

Review

Removal of Arsenic, Chromium and Uranium from Water Sources by Novel Nanostructured Materials Including Graphene-Based Modified Adsorbents: A Mini Review of Recent Developments

Athanasia K. Tolkou, Ioannis A. Katsoyiannis and Anastasios I. Zouboulis *D

Department of Chemistry, Aristotle University of Thessaloniki, GR-54124 Thessaloniki, Greece; tolkatha@chem.auth.gr (A.K.T.); katsogia@chem.auth.gr (I.A.K.)

* Correspondence: zoubouli@chem.auth.gr; Tel.: +30-231-099-7794

Received: 13 April 2020; Accepted: 2 May 2020; Published: 7 May 2020



Abstract: Groundwater is commonly used as a drinking water resource all over the world. Therefore, groundwater contamination by toxic metals is an important issue of utmost concern for public health, and several technologies are applied for their effective removal, such as coagulation, ion exchange, adsorption, and membrane applications like reverse osmosis. Adsorption is acknowledged as a simple, effective and economic technology, which has received increased interest recently, despite certain limitations regarding operational applications. The respective scientific efforts have been specifically focused on the development and implementation of novel nano-structured adsorbent materials, which may offer extensive specific surface areas, much higher than the conventional adsorbents, and hence, are expected to present higher removal efficiencies of pollutants. In this paper, the recent developments of nanomaterial applications for arsenic, chromium and uranium removal from groundwaters are critically reviewed. Particularly, the use of novel composite materials, based mainly on hybrid metallic oxide nanoparticles and on composites based on graphene oxide (GO) (i.e., graphene-based hybrids), showed promising evidences to achieve efficient removal of toxic metals from water sources, even in full scale applications.

Keywords: nanostructured adsorbents; hybrid processes; graphene; arsenic; chromium; uranium

1. Introduction

Water pollution by toxic metals and metalloids (e.g., arsenic, copper, mercury, cadmium, lead, uranium, chromium) is nowadays considered a serious global environmental problem, especially for groundwaters. Even in concentrations in the μ g L⁻¹ range, their presence in various water bodies is considered particularly dangerous for human health and hence, their maximum allowable concentration in waters is strictly regulated by international organizations (World Health Organization (WHO), US Environmental Protection Agency (EPA), EU). Therefore, the efficient treatment of contaminated waters for the removal of toxic contaminants is necessary to provide people with safe drinking water. In order to detoxify the polluted waters, various treatment techniques, such as coagulation–flocculation, lime softening, photocatalytic, chemical or biological oxidation, bioremediation, ion-exchange, reverse osmosis, and adsorption have been employed with different efficiency degrees, depending upon the specific applicable conditions [1].

Considerable interest has attracted the preparation and use of novel nanostructured adsorbent materials with average particle sizes below 100 nm, expecting that their properties will be superior to those of conventional materials with structures of bigger size [2]. The application of nano-scaled adsorbents comprises a novel and promising technology, especially for toxic metals removal from



water sources, because of their respective substantially higher surface areas, which may provoke higher reactivity and increased affinity, capacity and selectivity for different metals [3]. Recently, promising materials, i.e., activated carbons [4] and bamboo-based biochar/montmorillonite composites [5] have been used for oxoanions (i.e., pertechnetate) and anionic pollutant (i.e., nitrates) removal from aqueous solutions, respectively. The objective of this review paper is to summarize the recent developments of nano-structured materials, including graphene-based modified/hybrid adsorbents, applied particularly in the water treatment of arsenic, uranium or chromium removal from water sources, with specific emphasis given to groundwater treatment.

All the relevant compounds of the examined toxic metals have the characteristic of being present in waters as oxyanions, in pH relevant to ground/waters, i.e., 6.5–8.5. Arsenic is present in waters with two major valency states, i.e., either as trivalent As(III) or pentavalent As(V). As(III) cannot be easily removed by the application of conventional water treatment technologies; therefore, it is usually pre-oxidized to As(V), which in turn is usually present as the respective oxyanions of arsenic acid (H₂AsO₄⁻ or HAsO₄²⁻) [6]. Cr(VI) is present in waters mainly as chromate (CrO₄²⁻) or dichromate (Cr₂O₇²⁻). Cr(III) is rather insoluble in aqueous solutions, easily forming precipitates and interacting with other co-existing constituents; therefore, it is quite seldom found in considerable concentrations [7]. U(VI) is present mainly as the uranyl cation (UO₂²⁺), which, in waters containing bicarbonate anions however, is most probably complexed and presented as UO₂(CO₃)₂²⁻ [8].

These oxyanions can usually be removed from waters by the application of different technologies, due to differences in their aquatic chemistry. Arsenic, in most cases, is firstly oxidized by means of chemical or biological oxidation and then removed by conventional coagulation (with Fe or Al based salts), or by adsorption on Fe-oxides or activated alumina, which is also a widely applied technology [1]. Cr(VI) is mostly removed from water by reduction using Fe(II), which reduces to Cr(III), which is subsequently removed usually by precipitation as insoluble hydrous hydroxides [9]. U(VI) is mostly removed by lime softening or adsorption onto iron oxides [8]. In several cases, these oxyanions have been simultaneously present in natural ground/waters and their adsorption on efficient adsorbents with extended surface areas could be a perfect solution, when considering their simultaneous removal.

Adsorption is a conventional technology which can have applications in the removal of all these toxic oxyanions and therefore, in this review, several novel nanostructured adsorbents are critically evaluated, in order to present their ability regarding the removal of these metals from ground/water sources.

2. Nanostructure Materials for Arsenic Removal

2.1. Arsenic (As)

Arsenic (As) is considered as a contaminant of major concern, due to its extreme toxicity at relatively low doses and its worldwide occurrence in groundwaters. It is mostly naturally present in groundwaters, but several industrial processes and products, such as wood preservatives, semi-conductors and agricultural applications (pesticides), may also introduce arsenic into the environment [10,11]. Increased arsenic concentration levels in groundwaters cause significant issues in the supply of secured drinking water [12], because long-term arsenic contaminated water consumption has been linked with various diseases such as several types of cancers [13]. As a result, the WHO [12] has reduced the acceptable concentration value for arsenic in drinking water from 50 to 10 μ g L⁻¹ and most countries also apply the same maximum allowed concentration [14].

