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MHD Flow and Heat Transfer over Vertical Stretching Sheet with Heat Sink or Source Effect

Ibrahim M. Alarifi ¹, Ahmed G. Abokhalil ^{2,3}, M. Osman ^{1,4}, Liaquat Ali Lund ⁵, Mossaad Ben Ayed ^{6,7}, Hafedh Belmabrouk ^{8,9} and Iskander Tlili ^{1,*}

- ¹ Department of Mechanical and Industrial Engineering, College of Engineering, Majmaah University, Al-Majmaah 11952, Saudi Arabia; i.alarifi@mu.edu.sa (I.M.A.); m.othman@mu.edu.sa (M.O.)
- ² Department of Electrical Engineering, College of Engineering, Majmaah University, Al-Majmaah 11952, Saudi Arabia; a.abokhalil@mu.edu.sa
- ³ Electrical Engineering Department, Assiut University, Assiut 71515, Egypt
- ⁴ Mechanical Design Department, Faculty of Engineering Mataria, Helwan University, Cairo El-Mataria 11724, Egypt
- ⁵ Sindh Agriculture University, Tandojam Sindh 70060, Pakistan; balochliaqatali@gmail.com
- ⁶ Computer Science Department, College of Science and Humanities at Alghat, Majmaah University, Al-Majmaah 11952, Saudi Arabia; mm.ayed@mu.edu.sa
- ⁷ Computer and Embedded System Laboratory, Sfax University, Sfax 3011, Tunisia
- ⁸ Electronics and Microelectronics Laboratory, Faculty of Science of Monastir, University of Monastir, Monastir 5019, Tunisia; ha.belmabrouk@mu.edu.sa
- ⁹ Department of Physics, College of Science at Zulfi, Majmaah University, Al Zulfi 11932, Saudi Arabia
- * Correspondence: l.tlili@mu.edu.sa; Tel.: +96-650-910-7698

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Abstract: A steady laminar flow over a vertical stretching sheet with the existence of viscous dissipation, heat source/sink, and magnetic fields has been numerically inspected through a shooting scheme based Runge—Kutta–Fehlberg-integration algorithm. The governing equation and boundary layer balance are expressed and then converted into a nonlinear normal system of differential equations using suitable transformations. The impact of the physical parameters on the dimensionless velocity, temperature, the local Nusselt, and skin friction coefficient are described. Results show good agreement with recent researches. Findings reveal that the Nusselt number at the sheet surface augments, since the Hartmann number, stretching velocity ratio *A*, and Hartmann number *Ha* increase. Nevertheless, it reduces with respect to the heat generation/absorption coefficient δ .

Keywords: steady laminar flow; nanofluid; heat source/sink; magnetic field; stretching sheet

1. Introduction

The steady laminar flow and heat transfer of a viscous fluid over a vertical stretching sheet with the existence of heat source/sink and magnetic fields has gained significant interest because of its various usages in engineering procedures like geothermal energy extraction, glass fiber, and plasma studies, etc. Several researchers investigated numerically MHD mixed convective stagnation point flow lengthways a perpendicular widening piece in the presence of a heat source/sink in order to evaluate the impacts of relevant physical parameters especially Hartmann number, Stretching velocity ratio and Biot number on velocity and temperature profiles besides to skin friction and heat transfer properties. Using the Runge-Kutta-Fehlberg methods joined with shooting technique [1–4]. P.R. Sharma et al. [3] analyzed numerically the impacts of an external magnetic field. Tarek M. A. El-Mistikawy [5] focused on the flow resulting from a linearly stretching sheet with a transverse magnetic field. A. Mohammadeina et al. [1] investigated the impacts of thermal radiation and magnetic field on flow of CuO-water nanofluid past

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a stretching sheet characterized by forced-convection with a stagnation point with suction/injection. S.S. Ghadikolaei et al. [4] investigated the impact of thermal radiation and Joule heating. Wubshet Ibrahim [2] studied numerically the melting heat transfer and magneto hydrodynamic stagnation point flow of a nanofluid pasta extending piece.

