approximately 25% higher in capex than SWRO plants [36]. Thus, for every time period, the capex of MED-TVC was assumed to be 25% more than the corresponding SWRO capex. Moser et al. [61] explain that operating costs of MED-TVC are usually 3–3.3% of the capex. For our study, the opex was taken to be 3.3% of the capex.
- 2. The average Gain Output Ratio (GOR) of MED-TVC plants in 2015 was obtained from the GWI Desal database [47]. Fath et al. illustrate how the GOR of MED plants will improve in the coming decades [62]. Palenzuela et al. [63] explain that the GOR of MED-TVC plants are generally 20% higher than MED plants. Thus, for this work, the GOR numbers presented by Fath et al. were increased by 20%. From 2040 to 2050 there is assumed to be no increase in the GOR.

The thermal energy consumption in kWh/m^3 is determined from the corresponding GOR. The electrical energy consumption is assumed to be $1.5 kWh/m^3$ for all the years as found in Fath et al. [62].

2.4.3. MSF

- 1. The MSF capex number for 2015 is obtained as an average of all MSF plants built in 2015 [47]. The general value of the GOR is about 8 for MSF plants located in Saudi Arabia, based on the GWI Desal Database.
- 2. It is assumed that all cogeneration plants in KSA are a combination of a MSF desalination plant and OCGT—unfired with Heat Recovery Generator System (HRGS) [37].
- 3. The power-to-water ratio (PWR) is specific for cogeneration plants and indicate the amount of power produced per m³ of water produced a day. For MSF plants with an OCGT power plant and HRGS, this is about 2.25 kW/(m³·d) [37]. The profits gained through the electricity produced by the cogeneration plants are used to offset the input gas costs. This applies to both the MSF and MED cogeneration plants.

The water production cost presented in this research takes into account the water transportation costs. In [24], we determined the 2030 desalination demand for the whole world on a $0.45^{\circ} \times 0.45^{\circ}$ spatial resolution. In addition, we found the optimized vertical and horizontal water transportation distances for every desalination demand node. The optimized horizontal distance is the shortest distance from the desalination demand node to the coast line. The vertical height is the elevation between the desalination demand node and the optimized location on the coast line. The same

procedure was used to determine the desalination demand as well as optimized horizontal and vertical transportation distances, for every 5 year time step from 2015 to 2050, for Saudi Arabia.

For the current transition study we used the total desalination demand for every 5 year time step and the corresponding weighted average horizontal and vertical transportation distance. Table 9 illustrates the optimized horizontal and vertical distances for Saudi Arabia.

 Table 9. Weighted average horizontal and vertical water pumping distances.

	Unit	2015	2020	2025	2030	2035	2040	2045	2050
Horizontal distance	km	280	273	269	265	266	267	268	269
Vertical distance	m	711	721	729	736	743	749	754	758

2.5. Synthetic Natural Gas Production—Technical and Financial Assumptions

Figure 6 illustrates the expected growth in non-energy industrial gas demand in Saudi Arabia [64]. In our model the aim is to ensure that by 2050, the non-energy industrial gas demand is met from renewable energy. In 2015, the industrial gas demand is met with fossil natural gas. However, over time, PtG plants produce the SNG required. The increase in cost of fossil natural gas over time and the decrease in cost of PtG plants, makes it viable to produce SNG.

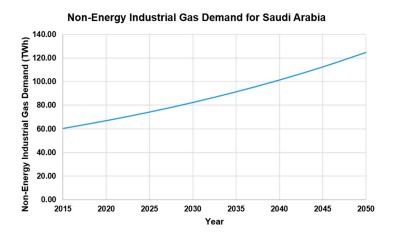


Figure 6. Industrial gas demand projection for Saudi Arabia from 2015 to 2050 [52].

3. Results

The following two scenarios are simulated by the model:

1. Non-integrated scenario

In this scenario, the model determines the optimal transition pathway for Saudi Arabia's power sector, discussed in Section 2.3, and the power plant capacities required for seawater desalination demand, discussed in Section 2.4. The gas sector is integrated with the power sector throughout from 2015 to 2050. Thus, the sum of the power plant capacities required for the three sectors present the total power capacities required to meet KSA's power, water and gas demands in the energy transition.

2. Integrated scenario

In this scenario, the seawater desalination demand and the gas demand are integrated into Saudi Arabia's power sector, throughout the transition from the fossil-based power system in 2015 up to a 100% renewable energy-based system in 2050. The desalination plants, integrated into the power system, will allow for the optimal use of the hourly energy produced by the renewable energy power plants. The excess energy produced by the renewable energy power plants can be stored as desalinated

water and, at times of low energy production, the stored water can be used. Thus, the desalination plants offer additional flexibility to the energy system.

The model determines the power capacities required for the integrated scenario and the two scenarios are compared to understand the impacts of the integrated desalination plants. The integration of the gas sector with the power sector in both scenarios, enables to identify the integration benefits, if any, of the desalination plants only.

In the following sections, the technical and financial results of the energy transition for the integrated scenario are presented. The financial results are ultimately compared with that of the non-integrated scenario to learn the impacts of integrated seawater desalination plants.

3.1. Integrated Scenario—Power Sector

Figure 7a presents the installed capacities of the different types of power plants required for the energy transition from 2015 up to 2050. The colors from top to bottom in the legend are shown from bottom to top in the figure. In 2015, the total power capacity was 66.4 GW, out of which 32.9 GW were internal combustion engines and 33 GW were gas turbines. The model is restricted from installing more fossil fuels thermal power plants after 2015 and can only install renewable technologies to meet the growing electricity demand. However, power-to-gas-based gas turbines are not restricted. Internal combustion generators are eliminated from the system by 2040 after exceeding their technical lifetime. Thermal power plants running on natural gas are also eliminated from the system by 2040. Power-to-gas-based electrolyser and methanation plants are used to produce synthetic natural gas (SNG) that is then used as fuel for existing open cycle gas turbines (OCGT) or combine cycle gas turbines (CCGT). The total capacity of all plants required by 2050 is about 600 GW. PV single-axis tracking accounts for 377 GW and wind power plants account for 83 GW of the 600 GW required by 2050. Figure 7b presents the electricity production of the different power plant categories. After 2030, electricity production from wind power plants remain constant at 217 TWh. The installed capacities of PV single-axis tracking continue to grow and start to dominate the Saudi power sector. By 2050, PV single-axis tacking contributes 922 TWh out of the total annual electricity generation of 1163 TWh, representing 79%. CSP plants for electricity generation are added from 2030 onwards but, by 2050, only account for 0.6% of the total electricity generation share. This is attributed to the higher costs of CSP for electricity generation compared to solar PV, based on the technical and financial assumptions in Appendix A (Table A1). Figure 7b also illustrates the diminishing use of fossil oil and gas in the energy system. The power capacities required for the energy transition can be found in the Appendix A (Table A4).

