



Article **Prediction of Thrust Force and Cutting Torque in Drilling Based on the Response Surface Methodology**

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Abstract: In this research, experimental studies were based on drilling with solid carbide tools and the material used was Al7075. The study primarily focused on investigating the effects of machining parameters (cutting speed, feed rate, diameter of the tool) on the thrust force (F_z) and the cutting torque (M_z) when drilling an Al7075 workpiece. The experimental data were analyzed using the response surface methodology (RSM) with an aim to identify the significant factors on the development of both the F_z and M_z . The application of the mathematical models provided favorable results with an accuracy of 3.4% and 4.7%, for the F_z and the M_z , respectively. Analysis of variance (ANOVA) was applied in order to examine the effectiveness of the model, and both mathematical models were established and validated. The equations derived proved to be very precise when a set of validation tests were executed. The importance of the factors' influence over the responses was also presented. Both the diameter of the cutting and the feed rate were found to be the factors of high significance, while cutting speed did not affect considerably the F_z and M_z in the experiments performed.

Keywords: Al7075; thrust force; cutting torque; response surface methodology

1. Introduction

A majority of products are directly or indirectly related to the metal cutting processes during their production processes. From the most commonly used processes, such as milling, turning, tapping and so forth, drilling constitutes the most commonly used. A significant number of holes are necessary for the assembly of different parts in order to be connected each other and develop the product itself.

Many researchers have developed empirical methodologies based on statistics, which can be used to learn the interactions between manufacturing factors. Response surface methodology (RSM) is one of the most widely used. RSM is a collection of an empirical modeling approach for defining the relationship between a set of manufacturing parameters and the responses. Different criteria are used and the significance of these manufacturing parameters on the coupled responses are examined. This methodology uses a number of techniques based on statistics, graphics, and mathematics, for both improving and optimizing a manufacturing process. Kumar and Singh [1] used ANOVA to investigate the material removal rate (MRR) and surface roughness of optical glass BK-7, which was drilled by a rotary ultrasonic machine. A number of manufacturing parameter combinations were used in order to effectively investigate the drilling process itself. The experimental process showed that the most

influential factor was the feed rate, while the developed prediction models kept the error within 5% at a 95% confidence level. RSM was used by Balaji et al. [2] on the drilling process of Ti-6Al-4V alloy. Drilling parameters (i.e., spindle speed, helix angle, feed rate) were tested and the surface roughness, flank wear, and acceleration of drill vibration velocity (ADVV) were measured. A multi-response optimization was performed with a view to optimize the drilling parameters for minimizing the output in each case (surface roughness, flank wear, ADVV). Similarly, Balaji et al. [3] investigated the effects of helix angle, spindle speed, and feed rate on surface roughness, flank wear, and ADVV during the drilling process of AISI 304 steel with twist drill tools. The significant parameters were retrieved based on the RSM, while the optimum drilling parameters were identified based on a multi-response surface optimization method.

Furthermore, Nanda et al. [4] used RSM to measure the responses, such as material removal rate (MRR), surface roughness, and flaring diameter, with the three input parameters—pressure, nozzle tip distance, and abrasive grain size—on a borosilicate-glass workpiece with zircon abrasives. Boyacı et al. [5] developed a fuzzy mathematical model using a multi-response surface methodology based on the drilling process of PVC samples in an upright drill. Cutting parameters, such as cutting speed, feed rate, and material thickness, were tested for the minimization of surface roughness and cutting forces. RSM was also used by Ramesh and Gopinath [6] during drilling of sisal-glass fiber reinforced polymer composites to predict the influence of cutting parameters on thrust force. The adequacy of the models was checked using the analysis of variance (ANOVA). The results showed that the feed rate was the most influencing parameter on the thrust force, followed by the spindle and the drill diameter. Jenarthanan et al. [7] developed a mathematical model in order to predict how the input parameters (tool diameter, spindle speed, and feed rate) influence the output response (delamination) in machining of the ARALL composite using different cutting conditions. RSM was used for the analysis of the influences of entire individual input machining parameters on the delamination.