Homotopy technique and shooting method have been widely used in many studies to obtain exact and wide-ranging analytic solution [6–9]. Arif Hussain et al. [6] focused on the thermal and physical properties of features of MHD hyperbolic refraction of fluid flow over a non-linear widening sheet taking into account convective boundary conditions and viscous dissipation. Tasawar Hayat et al. [9] studied convective stream of ferrofluid owing to nonlinear widening curved slip while M. N. Tufail et al. [7] analyzed numerically the heat transmission ended an unsteady widening sheet for an MHD Casson fluid through viscous dissipation impacts using the homotopy method. M. Y. Malik et al. [10] examined numerically an MHD flow of the Carreau fluid over a stretching sheet with inconstant thickness with the Keller box method. T.M. Agbaje et al. [11] proposed the spectral perturbation technique, which is a sequence development method which spreads the usage of the typical trepidation methods. When joined with the Chebyshev pseudo-spectral process, the SPM can provide higher order approximate mathematical resolutions for intricate increases faced in perturbation patterns. Siti Khuzaimah Soida et al. [12] analyzed numerically a stable MHD flow through a centrifugally widening or lessening floppy using the boundary value problem solver in Matlab software.

The temperature profile behavior was investigated by several researchers. U.S. Mahabaleshwar et al. [13] studied an MHD couple stress liquid caused by a perforated sheet experiencing lined widening with radiation. It was found that the temperature rises as the heat source/sink NI parameter and Chandrasekhar number Q augment [13]. M. Ferdows et al. [14] studied a steady two-dimensional free convective flow of a viscous incompressible fluid lengthways a perpendicular stretching sheet. The temperature profiles increase as the combined effect of porous diffusivity and magnetic field R, perturbation parameter increase. The temperature profile augments with the Eckert number Ec [15] and Biot number [6,13] and the magnetic field parameter, radiation and viscous dissipation [7,8,14–17]. In fact, when variable thickness exists, the radiative heat transfer and viscous dissipation enhance the nanofluid temperature [18]. When the unsteadiness of the stretching sheet extends, temperature rises [19]. The fluid temperature increases with increasing of Brownian motion, thermophoresis [20,21], temperature ratio [1] and heat source/sink parameter [3]. In the other hand, temperature drops when the Casson fluid parameter augments [7] and when the Prandtl number increases [13,20] and as the power law increases [6]. G.S. Seth et al. [19] reported that temperature is reduced when the stretching sheet is nonlinear. The fluid temperature declines with higher values of velocity ratio parameter, suction/injection parameter [1,16], Hartmann number Ha, Prandtl number Pr, thermal stratification parameter [18] or mixed convection parameter k [3]. Whereas, Kai-Long Hsiao [15] found that the temperature impact is improved in parallel with the rise of Prandtl number.

The impacts of significant factors on the solitary velocity for stretching sheet circumstance were discussed in many studies. Decrease in the velocity profile has been reported verses the increase of the Casson fluid parameter [7], non-linearity restriction, flow comportment index, the magnetic field, power law index and Weissenberg number [1,6–8]. However, the impacts of power law index and magnetic field parameter are more significant than nonlinearity parameter and Weissenberg number [6]. The dimensionless velocity is reduced when values of volume fraction and dimensionless velocity slip parameters augment [22]. It declines also when mass concentration parameter and permeability parameter augment [4]. Velocity profile is reduced by the combined effect of porous diffusivity [14], with the increase of Hartmann number and suction/injection parameter [23]. Greater values of suction and stretching parameter m and wall thickness parameter reduce velocity is improved in parallel with increase of velocity ratio, curvature parameter, electric field parameter and material parameter [4].

M. Ferdows et al. [14] reported that velocity profile is enhanced with the increase of the proportion of the flow velocity constraint to stretching sheet indicator and viscosity ratio. G.S. Seth et al. [24] reported that nanofluid velocity is reduced when the stretching sheet is nonlinear whereas when the unsteadiness of the stretching sheet augments velocity is decreased. M. N. Tufail et al. [7] found that as the unsteadiness parameter growths, the velocity decreases close the sheet and increases distant to the sheet. The higher of the slight order derivative causes the quicker velocity of viscoelastic fluids close the platter [25–32]. The temperature and velocity profile behavior was investigated by several researchers with the effect of heat generation/absorption on MHD flow though rare of them trait the effect of an external magnetic field and heat generation/absorption on mixed convictive flow lengthways a perpendicular extending piece [33–37].

An inclusive analysis of the works about nanofluids is presented by Wang et al. [19,20]. The inactivity point flow of a nanofluid near a stretching sheet has been explored by Khan and Pop [21], Mustafa et al. [22], Nazar et al. [23], and Ibrahim et al. [24]. Nadeem and Haq [29] inspected MHD three-dimensional flow of nanofluids past a shrinking sheet with thermal radiation. They employed Boungiorno model and considered the influences of thermophoresis and Brownian motion on the local Nusselt ad Sherwood numbers.

