



# Article The Role of κ-Carbides as Hydrogen Traps in High-Mn Steels

Tobias A. Timmerscheidt <sup>1</sup>, Poulumi Dey <sup>2</sup>, Dimitri Bogdanovski <sup>1</sup>, Jörg von Appen <sup>1</sup>, Tilmann Hickel <sup>2</sup>, Jörg Neugebauer <sup>2</sup> and Richard Dronskowski <sup>1,3,\*</sup>

- <sup>1</sup> Institute of Inorganic Chemistry, Chair of Solid-State and Quantum Chemistry, RWTH Aachen University, 52056 Aachen, Germany; tobias@totim.de (T.A.T.); dimitri.bogdanovski@ac.rwth-aachen.de (D.B.); Joerg.vonAppen@zhv.rwth-aachen.de (J.v.A.)
- <sup>2</sup> Max-Planck-Institute for Iron Research GmbH, 40237 Düsseldorf, Germany; dey@mpie.de (P.D.); t.hickel@mpie.de (T.H.); j.neugebauer@mpie.de (J.N.)
- <sup>3</sup> Jülich-Aachen Research Alliance (JARA-HPC), RWTH Aachen University, 52056 Aachen, Germany
- \* Correspondence: drons@HAL9000.ac.rwth-aachen.de; Tel.: +49-241-809-3642; Fax: +49-241-809-2642

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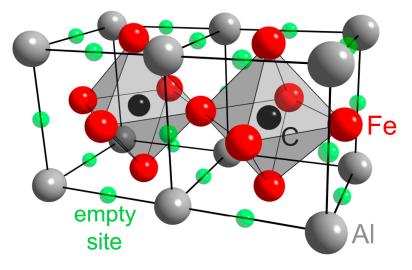
**Abstract:** Since the addition of Al to high-Mn steels is known to reduce their sensitivity to hydrogen-induced delayed fracture, we investigate possible trapping effects connected to the presence of Al in the grain interior employing density-functional theory (DFT). The role of Al-based precipitates is also investigated to understand the relevance of short-range ordering effects. So-called  $E2_1$ -Fe<sub>3</sub>AlC  $\kappa$ -carbides are frequently observed in Fe-Mn-Al-C alloys. Since H tends to occupy the same positions as C in these precipitates, the interaction and competition between both interstitials is also investigated via DFT-based simulations. While the individual H–H/C–H chemical interactions are generally repulsive, the tendency of interstitials to increase the lattice parameter can yield a net increase of the trapping capability. An increased Mn content is shown to enhance H trapping due to attractive short-range interactions. Favorable short-range ordering is expected to occur at the interface between an Fe matrix and the  $E2_1$ -Fe<sub>3</sub>AlC  $\kappa$ -carbides, which is identified as a particularly attractive trapping site for H. At the same time, accumulation of H at sites of this type is observed to yield decohesion of this interface, thereby promoting fracture formation. The interplay of these effects, evident in the trapping energies at various locations and dependent on the H concentration, can be expressed mathematically, resulting in a term that describes the hydrogen embrittlement.

**Keywords:** steel research; κ-carbides; short-range ordering; hydrogen trapping; hydrogen embrittlement; carbide-austenite interfaces; ab initio calculations; density-functional theory

# 1. Introduction

Fe-Mn-Al-C quaternary alloys form an important class of modern advanced high-strength steels (AHSS). Synthetic variations of the Mn, Al, and C contents accompanied by sophisticated steel-processing techniques have led to the availability of different phases and microstructures such as ferrite (body-centered cubic, bcc), martensite (body-centered tetragonal, bct), austenite (face-centered cubic, fcc), or a mixture of those as observed in dual-phase (ferrite/martensite), duplex (ferrite/austenite), or triplex (ferrite/austenite/carbide) steels. In particular, so-called high-Mn steels, comprising a broad spectrum of Fe-based alloys with Mn contents in the range of 20–30 wt % and Al and C contents in the ranges of 0–10 wt % and 0–2 wt %, respectively, have attracted attention [1]. These steels exhibit particular deformation mechanisms, such as transformation-induced plasticity (TRIP), twinning-induced plasticity (TWIP), or microband-induced plasticity (MBIP) [2], thereby yielding extraordinarily high strength and ductility. Steels containing considerable amounts of Al in addition to Mn have raised recent interest due to the precipitation of ordered carbides, both from

ferritic and austenitic matrices [1]. These  $\kappa$ -carbides have the stoichiometry Fe<sub>3</sub>AlC and crystallize in the perovskite structure type (also commonly labeled as  $E2_1$  or  $L1'_2$ ) as visualized in Figure 1. Such phases have been shown to have an additional strengthening effect on these steels [3–5].



**Figure 1.** Crystal structure of Fe<sub>3</sub>AlC, a  $\kappa$ -carbide crystallizing in the *E*2<sub>1</sub> type, shown as a 2  $\times$  1  $\times$  1 supercell. Grey, red, and black spheres denote Al, Fe, and C atoms, respectively. Green translucent spheres indicate the unoccupied octahedral sublattice sites.

A critical aspect with respect to the application of high-Mn steels is their large susceptibility to hydrogen-induced delayed fracture (HIDF) [6]. Hydrogen, which is in contact with steels during the production and/or the application process, may dissolve into the material, followed by migration and preferred enrichment in critical regions, such as grain boundaries or dislocations. As a consequence, local embrittlement occurs, which can finally lead to crack formation and propagation, resulting in eventual failure of the material. It has been empirically observed that the presence of small amounts of Al lowers the tendency for hydrogen embrittlement [7]. Complete prevention, however, cannot be ensured. While an alleviation of local stress due to a change in stacking fault energy (SFE) with Al inclusion has been proposed as one possible factor [8], this behavior may also be attributed to the presence of homogeneously distributed nano-sized κ-carbides or short-range ordering of similar atomic configurations which can serve as H traps, often at a precipitate/matrix interface.