Rajamurugan et al. [8] developed empirical relationships to model thrust force in the drilling of GFRP composites by a multifaceted drill bit. The empirical relationships were developed by the response surface methodology, incorporating cutting parameters such as spindle speed (N), feed rate (f), drill diameter (d), and fiber orientation angle (q). The result was that the developed model can be effectively used to predict the thrust force in drilling of GFRP composites within the factors and their limits of the study. Rajkumar et al. [9] used RSM to predict the input factors influencing the delamination and thrust force on drilled surfaces of carbon-fiber reinforced polymer composite at different cutting conditions with the chosen range of 95% confidence intervals. Ankalagi et al. [10] used response surface methodology to analyze the machinability and hole quality characteristics in the drilling of SA182 steel with an HSS drill. They investigated the effects of machining parameters, such as cutting speed, feed rate, and point angle, on (a) thrust force, (b) specific cutting coefficient, (c) surface roughness, and (d) circularity error. The experimental methodology showed that thrust force, specific cutting coefficient, and surface roughness decrease with the increase in cutting speed, whereas the circularity error increases with increased cutting speed and feed, on micro-EDM drilling process parameters. Natarajan et al. [11] analyzed the effect of the manufacturing parameters (i.e., feed rate, capacitance, voltage) on machining a stainless-steel shim with a tungsten electrode. In all cases, the surface roughness, the MRR, and tool wear were measured. RSM helped the development of statistical models for multi-response optimization, based on the desirability function with an aim to determine the optimum manufacturing parameters. Finally, Kyratsis et al. [12] investigated the relationship of three manufacturing parameters (diameter of the tools, cutting speed, feed rate) on the cutting forces developed when drilling an Al7075 workpiece. The response surface methodology was the main tool for establishing the appropriate mathematical prediction models.

This paper presents a study of the Al7075 drilling process when using solid carbide tools with different diameters. A series of appropriately selected cutting speeds and feed rates were applied and different mathematical models for the prediction of the thrust force (F_z) and the cutting torque (M_z) were calculated. Analysis of variance (ANOVA) was used in order to validate the adequacy of the

mathematical models and depict the significance of the manufacturing parameters. The novelty of this work is the development of mathematical models that can be used with high levels of confidence in order to predict the thrust force and torque expected during the drilling of Al7075, within a wide range of cutting parameters (cutting speed 50~150 m/min, feed rate 0.15~0.25 mm/rev). The optimum usage of cutting tools is something crucial for CNC users as it can affect the whole machining process.

2. Materials and Methods

2.1. Selection of Materials

Nowadays, the metal cutting process is a very important issue for the manufacturing sector. Al7075 is an aluminum alloy having zinc as the main alloying element. Due to its excellent properties (strength, density, thermal behavior), it is widely used in the manufacturing industry for vehicles. In addition, it provides the sector of aviation with a lighter, stronger aluminum component, as well as enabling safer, lighter, and more fuel-efficient vehicles. Furthermore, its ability to be highly polished makes it suitable for the mold tool manufacturing industry. The aforementioned reasons have led a number of researchers to focus their studies on these factors [13–15]. In this study, an Al7075 plate (150 mm \times 150 mm \times 15 mm) was selected for performing the experimental work. The material's mechanical properties and chemical composition is depicted in Table 1.

			Mech	anical I	Properties				
Young's Modulus	Der	nsity	Hardness, HV Yield Strength		Tensile Strength	Thermal Conductivity			
72 GPa	2800 l	kg/m ³	173	3	503 N	ЛРа	572 MPa	130 V	N/m-K
Chemical Composition									
Elements	Zn	Mg	Cu	Cr	Fe	Si	Mn	Ti	Al
Percentage	6	3	2	0.3	0.6	0.5	0.4	0.3	Balance

 Table 1. Mechanical properties and chemical composition of Al7075.

2.2. Response Surface Methodology

RSM is a popular method for deriving mathematical models of manufacturing systems, based on the principles of statistics. The same method can be the basis for applying optimization as well. The input parameters are identified together with their value ranges in the application under study. Then, the experimental process is set. Finally, mathematical models are calculated for the responses measured in each case. The effects of all input parameters and their interactions on the response are analyzed and their importance is derived. Different statistical methodologies (i.e., analysis of means and variances) are developed in order to establish the accuracy and adequacy of the derived mathematical model.

2.3. Experimental Details

In this research, an Al7075 block was used as a stock material. A HAAS VF1 CNC machining center was used to perform all the drilling tests. The machining center is able to perform with continuous speed and feed control within its operational limits. During the tests, three cutting speeds (V) and three feed rates (f) were applied in combination with three cutting tools' diameters (D). Table 2 depicts the factors used in this research together with their levels.