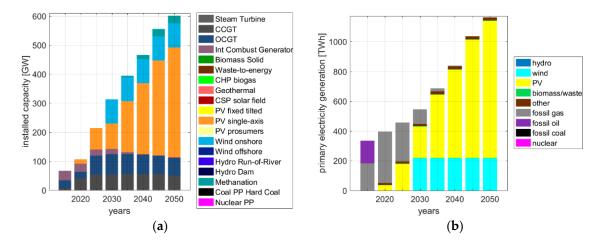


Figure 7. Installed capacities (**a**) and electricity produced (**b**) of the different power plants required from 2015 to 2050.

Figure 8a illustrates the full load hours (FLH) of the different power plants utilized by the model. The FLH of PV single-axis tracking, PV fixed tilted and wind onshore plants are constant at 2443, 1830 and 2618 h. The model determines the optimal FLH and the capacities of the power plants. The FLH of the internal combustion generator rapidly diminishes from 4625 to almost none by 2020. The high cost of oil renders the existing oil powered thermal power plants too expensive to run, since world market prices are taken into account to avoid subsidies for the energy system. In addition, the FLH of the OCGT reduces from 4756 FLH to zero FLH by 2030. The lower cost of the natural gas, in contrast to oil, still enables natural gas powered CCGT plants to be cost effective. However, after 2040, as shown in Figure 7b, there is no more contribution from natural gas powered thermal plants. The remaining CCGT plants are used with SNG to store and produce electricity as required in the Saudi power system.

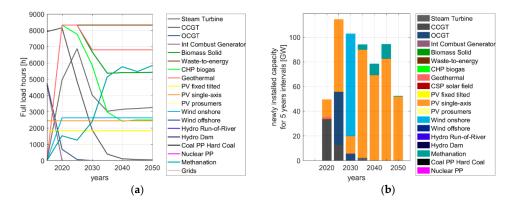


Figure 8. FLH variation of the different power plants used in model (**a**) and additional capacities of different power plants required from 2015 to 2050 (**b**).

Figure 8b represents the additional capacities of different power plants necessary to meet the growing electricity demand and to replace the fossil-based thermal power plants that are being phased out. Initially, there are more wind power plant installations than PV power plants. However, after 2030, the installation of wind power plants cease and PV single-axis tracking start to dominate the power sector. Methanation units are added for the first time in 2035, with additional capacities added until 2050, to meet the gas demands of the energy system and industrial gas demand through SNG.

Figure 9a represents the additionally installed storage capacities for every 5 years period. The large capacity of gas storage is required in 2045, and thereafter, less additional storage is required. Figure 9b represents the ratio of the total storage output for every time period. By 2025, electricity storage systems come into effect as it becomes a more cost effective option to balance the power system than the use of fossil powered thermal plants. By 2050, batteries provide a total output of about 413 TWh_{el} which accounts for about 41% of the total electricity demand and about 58% of the direct electricity supply.

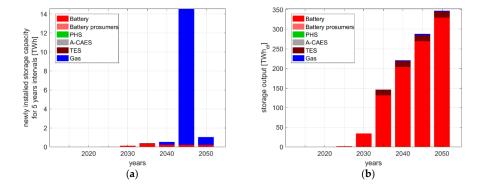


Figure 9. Additional storage capacity (a) and storage output (b) required from 2015 to 2050.

The total levelised cost of electricity of the system is the sum of the levelised cost of primary electricity generation (LCOE primary), levelised cost of storage (LCOS), levelised cost of curtailment (LCOC), fuel cost and the carbondioxide emission cost (CO₂ cost). Figure 10a represents the contribution of the different components to the total LCOE from 2015 to 2050. In 2015, the fuel cost accounts for the largest contribution due to the fuel prices of $52.50 \text{ €/MWh}_{\text{th}}$ for oil and $21.8 \text{ €/MWh}_{\text{th}}$ for gas. As the FLH of the fossil powered thermal plants decrease, as illustrated in Figure 8a, the fossil fuel consumption and consequently the contribution to the LCOE decreases. The OCGT storage and CCGT storage plants in Figure 8a refer to the gas plants utilising SNG.

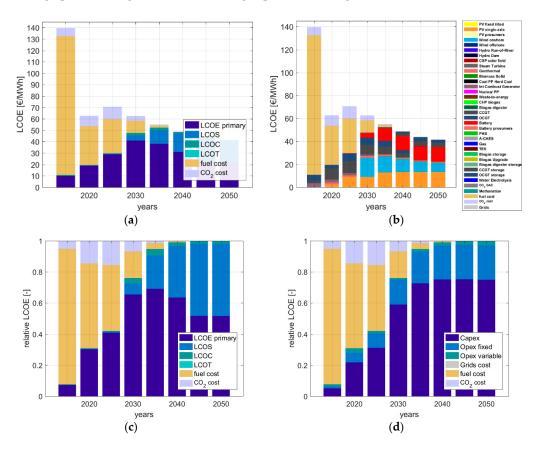


Figure 10. Contribution of different components (a), detailed contribution of components (b) relative contribution of different components (c) and relative contribution of financial components (d) to the total LCOE from 2015 to 2050.