Arsenic in natural waters is mainly found with its inorganic forms of As(III) (H₃AsO₃) and/or As(V) (H₃AsO₄, H₂AsO⁴⁻ and HAsO₃²⁻) [15,16]. The prevalence of these species in natural waters is mainly dependent on the existing oxidation–reduction conditions and pH values [17]. Under oxic conditions, the pentavalent form of As(V) is predominantly present as H₂AsO⁴⁻, HAsO₄²⁻ with pKa₁ = 2.19 and pKa₂ = 6.94, respectively. Conversely, when anoxic conditions prevail, e.g., in anaerobic groundwaters,

As(III) is the main species found, which at pH values relevant to groundwaters is present as the non-ionic arsenous acid (H_3AsO_3 , $pKa_1 = 9.22$) [7].

As(III) is less adsorbed than the As(V), when interacting with solid surfaces and, therefore, As(III) is less efficiently removed by the use of common treatment processes, such as adsorption and precipitation. To handle this problem, an oxidation stage is usually incorporated in the treatment train to convert As(III) to As(V) [15,16]. Several studies have indicated that As(III) removal to concentrations less than 10 μ g L⁻¹ by adsorption onto suitable adsorbent materials, such as iron oxides, is feasible [16,17], but requires relatively large quantities of the used adsorbent, which makes this method rather inadequate for full-scale applications.

Consequently, the development of more effective technologies to remove (particularly) the As(III) species from water sources is important. The use of nano-materials could serve as a viable alternative to provide more sustainable solutions, by offering extensive surface areas and using similar material quantity, leading potentially to enhanced As(III) removal without the need for the pre-oxidation step. In the following, the recent applications of newly synthesized nanomaterials, as applied for arsenic removal [17,18], will be presented, showing—in certain cases—improved sorption capacity for As(III).

2.2. Application of Hydrous Nanostructure Iron(III)–Titanium(IV) Binary Oxide for As(III) and As(V) Removal

Iron oxides are widely applied for arsenic removal from aqueous solutions [19]. The most recent developments include the incorporation of other metals into the structure of Fe(III) oxides to achieve increased efficiency, regarding arsenic removal. Gupta et al. (2008) [20] synthesized and used nano-structured hydrous Fe(III)–Ti(IV) bimetallic mixed oxides (NHITO) for the sorption of arsenic, because the incorporation of Ti(IV) was found to present enhanced material properties, namely surface sorption and photo-induced catalysis.

The ability of NHITO to remove arsenic from solution containing 50 mg As(III) L^{-1} to the permissible concentration value (i.e., 0.01 mg L^{-1}) was investigated with batch experiments at the pH value 7, by varying the dose of solid/adsorbent, while maintaining the other parameters constant. It was found that the residual concentration was decreased to 6.30 from 50 mg L^{-1} , when applying a sorbent dose of 2 g L^{-1} . By substantially increasing the sorbent dose to 38 g L^{-1} , the residual arsenic concentration 0.01 mg L^{-1} was achieved, corresponding to a relatively small sorption capacity of 1.3 mg g⁻¹ [20].

Similarly to Zhou et al. (2008) [21], Gupta et al. (2008) [20] developed the mesoporous hybrid adsorbent TiO_2/α -Fe₂O₃. This material has the ability to convert As(III) to As(V) by photocatalysis and to adsorb the formed As(V) by the iron oxides, because it was found that the properties of both components and nanoparticles, i.e., the photocatalytic activity of TiO₂ and the adsorptive feature of Fe₂O₃, remained quite unchanged in the composite form. The removal of As(III) was found to be linked directly with the pH value of water. In addition, Acry et al. (2011) [22] also synthesized TiO₂/ α -Fe₂O₃ composite adsorbent material, by applying a simple precipitating technique and examined it for arsenic removal. The highest capacity was found to be pH-dependent for this case, also.

2.3. Application of Iron(III)–Copper(II) Binary Oxide for As(V) and As(III) Removal

Recently, it was reported that cupric oxide was an effective sorbent for both As(V) and As(III) removals over a wide pH range values, relevant to drinking water treatment (i.e., for pH = 6.6–8.6), even in the presence of other competing anions, such as silica, sulfate and phosphate [23]. Zhang et al. (2013) [24] synthesized Fe–Cu binary oxides and evaluated their arsenic adsorption capacity. The results showed that the prepared Fe–Cu binary oxide particles are actually formed by smaller nano-sized particles and are very effective for the elimination of As(V) and As(III) species from waters. The highest adsorption capacities for As(V) and As(III) are 83 and 122 mg g⁻¹ at pH 7, correspondingly. Owing to its exceptional arsenic sorptive performance, straightforward and efficient synthesis process, and effective regeneration of depleted adsorbent materials, the Fe–Cu binary oxide

could serve as an adsorbent with promising application for both As(V) and As(III) species removal from water and wastewater [24].

Furthermore, this material shows increased capacity for As(III) sorption, which is very promising, because the problem with arsenic removal is that As(III) is usually less efficiently removed from waters by the application of conventional methods. Therefore, the application of such materials, showing increased As(III) sorption capacity, especially at the pilot–plant scale, would be very interesting and could show the potential of such methods to remove As(III) by circumventing the application of pre-oxidation step. Very recently, Jauckowicz-Sobala et al. (2020) [25] used these oxides (ratio Fe:Cu = 2:1) by depositing them onto polymer beads and showed that As(III) removal takes place through a two-step mechanism, namely catalytic oxidation and adsorption. The adsorptive ability was measured as 92 mg As g^{-1} of adsorbent, close to that previously referred by Zhang et al. (2013). Due to the formation of polymer beads, column experiments were performed, showing efficient removal of As(III) (reaching final concentrations below 10 µg L⁻¹) from quite high initial concentrations (up to 500 µg L⁻¹).