This study includes a numerically solution of MHD boundary layer flow over a vertical stretching sheet with company of heat sink/ source and magnetic fields effect. The governing equations for the problematic have been clearly described with some appropriate changes and then explained numerically via shooting arrangement based RKFI procedure. In this work the effects of relevant physical indicators essentially Hartmann number, Stretching velocity ratio and Biot number on velocity and temperature distributions in addition to the skin friction and heat transfer properties have been investigated. Comparison of the results with research results [3,26–30] shows a good agreement as shown in Table 1.

Pr	Ramchandran et al. [26]	Hassanien and Gorla [30]	Lok et al. [27]	Ishak et al. [28]	Ali et al. [29]	Sharma et al. [3]	Present
1	-	-	-	0.8708	0.8708	0.8707	0.87078
10	-	1.9446	-	1.9446	1.9448	1.94463	1.94465
20	2.4576	-	2.4577	2.4576	2.4579	2.4576	2.4577
40	3.1011	-	3.1023	3.1011	3.1017	3.1011	3.1015
60	3.5514	-	3.556	3.5514	3.5524	3.55142	3.55148
80	3.9055	-	3.9195	3.9095	3.9108	3.90949	3.90919
100	4.2116	4.2337	4.2289	4.2116	4.2133	4.21163	4.21135

Table 1. Numerical results of Nusselt number— $\theta(0)$ for diverse Prandtl number when A = 1, A = 0, Ha = 0, and $\delta = 0$.

2. Problem Description

The present study deals with a viscous incompressible fluid that was analyzed through steady laminar flow two-dimensional condition lengthways on an upright stretching sheet that was positioned in the *x* track and the y axis is perpendicular to the plan of this sheet.

u is the velocity component in x direction.

v is the velocity component in y direction.

Taking into consideration that mutually *c* then a are positive constants; $u = u_e(x) = ax$ represents the unrestricted stream velocity, while $u = u_w(x) = cx$ represents the velocity when there is stretching on the sheet.

When a heat source/sink is present, H_0 is an outside magnetic field that is practically perpendicular to the sheet.

The principal equations of continuity, momentum, and energy are written as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{dp}{dx} + v\frac{\partial^2 u}{\partial y^2} - \frac{\sigma\mu_e^2 H_0^2}{\rho}u + g\beta(T - T_\infty),$$
(2)

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{k}{\rho C_p}\frac{\partial^2 T}{\partial y^2}P + \frac{Q}{\rho C_p}(T - T_\infty),$$
(3)

where

 σ is the electrical conductivity,

 μ_e is the magnetic permeability,

 T_{∞} is the temperature of free stream,

g is acceleration due to gravity,

 β is the volumetric coefficient of thermal expansion,

k is the thermal conductivity,

 $v(=\mu/\rho)$ is the kinematic viscosity, and

 $T_w = T_\infty + bx$ is the temperature of the sheet.

When the superficial is heated b > 0 so that cfr4 whereas for cooled superficial b < 0 and $T_w \langle T_\infty$. The boundary conditions are

$$v = 0, \ u = u_w(x) = cx, \ -k\frac{\partial T}{\partial y} = h_f(T_f - T) \ at \ y = 0,$$

$$u = u_e(x) = ax, \ T = T_{\infty}asy \to \infty,$$

(4)

The forces will be in equilibrium because of the presence of the hydrostatic and magnetic pressure gradient, as mentioned below

$$-\frac{1}{\rho}\frac{dp}{dx} = u_e\frac{du_e}{dx} + \frac{\sigma\mu_e^2H_0^2}{\rho}u_e,$$
(5)

Therefore, the momentum equation turns into

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = u_e \frac{du_e}{dx} - \frac{\sigma \mu_e^2 H_0^2}{\rho} (u - u_e) + v\frac{\partial^2 u}{\partial y^2} + g\beta(T - T_\infty).$$
(6)

3. Scheme Analysis

The subsequent change and dimensionless quantities are used into equations, while taking into account the mentioned boundary condition (4) within the solution of Equations (1) to (3), Equation (7), obtained as:

$$\eta = \sqrt{\frac{a}{v}}y, = \psi = x\sqrt{av}f(\eta), \ \theta(\eta) = \frac{T - T_{\infty}}{T_w - T_{\infty}} \text{and} u = \frac{\partial\psi}{\partial y}, \ v = -\frac{\partial\psi}{\partial x}$$
(7)

Therefore, the equation of continuity is approved.