For instance, experimental studies using atom probe tomography have demonstrated segregation of hydrogen at an interface of TiC with a ferritic matrix [9]. This was later confirmed by first-principles calculations [10], which further demonstrated that H accumulation can weaken the interface, resulting in hydrogen-enhanced decohesion and subsequent fracture formation.

In the case of  $\kappa$ -carbides it is interesting to note that, in real materials where they are formed as precipitates, their composition (Fe,Mn)<sub>3+y</sub>Al<sub>1-y</sub>C<sub>x</sub> may significantly deviate from the ideal stoichiometry (Fe,Mn)<sub>3</sub>AlC of phase-pure  $\kappa$ -carbides such as the (nearly ideal) ternary Mn-rich carbide studied in a previous work [11]. For  $\kappa$  precipitates, the Al content depends on its concentration in the bulk phase, which leads to different values reported in the literature. For example, Andryushchenko et al. [12] quoted a range of -0.2 < y < 0.2, whereas Seol et al. [13] measured much lower Al contents with  $y \approx 0.6$ . In recent works [14,15], the Al depletion in  $\kappa$ -carbide is correlated with the reduced C content in these precipitates. The latter varies a lot and is typically between 0.4 < x <0.72 [13,16]. We explained the C off-stoichiometry as a compromise between the gain in chemical energy during partitioning and the elastic strains emerging in coherent microstructures. This off-stoichiometry is relevant for the interaction with H, because the vacant C positions are favorable trapping sites.

Traps are sometimes designated beneficial or benign [17] because they may capture diffusive hydrogen and delay its further migration to malign traps causing HIDF. By definition, the trapping

energy  $E_{trap}$  is the capability of a microstructure feature to bind hydrogen better than the bulk matrix. The usual experimental approach to determine  $E_{trap}$  is thermal desorption spectroscopy (TDS) after galvanostatic or potentiostatic charging of the specimen with hydrogen. The relatively large scattering in the  $E_{trap}$  values collected from different experiments can be attributed to several causes. One particular problem is the absence of a definite reference. Measured trapping energies are often quoted relative to solution enthalpies of hydrogen in the respective bulk matrix. Since these depend on the crystal structure and the composition, a common reference state would ensure a better comparability of trapping energies from different studies.

Within theoretical studies, trapping energies have been calculated for various materials. In the case of Fe, the relevance of substitutional transition-metal atoms [18], vacancies [19], grain boundaries [20] and some precipitate phases [10] have been discussed. To the best of our knowledge, however, the hydrogen trapping by  $\kappa$ -phases has not been explicitly addressed theoretically. There are two experimental publications which assume an irreversible hydrogen trapping at the interface between  $\kappa$ -carbides and the Fe matrix [21,22], and another contribution attributing rather large activation energies of 76 and 80 kJ/mol for hydrogen desorption in the  $\kappa$ -carbides [23]. The mechanistic details, however, are not yet understood.

In the present work, the capability of  $\kappa$ -carbides to bind hydrogen is investigated using ab initio electronic-structure techniques within the framework of density-functional theory. We will analyze the role of C vacancies, as well as that of the interface between  $\kappa$ -carbide and Fe matrix in trapping H. In order to reveal the chemical nature of this trapping, the C–H and H–H interactions in the  $L1_2$ -Fe<sub>3</sub>Al phase are assessed. Further, the influence of manganese substitution on the trapping capability is calculated. Finally, the suitability of the  $\kappa$ -carbide/austenitic Fe matrix interface as a hydrogen trap is investigated, followed by the study of enhanced decohesion caused by the presence of hydrogen at the interface.

#### 2. Computational Methods

All quantum-mechanical structure optimizations and total-energy calculations were performed with the Vienna ab initio Simulation Package (VASP, version 5.4.1, Computational Materials Physics, University of Vienna, Vienna, Austria, 2015) [24–27], a software package employing density-functional theory (DFT) and utilizing plane waves together with PAW/pseudopotentials, thereby especially suited for simulations of periodic systems. The crystal orbitals were expanded in plane waves by means of the projector-augmented wave method (PAW) [28,29] with a kinetic energy cutoff of 500 eV. Contributions from exchange and correlation interactions were approximated utilizing the generalized-gradient approximation (GGA) functional in the parametrization by Perdew, Burke, and Ernzerhof [30]. Brillouin zone integration was performed by the scheme of Monkhorst and Pack [31] using k-point grids of  $n \times n \times n$  with n = 12, 8, 4, and 4 for the four-atom (stoichiometric compounds), 32-atom (2  $\times$  2  $\times$  2 fcc supercell), 108-atom (3  $\times$  3  $\times$  3 fcc supercell), and 128-atom (4  $\times$  4  $\times$  4 bcc supercell) metal lattices, respectively. The interface (between κ-carbide and fcc-matrix) calculations were performed for a 92-atom (2  $\times$  2  $\times$  5 supercell) and 108-atom (2  $\times$  2  $\times$  6 supercell) system, where the total number of atoms varies with the thickness of the  $\kappa$ -carbide. The corresponding **k**-point grids employed were  $8 \times 8 \times 5$  and  $8 \times 8 \times 3$ , respectively. Partial band occupancies were considered using the smearing scheme of Methfessel and Paxton [32] with the  $\sigma$  value set to 0.2 eV. The magnetic properties of the bulk κ-phases were taken into account by performing spin-polarized computations assuming a ferromagnetic model; nonetheless, this was restricted to ordered collinear magnetism. Non-collinearities are known to reduce the ground state energy in Fe-Mn alloys only slightly and will have little relevance at finite temperatures [33]. All other calculations, including interface models, were performed for the non-magnetic case, unless otherwise indicated.