2.4. Application of Hierarchically Porous CeO₂-ZrO₂ Nanospheres for As(V) and As(III) Removal

Hierarchically porous CeO₂–ZrO₂ nanospheres were synthesized by Xu et al. (2013) [26], and their suitability as arsenic sorbents was examined. The CeO₂–ZrO₂ hollow nanospheres showed strong affinity and selectivity to arsenic with an adsorption capacity of 27 and 9 mg g⁻¹ for As(V) and As(III), respectively. These results were obtained at the equilibrium arsenic concentration of 0.01 mg L⁻¹ under circumneutral pH values (pH 6.9 ± 0.2). As(V) removal could be so efficient as to achieve residual concentration below 10 µg L⁻¹ (from starting As(V) concentrations 12 mg L⁻¹) by the CeO₂–ZrO₂ nanospheric materials with an adsorbent dose of 0.2 mg mL⁻¹, while for the case of As(III), this could be also reduced to below 10 µg L⁻¹, but from As(III) concentrations of 1 mg L⁻¹. Both cases are considered as very efficient, since the usual arsenic concentrations in groundwaters are much lower, i.e., between 20–500 µg L⁻¹. The significant adsorption capacity of CeO₂–ZrO₂ nanospheres is mainly due to the respective better pore accessibility and the abundant surface hydroxyl groups, participating to their substitution with arsenic species [26].

2.5. Application of Graphene Oxide-Ferric Hydroxide GO/Fe(OH)₃ (GO–Fe) Composites for As(V) Removal

Graphene is a two-dimensional (2-D) nanosheet of graphite with one atom thickness; it was firstly found in 2004 by Geim and Novoselov [27], and since then, a wide range of applications has been exploited, e.g., in transparent conductors, field-effect transistors, fuel cells, batteries, solar cells, and water purifiers [28–30], as well as in the food industry [31]. Graphene holds some exceptional properties, for instance, extremely large specific surface area (~2600 m² g⁻¹) and very strong chemical stability [27,32], making it an efficient material for use in the water industry, mainly as a support material, e.g., for the nano-scaled iron oxides, which were proven to be excellent adsorbents for the removal of arsenic [6].

Zhang et al. (2010) [33] developed a series of innovative composites, based on graphene oxide (GO) cross-linked with Fe-hydroxides with several GO/FeSO₄·7H₂O ratios, i.e., GO–Fe-1, GO–Fe-2, for the successful treatment of arsenic contaminated drinking water. GO was mainly used as a supporting substrate of ferric hydroxide, due to its several interesting properties, such as high mechanical strength, large surface area and simple preparation using inexpensive natural graphite.

The efficient As(V) sorption, using GO–Fe-5, was identified over a broad pH range, i.e., for pH 4–9, and different initial As(V) concentrations (0.5–20.0 mg L⁻¹), but the efficiency was decreased at pH values higher than 8, where iron oxides exhibit a negative overall surface charge, which repulses the negatively charged arsenate species, such as $HAsO_3^{2-}$ [19,34]. However, in all examined cases, the remaining Fe levels in the finished water were rather low (<1.0 mg L⁻¹), indicating that iron stays mostly stable on the support material and can be further tested in pilot-scale applications, e.g., using continuous operating adsorption columns [33].

2.6. Application of Magnetite Fe_3O_4 -Reduced Graphite Oxide–MnO₂ Nanocomposites for As(V) and As(III) Removal

Luo et al. (2012) [35], in their study, combined the oxidizing ability of manganese dioxide, the large surface area of GO and the magnetic characteristics of Fe₃O₄, aiming at synthesizing a new adsorbent for arsenic, i.e., Fe₃O₄ and MnO₂ nanoparticles modified GO (Fe₃O₄-RGO–MnO₂) nanocomposites. The preparation of this material was carried out by a two-stage precipitation reaction, starting with graphite oxide (GO) as the raw material, followed by the reduced Fe₃O₄-RGO as intermediate product, and forming finally a material with a specific area of 114 m² g⁻¹.

This adsorbent presents a high removal capacity towards both As(III) and As(V), i.e., 14 mg g⁻¹ and 12 mg g⁻¹, respectively (using a solution containing NaAsO₂ and Na₂HAsO₄·7H₂O), with specific emphasis given to the higher adsorption capacity of As(III). In addition, arsenic adsorption remained rather constant for a broad pH span between 2–10. The aforementioned adsorbent provides a prominent advantage that can be further separated from the treated water sample by the application of magnetic separation [36]. Consequently, from the pragmatic point of view, the Fe₃O₄-RGO–MnO₂ nanocomposites could serve as excellent adsorbents for treating arsenic polluted waters in the future [35].

2.7. Application of Graphene Oxide-Hydrated Zirconium Oxide for As(V) and As(III) Removal

Zirconium oxide is a generally applied inorganic substance that is chemically inert, non-toxic, and highly insoluble in water. It was stated that zirconium oxide demonstrated solid arsenic adsorption capacity, particularly for As(III) [37]. Luo et al. (2013) [38] described the use of GO as substrate to support zirconium hydroxide (ZrO(OH)₂) nanoparticles for the concurrent removal of As(III) and As(V) from aqueous solutions. The forming nanocomposites (GO–ZrO(OH)₂) were prepared by the hydro-thermal co-precipitation reaction. It was observed that this material exhibited very high adsorption capacity for As(V) and As(III), i.e., 95 and 85 mg g⁻¹, respectively, reaching the equilibrium within 15 min. The obtained results showed that GO–ZrO(OH)₂ (ratio 1:100) is exceedingly effective for the concurrent elimination of As(III) and/or As(V) [38].

2.8. Application of Nano-Scaled Activated Carbon Modified by Iron and Manganese Oxides for As(V) Removal

Recent developments include the successful removal of arsenic by activated carbon altered by iron and manganese oxides [39]. According to this study, a microporous activated carbon was impregnated with iron, iron/cobalt and iron/manganese mixtures by applying a novel and simple impregnation method, used for the preparation of magnetic activated carbons containing Fe₃(or Mn²⁺)O₄. The modified carbons were assessed for As(V) removal and showed enhanced capabilities. The best As(V) adsorption capabilities were obtained for the Fe₃-xMn_xO₄-modified activated carbon, where Mn ions were also integrated in the magnetite lattice. The inclusion of Mn influenced the textural properties of the carbon, which was concluded because of the decrease of the surface area, as well as of surface pH and the pH_{pzc} values and the rise of crystallinity values. It was indicated that arsenate, considered to be a Lewis base, becomes selectively adsorbed through the creation of inner-sphere bidentate complexes on the modified carbon surface. The impregnation of activated carbon with Fe gave an increment of As(V) maximum adsorption capability (Q_{max}) from about 4 mg g⁻¹ (for the raw carbon) up to 11 mg g⁻¹, while the inclusion of Mn caused an additional improvement in the adsorption capacity up to 19 mg g⁻¹.