The LCOC is as a result of curtailment of the excess energy produced by the renewable energy power plants. The remaining thermal power plants contribute to the CO₂ emissions cost. The batteries and gas storage contribute to the LCOS of the power system. The figure illustrates that with the transition to renewable power plants and the phasing out of the thermal powered plants, the total LCOE of the system decreases. By 2050, the LCOE is estimated to be about $41 \notin$ /MWh as opposed to $139 \notin$ /MWh in 2015. Figure 10b separates the LCOE primary and LCOS to the individual components and presents the specific contributions towards the LCOE. The rapid drop in LCOE from 2015 to 2020 is due to the phasing out of unsubsidized expensive oil power plants. This eliminates the large fuel cost that contribute towards the LCOE cost in 2015, as shown in Figure 10a,b. In 2020, the oil power plants are substituted by more economical solar PV and gas plants. By 2050, the largest contributors to the cost will be the PV single-axis tracking and battery plants. The contribution of wind decreases after 2030, due to no more wind plant installations and a highly competitive combination of hybrid PV-battery plants, as already found by Afanasyeva et al. for the case of Morocco [65]. However, there

is still a substantial contribution from wind to the LCOE in 2050 due to the large installed capacities of wind power plants in 2030.

Figure 10c presents the relative contribution of the different components to the LCOE. It can be seen that over time, the LCOE primary increasing accounts for the final LCOE. The relative contribution of the fossil fuel cost, and therefore also the CO₂ emission costs, disappear. From 2030 onwards, the relative contribution of the storage increases and ultimately by 2050, the LCOS and LCOE primary have almost equal contributions to the LCOE. This is also reflected in Figure 10d. Figure 10c presents the relative contribution of the financial components to the LCOE. In 2015, the fossil fuel costs determine the LCOE. As the fossil fuel usage diminishes, the total capex of the power system is the largest relative contributor to the LCOE. From 2040 onwards, when there is a 100% renewable energy system, the capex of the system contributes up to 75% of the LCOE. The fixed opex of the energy system components mostly account for the remainder of the LCOE.

Figure 11 illustrates the annual CO_2 emissions during the energy transition illustrated in the previous figures. The annual CO_2 emissions are reduced from about 250 Mton/a to 0 by 2040. The red line diagram represents the ratio of CO_2 emitted for every kWh of electricity produced. In 2015, this value is at about 800 g of CO_2 per kWh and drops to 0 by 2040. The CO_2 emission calculations are explained in [65].

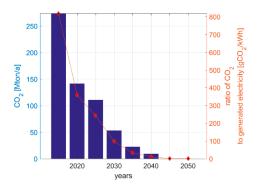


Figure 11. Annual CO₂ emissions during the energy transition and the ratio (blue bars) and CO₂ emissions per kWh of electricity produced (red line).

Figure 12 provides an overview of the gas sector after integration with the power sector. Figure 12a shows how the levelised cost of gas (LCOG) varies over time, while the non-energetic industrial gas demand increases. The LCOG increases from $23 \notin /MWh_{th}$ in 2015 to $95 \notin /MWh_{th}$ in 2045. After 2045, the LCOG decreases and by 2050, the LCOG is $90 \notin /MWh_{th}$. There is a steep increase in the LCOG from 2030 to 2035. This due to the production of SNG in 2035, as shown by Figure 12b. By 2040, the gas utilized in the system is fully renewable SNG.

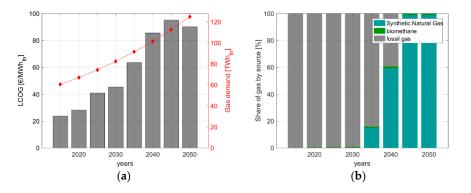


Figure 12. The increase in industrial gas demand (red line) and the variation in levelised cost of gas (LCOG) (grey bars) (**a**) and gas in the system by source (**b**) from 2015 to 2050.

3.2. Integrated Scenario—Desalination Sector

Figure 13 illustrates the growth of the Saudi Arabian desalination sector assumed in the model. The difference between the total water demand and the installed desalination capacity is met by renewable water sources and non-renewable groundwater sources. As explained in Section 2.4, the desalination demand increases to meet the growing total water demand and is met through SWRO and MED stand alone plants. The model optimizes the installed capacities of SWRO and MED depending on the electricity costs and availability of heat in the system.

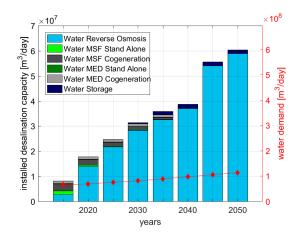


Figure 13. Water desalination capacities required to meet KSA's total water demand from 2015 to 2050.

The MSF and MED cogeneration plants are phased out based on the lifetime of the plants. By 2050, it is expected that there is a total water demand of 112 million m³/day and SWRO plants meet 52% of the total water demand. MED stand alone provides less than 1% of the total water demand. This is due to the lower excess heat available in the system. In addition, water storage is found to vary daily after 2020. Figure 14 illustrates the variation in water storage for the year 2030. Thus, the water storage acts a daily or seasonal storage optimizing the operation of the desalination plants. With the increase in SWRO desalination capacity there is an increase in water storage capacity.

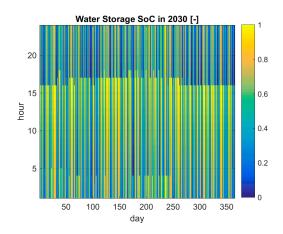


Figure 14. Water storage relative state of charge in 2030.

Figure 15a presents the capex breakdown of the desalination plant capacities installed for the 5 year intervals. The contribution of water transportation increases as the installed desalination capacities increase. By 2050, the transportation infrastructure is the largest contributor to the capex. The total capex required for the period from 2015 up to 2050 for the desalination sector is 1125 b \in .