The momentum and energy equation becomes

$$f''' + ff'' - (f')^{2} + 1 + H_{a}^{2}(1 - f') + \lambda\theta = 0$$
(8)

$$\theta'' + P_r (f\theta' - f'\theta + \delta\theta) = 0 \tag{9}$$

where major represents the derivative according to η ,

 $Ha\left(=\mu_e H_0 \sqrt{\frac{\sigma}{\rho a}}\right) \text{ is the Hartmann number,}$ $\lambda\left(=\frac{Gr_x}{Re_x^2}\right) \text{ is mixed convection parameter,}$

 $Gr_x \left(=g\beta(T_w-T_\infty)\frac{x^3}{v^2}\right)$ is the local Grashof number, $\operatorname{Re}_{x}\left(=u_{e}(x)\frac{x}{v}\right)$ and $P_{r}\left(\frac{v}{x}\right)$, and $\delta\left(=\frac{Q}{\rho a C_p}\right)$ represent the factor of heat generation/absorption. The related boundary circumstances are limited to

$$f = 0, \ f' = c/a = A, \ \theta' = B(\theta - 1)at \ \eta = 0$$

$$f' = 1, \ \theta = 0as\eta \to \infty$$
 (10)

where $A(=\frac{c}{a})$ represent the rate of velocity

Also, $B = \frac{h_f}{k} \sqrt{\frac{v}{a}}$. Therefore, the Nusselt number and Skin friction are expressed by

$$C_f = \frac{2\tau_w}{\rho u_e^2} = \operatorname{Re}_x^{-1/2} f''(0), \ Nu_x = \frac{xq_w}{k(T_w - T_\infty)} = -\operatorname{Re}_x^{1/2} \theta'(0).$$
(11)

Additionally, respectively, the wall shear stress τ_w and the heat flux q_w are illustrated, as below:

$$\pi_w = \mu \left(\frac{\partial u}{\partial y}\right)_{y=0}, \ q_w = -k \left(\frac{\partial T}{\partial y}\right)_{y=0}$$

It is intricate to get the locked procedure explanations because calculations (8) and (9) are significantly nonlinear. Consequently, schemes are obtained by replacing

$$f = f_1, f' = f_2, f'' = f^3, f''' = f'_3, \theta' = f_5, \theta'' = f'_5$$

Thus, the scheme of calculations becomes

$$\begin{aligned} f_1' &= f_2, f_2' = f_3, f_3' = f_2^2 - f_1 f_3 - 1 + Ha^2 (f_2 - 1) - \lambda f_4 \\ f_4' &= f_5, f_5' = P_r (f_2 f_4 - f_1 f_5 - \delta f_4) \end{aligned}$$

Depending on the next conditions

$$f_1(0) = 0, f_2(0) = A, f_3(0) = s_1, f_4(0) = 1, f_5(0) = s_2 \text{ and } f_2(\infty) = 1, f_4(\infty) = 0$$

In order to obtain stage-by-stage integration and scheming, which are determined by relying on MATLAB software; the Runge–Kutta fourth order method with the shooting technique is actually used.

4. Stability Analysis

When there exists more than one solution in any fluid flow problem, the stability of solution is necessary to perform in that problem. In order to perform stability analysis, we adopt the algorithm of Merkin [33], Weidman et al. [36], and Rosca and Pop [37].

Step 1: To convert the governing Equations (2) and (3) of fluid flow in unsteady form, we have

$$\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{dP}{dx} + v\frac{\partial^2 u}{\partial y^2} - g\beta(T - T_\infty) - \frac{\sigma\mu_e H_0^2 u}{\rho}$$
(12)

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{k}{\rho C_p} \frac{\partial^2 T}{\partial y^2} + \frac{k}{\rho C_p} (T - T_\infty)$$
(13)

Step 2: To introduce a new non-dimensional time variable $\tau = a.t$, and all other similarity variables are also a function of τ , can be written as,

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$$\psi = x\sqrt{av}f(\eta,\tau); \eta = y\sqrt{\frac{a}{v}}; \theta(\eta,\tau) = \frac{(T-T_{\infty})}{(T_w - T_{\infty})};$$
(14)