For ideal κ-structures, the formation energies were calculated using:

$$\Delta E_{\rm el} = E_{\rm el}({\rm Fe_3AlX}) - [E_{\rm el}({\rm fcc-Al}) + 3 E_{\rm el}({\rm fcc-Fe}) + E_{\rm el}({\rm X})]$$
(1)

where  $E_{el}(X)$  is the ground-state energy of graphite (X = C) or half the energy of an H<sub>2</sub> molecule (X = H). We note that  $\Delta E_{el}$  is a theoretical energy, often provided in the ab initio community and used here solely for comparisons with earlier contributions in other studies. In order to evaluate precipitation behavior, not pure reference materials but the chemical potentials of the components as determined by the matrix materials are relevant. For both educts, the fcc structure was used as a reference, being the stable phase of Al and high-Mn steels, and forming a coherent interface with the perovskite-type  $\kappa$ -carbide.

The trapping energies were determined by the solution enthalpy (corresponding to the local chemical potential) of a hydrogen atom on the site in question as compared to an H atom in a  $\gamma$ -Fe (fcc) matrix, which is thus the reference state:

$$E_{\text{trap}} = [E_{\text{el}}(\kappa - \text{Al}_8\text{Fe}_{24}\text{C}_x\text{H}) - E_{\text{el}}(\kappa - \text{Al}_8\text{Fe}_{24}\text{C}_x)] - [E_{\text{el}}(\text{fcc-Fe}_{108}\text{H}) - E_{\text{el}}(\text{fcc-Fe}_{108})]$$
(2)

For determining the H solubility at a given site, (zero-point) vibrations can be important [34]. Our study, however, is primarily concerned with trapping energies of hydrogen, i.e., the difference in the solution enthalpy of hydrogen for different sites and regions of steel materials comprising ferritic and austenitic metal matrices, carbide precipitates, as well as the carbide/matrix interface. While the (zero-point) vibrational energies of hydrogen in a gas phase of H<sub>2</sub> molecules and of interstitial hydrogen in a metal matrix differ substantially, the difference is negligible when various interstitial sites are compared with each other. Thus, for the remainder of our study, the total energy of all calculated structures is approximated as their DFT energy.

The choice of the reference state in Equation (2) does not alter the conclusions if different positions and configurations within the same trapping phase are compared, which is the primary scope of this work. Furthermore, the potential of a phase to trap diffusive hydrogen with respect to other metal matrices than  $\gamma$ -Fe (fcc) can be obtained by adding the trapping energy for such a matrix with respect to  $\gamma$ -Fe. Determining the trapping energy of solid solutions such as Al-containing ferrite or Mn-containing austenite can, however, be exhaustive since a very large number of possible hydrogen positions would have to be considered due to the statistically random, i.e., disordered, nature of these alloys.

Similarly to Equation (2), the hydrogen solution enthalpy in the interface was computed using the following expression:

$$E_{\text{trap}}(\text{int}) = [E_{\text{el}}(\text{H} @ \kappa-\text{Al}_{12}\text{Fe}_{28}\text{C}_{12}/\text{fcc-Fe}_{56}) - E_{\text{el}}(\kappa-\text{Al}_{12}\text{Fe}_{28}\text{C}_{12}/\text{fcc-Fe}_{56})] - [E_{\text{el}}(\text{fcc-Fe}_{108}\text{H}) - E_{\text{el}}(\text{fcc-Fe}_{108})]$$
(3)

where the first two electronic energies on the right-hand side of the expression correspond to the fully-relaxed energies of the supercell comprised of  $\kappa$ -carbide and fcc-Fe with and without hydrogen, respectively.

## 3. Results and Discussion

#### 3.1. Stoichiometric Phases of L1<sub>2</sub> and E2<sub>1</sub> Symmetry

The formation of  $\kappa$ -carbide requires the simultaneous partitioning of substitutional Al and interstitial C from the solid solution. Here, we focus on the competing C and H interstitials and consider their energetics in Fe<sub>3</sub>Al. Although we cannot confirm a previous first-principles result that the  $L1_2$  structure is the ground state of Fe<sub>3</sub>Al [35], but obtain  $D0_3$  instead (Table 1), we will use  $L1_2$  as a matrix phase in the upcoming considerations. This is because the small energy difference of approx. 1 kJ/mol is compensated by the stabilization effect due to C insertion, yielding the perovskite  $E2_1$ -Fe<sub>3</sub>AlC, commonly known as  $\kappa$ -carbide (Figure 1). Our calculations of the lattice parameter, total energy, and the local magnetic moments as given in Table 1 agree well with other calculations [35–37].

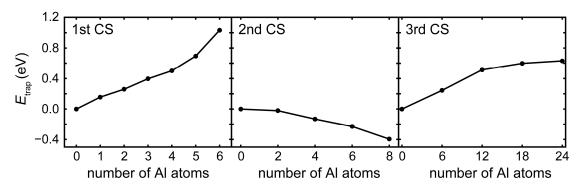
In particular, we confirmed earlier findings [15] that the formation of this phase out of pure elements is exothermic.

Compound	Structure	<i>a</i> <sub>0</sub> (Å)	$\mu_{\rm theo}$ ( $\mu_{\rm B}/{ m Fe}$ atom)	$\Delta E_{\rm el}$ (kJ/mol)
Fe <sub>3</sub> Al	BiF <sub>3</sub> , D0 <sub>3</sub>	5.74	2.0	-78
Fe <sub>3</sub> Al	$Cu_3Au, L1_2$	3.65	2.3	-77
Fe <sub>3</sub> AlC	perovskite, E2 <sub>1</sub>	3.75	1.0	-90
Fe <sub>3</sub> AlH	perovskite, E2 <sub>1</sub>	3.68	2.1	-85

**Table 1.** Lattice parameter *a*, magnetic saturation moments  $\mu_{\text{theo}}$  and formation energies  $\Delta E_{\text{el}}$  at T = 0 K of various compounds related to the  $\kappa$ -phase.

When investigating the relevance of these  $\kappa$ -carbides as a trap for H, we first consider the ideal phase with the composition Fe<sub>3</sub>AlC. The calculations confirm the finding for pure fcc-Fe [38] that the empty octahedral sites (green spheres in Figure 1) are more favorable for H ( $E_{trap} = 0.13 \text{ eV}$ ) than the tetrahedral ones ( $E_{trap} = 0.75 \text{ eV}$ ). Nonetheless, the absolute value is endothermic, i.e., H would not enter this phase. The reason for this repulsion can be the local atomic configuration with two Al atoms in nearest-neighbor positions (first coordination sphere, CS) and/or the presence of C in the adjacent octahedral sublattices.