Table 1 shows the reviewed nanomaterials when utilized for removal of As(III) and As(V) from aquatic sources and provides some more information about their structural characteristics and applications in water treatment. As shown in this Table, most of the proposed materials are efficient at pH values around 7, for the removal of both As(III) and As(V) species. It is worth noting that the Fe–Cu binary oxide material was found to be effective for removing both As(V) and As(III) species, providing an adsorption capacity of 122 mg g⁻¹ at pH 7 for As(III), while the hierarchically porous CeO₂–ZrO₂ nanospheres showed an adsorptive ability of only 9 mg g⁻¹ for the case of As(III). An increased

adsorption capacity was achieved when graphene oxide was combined with hydrated zirconium oxide (GO–ZrO(OH)₂) and the obtained adsorption capacity was found to be greatly increased (up to 95 mg g⁻¹). The latter material presents also a substantially larger surface area (421 m² g⁻¹), when compared with the 30 m² g⁻¹ of CeO₂–ZrO₂ nanospheres. In addition, the Fe–Cu binary oxides material presented specific surface area 282 m² g⁻¹.

Novel Nano-Materia	Fe(III)–Ti(IV) Oxide (NHITO)	Fe(III)-Cu(II) Oxide	CeO ₂ -ZrO ₂	GO/Fe(OH) ₃	Fe ₃ O ₄ -RGO–MnO ₂	GO–ZrO(OH) ₂
As species removal	As(III)	As(V)/As(III)	As(V)/As(III)	As (V)	As(V)/As(III)	As(V)/As(III)
Application	Groundwater	Simulated Ground water	Contaminated natural water	Simulated drinking	Simulated Ground water	Simulated drinking
Pore size (nm)	11	4.3	90	-	-	2.3
Dose (gL^{-1})	2	0.2	0.2	-	0.005	0.5
C initial (mg L ⁻¹)	0.11	10	0.01	51	5	1
pН	7.0	7.0	6.9	4.0-9.0	7.0	2.0-7.0
Adsorption capacity (mg g ⁻¹)	0.1	83/122	27/9	24	12/14	85/95
BET $(m^2 g^{-1})$	78	282	30	-	114	421
References	Gupta et al. (2009) [20]	Zhang et al. (2013) [24]	Xu et al. (2013) [26]	Zhang et al. (2010) [33]	Luo et al. (2012) [35]	Luo et al. (2013) [38]

Table 1. Novel nanostructured materials utilized for the removal of arsenic from waters.

Table 2 provides the comparison of Langmuir monolayer sorption capacities between different adsorbents, when applied for the removal of arsenic (III or V). As can be observed by comparing the relevant data of Table 2 with those in Table 1, the sorption ability of the previously described nanostructured materials (Table 1) was generally substantially higher.

Table 2. Comparative results of Langmuir monolayer sorption capacity for arsenic using the aforementioned materials.

	лU	Langmuir Q _{max}	Capacity (mg g ⁻¹)	Deferrere	
Sorbent Material	pn	As(III)	As(V)	- Keference	
Crystalline hydrous ferric oxide	7.0	33	25	Manna et al. (2003) [40]	
Crystalline hydrous titanium oxide	7.0	32	-	Manna et al. (2004) [41]	
Nanoscale zero valent iron	7.0	3	-	Kenel et al. (2005) [42]	
Nano-TiO ₂	7.0	60	37	Pena et al. (2005) [43]	
Hydrous stannic oxide	7.0	16	4	Manna et al. (2007) [44]	
Akaganeite nanocrystal	7.5	-	134	Deliyanni et al. (2003) [45]	

3. Nanostructured Materials for Chromium Removal

3.1. Chromium (Cr)

Chromium is an odorless and tasteless metallic element, and it can be found naturally in rocks, plants, soil and volcanic dust. The most widespread forms of chromium that appear in real waters are the trivalent and hexavalent species. Cr(VI) is 100 times more toxic than Cr(III), showing high carcinogenic, mutagenic and teratogenic action to biological systems [46]. Therefore, the Environmental Protection Agency (EPA) has set the maximum concentration limit of 0.1 mg L⁻¹ for the case of total chromium in water, whereas the World Health Organization (WHO) has set a lower respective limit (0.05 mg L⁻¹) in drinking water for Cr(VI) [47].

Chromium has been applied traditionally in the chrome plating of metallic surfaces, and also as an element in dyes and pigments, in steel, in the leather tanning process and as a wood preservative. It is frequently discharged to the environment, after the discarding of chromium-containing materials, or as a by-product of the industrial processes that use it. There are also demonstrated cases of chromium being released to the environment by leakage, poor storage or inadequate industrial waste disposal practices, causing severe anthropogenic groundwater contamination and human health problems [48]. The serious toxicity of Cr(VI) has attracted the attention of the scientific community and environmental associations, provoking an growing number of headlines and a general increase of public awareness. In that direction, on 1 July 2014, the US State of California adopted a lower Maximum Concentration Level (MCL) of 0.01 mg L⁻¹ for the presence of hexavalent chromium in drinking water [49].

To reduce Cr concentration from contaminated water sources, various treatment methods, such as coagulation followed by filtration [9], adsorption and membrane filtration, have been successfully applied. Nevertheless, for each of these treatment methods, some constraints exist, and therefore, it is challenging to address the newly imposed concentration limits [50].

The effective removal of Cr(VI), usually involves its preliminary reduction to Cr(III). In the trivalent state, chromium instantly forms $Cr(OH)_3$ or $(Cr,Fe)(OH)_3$, which are both very insoluble. The fairly lower solubility of $Cr(OH)_3$ and $(Cr,Fe)(OH)_3$ is mainly responsible for the generally low Cr(III) concentrations in waters, lower than the drinking water standards over the entire pH range relevant to drinking water [51].

However, it would be very useful for the drinking water treatment plants if Cr(VI) could be efficiently directly removed by sorption onto suitable materials, without the need for preliminary Cr(VI) reduction. Therefore, the current research is focusing on the development of novel adsorbent materials, with superior performance/competence against the removal of Cr(VI).