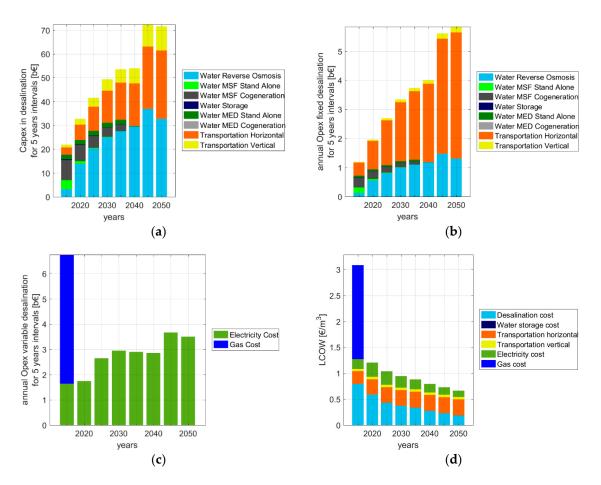


Figure 15. Capex of all desalination sector components (**a**), annual fixed opex for desalination sector components (**b**), annual variable opex for desalination sector components (**c**) and LCOW variation (**d**) from 2015 to 2030.

Figure 15b presents the variation in the annual fixed opex of the desalination capacities. With the increase in desalination capacities, the fixed opex increases. The fixed opex excludes the electricity consumption of the desalination plants and water transportation infrastructure. Figure 15c represents the variation in the annual variable opex. The annual variable opex accounts for both the gas and electricity consumption of the desalination plants. In 2015, due to the electricity produced by the cogeneration plants, there is no resulting electricity costs—the variable cost is finally the gas cost. The increase in the electricity cost maybe explained by the considerable increase in installed SWRO capacities with time and the variation in energy efficiency of the plants. There is only a minimal gas cost for existing cogeneration plants. SWRO and MED stand-alone plants utilize electrical energy and heat from the energy system as required.

Finally, Figure 15d illustrates the contribution of the different aspects of the desalination system to the final LCOW for every time period. The LCOW of the final system decreases from $3.29 \text{ }\text{e}/\text{m}^3$ in 2015, assuming non subsidized oil and gas prices, to $0.66 \text{ }\text{e}/\text{m}^3$ in 2050. The costs reduction is mainly due to the elimination of gas consumption and decrease in electricity costs, but also in an increase in the efficiency of RO and MED desalination plants in the decades to come.

Table 10 shows the energy consumption of the different desalination technologies during the transition. The total electricity consumption of the SWRO plants increase due to the high installed capacities. The MSF and MED cogeneration plants only produce water up to 2030 and then are decommissioned due to end of lifetime. The MED stand alone plants continue to produce water but at lower volumes than in 2015. This is because of the low availability of heat in the energy system.

	Unit	2015	2020	2025	2030	2035	2040	2045	2050
SWRO electricity cons	GWh	4496.5	22,622.5	29,622.5	37,033.8	40,996.5	45,209.6	64,212.8	63,011.9
MSF-S electricity cons	GWh	1386.8	0	0	0	6.5	0	0	0
MSF-C electricity cons	GWh	2153.8	0	0	0	0	0	0	0
MED-S electricity cons	GWh	114.6	0	0	0	19.4	0	0	0
MED-C electricity cons	GWh	689.2	0	0	0	0	0	0	0
MSF-S heat cons	GWh _{th}	47,151.0	0	0	0	219.4	0	0	0
MSF-C gas cons	GWh _{th}	174,456.5	0	0	0	0	0	0	0
MED-S heat cons	GWh _{th}	3898.6	2.3	1.9	4.7	309.8	1.7	1.5	4
MED-C gas cons	GWh _{th}	59 809.7	0	0	0	0	0	0	0

Table 10. Energy Consumption of the desalination technologies during the transition.

Table A4, in the Appendix A, summarises the key power capacities determined for the energy transition pathway for KSA from 2015 to 2050.

3.3. Comparison of the Integrated and Non-Integrated Scenarios

As discussed in Section 3, the model was run for a non-integrated scenario where the power capacities to meet the electricity demand and the desalinated water sector are found separately. To compare the integrated and non-integrated scenarios, the annual levelised cost for both scenarios from 2020 to 2050 was found. This is represented in Figure 16a. The annual levelised cost for the non-integrated scenario is higher than that for the integrated scenario. It is found that the approximate percentage benefit of the integrated scenario is between 1% and 3%, as a consequence of increased flexibility to the integrated energy system.

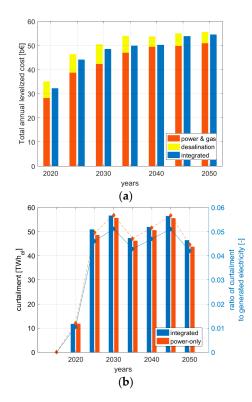


Figure 16. Comparison of total annual levelised cost (**a**) and the curtailed electricity (**b**) for the integrated and non-integrated scenarios.

Figure 16b illustrates the curtailment of electricity for the two scenarios, for the time period from 2015 to 2050. The bars represent the value of the energy curtailed and the dashed lines represent the ratio of the curtailed energy to the total generated electricity. It can be seen that there is more curtailed energy in the integrated scenario. However, the ratio of the curtailed energy to the total electricity

generated is lower in the integrated scenario. This can be attributed to the increased flexibility provided by the desalination plants and therefore better utilization of the hourly produced renewable energy, hence the integrated energy system can be run in a more efficient way than the separated systems.

It has to be mentioned that in the integrated scenario, for the total time period of 2015 to 2050, the power-to-gas (PtG) electrolyser capacity is reduced by 1%, compared to the separated scenario. For the integrated scenario, the PtG electrolyser capacity was estimated to be 73.6 GW_e, respectively. For the non-integrated scenario, the corresponding values was estimated to be 75.4 GW_e.

4. Discussion

The results show how the integration of seawater desalination with power and gas sectors contribute to the least cost transition path to achieving a 100% renewable energy sector in Saudi Arabia before the proposed year 2050.