Step 3: By applying Equation (14) on Equations (12) and (13), we have

$$\frac{\partial^3 f(\eta,\tau)}{\partial \eta^3} + f \frac{\partial^2 f(\eta,\tau)}{\partial \eta^2} - \left(\frac{\partial f(\eta,\tau)}{\partial \eta}\right)^2 + 1 + Ha^2 \left(1 - \frac{\partial f(\eta,\tau)}{\partial \eta}\right) - \lambda \theta(\eta,\tau) - \frac{\partial^2 f(\eta,\tau)}{\partial \tau \partial \eta} = 0$$
(15)

$$\frac{1}{Pr}\frac{\partial^2\theta(\eta,\tau)}{\partial\eta^2} + f(\eta,\tau)\frac{\partial\theta(\eta,\tau)}{\partial\eta} - \frac{\partial f(\eta,\tau)}{\partial\eta}\theta(\eta,\tau) + \delta\theta(\eta,\tau) - \frac{\partial\theta(\eta,\tau)}{\partial\tau} = 0$$
(16)

and the related boundary conditions are

$$f(0,\tau) = 0; \ \frac{\partial f(0,\tau)}{\partial \eta} = A; \ \frac{\partial \theta(0,\tau)}{\partial \eta} = B(\theta(0,\tau) - 1), \\ \frac{\partial f(\eta,\tau)}{\partial \eta} \to 1; \ \theta(\eta,\tau) \to 0 \ as \ \eta \to \infty$$
(17)

Step 4: To check the stability of steady flow solutions $f(\eta) = f_0(\eta)$ and $\theta(\eta) = \theta_0(\eta)$ will satisfy the basic model by introducing the following functions

$$f(\eta, \tau) = f_0(\eta) + e^{-\tau} F(\eta, \tau); \ \theta(\eta, \tau) = \theta_0(\eta) + e^{-\tau} G(\eta, \tau)$$
(18)

Here, $F(\eta, \tau)$, and $G(\eta, \tau)$ are small relative to $f_0(\eta)$, and $\theta_0(\eta)$. The unknown eigenvalue is γ , which is to be found out.

Step 5: By putting Equation (18) into Equations (15) and (16) and keeping $\tau = 0$, we have

$$F_0^{\prime\prime\prime} + f_0(\eta)F_0^{\prime\prime} + F_0f_0^{\prime\prime} - 2f_0^{\prime}F_0^{\prime} - \lambda G_0 - Ha^2F_0^{\prime} + \gamma F_0^{\prime} = 0$$
(19)

$$\frac{1}{Pr}G_0'' + f_0G_0' + F_0\theta_0' - f_0'G_0 - F_0'\theta_0 + \delta G_0 + \gamma G_0 = 0$$
⁽²⁰⁾

Along with boundary conditions

$$F_0(0) = 0, \ F'_0(0) = 0, \ G'_0(0) = BG_0$$

$$F'_0(\eta) \to 0, \ G_0(\eta) \to 0, \ as \ \eta \to \infty$$
(21)

Step 6: To relax one boundary condition into an initial condition, as suggested by Weidman et al. [36] and Harris et al. [34]. In this problem, we relaxed $G_0(\eta) \rightarrow 0$, as $\eta \rightarrow \infty$ into $G'_0((0) = 1$. We have to solve Equation (19) and (20) with boundary and relaxed initial condition in order to find the values of smallest eigenvalue γ .

It is worth mentioning that the negative values of γ indicate the growth of disturbance and the flow becomes unstable. On the other hand, if the values of γ are positive, which means that the flow is stable and shows an initial decay. The values of smallest eigenvalue are given in Table 2, which indicate that only first (second) solution is stable (unstable).

Table 2. Smallest eigenvalue γ when $\lambda = -0.2$, Pr = 1, A < 0 (for Shrinking surface) and A > 0 (for Stretching surface).

6	TT	γ	-	
ε	На	1st Solution	2nd Solution	
0.5	0.3	0.97533	-0.09572	
	0.5	0.65753	-0.06946	
-0.5	0	1.34857	-0.75392	
-	0.5	1.02349	-0.58327	

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The bvp4c solver function has performed stability analysis. According to Rahman et al. [35], "this collocation formula and the collocation polynomial provides a C^1 continuous solution that is fourth order accurate uniformly in [a,b]. Mesh selection and error control are based on the residual of the continuous solution". As we know, only the first solution is the stable and only the stable solution has physical meaning. In these regards, the various effect of different physical parameters on velocity and temperature profiles have been demonstrated for the first solution only. Finally, from Figure 1a,b, we draw some graphs in order to show the existence of multiple solutions for the opposing flow case.

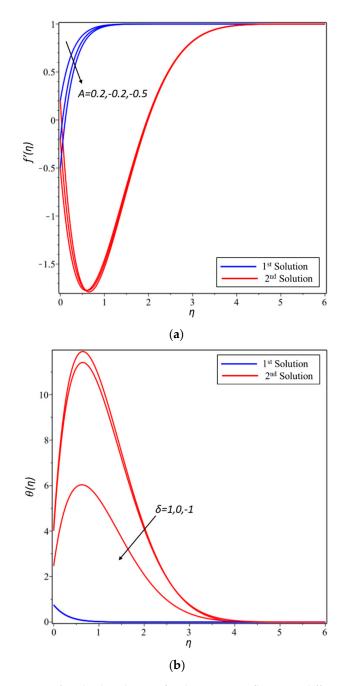


Figure 1. (a) The existence of multiple solutions for the opposing flow case different parameter *A*; and, (b) the existence of multiple solutions for the opposing flow case different parameter δ .