3.2. Application of NiO Nanoparticles for Cr(VI) Removal

Nickel oxide nanoparticles (NiO), as an adsorbent material, have been used to control the mobility of metal ions in the environment, because of their high surface area, low production cost and natural porosity for the removal of heavy metals from aqueous solutions [52]. In a recent study, Behnajady and Bimeghdar (2014) [53] synthesized NiO nanoparticles by a simple precipitation method, using sodium hydroxide, for the removal of Cr(VI) from aqueous solutions. The main parameters (i.e., starting concentration of Cr(VI), dose of material, initial pH value and temperature) were investigated, regarding their effect on adsorption capacity.

The results show that NiO nanoparticles with a mean size of 11 nm were efficient adsorbents for Cr(VI) with a reported adsorption capacity of 5 mg g⁻¹ for the initial Cr(VI) concentration 20 mg L⁻¹, by using 0.6 g L⁻¹ of absorbent at T = 30 °C. The pH variation under the aforementioned conditions, indicated that at the pH value of 4.7 the adsorption of Cr(VI) was the highest, approximately 98% [53].

3.3. Application of Graphene Oxide Functionalized with Magnetic Cyclodextrin–Chitosan for Cr(VI) Removal

A simple chemical bonding method to synthesize magnetic cyclodextrin–chitosan/graphene oxide (CCGO) was published in 2013 by Li et al. [54]. Cyclodextrins are cyclic oligosaccharides endued with a hydrophilic outer surface and a hydrophobic inner cavity, capable of developing inclusion complexes with a broad variety of guest molecules, certainly affecting their physicochemical properties [55]. Chitosan-based sorbents have exhibited relatively elevated sorption capacities for heavy metals, due to their high nitrogen content and porosity. On the other hand, graphene oxide (GO), comprising several oxygen-containing functional groups on its surface, shows high-level adsorption performance for metal ions, but cannot be easily separated from the finished water. Magnetic β -cyclodextrin–chitosan nanoparticles have attracted attention, due to their excellent properties, such as easy separation and elevated adsorption capability.

Thus, the magnetic β -cyclodextrin–chitosan/graphene oxide materials were formulated via a staged process, where the carboxyl groups of GO chemically react with the amine groups of magnetic

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 β -cyclodextrin–chitosan with the subsequent creation of chemical bonds between GO and chitosan. It was found that the Cr(VI) adsorptive capacity of CCGO strongly depends on the surface charge concentration, as well as on the specific surface area, and the respective adsorption capacity was found to be 68 mg g⁻¹ of Cr(VI) using the CCGO material. The observable differences between graphene oxide and CCGO originated mainly from the greater surface area in case of CCGO (446 m² g⁻¹) in contrast with the pure graphene oxide (342 m² g⁻¹), enhancing the availability of effective surfaces for sorption. Thus, the more effective deployment of relevant adsorption sites can be accomplished by the new adsorbent [54].

pH is an extremely significant variable affecting both the adsorption characteristics and the speciation of chromium. There are several forms of Cr(VI), namely chromate (CrO_4^{2-}) , dichromate $(Cr_2O_7^{2-})$ and hydrogen chromate $(HCrO_4^{-})$ [46]. These ionic forms are related to the solution pH, as well as to the total chromate concentration. During the adsorption, Cr(VI) is partially reduced to Cr(III) by the reductive surface hydroxyl groups, existing on the CCGO surface. According to the obtained results, when increasing the pH value, the uptake of Cr(VI) decreases, which is due to the higher concentration of OH^- ions present in the solution, competing with the Cr(VI) species. On this basis, when the pH is low (i.e., pH < 4), the uptake of Cr(VI) is about 55 mg g⁻¹, but at higher pH levels (i.e., pH > 6.5), the uptake of Cr(VI) decreases to 38 mg g⁻¹, when the initial Cr(VI) concentration is 50 mg L⁻¹ and the dosage of CCGO is 1 g L⁻¹. These results show the high potential of CCGO as an example of new composite materials, to remove effectively metal ions from wastewaters [54,55].

A recent study [56] involves the adsorption of hexavalent chromium, using chitosan grafted graphene oxide nanocomposite (CS-GO) in batch mode, providing an adsorption capacity of 104 mg g⁻¹, achieved at pH 2.0 and for the contact time of 420 min, noting also that the CS-GO material is recyclable up to 10 cycles with the minimum loss of adsorption capacity.

3.4. Application of Poly-Pyrrole Graphene Oxide Nanocomposite (PPy-GO NC) for Cr(VI) Removal

The sorption of Cr(VI) onto poly-pyrrole graphene oxide nanocomposite (PPy–GO NC) from waters was examined by Setshedi et al. (2015) [57], using batch and packed-bed column operational modes. The batch sorption isotherm data at the optimal solution pH value 2 were adequately described by the Langmuir isotherm model with a maximum sorption capacity 625 mg g⁻¹ at 25 °C. The sorption of Cr(VI) onto the PPy–GO NC adsorbent from binary ions systems was also assessed and the results revealed that the existence of ions had no significant effect on Cr(VI) removal. In addition, a volume of Cr(VI) contaminated water (64 L), with 10 mg L⁻¹, was effectively treated in column experiments, using 2 g of PPy–GO NC at a flow rate of 3 mL min⁻¹, effectively achieving the maximum allowable discharge limit.

3.5. Application of a Reductive and Magnetic Graphene/Fe₃O₄ Composite for Cr(VI) Removal

A highly reductive and magnetic graphene/Fe₃O₄ composite (HR-M-GO/Fe₃O₄) was created via the graphene oxide (GO) in situ oxidation of FeCl₂ by Hou et al. (2016) [58]. This super-paramagnetic composite material could be utilized for the exceedingly efficient removal of Cr(VI) from wastewaters, appropriately separated by employing an external magnet. The maximum adsorption capacity of the HR-M-GO/Fe₃O₄ for Cr(VI) achieves 32 mg g⁻¹, which is bigger than the simple graphene/ γ -Fe₂O₃ composite. The probable mechanism of HR-M-GO/Fe₃O₄, removing Cr(VI) efficiently was that Cr(VI) reduced to Cr(III) by the occurrence of ferrous hydroxide in the graphene structure and the resulting Cr(III) ions were simply captured by the negatively charged composite materials (HR-M-GO/Fe₃O₄).