Figure 7b illustrates that this milestone is feasible for Saudi Arabia by 2040. By 2040, PV single-axis tracking and wind power plants will dominate the Saudi power sector with 243 GW of the former and 83 GW of the latter. However, by 2050, due to the steeper decrease in the PV single-axis tracking and battery capex than the wind onshore plants, as presented in Figure 4c, it is more economical to have PV single-axis tracking as the dominant energy source in the power sector of Saudi Arabia. By 2050, about 377 GW of PV single-axis tracking are required while the capacities of wind power plants remain at 83 GW. Thus, there are no further installations in wind power plants after 2030. This result documents the outstanding impact of low cost solar PV supported by low cost battery storage that lead to a solar PV electricity generation share of 79%, which is significantly higher than the average of about 40% found in the global average assumptions for the year 2030 [25], but also higher than the 48% solar PV share for the MENA region [66]. However, comparable results had been found already earlier for the case of Israel [30], where the solar PV share had be found for cost optimized systems to about 90% of the total electricity supply. It has to be noted that Israel has less good wind conditions as in Saudi Arabia, and [30] was done for assumptions about the year 2030. Breyer et al. [41] discuss the significant role of solar photovoltaics, estimated to have an electricity generation share of 69% by 2050, in the global energy transition. The low cost for solar PV and battery storage can be explained by the standard experience curves in Figure 4 [67-69].

With the phasing out of fossil fueled thermal power plants, battery storage comes into play by 2025. By this time period, about 22% of the energy generation share is accounted for by fossil fueled thermal power plants. As the electricity demand increases and the share of renewables in the system increases, the battery storage required continues to increase. By 2050, batteries provide a total output of about 329 TWh_{el} accounting for approximately 40% of the total electricity demand. For a 100% RE scenario by 2040, the required battery storage output is 203 TWh_{el} accounting for approximately 32% of the total electricity demand. Between, 2025 and 2050, the battery full charge cycles required are between 300 and 330 cycles a year, indicating the almost daily usage of the battery capacity.

PtG plants come into effect in 2035 with 12 GW_{el} of input capacity and increases to 73 GW_{el} by 2050. Similarly, the FLH of the PtG plants increase from about 4313 h in 2035 to 4900 h by 2050. However, the gas storage output contributes about 2.3% towards the total electricity demand by 2050, significantly less than the 40% of batteries. The PtG plants also produce the SNG required to meet the industrial gas demand, as highlighted in Figure 12a.

The LCOE of the energy system is dominated by the high fuel cost in 2015. However, with the phasing out of the fossil powered thermal plants and the decreased consumption of fossil fuel, the LCOE of the energy system reduces from $139 \notin /MWh_{el}$ in 2015 to $43 \notin /MWh_{el}$ in 2040 and further to $41 \notin /MWh_{el}$ in 2050.

Figure 10c illustrates that by 2020 onwards, the dominating contributor to the LCOE is the LCOE_{primary}. With the increase in storage capacities, both the LCOE_{primary} and LCOS are the largest contributors to the system LCOE. Figure 9d further shows that by 2050, the largest contributors are PV single-axis tracking and battery storage. However, by 2040, there is still a significant contribution by

the existing wind power plants to the LCOE. This is in spite of the fact that new installations of wind power plants cease after 2030, due to the arising competitiveness of hybrid PV-battery plants.

Figure 13 presents the increasing desalination demand in the Kingdom of Saudi Arabia and the desalination capacities installed to meet the total water demand. The difference between the total water demand and desalination capacity is to be met through renewable water resources and some non-renewable ground water resources. SWRO and MED stand alone desalination plant capacities are optimized to meet the increasing desalination demand. The heat demand of the MED stand alone plants are met through the energy system. The existing MSF cogeneration and stand alone plants are phased out by 2035. After 2015, MSF stand alone plants are not allowed in the model due to the high thermal energy consumption. Similarly, MSF and MED cogeneration plants are not modelled due to the need for fossil powered gas plants. In an integrated scenario, the desalination capacities are used to better utilize the hourly renewable energy production of the power system. Figure 15 presents the variation in the average LCOW from $3.3 \notin/m^3$ in 2015 to $0.66 \notin/m^3$ in 2050.

The reduction in the LCOE of the system, contributes to the rapid decrease of the LCOW. The electricity costs for the desalination sector includes the energy consumption for water production at the desalination plant and transportation of water (vertical and horizontal transportation) to the demand site. By 2050, the transportation costs is the highest contributor to the LCOW followed by the desalination costs. Due to the low availability of heat losses in the system, there is a dominance of SWRO desalination plants which utilize no thermal energy.

To understand the impacts of integrating the desalination and power sectors in KSA, the LUT energy systems model was used to analyse both an integrated and non-integrated scenario. Thus, for the non-integrated scenario, the same desalination capacities are required, but they are not used to increase the flexibility of the power system. Figure 16a illustrates that the annualized levelised cost of the non-integrated scenario is higher than that of the integrated scenario for all time periods from 2020 to 2050. In fact, it is found that between 2040 and 2050, this reduction is between 1% and 3%, representing an annual cost decrease between 0.5 and 1.6 bn€. The lower cost is attributed to the reduced amounts of electricity storage, in the form of power-to-gas, required in the integrated scenario and the better utilization of the hourly renewable energy production.

Therefore, the above work presents a pathway for Saudi Arabia to transition to a 100% renewable energy power sector and shows that the integration of the country's power and desalination sectors provides the least cost solution for both sectors.

It may be argued that the current electricity production costs in Saudi Arabia are lower than what this research presents for 2015. However, the artificially low fossil fuel prices in Saudi Arabia are a result of the high subsidies which, according to Al-Iriani et al. [70], account for 10% of the country's GDP. As the energy consumption increases, the economic price the country has to pay increases. This is due to the heavily subsidized fuel prices that result in economic losses in the form of opportunity costs, since the export value of fuel would be much higher than the subsidized domestic consumption. With the decrease in oil prices and resulting revenue, as well as concerns about availability of fossil fuel resources to meet the country's growing energy demand, Saudi Arabia has started the transition to less or no subsidies. Thus, our work offers a solution for Saudi Arabia to meet its growing energy demands through renewable energy, without hindering the future economic growth of the country. In addition, as demonstrated in this work, KSA can meet its own industrial gas demands by exploiting the country's wealth of solar and wind resources.

This research also addresses how Saudi Arabia can meet the country's growing water demand through the use of 100% renewable energy powered SWRO desalination plants. The average LCOW of KSA is found to be $0.66 \text{ } \text{ /m}^3$ by 2050. This includes the cost for water desalination, water transportation to the demand site and water storage. Fthenakis et al. [71] estimated the current LCOW of a 190,000 m³/day SWRO plant, located in Al-Khajfi, on the east coast of KSA, powered by fixed-tilted PV to be $0.70 \text{ } \text{ /m}^3$. Current water production costs of fossil powered SWRO plants in KSA lie between

 $0.65 \notin /m^3 - 1.90 \notin /m^3$ [36]. However, this excludes the cost of transporting the desalinated water to the demand site and water storage.