In order to confirm the impact of the metallic atoms, we have investigated the Al–H interaction in an fcc-Fe matrix (Figure 2). Considering H as the central atom, the interaction turns out to be repulsive if Al is located in the first CS, but an energetic optimum exists if Al and H are second-nearest neighbors, Al being in the second CS. While the first configuration matches the H position in the empty octahedral sublattice sites of  $\kappa$ -carbide, the second corresponds to an H atom replacing a C atom on the central interstitial site (green and black spheres in Figure 1, respectively). Thus, the central interstitial site is energetically preferred for H incorporation while the non-central octahedral sites are generally assumed to be empty and, thus, not considered in the numbering of CS.



**Figure 2.** Hydrogen trapping energy  $E_{trap}$  as a function of the local atomic environment with respect to the amount of Al atoms in the first, second, or third coordination sphere (CS) around a single interstitial H atom in a  $3 \times 3 \times 3$  supercell of fcc-Fe. Al atoms occupy Fe sites in the host matrix. The energies are defined according to Equation (2).

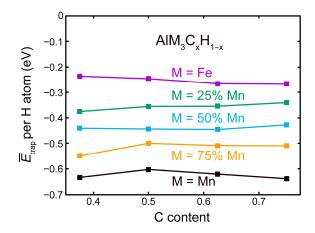
The attractive interaction between a single Al and a single H atom in the second CS lets one expect that the central (body-centered) interstitial sites in an  $L1_2$ -Fe<sub>3</sub>Al matrix could be completely occupied by H. This would result in an  $E2_1$ -Fe<sub>3</sub>AlH phase ( $\kappa$ -hydride), which has not been observed experimentally and has also been identified as chemically unstable in a theoretical contribution [35]. In contrast to said contribution, we obtain that the formation of this phase out of the pure elements according to Equation (1) is exothermic (-85 kJ/mol). In such a hypothetical  $E2_1$ -Fe<sub>3</sub>AlH phase, the effects of H on the  $\kappa$ -phase formation are qualitatively similar to those of C, but quantitatively

much smaller: the lattice parameter increases by 0.8% from 3.65 to 3.68 Å (2.7% increase for C), and the local magnetic moments of the Fe atoms lower by 9% from 2.3 to 2.1  $\mu_B$  (57% for C).

We note, however, that C also prefers a local coordination with Al atoms in the second CS, as shown in previous studies [39,40]. There is, therefore, a competition between the interstitial elements C and H for the formation of the  $\kappa$ -phase. At T = 0 K, the formation energy of the  $\kappa$ -carbide Fe<sub>3</sub>AlC is slightly larger (-90 kJ/mol) than the one of  $\kappa$ -hydride (-85 kJ/mol). More important is the fact, however, that H already becomes too mobile to remain in the steel matrix before those temperatures are reached at which Al can form locally-ordered structures (approx. 600 °C for typical annealing times). We can, therefore, expect that the *E*2<sub>1</sub> phase is primarily formed as  $\kappa$ -carbide.

#### 3.2. Competition of H and C in the L1<sub>2</sub> and E2<sub>1</sub> Structure

Despite the preference of  $\kappa$ -carbide formation, the typically observed C depletion in this phase yields various vacancies on its sublattice, i.e., potential sites for H that are in a favorable configuration with respect to Al. To further elaborate on this, the average trapping energy per H atom in a fully filled  $\kappa$ -matrix was calculated as a function of the C concentration. Carbon concentrations of 37.5–75 at % were taken into account in accordance with the typically experimentally observed C contents of Fe-rich  $\kappa$ -carbide precipitates. The distribution of C atoms among the different positions (central interstitial sites, referred to as  $\kappa$  positions) was random, while the remaining  $\kappa$  positions were occupied by H atoms. The calculations were performed employing  $3 \times 3 \times 3$  supercells with full structural optimization with respect to shape and volume. The results show, surprisingly, that the average trapping energy per H atom is largely independent of the C concentration (Figure 3, purple, uppermost curve).

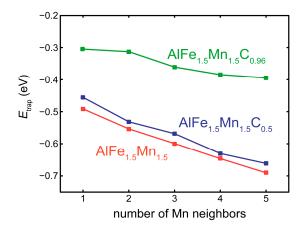


**Figure 3.** Average trapping energy  $\bar{E}_{trap}$  per H atom as a function of the C content for a 3 × 3 × 3  $E2_1$ -(Fe,Mn)<sub>3</sub>Al(C,H) supercell with all  $\kappa$  positions filled and considering different Mn contents.

The calculations in Figure 3 have also been performed for different Mn contents, the reason being that  $\kappa$ -carbides growing from Mn-rich austenitic matrices contain high amounts of manganese as a substituent for iron. For this purpose, the aforementioned calculations were repeated for a 3 × 3 × 3  $E2_1$ -(Fe,Mn)<sub>3</sub>Al(C,H) supercell with randomly-distributed Mn atoms. Upon introducing manganese, no change can be observed with regard to the average trapping energy being independent of the carbon content (Figure 3).

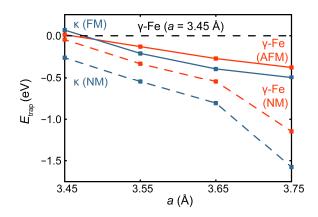
The trapping capability, however, increases (i.e., the trapping energy is lowered) with increasing Mn content. This is consistent with previous findings that the short-range Mn–H interaction in austenitic alloys is attractive [38]. To study said interaction in  $\kappa$ -carbides, a  $3 \times 3 \times 3 L_{12}$ -Fe<sub>1.5</sub>Mn<sub>1.5</sub>Al supercell was used, where the Mn and Fe atoms were distributed randomly. The H atom was placed on  $\kappa$  positions with different numbers of Mn atoms (positions with 1–5 Mn atoms are present in the given supercell) in the surrounding octahedron. Our results show an almost linear dependence of the trapping energy on this number (Figure 4), confirming that previous findings apply to Al-containing

systems as well. However, the results do not fully capture the changes of trapping energies with increased Mn content as seen in Figure 3. An important reason is that the data points in Figure 4 (for a fixed C content) all correspond to the same volume, while each Mn concentration in Figure 3 has its own equilibrium volume.