3.6. Application of Graphene Oxide/Poly-Amido-Amine Dendrimer (GO/PAMAMs) Composites for Cr(VI) Removal

Graphene oxide/poly-amido-amine dendrimer (GO/PAMAMs) composites [59] were utilized to remove Cr(VI) from mimicked effluents. The results exhibited that the optimal pH value was 2.5, the removal percentage reached 91% for 30 mg L^{-1} initial concentration of Cr(VI) within 120 min

and the maximum adsorption capacity reached 211 mg g⁻¹ at 40 °C; while in the pH range of values 2.5–7.0, there was a sharp decline, regarding the removal efficiency of Cr(VI), i.e., it decreased as the pH value increased.

Table 3 shows the reviewed nanomaterials applied for Cr(VI) removal from water sources, providing information about their major structural characteristics and applications in water treatment. A comparison between the sorption capacities of selected adsorbents, recently reported in literature for the removal of Cr(VI) from aqueous solutions, is presented in Table 4, indicating that the previously presented nanomaterials (i.e., NiO and CCGO) showed enhanced sorption capacities (Table 3).

Novel Nano-Material	NiO	CCGO	CS-GO	PPy-GO NC	HR-M-GO/Fe ₃ O ₄	GO/PAMAMs
Cr species removal	Cr(VI)	Cr(VI)	Cr(VI)	Cr(VI)	Cr(VI)	Cr(VI)
Dose (g L^{-1})	0.6	1	2	2	0.5	0.5
C initial (mg L ⁻¹)	20	50	50	10	10	50
pH	4.7	3.0	2.0	2.0	3.0	2.5
Adsorption capacity (mg g ⁻¹)	5	68	104	625	32	211
References	Behnajady and Bimeghdar (2014) [53]	Li et al. (2013) [54]	Samuel et al. (2019) [56]	Setshedi et al. (2015) [57]	Hou et al. (2016) [58]	Liu et al. (2019) [59]

Table 3. Novel nanostructured materials applied for the removal of chromium mainly from wastewater sources.

Table 4.	Comparison	of the sorption	capacities of	various sorbents	towards Cr(VI) ions.

	Sorption Capacity (mg g^{-1})	D a farrara an		
Sorbent Material	Cr (VI)	Kelerence		
Amino starch	12	Dong et al. (2010) [60]		
Silica matrices	18	Alvarez et al. (2011) [61]		
Mesoporous TiO ₂	33	Asuha et al. (2010) [62]		
Alumina	4	Rajiv Gandhi et al. (2010) [63]		
Alumina/chitosan composite	9	Rajiv Gandhi et al. (2010) [63]		
Activated Alumina	2	Bishnoi et al. (2004) [64]		

Table 3 displays comparative results obtained from the different materials presented in this paper. Regarding Cr(VI) adsorption, it was shown that the most efficient adsorption takes place at pH values between 2 and 5 (i.e., acidic conditions) for almost all reviewed materials. Poly-pyrrole graphene oxide nanocomposite (PPy–GO NC) presents maximum sorption capacity 625 mg g⁻¹ at 25 °C. Higher adsorption capacity was observed by graphene based materials, compared especially to nickel oxide nanoparticles (NiO), which contain no graphene in its structure and provide the relatively lower absorption capacity (5 mg g⁻¹). The low (acidic) pH values is the main reason why adsorption is not considered as a favorable method for the removal of Cr(VI) at pH values more relevant to drinking water sources (i.e., 6.5–8.5). However, these adsorbents could be useful for the treatment of acidic wastewaters.

4. Nanostructured Materials for Uranium Removal

4.1. Uranium (U)

Identified as a harmful element, uranium (U) is plentiful in nuclear waste disposal facilities (and testing sites), as well as in uranium mining, processing and milling sites. In groundwaters,

it is usually present in the form of U(VI). Uranium contamination poses a threat to both surface and groundwaters [65,66]. Uranium disposed into the environment can ultimately reach the top of food chain and be consumed by humans, initiating severe kidney or liver damage and even death [67]. Thus, the WHO and US EPA recognized U(VI) as a human carcinogen and recommended 30 μ g L⁻¹ as the temporary guideline level for its presence in drinking water, after the 2012 relevant revision [68]. The contamination of groundwaters with uranium is a subject of concern in several countries around the world, such as in the USA, Canada, Germany, Finland, Norway, and Greece [68]. Therefore, it is very important to choose a suitable and effective method to remove uranium from water sources.

U(VI) is the most ubiquitous species of uranium in aerated waters, whereas in anoxic groundwaters, uranium is usually absent, because the respective reduced form (U(IV)) is insoluble in water [69]. The major uranium species in water supplies are the anionic carbonate complexes, i.e., the UO₂ (CO₃)^{2–}₂ at pH values lower than 7 and the UO₂ (CO₃)^{4–}₃ at pH greater than 8, whereas at pH values between 5 and 6.5 the neutral UO₂CO₃ species may also make up an important part, which depending on pH, could vary between 20%–90% [69].

The creation of the aforementioned complexes with carbonates determines its removal from water, depending on the application of specific treatment processes. For example, conventional methods, such as coagulation or lime softening, can remove uranium from water, but they are very sensitive to pH changes and water composition [8]. On the contrary, ion-exchange [70,71] is the most efficient removal method, because it can remove about 98% of uranium from water, mainly through the removal of anionic uranium carbonate species; the ion exchange resins used in this case are usually selective strong base (anionic) [8]. Membrane treatment methods, such as nano-filtration [72] or reverse osmosis, were also found to be efficient for the removal of uranium, removing the respective carbonate complexes by more than 90%, but their application requires experienced personnel and their use is quite expensive, especially when designed for the treatment of small volumes of contaminated water [8,73,74].