Factors	Notation	Levels			
Tactors	INOLALIOII	Ι	II	III	
Cutting speed (m/min)	V	50	100	150	
Feed rate (mm/rev)	f	0.15	0.2	0.25	
Tool diameters (mm)	D	8	10	12	

Table 2. Machining factors and their levels.

A mechanical vise was used for clamping the workpiece and a Weldon clamping device with high rigidity was used to clamp the drill. The type of cutting fluid was KOOLRite 2270 which was provided by the delivery system near to the cutting tool. A Kistler dynamometer type 9123 (capable of measuring four components at the same time) measured the thrust force (F_z) and torque (M_z) values in each case of a set of twenty-seven experiments, which were executed by using 27 different (one tool for each hole) non-through coolant solid carbide drill tools (Kennametal B041A, flute helix angle of 30 degrees). All the possible combinations of the manufacturing parameters were used (cutting speed, feed rate, tool diameter). Figure 1 depicts the steps of the research conducted. The main shape of the cutting tools and all the dimension details are illustrated in Figure 2.

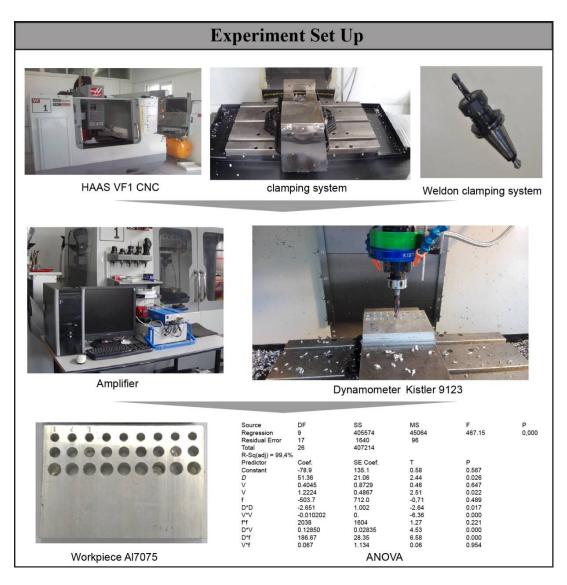


Figure 1. The workflow used for the research.

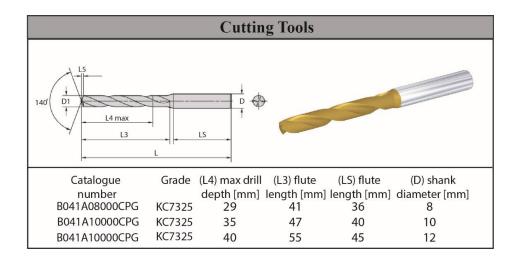


Figure 2. Cutting tool geometry details.

Figure 3 demonstrates a sample graph of the measurements of thrust force and cutting torque. As mentioned, Kistler 9123 dynamometer has been used to measure the thrust force and cutting torque during the drilling process. Dynoware software (type 2825D-02) was used in order to monitor and record the values through a three-channel charge amplifier with a data acquisition system. During the tests, the thrust force and cutting torque were displayed graphically on the computer monitor and analyzed, enabling early error detection, and ensuring a steady state condition. As the sampling rate was high (approximately 10 kHz), the mean value was used as the final data in order to secure the value accuracy. The thrust force and cutting torque monitoring was developed as a means of enhancing the process monitoring capabilities.

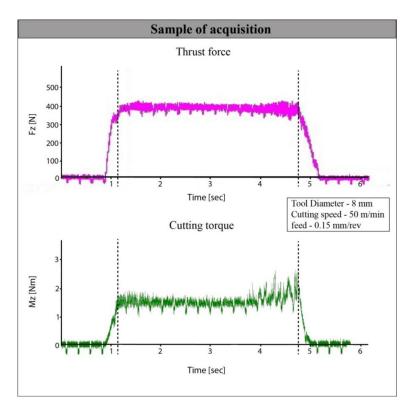


Figure 3. Experimental value (mean value) of thrust force and torque for a step drill with tool diameter of 8 mm, cutting speed of 50 m/min, and feed rate of 0.15 mm/rev.

Figure 4 illustrates all the experimental values derived from the dynamometer. It is obvious from the figure that when the diameter of the tool increases, both the F_z and M_z values increase. The same happens in the case of the feed rate. As the feed rate values increase, the F_z and the M_z increase, respectively. On the other hand, the different values of cutting speed do not noticeably affect their value in both cases.