5. Results and Discussion

A steady laminar flow above a vertical stretching sheet with the existence of viscous dissipation, heat sink/source, and magnetic fields has been numerically explored by using of RKFI process through

shooting scheme. In this work, the effects of pertinent physical parameters are essentially Hartmann number, Stretching velocity ratio, and Biot number on temperature and velocity distributions; also, the skin friction and heat transfer properties have been examined.

The effect of Hartmann number on dimensionless velocity for mutually opposing and assisting flow are shown in Figure 2a,b respectively, with supplementary parameters are usually the regularly of velocity ratio parameter A = 1, Heat generation/absorption coefficient $\delta = 1$, Prandtl number Pr = 1, and Biot number $B_i = 1$. It is perceived that, for assisting flow ($\lambda > 0$), the dimensionless velocity is the maximum at the superficial of the vertical stretching sheet and it increasingly reduces to the minimum value f' = 1 as it changes to gone after the superficial, while for opposing flow $(\lambda < 0)$, the dimensionless velocity is the lowest at the surface of the vertical stretching sheet and gradually increases to the maximum value f' = 1, as it changes away from the superficial, this effect is mathematically obvious in Equation (10). It is additional observed that the velocity profile decreases with the Hartmann number for the assisting flow, whereas, it increases with the Hartmann number for the opposing flow. Consequently, the hydrodynamic boundary layer thickness also depends upon Ha. It is well known that the Hartmann number represents the proportion of electromagnetic force to the viscous force, thus, in the case of assisting flow, increasing the Hartmann number means that electromagnetic force was enhanced when compared to viscous force, which in turn Lorentz force augments, then opposes the flow, and then reduces the velocity profile. Nonetheless, in the situation of opposing flow, there is a reverse effect of the Hartmann number on dimensionless velocity. It should be pointed out that, in the case of assisting flow, ($\lambda > 0$) means the heating of the fluid, therefore the thermal buoyancy forces were enhanced. It can be interpreted on this fact that the highest value of dimensionless velocity is near the stretched surface; however, for opposing flow ($\lambda > 0$), which means that the fluid is consequently cooled; the thermal buoyancy forces decreases and then we realize the lowest value of dimensionless velocity near the stretched surface. It is worthwhile to note that the velocity profile increases with the mixed convection parameter λ for mutually case opposing and assisting flow due to an increasing of the thermal buoyancy forces. It can be seen that, for buoyancy opposed ($\lambda < 0$, opposing), the velocity profile will be significantly affected.

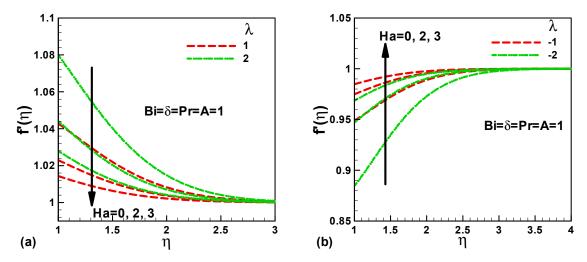


Figure 2. Variation of dimensionless velocity with Hartmann number for (**a**) assisting flow and (**b**) opposing flow.

Figure 3a,b, respectively, show the effects of stretching velocity ratio A when stretching in the flow and in the opposite direction, with further parameters sustaining the constant Heat generation/absorption coefficient $\delta = -1$, Prandtl number Pr = 1, Biot number $B_i = 1$, and Hartmann number Ha = 1. It can be seen that the velocity profile increases with stretching velocity ratio when stretching in the flow direction. Whereas, the velocity profile decreases with stretching velocity ratio when stretching in the opposite direction, this can be attributed to the significant enhancement

in pressure on the sheet. Furthermore, it is remarked that the velocity profile augment with mixed convection parameter λ for both stretching in the flow direction and stretching in the opposite direction, as proven in Figure 1. The physical reason behind this is that, by augmenting the mixed convection parameter, the thermal buoyancy forces rise and help to push the flow in y direction, which in turn increases the velocity profile.