4.2. Application of Fe₃O₄@SiO₂ Composite Nanoparticles for U(VI) Removal

Das et al. (2010) [75] studied the sorption of U(VI) on magnetite (Fe₃O₄) nanoparticles, but the sorption capacity was relatively small. Silica has been known as one of the most ideal coating layers for the magnetic Fe₃O₄ nanoparticles, due to its reliable chemical stability, biocompatibility, and facile surface modification. Magnetic Fe₃O₄@SiO₂ composite particles were successfully applied by Fan et al. (2012) [66] as a novel and effective adsorbent material for the removal of U(VI) from aqueous solutions. The sorption of U(VI) onto magnetic Fe₃O₄@SiO₂ composite particles was strongly dependent on pH values. With increasing pH (i.e., from 2 to 6), the adsorption capacity was also increased. When the initial pH value varied from 2 to 4, the sorption capacity of U(VI) increased from 0 to 8.5 mg g⁻¹, while when the initial pH was further increased from 4 to 6, the sorption capacity of uranium increased substantially (i.e., from 8 to 20 mg g⁻¹). However, when increasing the pH value from 6 to 8, the sorption capacity started to decrease. The maximum sorption value for U(VI) onto Fe₃O₄@SiO₂ magnetic composites was about 20 mg g⁻¹, when the initial concentration of U was 50 mg L⁻¹. Therefore, the optimum (initial) pH value was 6, when applying this treatment technique, which is in agreement with other relevant studies regarding the sorption of U(VI) onto iron oxides or hydroxides, i.e., they present a maximum sorption capacity in the pH range between 6–7 [76–78].

The aforementioned magnetic $Fe_3O_4@SiO_2$ composite particles showed an excellent ability to remove uranium from aqueous solutions and the maximum U(VI) sorption capacity was about 52 mg g⁻¹ at 25 °C. Hence, this adsorbent material could be a potential candidate to remove the toxic U(VI) forms from aqueous solutions and the results of this study can also provide a technique for the removal or recovery of other heavy/toxic metal ions from aqueous solution [66].

4.3. Application of a Novel Graphene Oxide-Activated Carbon Felt Composite for U(VI) Removal

Chen et al. (2013) [67], prepared a composite material, Graphene oxide (GO)-activated carbon felt(ACF)(GO-ACF) and tested for the removal of U(VI) from aqueous solution, comparing the simple

ACF and the composite GO-ACF materials. The adsorption of U(VI) on ACF is remarkably improved by the presence of GO, covalently bonding with ACF. The maximum sorption capacity of GO-ACF for U(VI) was evaluated to be 298 mg g⁻¹ at pH 5.5, i.e., much higher than that of ACF (173 mg g⁻¹), suggesting that the carboxyl functional groups of GO-ACF can play an important role in the sorption.

4.4. Application of a Three-Dimensional Layered Double Hydroxide-Graphene Hybrid Material for *U(VI)* Removal

Graphene has recently attracted attention for its U(VI) sorption and recent studies have reported a substantially high maximum sorption capacity of 299 mg g^{-1} at the pH value 4 [79], mainly due to the formation of inner-sphere surface complexes of U(VI) on GO. In the past few years, the layered double hydroxides (LDHs) containing transition metals, have also been employed as effective adsorption materials. Their large interlayer space and the high concentration of active sites have allowed the preparation of several multi-functional LDH materials to be used as anion exchangers, adsorbents, or magnetic materials. Tan et al. (2015) [80] synthesized a 3-D hierarchical composite with graphene sandwiched between two layers of NiAl–LDH nanosheets, by using a simple and cost effective in situ growth procedure; during the in situ crystallization process NiAl–LDH nanosheets grew on the surface of GO@AlOOH sheets, obtained by mixing boehmite AlOOH primer sol with GO solution, under specific conditions [80].

When examined as an adsorbent for U(VI) removal, several advantages of this NiAl–LDH composite material make it specifically attractive, because: (1) it is manufactured using an easy, non-toxic synthesis procedure; (2) the larger specific surface area of 257 m² g⁻¹ can provide more adsorptive sites; (3) it can be used for the effective adsorption/removal of uranium(VI) ions.

The adsorption of U(VI) onto rGO/LDH was carried out by varying the pH values (2–12); it was found that the adsorption capacity was highly dependent on pH value. At pH less than 4, U(VI) is present in solution predominantly in the form of UO_2^{2+} with a lower sorption capacity, mainly due to the competition of H⁺ ions for the binding sites of adsorbent. At the pH range 4–8, the hydrolysis of uranyl ions occurs, producing several uranium species that include $UO_2(OH)^+$, $(UO_2)(OH)_2$, $(UO_2)_3(OH)_5^+$ and $(UO_2)_2(OH)_2^{2+}$, which are available for adsorption onto rGO/LDH, and the sorption reaches a maximum value, especially in the absence of carbonates. In pH values > 8, the fraction of $(UO_2)_3(OH)_7^-$ anions (known for their generally low sorption affinity) increases, leading to a decrease of uranium(VI) uptake. As a consequence, the pH value 4 is considered optimum for the adsorption of U(VI) onto rGO/LDH with maximum sorption capacity of the rGO/LDH composite for uranium (VI) 278 mg g⁻¹. Therefore, rGO/LDH is a novel adsorbent, exhibiting a bright future for practical application, regarding the removal of U(VI) from aqueous solutions [80].

4.5. Application of Graphene Oxide and Its Amine-Functionalized Composite (GO-NH₂) for U(VI) Removal

A new amine-functionalized graphene oxide (GO-NH₂) nanosheet was prepared via covalently grafting reaction by Liu et al. (2016) [81]. The adsorption capacities of GO and of GO-NH₂ were found to be 97 and 215 mg g⁻¹ at 298 K, respectively. These results showed that the adsorption capacity of GO was significantly improved by amine functionalization. The adsorption of UO_2^{2+} ions depends upon the uranium species distribution in solution, which mostly depends on the respective pH value. Uranium can be hydrolyzed into different mononuclear and polynuclear hydrolysis products in the form of $(UO_2)_m(OH)_n]^{(2m-n)+}$ [82]. As the pH value is lower than 4, the UO_2^{2+} ions exist predominantly in the aqueous solution as the monomeric species. However, with the increase of pH, the hydrolysis of U(VI) ions will occur. Both materials achieved their maximum sorption capacity at the pH value 5.5.

4.6. *Application of a Novel Graphene Oxide-Immobilized Saccharomyces Cerevisiae Gel Beads for U(VI) Removal*

According to a recent study by Chen and Wang (2016) [83], the waste biomass of Saccharomyces cerevisiae was immobilized using several agents, including Ca-alginate (Ca-SA), Ca-alginate plus

graphene oxide (Ca-SA-GO), or in combination with polyvinyl alcohol (PVA, 5% or 10%, w/v), i.e., PVA-Ca-SA-GO, using a CaCl₂-boric acid solution, in order to evaluate their ability to adsorb dissolved U(VI). The obtained experimental results showed that graphene oxide at 0.01% (w/v) could enhance the performance of immobilized cells.