**Figure 4.** Trapping energy  $E_{trap}$  of a single H atom as a function of the number of Mn atoms in its first CS for a 3 × 3 × 3  $L_{12}$ -Fe<sub>1.5</sub>Mn<sub>1.5</sub>Al supercell with C sublattice concentrations of 0% (red), 50% (blue), and 96% (green).

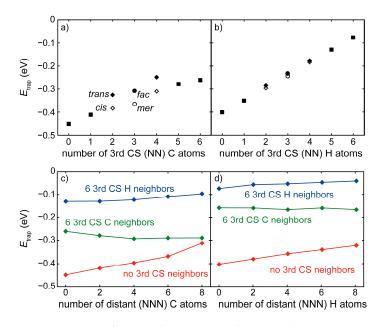
To understand this effect, the trapping energy was calculated as a function of the lattice parameter (Figure 5). The calculation was performed for the  $L1_2$  configuration of Fe<sub>3</sub>Al, which has an equilibrium lattice parameter of  $a(L1_2) = 3.65$  Å as well as pure fcc-Fe with  $a(\gamma$ -Fe) = 3.45 Å. The matrices consisted of 32-atom 2 × 2 × 2 supercells. In the  $L1_2$ -Fe<sub>3</sub>Al matrix a single H atom was again placed on an octahedral sublattice site normally occupied by C in the  $\kappa$ -phase. The calculations were performed for two different magnetic states. In all cases, the trapping capability increases with the volume. For the nonmagnetic state the H atom clearly favors the  $L1_2$ -matrix over pure fcc-Fe at all lattice parameters and, thus, volumes. If magnetism is considered, the ferromagnetic  $L1_2$  matrix is, again, favored, apart from the special case when its volume is identical to the equilibrium volume of pure fcc-Fe (3.45 Å). Comparing both phases at the same lattice parameter, however, is only relevant in the case of a perfectly coherent interface between the matrix and the precipitate phase. Otherwise, the larger lattice parameter of the  $L1_2$  phase will always yield a lower  $E_{trap}$ .



**Figure 5.** Trapping energy  $E_{\text{trap}}$  of a single H atom as a function of cell volume (via the lattice parameter *a*) for fcc-Fe (red) and the *L*1<sub>2</sub>-Fe<sub>3</sub>Al matrix (blue) considering different magnetic states, with the dashed/solid lines signifying the nonmagnetic/magnetic cases.

Additionally, the influence of carbon atoms on the Mn–H interaction was investigated (Figure 4). For this purpose, the supercell offering 27  $\kappa$  positions was filled with 0, 14, or 26 C atoms (corresponding to a C sublattice concentration of 0, 50, or 96%), avoiding nearest-neighbor C–H configurations in the case of 14 C atoms. We observe that the  $E(x_{Mn})$  linearity is independent from the C content although the attractive interaction between Mn and H seems to be reduced in the 96% C case. More importantly, however, one observes a small shift in the trapping energy if half the cell's  $\kappa$  positions are filled with carbon, but a significantly larger shift if the entirety of these positions is filled, the latter being attributable to the interaction between direct C–H neighbors. One may, therefore, expect that the interaction of H with C affects the trapping energy, and this raises the question why such an effect is not observed in Figure 3.

In the next step we, therefore, investigated the interaction of H with other C and H atoms (Figure 6). For this purpose, we chose  $3 \times 3 \times 3 L1_2$ -Fe<sub>3</sub>Al supercells. The trapping energy of a hydrogen atom was first calculated as a function of the number of neighboring C atoms in the third CS (being the nearest neighboring  $\kappa$  positions if other octahedral sites are unoccupied, labeled NN), keeping the shape and volume of the supercells fixed (Figure 6a). Similar to Figure 4, we observe a repulsive effect which results in an almost linear increase of  $E_{trap}$ . Furthermore, the trapping energy depends on the configuration of the neighboring C atoms. This observation, however, is partially due to the choice of the supercell: two C atoms in the *trans* isomer case are located in neighboring unit cells of the  $3 \times 3 \times 3$  supercell (energy difference to the *cis* isomer is 0.06 eV), while this is not the case in a 144-atom  $4 \times 3 \times 3 L1_2$ -Fe<sub>3</sub>Al supercell (respective energy difference is 0.04 eV).



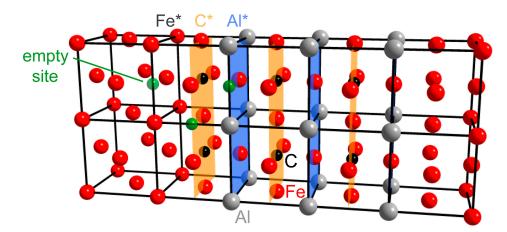
**Figure 6.** Trapping energies  $E_{\text{trap}}$  for a single H atom in the central  $\kappa$  position as a function of the number of C or H atoms in various  $\kappa$  positions in a 3 × 3 × 3  $L1_2$ -Fe<sub>3</sub>Al supercell. (a) C atoms are present as nearest neighbors for H in the third CS (nearest  $\kappa$  neighbors, NN), under consideration of structural isomers. The lattice parameter is *a* = 3.69 Å. Squares signify arrangements without structural isomers with zero, one, five, or six neighbors; open/closed diamonds signify the two isomers for two neighbors (*cis* and *trans*); open/closed circles signify the two arrangements for three neighbors (*mer* and *fac*). (b) As before but for H atoms in the third CS. Energetic differences between structural isomers are negligible in this case. The lattice parameter is *a* = 3.65 Å. (c) C atoms are next-nearest neighbors (NNN) located at the cell corners ( $d_{C-C} = 6.4$  Å), with no atoms (red diamonds), six H atoms (blue diamonds) or six C atoms (green diamonds) located simultaneously in the third CS (NN)  $\kappa$  positions, respectively. Lattice parameter as in (a). (d) As in (c), but considering H atoms as NNN neighbors. Lattice parameter as in *a* explains the slight energetic difference in the case of zero NN/NNN neighbors.