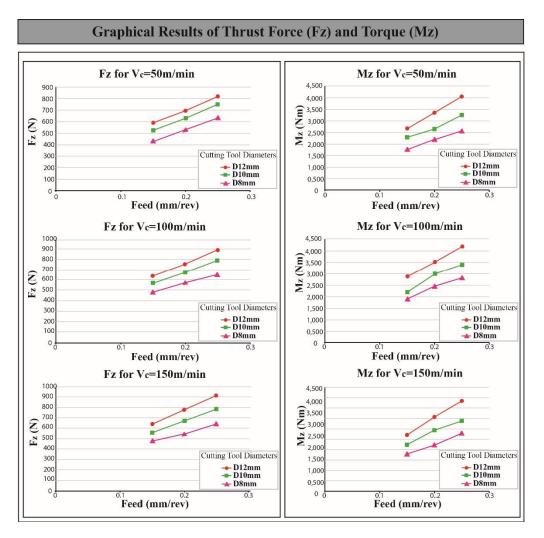


Figure 4. Experimental values derived from Kistler 9123.

3. Results

RSM was employed with a view to developing mathematical models for the F_z and the M_z in terms of cutting speed, feed rate, and cutting tool diameters. Least square fitting was used with the mathematical models in order to offer reliability. A full factorial strategy was applied and twenty-seven drilling experiments were performed, and both the F_z and M_z were modelled separately using polynomial mathematical models.

RSM-Based Predictive Models

The RSM is a precise tool used in order to examine the influence of a series of input variables on the response, when studying a complex phenomenon. The analysis of variance (ANOVA) was performed to check the adequacy and accuracy of the fitted models. MINITAB was used for the statistical analysis. The models produced used least square fitting and provided reliable mathematical modeling. The 2nd order nonlinear model with linear, quadratic, and interactive terms is indicated by the following equation:

$$Y = b_0 + b_1 X_1 + b_2 X_2 + b_3 X_3 + b_4 X_1^2 + b_5 X_2^2 + b_6 X_3^2 + b_7 X_1 X_2 + b_8 X_1 X_3 + b_9 X_2 X_3$$
(1)

where:

Y is the response,

 X_i stands for the coded values, and

 b_i stands for the model regression coefficients.

According to the experimental values derived from Kistler 9123 (Figure 2) and the aforementioned mathematical model, the following equations were derived for the thrust force (in N) and the cutting torque (in Nm) respectively:

$$F_z = -79 + 51.4D + 1.22V - 504f - 2.65D^2 - 0.0102V^2 + 2038f^2 + 0.128DV + 187Df + 0.07Vf(N)$$

and

$$M_z = 1.51 - 0.309D + 0.00236V + 1.06f + 0.016D^2 - 0.000037V^2 - 12.5f^2 + 0.000208DV + 1.33Df + 0.0213Vf(Nm)$$

where:

D is the diameter of the tool in mm,

f is the feed rate in mm/rev, and

V is the cutting speed in m/min.

The adequacy of the models is secured at a 0.05 level of significance. The validity of the developed models is proved by the use of ANOVA. The R-sq(adj) is very high in both cases (99.4% for the F_z and 98.9% for the M_z). In addition, when a 0.05 level of significance is used, the main contributors of the models are those with a *p*-value less than 0.05. In the case of the F_z , these contributors are: D (p = 0.026), V (p = 0.022), D^2 (p = 0.017), V^2 (p = 0.000), DxV (p = 0.000) and Dxf (p = 0.000), while in the case of the M_z the main contributors are: D^2 (p = 0.048), V^2 (p = 0.007), Dxf (p = 0.000), Vxf (p = 0.023).

The validity of the models is also proved from the values of *F* and *p*. They indicate the significance of the mathematical model. The quality of the entire mathematical model can be proved by the *F* value which considers all the manufacturing parameters at a time. The *p* value depicts the probability of the manufacturing parameters having insignificant effect on the response. A large *F* value signifies better fit of the mathematical model with the acquired data from the experiments. The derived values of F-ratio for the models of F_z and M_z (Tables 3 and 4) are calculated equal to 467.15 and 261.36, respectively. They are both higher than the standard tabulated values. A mathematical model is considered reliable when the *F* value is high and the *p*-value is low (below 0.05 at a 0.05 level of significance).