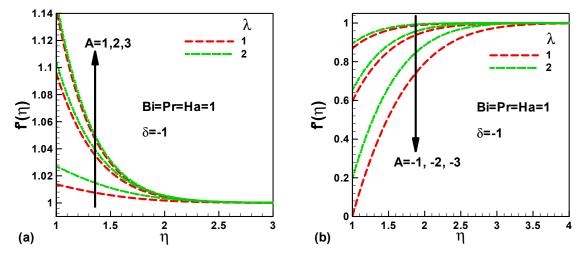


Figure 3. Variation of dimensionless velocity with stretching velocity ratio when (**a**) stretching in the flow direction and (**b**) stretching in the opposite direction.

The effects of Biot number in the presence of heat source on the dimensionless temperature for assisting and opposing flow are shown in Figure 4a,b, respectively at $P_r = H_a = A = 1$. It is clear that the temperature profile is greater at the stretching sheet surface and then exponentially lessens along the streamwise path up to the zero value for both assisting and opposing flow; this effect is proved and designated by the choice of boundary conditions and it is mathematically noticeable in Equation (10). It is worthwhile to note that the dimensionless temperature augment with both Biot number Bi and Heat generation/absorption coefficient δ for both case assisting and opposing flow; therefore, the thermal boundary layer thickness increases. It is well known that the Biot number signifies the proportion of heat convection to heat conduction; therefore increasing the Biot number leads to more heat will be released to the fluid flow, which in turn augments the temperature profile. Similarly, augmenting heat source leads to applying more heat to the fluid flow and it results in enhancing the dimensionless temperature.

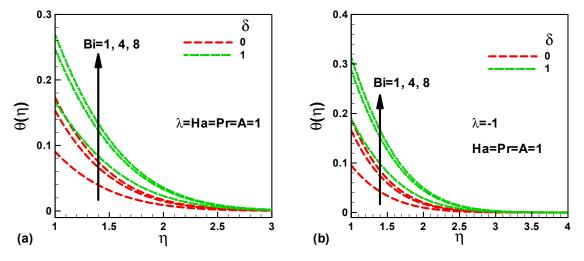


Figure 4. Variation of dimensionless temperature with Biot number in the presence of heat source for (a) assisting flow and (b) opposing flow.

Figure 5a,b, respectively, illustrate the result of Biot number in the company of heat sink on the dimensionless temperature for assisting and opposing flow at $P_r = H_a = A = 1$. As expected, the temperature profile satisfies the boundary conditions, starting with a higher value at the surface of the sheet and then meaningfully declining to zero value when η increases. Furthermore, it is remarked that dimensionless temperature increases with Biot number, even in the company of heat sink, as shown in Figure 3 in the circumstance of heat basis, so it can be concluded that the temperature profile increase with biot number independent of Heat generation/absorption coefficient δ . It should be pointed out that, for positive values of Heat generation/absorption coefficient, δ acts as a heat source, but for a negative value of Heat generation/absorption coefficient, δ acts as sink source, this signifies that the dimensionless temperature reduced in case of a negative value of δ (heat sink) when compared to a positive value of δ (heat source), as presented in Figure 3. Similarly, the thermal boundary layer thickness decreases.

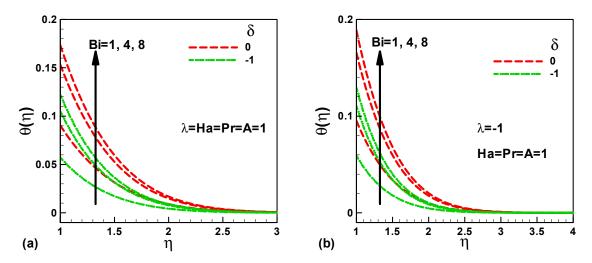


Figure 5. Variation of dimensionless temperature with Biot number in the presence of heat sink for (a) assisting flow and (b) opposing flow.

Figure 6a,b, respectively, display the effects of stretching velocity ratio and mixed convection parameter on dimensionless skin friction for both assisting and opposing flow. It is found that the skin friction increases with the mixed convection parameter and Hartmann number *Ha*, although it drops with the stretching velocity ratio for mutually opposing and assisting flow. This can be attributed to the result of velocity profile in the boundary layer and consequently disturbs the boundary layer thickness, as shown by Figures 1 and 2. On the other hand, the decreasing of skin friction with stretching velocity ratio can be associated to the augmentation of the velocity; therefore, the velocity boundary layer increases. It is well recognized that augmenting velocity means growing the Reynold number which in turn leads to lessening viscous force regarding inertial force, consequently the dropping in viscous force will reduce skin friction. It is valuable to mention that the effect of assisting flows on dimensionless skin friction is slightly more pronounced than that of opposing flow, because the pressure near to the surface is greater than not near to the surface. As observed, the skin friction continually and significantly increases with the Hartmann number, since it represents the ratio of electromagnetic force to the viscous force, therefore the magnetic field will increase and accordingly the Lorentz force will oppose and push the flow to the surface, which in turn augments the skin friction.