We further note that the C–H interaction for H on a  $\kappa$  position and C in the non-central interstitial site coplanar to Al is attractive (not shown). Concerning H–H interactions, we observe a similar, almost linear dependence of  $E_{trap}$  on the number of neighboring H atoms in the third CS (Figure 6b). This trend is (up to four third CS H atoms) almost identical to the C–H case and has a significantly lower dependence on the atomic configuration (rendering a distinction between the various configurations unnecessary). The similarity of C–C and C–H interactions explains the constant behavior in Figure 3, since the number of third CS H and C atoms is always six in this figure.

The impact of neighboring C atoms was compared to that of C atoms in other shells. In Figure 6c the situation is exemplified for C atoms in next-nearest-neighbor (NNN) positions (corners of a  $3 \times 3 \times 3 L_{12}$ -Fe<sub>3</sub>Al supercell). Despite a rather long distance of  $\sqrt{3} \times 3.69$  Å = 6.4 Å, a repulsive effect is still observed (red diamonds). The slope of the C dependence, however, is smaller than for the third CS neighbors by a factor of  $\approx 2$ . It is further observed that the dependence on the number of NNN carbon neighbors is strongly suppressed if the NN  $\kappa$  positions are occupied either by C or by H. These trends can be understood as resulting from local relaxations. They indicate, once again, that the nearest  $\kappa$  positions are most relevant for the value of the H solubility. The trends for distant H–H interactions are, as in the case of the third CS interactions, qualitatively identical to the C–H case, as seen in Figure 6d.

## 3.3. *H at Interfaces between* $\kappa$ *-Carbide and the fcc-Fe Matrix*

The insights obtained for the Al–H and C–H interactions are used to understand chemical trends for incorporating hydrogen in the (100) interface between  $\kappa$ -carbide and the fcc-Fe matrix. In this case, however, we limit ourselves to a single H atom. Various scenarios for said incorporation are possible. We first note that stoichiometric  $\kappa$ -carbide has two kinds of (100) layers, one containing Al atoms in one of the fcc sublattices, the other containing C atoms in the central interstitial  $\kappa$  positions. The considered layers for the representation of the  $\kappa$ -carbide in Figure 7 are indicated by a stacking sequence, e.g., C\*–Al\*–C\*–Al\*. The termination layer, which can contain C or Al, is considered as the interface plane.



**Figure 7.** The  $5 \times 2 \times 1$  supercell composed of  $\kappa$ -carbide and fcc-Fe (assuming coherent interfaces) for a given thickness of the  $\kappa$ -phase. Orange planes, labeled C\*, signify (100) layers containing C and Fe atoms, while blue planes, labeled Al\*, contain Fe and Al. Layers containing Fe only are unmarked and labeled Fe\*. The translucent green spheres represent empty octahedral sites which (in addition to C vacancies) may incorporate H atoms.

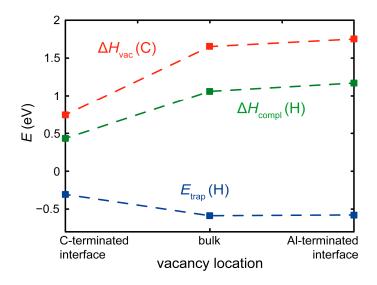
The results for three different supercells, as given in Table 2, can be interpreted as follows: on the one hand, H tries to avoid positions with Al as closest neighbor in the first CS (compare with Figure 2), so incorporation into an Al-containing layer is unfavorable. On the other hand, a configuration with C in a second CS position (in contrast to the NN site shown in Figure 6a) yields an improved trapping

behavior. The non-central octahedral sites in the C layer in a Fe–C–Al scenario (green sphere in orange-colored C\* layer, Figure 7) are, therefore, most attractive for H, because they allow for four second CS neighbor C atoms, but only one first CS neighbor Al atom. Only slightly less favorable are the octahedral sites in Fe layers adjacent to a C-terminated  $\kappa$ -carbide (green sphere in Fe\* layer, Figure 7), because in this case two second CS C atoms are available, but no first CS Al atoms are present. These configurations already yield a trapping at the interface.

**Table 2.** Hydrogen trapping energies  $E_{\text{trap}}$  for octahedral sites at the interface layer between  $\kappa$ -carbide and fcc-Fe, or one of the adjacent layers. Three kinds of stacking sequences in a 2 × 2 × 5 supercell (SC) are provided, where layers used for H incorporation are highlighted in bold face.

Stacking Sequence of Layers in SC	E <sub>trap</sub> (H) Adjacent Fe Layer (eV)	E <sub>trap</sub> (H) Interface Layer (eV)	E <sub>trap</sub> (H) Adjacent κ Layer (eV)
<b>Fe*–C*–Al*–</b> C*–Fe*–Fe*–Fe*–Fe*–Fe*–Fe*	-0.20	-0.18 ( <b>C</b> )	0.04 ( <b>Al</b> )
Fe*-Al*-C*-Al*-C*-Fe*-Fe*-Fe*-Fe*-Fe*	0.01	0.003 (Al)	-0.05 (C)
Fe*-C*-Al*-C*-Al*-C*-Al*-Fe*-Fe*-Fe*	-0.20	-0.24 ( <b>C</b> )	0.04 ( <b>Al</b> )

Competing with the H incorporation discussed so far, the replacement of a C atom by an H atom should also be considered for the interface. To understand how efficiently C vacancies act as hydrogen traps near the interface, we also compare the vacancy formation energy at different positions (Figure 8). This energy amounts to 1.65 eV for a vacancy in the bulk of the  $\kappa$ -carbide phase, is almost the same (1.75 eV) for C atoms next to Al-terminated interfaces, but is significantly lower (approx. 0.75 eV) for C atoms at C-terminated interfaces. This is not surprising, since these C atoms have a lower number of Al neighbors in the second CS.