Figures 5 and 6 both depict the main effect and interaction plots for the F_z and M_z . In the interaction plot the interaction between diameter of the tool versus the cutting speed, and diameter of the tool versus the feed rate in all cases has been highlighted. As can be seen in Table 3, V^2 (p = 0.000), which implies that the square of the cutting speed affects the value of F_z and M_z . This is more obvious when observing the main effect plots for F_z and M_z where the three means of the V depict a second order shape, compared to the rest of the mean effects plots that form almost straight lines. The same happens in the case of the cutting torque.

Source	Degree of Freedom	Sum of Squares	Mean Square	<i>f</i> -Value	<i>p</i> -Value
Regression	9	405,574	45,064	467.15	0.000
Residual Error	17	1640	96		
Total	26	407,214			
R-Sq(adj) = 99.4%					
Predictor	Parameter Estimate Coefficient	Standard Error Coefficient	<i>t-</i> Valu	e	<i>p</i> -Value
Constant	-78.9	135.1	0.58		0.567
D	51.36	21.06	2.44		0.026
V	1.2224	0.4867	2.51		0.022
f	-503.7	712.0	-0.71		0.489
D*D	-2.651	1.002	-2.64		0.017
V^*V	-0.010202	0.	-6.36		0.000
f*f	2038	1604	1.27		0.221
D^*V	0.12850	0.02835	4.53		0.000
D*f	186.67	28.35	6.58		0.000
V*̂f	0.067	1.134	0.06		0.954

Table 3. ANOVA table for F_z (thrust force).

Table 4.	ANOVA	table for	M_z	(torque).
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Source	Degree of Freedom	Sum of Squares	Mean Square	<i>f</i> -Value	<i>p</i> -Value
Regression	9	12.7870	1.4208	261.36	0.000
Residual Error	17	0.0924	0.0054		
Total	26	12.8794			
R-Sq(adj) = 98.9%					
Predictor	Parameter Estimate Coefficient	Standard Error Coefficient	t-V	alue	<i>p</i> -Value
Constant	1.505	1.014	1.48		0.156
D	-0.3086	0.1581	_	1.95	0.068
V	V 0.002357		0.65		0.527
f	1.057	5.345	0	.20	0.846
D*D	0.016014	0.007525	2	.13	0.048
V^*V	-0.00003691	0.00001204	3	.07	0.007
f*f	-12.51	12.04	_	1.04	0.313
D^*V	0.0002075	0.0002128	0	.97	0.343
D*f	1.3317	0.2128	6	.26	0.000
V^*f	0.021300	0.008514	2	.50	0.023

Residual analysis was performed in order to test the models' accuracy in both cases. The result was that the residuals appear to be normally distributed. They follow the indicated straight lines (almost linear pattern) while at the same time they are distributed almost symmetrically around the zero residual value proving that the errors are normally distributed. For both cases, there is not considerable variation of the observed values around the fitted line. The discrepancy of a particular value from its predicted value is called the residual value. When the residuals around the regression line are small, it means that the mathematical model is of high accuracy. All the scatter diagrams of the F_z and M_z residual values versus the fitted values provide enough evidence that the residual values versus the order that the experiments were conducted (Figure 7). There is no evidence of any particular pattern in the residual values and, thus, the models proved their efficiency.

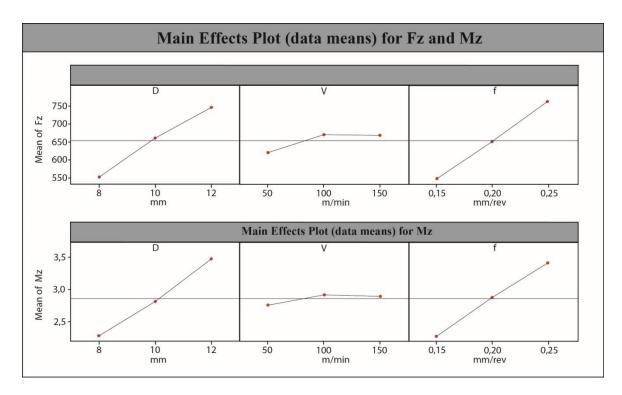


Figure 5. Main effects plot for F_z and M_z .

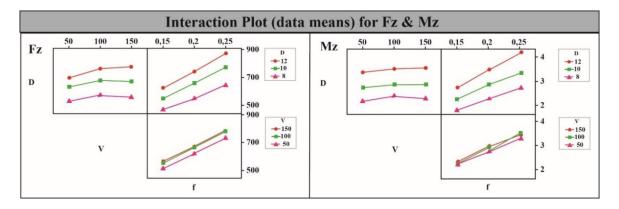


Figure 6. Interaction plot for F_z and M_z .