There is a fast growing number of publications on 100% renewable energy-based energy systems [72], which helps to overcome the past concern that such systems would be neither technically feasible nor economically viable. This research on the case of Saudi Arabia is another confirmation of the high competitiveness of 100% RE systems. Recently Clack et al. [73] claimed that fossil-CCS and nuclear should be part of an energy system solution, which attracted stark criticism by Jacobson et al. [74]. One of the motivations for the critique was the fact that no single one of the about 60 existing articles on 100% RE systems had been mentioned in [73]. This reveals an imbalanced literature basement of the authors. Recent publications of IPCC researchers [75,76] also emphasize the substantial shares of renewable energy, and in particular on solar PV. Breyer et al. [41], recently presented an energy transition scenario for the world structured in 145 regions and simulated in full hourly resolution for the period 2015 to 2050 in 5 years steps. The research showed that 100% RE in the power system is possible, for lower global averaged cost than for the energy system of the year 2015. The energy transition has been further investigated by Ram et al. [77] who show that the transition also implies zero greenhouse gas emissions and a drastic increase in jobs in the power sector.

5. Conclusions

There is growing interest in the energy transition towards a 100% renewable energy-based power system in many countries and regions. Meanwhile, as the global renewable freshwater resource diminishes, seawater reverse osmosis desalination is expected to play a key role in securing future water supplies.

Saudi Arabia is the world's largest producer of crude oil and the 11th largest consumer. Economic growth of the country is tied closely to oil prices. To secure the country's economy, the government recently heralded a future without oil. The new vision calls for increase in renewable energy capacities and at least 9 GW of installed RE capacity by 2023. Saudi Arabia is also the largest producer of desalinated water in the world and desalination will remain vital to the country's future water supply.

The purpose of this research is to analyse the impact of integrating the large desalination demand into the country's 100% RE-based power system by 2050. The power sector is integrated with the non-energy industrial gas sector of Saudi Arabia. Thus, RE is used to produce SNG to satiate the industrial gas demands. The increasing desalination demand is met through SWRO and MED stand alone plants.

It is found that the integration of the power, gas sector and the desalinated water sector, allows for a reduction of 1–3% of the levelised annual costs, in comparison to the non-integrated scenario. The LCOE and LCOW for Saudi Arabia by 2050, in the integrated scenario, is estimated to be $41 \notin /MWh$ and $0.66 \notin /m^3$, respectively. By 2050, PV single-axis tracking dominates the power sector in Saudi Arabia with about 79% of total generated electricity due to the further reduction in capex of solar PV and supporting battery technology over wind power plants. In addition, SWRO plants produce most of the desalinated water required. MED stand alone plants contribute when there is sufficient heat available in the energy system. In future research, it is planned to integrate the heat sector into the model. This may lead to more free heat in the energy system resulting in an increase in the MED capacities installed. In the presence of cheap heat source, MED is favourable to SWRO due to its lower electricity consumption.

Thus, the results present a least cost transition path for Saudi Arabia to meet the country's future electricity and water demands through a 100% RE system.

However, there are gaps in the research methodology and data for Saudi Arabia that could be summarised as below:

1. Better understanding of the potential for geothermal and CSP heat use for MED desalination in Saudi Arabia.

2. No well-defined learning curve for SWRO desalination plants: This makes it difficult to project the future SWRO costs.

By filling in the gaps in our research, we can further refine our results and provide the optimal transition pathway for Saudi Arabia to finally start the country's future without oil. By capitalising on the country's excellent solar and wind resources through the implementation of renewable energy, Saudi Arabia can indeed meet the country's future electricity, water and gas demands in a lucrative manner.

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Nomenclature

а	annum
d	day
A-CAES	adiabatic compressed air storage
BWRO	brackish water reverse osmosis
Capex	capital expenditures
CCGT	combined cycle gas turbine
CSP	concentrating solar power
crf	capital recovery factor
GCC	Gulf Corporation Council
GOR	gain output ratio
GWI	global water intelligence
HRSG	heat recovery steam generator
IWPP	independent water and power project
KSA	Kingdom of Saudi Arabia
LCOC	levelised cost of curtailment
LCOE	levelised cost of electricity
LCOG	levelised cost of gas
LCOW	levelised cost of water
MSF	multi stage flash
MED	multi effect distillation
NWS	national water strategy
OCGT	open cycle gas turbine
Opex	operational expenditures
PtG	power-to-gas
PtH	power-to-heat
PV	photovoltaic
RE	renewable energy
SEC	specific energy consumption
SoC	state of charg
SNG	synthetic natural gas
SWRO	seawater reverse osmosis
WACC	weighted average cost of capital

Appendix A

Table A1. Technical and Financial Assumptions of all energy system components used in the energy transition from 2015 to 2050 for KSA. Assumptions are taken from Pleßmann et al. [78] and European Commission [79] and further references are individually mentioned.