**Figure 8.** C vacancy formation energy (shown in red), H trapping energy within the vacancy (shown in blue) and their combination, i.e., the H–vacancy complex formation energy, (shown in green) for three different positions of vacancies. Note that trapping of H by vacancies near C-terminated interfaces is energetically the most favorable.

The differences in H trapping energies for the three different vacancy positions are less pronounced. For C vacancies in the bulk of the  $\kappa$ -carbide, H has a favorable configuration with respect to the Al atoms, but an unfavorable configuration with respect to the other C atoms. The resulting trapping energy is -0.59 eV. (Note that this data refers to non-magnetic calculations, so that the absolute values cannot be compared directly with Figure 4.) The situation is almost unchanged (-0.58 eV) for the C positions next to Al-terminated interfaces. If H is incorporated into C vacancies in

a C-terminated interface, then both the number of Al neighbors in the second CS and the number of C atoms in NN positions are reduced from 8 to 4 and from 6 to 5, respectively. Since the change in the number of Al neighbors is more significant, the trapping energy for H in these sites is reduced (-0.31 eV).

It should be noted, however, that C vacancies which are more likely to form near the interface are more accessible, at least kinetically, to H atoms trapped near the interface than vacancies formed in the interior of the precipitate phase. Another possible scenario can be the formation of percolating networks of C vacancies which act as energetically favored pathways for hydrogen to diffuse from the interface to the bulk of the carbide, as observed for TiC [10]. We can further define the hydrogen–vacancy complex formation energy as the sum of the C vacancies at different positions (near the interface) shows that this energy is lowest for vacancies at C-terminated interfaces and, hence, such a scenario is, energetically, the most favorable.

#### 3.4. H Enhanced Decohesion of Interfaces

It is a decisive follow-up question whether the trapped H in the interface causes decohesion along the interface, which might serve as a mechanism of hydrogen embrittlement. To understand this, we need to answer the question whether the presence of H in the interface enables or suppresses the separation of the interface into respective free surfaces. To do so, the adsorption energy of H at the interface was compared to the energy of H at the free surfaces of the carbide and the austenitic Fe matrix after possible crack formation. The corresponding energy of separation is given by the expression:

$$E_{\text{sep}} = [E_{\text{el}}(\text{int}) - E_{\text{el}}(\kappa - \text{surf}) - E_{\text{el}}(\text{Fe-surf})] + [c_{\text{H}}(\text{int}) E_{\text{trap}}(\text{int}) - c_{\text{H}}(\kappa) E_{\text{ads}}(\kappa - \text{surf}) - c_{\text{H}}(\text{Fe}) E_{\text{ads}}(\text{Fe-surf})]$$
(4)

where  $E_{el}(int)$  is the total energy of the supercell containing the interface of  $\kappa$ -carbide and fcc-Fe without H.  $E_{el}(\kappa$ -surf) and  $E_{el}(Fe$ -surf) are the total energies of supercells containing  $\kappa$ -carbide and fcc-Fe, respectively, with a surface adjacent to a vacuum layer.  $c_H$  is the concentration of H at the planar defects, which depends on its chemical potential  $\mu_H$ .  $E_{trap}(int)$  and  $E_{ads}(X$ -surf) are the corresponding trapping and adsorption energies of hydrogen at the interface or the surface (X =  $\kappa$  or Fe) given by:

$$E_{\text{trap}}(\text{int}) = E_{\text{el}}(\text{H}@\text{int}) - E_{\text{el}}(\text{int}) - \mu_{\text{H}} \text{ and}$$

$$E_{\text{ads}}(\text{X-surf}) = E_{\text{el}}(\text{H}@\text{X-surf}) - E_{\text{el}}(\text{X-surf}) - \mu_{\text{H}}$$
(5)

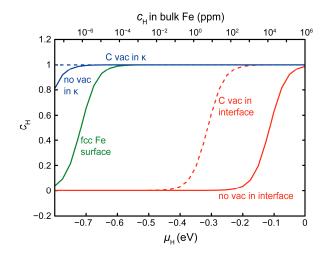
The tendency of trapped H to cause decohesion at the interface is indicated by the "embrittlement term" as given by the second term in Equation (4), namely:

$$\varepsilon = c_{\rm H}(\rm{int})E_{\rm trap}(\rm{int}) - c_{\rm H}(\kappa)E_{\rm ads}(\kappa-\rm{surf}) - c_{\rm H}(\rm{Fe})E_{\rm ads}(\rm{Fe-surf}).$$
(6)

A positive value of  $\varepsilon$  implies that it is energetically favorable to have hydrogen on free surfaces rather than at the interface, which provides a driving force for the formation of free surfaces. On the other hand, a negative value indicates that H prefers to stay at the interface, thereby stabilizing it.

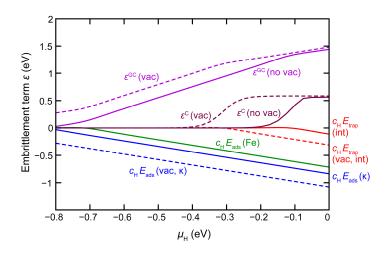
The equilibrium concentration of hydrogen at the interface is given by its trapping energy, i.e.,  $c_{\rm H}({\rm int}) = 1/(\exp(\beta E_{\rm trap}({\rm int})) + 1)$  with  $\beta = 1/(k_{\rm B}T)$ , and depends via Equation (5) on the chemical potential  $\mu_{\rm H}$  (Figure 9). We compare an interface without C vacancies (solid line) with an interface that contains a single C vacancy (dashed line). In the first case, a maximum concentration of 1 H atom per  $2 \times 2$  interface area is considered (corresponding to  $c_{\rm H} = 1$ ), to avoid strong H–H interactions. In the second case, only the filling of the single vacancy per  $2 \times 2$  interface area with H is considered. Due to the lower trapping energy, the occupation of the vacancy sets in at much lower chemical potentials than for the perfect interface. The concentration of H at the free surfaces depends on the kinetics of the separation process. If it is very fast, then the particle conservation  $c_{\rm H}(\kappa) + c_{\rm H}({\rm Fe}) = c_{\rm H}({\rm int})$  can be assumed, corresponding to the canonical limit. If the diffusibility of H is faster than the

separation, then an equilibrium H concentration  $c_{\rm H}(X) = 1/(\exp(\beta E_{\rm ads}(X-{\rm surf})) + 1)$  can also be used for the surfaces, corresponding to the grand-canonical limit. Our result points in this limit towards a strong driving force for H to segregate to a free  $\kappa$ -carbide surface with respect to a position at the interface (Figure 9).