That is the characteristic of well suited mathematical modeling and reliable data derived from the equations provided. The derived mathematical models can be considered as very accurate and can be used directly for predicting both the F_z and the M_z within the limits of the manufacturing parameters used (diameter of tool, feed rate, cutting speed). The accuracy achieved is very high when comparing the measured values and those calculated from the mathematical models (3.4% and 4.7%, respectively).

A set of experiments was conducted with a view to validate the given mathematical models for the prediction of the F_z and M_z . Values of feed rate and cutting speed, within the range of experiments, were randomly selected (*V*: 70 m/min, *f*: 0.2 mm/rev) and tested with the three different cutting tools (*D*: 8-10-12 mm). The produced results can be considered satisfactory with less than 5.4% variation (Table 5). Especially, for the thrust force derived with the values (*D*: 10 mm, *V*: 70 m/min, *f*: 0.2 mm/rev), the variation was 0%.

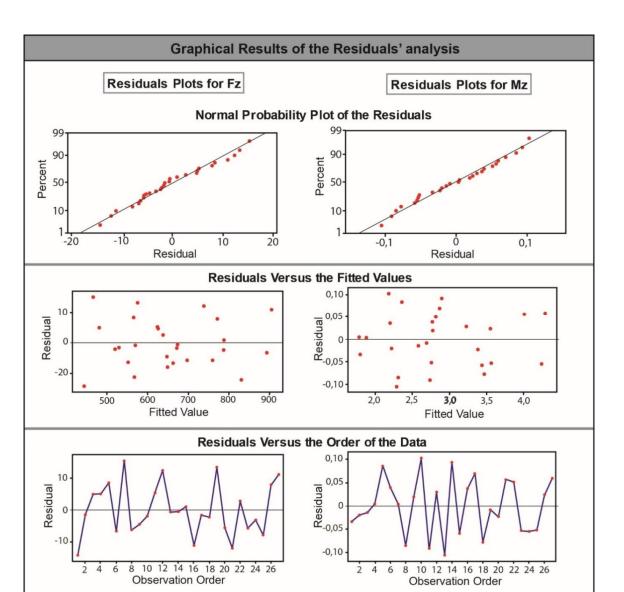


Figure 7. Residuals analyses for the F_z and M_z .

Table 5. Experimental confirmation.

Factors		<i>Fz</i> (N)	Mz (Nm)
D: 8 mm, V: 70 m/min f: 0.2 mm/rev	Predicted	707	1.899
	Exp. Result	692	1.855
Variation %		2.1%	2.4%
<i>D</i> : 10 mm, <i>V</i> : 70 m/min <i>f</i> : 0.2 mm/rev	Predicted	875	2795
	Exp. Result	875	2955
Variation %		0%	-5.4%
D: 12 mm, V: 70 m/min f: 0.2 mm/rev	Predicted	1060	4.129
	Exp. Result	1057	4.041
Variation %		0.3%	2.2%

4. Conclusions

The aim of this study was the generation of mathematical models for the prediction of the thrust force (F_z) and cutting torque (M_z) related to the diameter of the drilling tool and other crucial manufacturing parameters (feed rate, cutting speed) during the drilling process. Research shows clearly that the prediction models sufficiently explain the relationship between the thrust force and cutting torque with the independent variables. A full factorial experimental process was executed under different conditions of the aforementioned parameters using an Al7075 workpiece and a full set of solid carbide tools. Response surface methodology was used as the base for the prediction of both the F_z and the M_z in a series of drilling operations with Al7075 as the material under investigation. The developed models were considered as very accurate for the prediction of the F_z and M_z within the range of the manufacturing parameters used. The outcomes proved that when using these models, the accuracy achieved was 3.4% and 4.7%, respectively. People working with CNC machines very often are faced with dilemmas about which cutting parameters are the most appropriate for the available cutting tools in order to treat materials, such as aluminum alloy 7075, which is suitable for a variety of specific applications in aerospace and chemical industries. Prediction of the thrust force and the cutting torque can lead to higher productivity when selecting manufacturing parameters due to the reduced wear effect on the drilling tool and the related energy consumption.

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Conflicts of Interest: The authors declare no conflicts of interests

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