Name of Component		Unit	2015	2020	2025	2030	2035	2040	2045	2050	Referenc
	Capex	€/kWp	1000	580	466	390	337	300	270	246	[80,81]
PV optimally tilted	Opex fix	€/(kWp·a)	15	13.2	11.8	10.6	9.6	8.8	8.0	7.4	
* 5	Opex var	€/(kŴh)	0	0	0	0	0	0	0	0	
	Lifetime	years	30	30	35	35	35	40	40	40	
	Capex	€/kWp	1150	638	513	429	371	330	297	271	[80,81]
PV single-axis tracking	Opex fix	€/(kWp·a)	17.3	15.0	13.0	12.0	11.0	10.0	9.0	8.0	
	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Lifetime	years	30	30	35	35	35	40	40	40	
	Capex	€/kW	1250	1150	1060	1000	965	940	915	900	[82]
Wind onshore	Opex fix	€/(kW·a)	25	23	21	20	19	19	18	18	
	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Lifetime	years	25	25	25	25	25	25	25	25	
	Capex	€/m ²	270	240	220	200	180	170	150	140	[83,84]
CSP (solar field, parabolic trough)	Opex fix	%	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	
	Opex var	-	0	0	0	0	0	0	0	0	
	Lifetime	years	25	25	25	25	30	30	30	30	
	Capex	€/kW	5250	4970	4720	4470	4245	4020	3815	3610	[79,85]
Geothermal	Opex fix	€/(kW·a)	80.0	80.0	80.0	80.0	80.0	80.0	80.0	80.0	
	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Lifetime	years	40	40	40	40	40	40	40	40	
	Capex	€/kW	800	685	500	380	340	310	280	260	[86,87]
Water electrolysis	Opex fix	€/(kW·a)	32	27	20	15	14	12	11	10	
	Opex var	€/(kWh)	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	
	Lifetime	years	30	30	30	30	30	30	30	30	
	Capex	€/kW	492	421	310	234	208	190	172	160	[86,87]
Methanation	Opex fix	€/(kW·a)	10	8	6	5	4	4	3	3	
	Opex var	€/(kWh)	0.0015	0.0015	0.0015	0.0015	0.0015	0.0015	0.0015	0.0015	
	Lifetime	years	30	30	30	30	30	30	30	30	
	Capex	€/kW	749	641	470	356	314	286	258	240	[86,87]
CO ₂ direct air capture	Opex fix	€/(kW·a)	29.9	25.6	18.8	14.2	12.6	11.4	10.3	9.6	
	Opex var	€/(kWh)	0.0013	0.0013	0.0013	0.0013	0.0013	0.0013	0.0013	0.0013	
	Lifetime	years	30	30	30	30	30	30	30	30	

Name of Component		Unit	2015	2020	2025	2030	2035	2040	2045	2050	Referen
	Capex	€/(kW _{el})	775	775	775	775	775	775	775	775	[88]
	Opex fix	€/(kW _{el} ·a)	19.4	19.4	19.4	19.4	19.4	19.4	19.4	19.4	
CCGT	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Efficiency	%	58	58	58	58	59	60	60	60	
	Lifetime	years	35	35	35	35	35	35	35	35	
	Capex	€/(kW _{el})	475	475	475	475	475	475	475	475	[88]
0007	Opex fix	€/(kW _{el} ·a)	14.25	14.25	14.25	14.25	14.25	14.25	14.25	14.25	
OCGT	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Efficiency	%	43	43	43	43	43	43	43	43	
	Lifetime	years	35	35	35	35	35	35	35	35	
	Capex	€/(kW _{el})	760	740	720	700	670	640	615	600	[88,89
Steam turbine (CSP)	Opex fix	€/(kW _{el} ·a)	15.2	14.8	14.4	14	13.4	12.8	12.3	12	
	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Efficiency	%	42	42	42	43	44	44	45	45	
	Lifetime	years	25	25	25	25	30	30	30	30	
Steam turbine (coal-fired PP)	Capex	€/(kW _{el})	1500	1500	1500	1500	1500	1500	1500	1500	[88,89
	Opex fix	€/(kW _{el} ·a)	20	20	20	20	20	20	20	20	
	Opex var		0	0	0	0	0	0	0	0	
	Efficiency	%	45	45	45	45	46	46	47	47	
	Lifetime	years	40	40	40	40	40	40	40	40	
	Capex	€/kW	3400	2900	2700	2500	2300	2200	2100	2000	
P: CUP	Opex fix	€/(kW·a)	238	203	189	175	161	154	147	140	
Biomass CHP	Opex var	€/(kWh)	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	
	Efficiency	%	36	37	40	43	45	47	47.5	48	
	Lifetime	years	30	30	30	30	30	30	30	30	
	Capex	€/kW	503	429	400	370	340	326	311	296	
Biogas CHP	Opex fix	€/(kW·a)	20.1	17.2	16.0	14.8	13.6	13.0	12.4	11.8	
biogas Crif	Opex var	€/(kWh)	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	
	Efficiency	%	35	36	39	42	44	46	46	47	
	Lifetime	years	30	30	30	30	30	30	30	30	
	Capex	€/kW	5940	5630	5440	5240	5030	4870	4690	4540	
Waste incinerator	Opex fix	€/(kW·a)	267.3	253.35	244.8	235.8	226.35	219.15	211.05	204.3	
waste incinerator	Opex var	€/(kWh)	0.0069	0.0069	0.0069	0.0069	0.0069	0.0069	0.0069	0.0069	
	Efficiency	%	27	31	32.5	34	35.5	37	29.5	42	
	Lifetime	years	30	30	30	30	30	30	30	30	

Table A1. Cont.

Name of Component		Unit	2015	2020	2025	2030	2035	2040	2045	2050	Reference
	Capex	€/kW	771	731	706	680	653	632	609	589	
Pierce disector	Opex fix	€/(kW·a)	30.8	29.2	28.2	27.2	26.1	25.3	24.3	23.6	
Biogas digester	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Efficiency	%	100	100	100	100	100	100	100	100	
	Lifetime	years	20	20	20	20	25	25	25	25	
	Capex	€/kW	340	290	270	250	230	220	210	200	[90]
Biogas upgrade	Opex fix	€/(kW·a)	27.2	23.2	21.6	20	18.4	17.6	16.8	16	
biogas upgrade	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Efficiency	%	98	98	98	98	98	98	98	98	
	Lifetime	years	20	20	20	20	25	25	25	25	
	Capex	€/(kWh _{el})	600	300	200	150	120	100	85	75	[91]
Battery, Li-ion	Opex fix	€/(kWh _{el} ·a)	24	12	8	6	4.8	4	3.4	3	
Dattery, Li-ton	Opex var	€/(kWh _{through}	pu()).0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	
	Efficiency	%	90	91	92	93	94	95	95	95	
	Lifetime	years	15	20	20	20	20	20	20	20	
	Capex	€/(kWh _{th})	50	40	30	30	20	20	20	20	
Thermal Energy Storage (TES)	Opex fix	€/(kWh _{th} ·a)	0.75	0.6	0.45	0.45	0.3	0.3	0.3	0.3	
	Opex var	€/(kWh _{through}	_{put}) 0	0	0	0	0	0	0	0	
	Lifetime	years	25	25	25	25	30	30	30	30	
	Capex	€/kWh	35.0	35.0	33.0	31.1	30.4	29.8	28.0	26.3	
Adiabatic compressed air energy	Opex fix	€/(kWh·a)	0.46	0.46	0.43	0.40	0.40	0.39	0.36	0.34	
storage (A-CAES)	Opex var	€/(kWh)	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	
~	Efficiency	%	54	59	65	70	70	70	70	70	
	Lifetime	years	40	55	55	55	55	55	55	55	
	Capex	€/kWh _{th}	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
Gas storage	Opex fix	€/(kWh·a)	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	
č	Opex var	€/(kWh)	0	0	0	0	0	0	0	0	
	Lifetime	years	50	50	50	50	50	50	50	50	