**Figure 9.** Equilibrium concentration of H at the C-terminated interface, free  $\kappa$ -carbide (C-terminated) and fcc-Fe surfaces as a function of the chemical potential of hydrogen. A perfect  $\kappa$ -carbide (solid lines) is compared with a  $\kappa$ -carbide that contains a C vacancy (dashed lines).

Based on these concentrations, the embrittlement term was determined for both limits according to Equation (6) and plotted in Figure 10. Looking first at the results for the perfect interface in the grand-canonical (GC) limit, we observe large positive values for all considered chemical potentials of H. This is because the free surfaces of  $\kappa$ -carbide and fcc-Fe are substantially more favorable for H than the interface. A similar effect has been observed for several other precipitate phases [41]. We note, however, that this is a purely thermodynamic argument. It ignores the fact that the H concentration at the perfect interface is negligibly small for  $\mu_{\rm H} < -0.3$  eV and that kinetics would not provide H significantly fast in order to stabilize the forming free surfaces. Therefore, we have plotted the canonical (C) limit in addition, for which the embrittlement term is almost vanishing for these chemical potentials. The processes in reality will occur between these two limits.



**Figure 10.** Embrittlement term  $\varepsilon$  and the different energy contributions in Equation (6) as a function of  $\mu_{\text{H}}$ . A perfect  $\kappa$ -carbide (solid lines) is compared with a  $\kappa$ -carbide that contains a C vacancy (dashed lines). Furthermore, the grand-canonical (GC) and the canonical (C) limit are compared (see text for details).

In order to come closer to reality, it is also important to consider the existence of C vacancies in the interface. Due to the substantial trapping effect of these defects, these sites will be quickly filled with H for chemical potentials  $\mu_{\rm H} > -0.5$  eV. This affects the first term of Equation (6), indicated by the red dashed line in Figure 10. At the same time, the H incorporation at the forming  $\kappa$ -carbide surface, which contains this vacancy as well, also becomes even more favorable (blue dashed line in Figure 10). Depending on the H kinetics, i.e., the grand-canonical vs. the canonical limit, the combined embrittlement term  $\varepsilon$  increases further (purple and maroon dashed lines in Figure 10). Since in particular the canonical line shifts substantially upwards, we can conclude that the presence of these lattice imperfections is decisive for a destabilization of the interface if H comes into play.

#### 4. Conclusions

The potential of  $\kappa$ -carbides to trap diffusive hydrogen was studied using density-functional theory. The hydrogen analog of the  $\kappa$ -carbide, the  $\kappa$ -hydride, was shown to be a theoretically stable compound. Its formation, however, is kinetically disadvantageous when compared to the carbide.

Substituting Mn for Fe was clearly shown to be preferable to the trapping energy, since the chemical potential of hydrogen decreases linearly with the number of manganese atoms in the octahedron surrounding the hydrogen atom. This effect is independent of the overall carbon concentration although directly neighboring carbon atoms seem to reduce the Mn–H attraction. As a result, the trapping capability of  $\kappa$ -carbides is proportional to the manganese content of the carbide.

The interaction of hydrogen with different metal matrices, including the  $L1_2$ -Fe<sub>3</sub>Al matrix, was investigated, and it was observed that the  $\kappa$ -matrix is a favorable environment for H as a result of both its chemical environment, owing to attractive Al–H interactions in  $\kappa$ -like arrangements, and the increased lattice parameter. The interaction between carbon and hydrogen as well as between different hydrogen atoms within the  $\kappa$ -matrix was examined. Both the C–H and the H–H interaction proved to be repulsive, with the H–H interaction showing a stronger repulsion in the short range while C–H repulsion is stronger in the long range. Additionally, directly neighboring C and H atoms suppress the long-range interaction.

For  $\kappa$ -carbides with a carbon content of about 35–75% with respect to the stoichiometric compound, the repulsion between the interstitials is compensated by the increase in trapping capability due to an increase of the lattice parameter. The average trapping energy of a fully filled  $\kappa$ -carbide is, thus, independent from the carbon loading of the carbide.

We conclude that the trapping efficiency of diffusive hydrogen by  $\kappa$ -carbides depends on its C, as well as its Mn, content. While the C content determines the number of vacant  $\kappa$  positions and thereby the capacity of the phase to trap hydrogen, the manganese content determines the overall trapping efficiency, i.e., the average gain in energy if an H atom is removed from the matrix and stored in the carbide precipitate. Efficient strategies to control diffusive H in steel materials should thus consider lowering the carbon contents of  $\kappa$ -carbide precipitates while raising their manganese contents.

Finally, we demonstrate that hydrogen located in the interface between carbides and the matrix material has a high solubility only in the presence of vacancies near the interface, thereby making the carbide/austenite interface an efficient trapping center for hydrogen. Our DFT calculations further suggest a possible hydrogen-induced separation of the interface into free surfaces of  $\kappa$ -carbide and fcc-Fe, thereby leading to embrittlement caused by a hydrogen-enhanced decohesion mechanism. Said embrittlement can be expressed via a quantitative model to assess the dependence of the interface decohesion upon hydrogen concentration.

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Conflicts of Interest: The authors declare no conflict of interest.

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