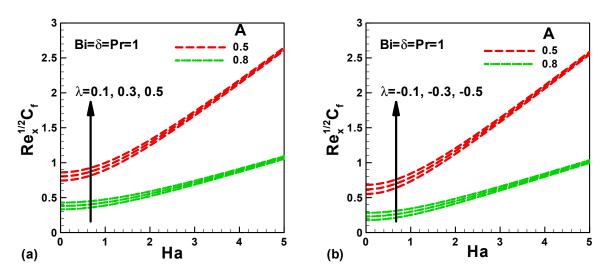


Figure 6. Variation of dimensionless skin friction with several parameters in the presence of heat source for (**a**) assisting flow and (**b**) opposing flow.

The effects of Biot number Bi, Heat generation/absorption coefficient δ , and mixed convection parameter λ on the dimensionless heat transfer rate for both assisting and opposing flow are illustrated, respectively, in Figure 7a,b. It is indicates that the dimensionless heat transfer rate increase with the Biot number and mixed convection parameter; whereas, it decreases with heat generation/absorption coefficient for both assisting and opposing flow. Physically, this can be attributed to the increase of temperature gradient with respect to the Biot number and mixed convection parameter, as presented by Figures 3 and 4. However, in an unexpected and perplexing result, it can be seen that the dimensionless heat transfer rate decrease with heat generation/absorption coefficient δ , it is well known that Nusselt numbers represent the proportion of convection to conduction heat transfer and in both situation assisting and opposing flow the effect of heat generation/absorption coefficient is more pronounced in conduction more than the convection heat transfer. It is clear that the effect of the mixed convection parameter on the heat transfer rate is slightly perceptible. Finally, the Nusselt number at the sheet surface augments, because the Hartmann number, stretching velocity ratio *A*, Hartmann number *Ha*, and mixed convection parameter λ increase. Though, it declines with respect to heat generation/absorption coefficient δ .

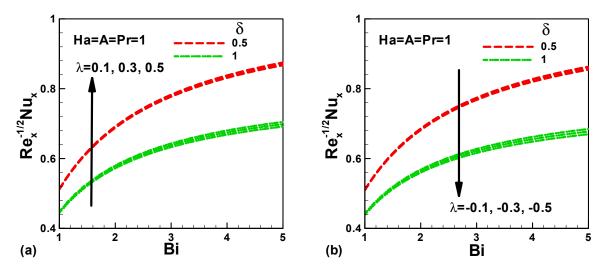


Figure 7. Variation of dimensionless heat transfer rate with several parameters in the presence of heat source for (**a**) assisting flow and (**b**) opposing flow.

6. Conclusions

A steady laminar flow over a vertical stretching sheet with the existence of viscous dissipation, heat source/sink, and magnetic fields has been mathematically explored through shooting arrangement based RKFI procedure. A comparison of the results with research results [3,26–29] demonstrates good agreement. The influence of relevant involved indicators on temperature and velocity, as well as the Nusselt number and skin friction coefficient are perceived. The main results that are enclosed in this work are concluded, as follows:

- 1. It is perceived that, for assisting flow ($\lambda > 0$), the dimensionless velocity is the maximum at the superficial of the vertical stretching sheet and it gradually lessens to the minimum value f' = 1, as it transfers to gone after the superficial, while for opposing flow ($\lambda < 0$), the dimensionless velocity is the lowest at the superficial of the vertical stretching sheet and gradually increases to the maximum value f' = 1.
- 2. The velocity profile augments with mixed convection parameter λ for both stretching in the flow direction and stretching in the opposite direction.
- 3. The temperature profile is greater at the stretching sheet superficial then exponentially lessens along the streamwise path up to the zero value for both assisting and opposing flow.
- 4. Skin friction increase with a mixed convection parameter and Hartmann number Ha, though it declines by stretching speed ratio for together opposing and assisting flow.
- 5. The effect of mixed convection parameter on the heat transfer rate is slightly perceptible. The Nusselt number at the sheet surface augments, because the Hartmann number, Hartmann number Ha, stretching velocity ratio *A*, and mixed convection parameter λ increase. Though, it declines according to heat generation/absorption coefficient δ .

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