	Name of Component		2015	2020	2025	2030	2035	2040	2045	2050
	Capex	€/(m ³ ·day)	1150	960	835	725	630	550	480	415
Con Water Powerse Compasie	Opex fix	€/(m ³ ·day)	46	38	33	29	25	22	19	17
Sea Water Reverse Osmosis	Energy consumption	kWh/m ³	4.1	3.6	3.35	3.15	3	2.85	2.7	2.6
	Lifetime	years	25	25	30	30	30	30	30	30
	Capex	€/(m ³ ·day)	1437	1200	1043	906	787	687	600	519
Multi Effect Distillation—Thermal Vapor	Opex fix	€/(m ³ ·day)	10	13.2	15.6	18	21.6	24	24	24
Compression	Thermal energy consumption	kWh _{th} /m ³	68	51	44	38	32	28	28	28
for stand alone	Electrical energy consumption	kWh _{el} /m ³	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
	Lifetime	years	25	25	25	25	25	25	25	25
	Capex	€/(m ³ ·day)	1437	1437	1437	1437	1437	1437	1437	143
Multi Effect Distillation—Thermal Vapor	Opex fix	€/(m ³ ·day)	47.4	47.4	47.4	47.4	47.4	47.4	47.4	47.
Compression for cogeneration	Thermal energy consumption (Total gas input required for water and electricity)	kWh _{th} /m ³	168	168	168	168	168	168	168	16
	Electrical energy consumption	kWh _{el} /m ³	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
	Lifetime	vears	25	25	25	25	25	25	25	25
	Capex	€/(m ³ ·day)	2000	2000	2000	2000	2000	2000	2000	200
Multi Stage Flash	Opex fix	€/(m ³ ·day)	100	100	100	100	100	100	100	100
for cogeneration Gain Output Ratio: 8	Thermal energy consumption (Total gas input required for									
Power-to-Water: 2.25 kW/(m ³ ·day)	water and electricity)	kWh _{th} /m ³	202.5	202.5	202.5	202.5	202.5	202.5	202.5	202
	Electrical energy consumption	kWh _{el} /m ³	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
	Lifetime	years	25	25	25	25	25	25	25	25
Multi Stage Flash for stand alone Gain Output Ratio: 8	Capex	€/(m ³ ·day)	2000	2000	2000	2000	2000	2000	2000	200
	Opex fix	€/(m ³ ·day)	100	100	100	100	100	100	100	100
	Thermal energy consumption	kWh _{th} /m ³	85	85	85	85	85	85	85	85
	Electrical energy consumption	kWh _{el} /m ³	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
	Lifetime	years	25	25	25	25	25	25	25	25
	Water Tran	sportation								
Piping	Capex	€/(m ³ ·a·km)	0.053	0.053	0.053	0.053	0.053	0.053	0.053	0.05
	Fixed Opex	€/(m ³ ·a·100 km)	0.023	0.023	0.023	0.023	0.023	0.023	0.023	0.02
	Lifetime	years	30	30	30	30	30	30	30	30
Vertical Pumping	Capex	€/(m ³ ·h·m)	15.4	15.4	15.4	15.4	15.4	15.4	15.4	15.
	Fixed Opex	$\epsilon/(m^3 \cdot h \cdot m)$	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3
	Energy consumption	$kWh/(m^3 \cdot h \cdot 100)$	0.36	0.36	0.36	0.36	0.36	0.36	0.36	0.3
	Lifetime	m) years	30	30	30	30	30	30	30	30
Horizontal Pumping		€/(m ³ ·h·km)								
	Capex Fixed Opex	€/(m ³ ·h·km) €/(m ³ ·h·km)	19.26 0.4	19.2 0.4						
	1	$kWh/(m^3 \cdot h \cdot 100)$	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4
	Energy consumption	kwii/(iii//ii//100	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.0
	Lifetime	years	30	30	30	30	30	30	30	30
	Capex	€/m ³	65	65	65	65	65	65	65	65
Water Storage	Fixed Opex	€/m ³	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3
	Lifetime	vears	30	30	30	30	30	30	30	30

Table A2. Technical and financial parameters of the seawater desalination technologies from 2015–2050 [36,37,47,54–62].

Technology	Energy/Power Ratio (h)	Self-Discharge		
Battery	6	0		
TES	10	0.002		
A-CAES	100	0.001		
Gas Storage	80 imes 24	0		

Table A3. Energy to power ratio of the storage technologies.

Table A4. Key power capacities required for the energy transition pathway for KSA from 2015 to 2050.

Technology	Unit	2015	2020	2025	2030	2035	2040	2045	2050
PV single-axis tracking	GWp	0	14	73	87	174	243	326	378
PV optimally tilted	GWp	0.08	0.08	0.08	0.08	0.08	0.07	0.07	0.002
Wind power plants	GŴ	0	0	0	83	83	83	83	83
Geothermal	GW	0	1.6	1.7	2	2	2	2	2
Battery storage output	TWh	0	0	1.4	33.7	131	203	269	329
PtG electrolyser input	GWe	0	0	0	0	12	39	72	74
Gas Storage	TWh _{th}	0	0.002	0.002	0.003	0.005	0.5	15	16

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