The yeast gel beads, prepared with 5% PVA, 1% SA, 2% yeast, 0.01% GO, 2% CaCl₂ and saturated boric acid, generally showed better physical–chemical properties, such as higher tolerance, when unfavorable environmental conditions were applied. Moreover, the gel beads exhibited more stable capacity for U(VI) sorption and desorption at various conditions, such as pH in the range of 3–9. The effects of initial pH at acidic (pH = 3), neutral (pH = 7) and alkaline conditions (pH = 9) on U(VI) adsorption were studied and the results suggested that the optimum pH value for U(VI) adsorption is between 2.6 and 5. The immobilized *Saccharomyces cerevisiae* biomass, using SA, PVA and/or GO substrate materials, showed particular changes in the molecular vibration of functional groups, such as carboxyl, amide and hydroxyl groups, which may be involved in the U(VI) binding, when compared with the raw yeast biomass.

4.7. Application of Carboxyl-Functionalized Graphene Oxide (COOH-GO) Material for U(VI) Removal

The effect of increasing the presence of specific chemical functional groups, such as the carboxyl groups, on the selectivity of uranium sorption was investigated by using a carboxyl-functionalized graphene oxide (COOH-GO) modified material, which was studied in comparison with the simple graphene oxide (GO) and with graphite [84]. According to Mohamud et al. (2018), the modified COOH-GO demonstrated superior performance as a sorbent material for the selective removal of uranyl ions from aqueous solution with distribution coefficient value, *K*, $3.72 \pm 0.19 \times 10^3$ mL g⁻¹ in comparison to $3.97 \pm 0.5 \times 10^2$ and $2.68 \pm 0.2 \times 10^2$ mL g⁻¹ values for GO and graphite, respectively. Moreover, COOH-GO presents a higher sorption capacity for U ($Q_{max} = 169 \text{ mg g}^{-1}$) and shows a greater selectivity towards U with 65.9 ± 2.7% retained in the presence of competing ions in comparison to $38.9 \pm 1.2\%$ value, observed for GO, at the optimum pH 4. These enhanced values are most probable due to the effect of selective surface groups presence, such as the carboxyl.

4.8. Application of a Composite Material (GO-DTPAA) for U(VI) Removal

A novel chelator diethyl-enetri-amine-penta-acetic phenyl-enedi-amine (DTPAA) was covalently bonded to a supporting matrix of graphene oxide (GO), and a composite material (GO-DTPAA) was obtained recently by Liu et al. (2018) [85]. The obtained results indicated that GO-DTPAA was a highly efficient absorbent for the removal of U(VI) from aqueous solutions at pH 6.5. The adsorption capacity of GO-DTPAA was as high as 485 mg g⁻¹ at 298 K, which was far greater than that of pristine GO (97 mg g⁻¹) at the same temperature. The thermodynamic parameters revealed that the adsorption of uranium ions onto the pristine GO and by the GO-DTPAA composite material are feasible, spontaneous and endothermic.

4.9. Application of a Magnetic Reduced-Graphene Oxide/Tea Waste Composite for U(VI) Removal

Recently, Yang et al. (2019) [86] studied the preparation and application of relatively low-cost and highly efficient adsorptive materials for the removal of uranium from nuclear wastes, such as composites of graphene oxide (GO) and tea waste (TW). The composites GO-TW and the magnetic rGO/Fe₃O₄/TW exhibited higher adsorption capacities and faster adsorption kinetics than the simple materials GO and TW ($Q_{max (TW)} = 92 \text{ mg g}^{-1}$, $Q_{max (GOTW)} = 112 \text{ mg g}^{-1}$ and $Q_{max (rGO/Fe3O4/TW)} = 105 \text{ mg g}^{-1}$), resulting to higher removal rates (~99%) for U(VI). As aforementioned, the solution pH substantially affects the speciation of uranium in the aqueous solutions, and hence, significantly influences the uranium adsorption process. The adsorption of U(VI) on TW, GOTW and rGO/Fe₃O₄/TW significantly increased with increasing the pH value from 2.0 to 5.0. At the pH 5, the removal rate of uranium by TW, GOTW and rGO/Fe₃O₄/TW materials reached the highest values, noting that at pH value < 4.0, uranium exists mainly in the form of UO₂²⁺. Furthermore, due to the advantageous magnetic

properties, rGO/Fe₃O₄/TW can be easily separated from the treated aqueous solutions, thus enhancing the post-treatment efficiency for further practical applications.

Table 5 shows the reviewed nanomaterials applied for U(VI) removal from waste/water sources, providing major information about their structural characteristics and their applications in water treatment.

Novel Nano-Material	Fe ₃ O ₄ @SiO ₂	GO	GO-ACF	rGO/ NiAl-LDH	GO-NH ₂	SA-GO	COOH-GO	GO-DTPAA	rGO/Fe ₃ O ₄ / TW
Dose (g L ⁻¹)	2.5	0.4	0.2	0.5	0.2	0.1	1.0	0.1	0.5
C initial (mg L ⁻¹)	50	119	50	130	60	35.6	10	50	10
рН	6.0	4.0	5.5	4.0	5.5	5.0	4.0	6.5	5.0
Adsorption capacity (mg g ⁻¹)	52	299	298	278	215	162	169	485	105
References	Fan et al. (2012) [66]	Li et al. (2012) [79]	Chen et al. (2013) [67]	Tan et al. (2015) [80]	Liu et al. (2016) [81]	Chen and Wang (2016) [83]	Mohamud et al. (2018) [84]	Liu et al. (2018) [85]	Yang et al. (2019) [86]

Table 5. Novel nanostructured materials applied for the removal of U(VI) from waste/water sources.

As revealed from Table 5, the proposed materials seem to work more efficiently for the U(VI) removal at pH values between 4–6. The composite material (GO-DTPAA) exhibits maximum absorption capacity 485 mg g⁻¹. The other proposed materials with graphene, showed an average high adsorption capacity of 200–300 mg g⁻¹.

Table 6 provides the comparison of sorption capacity between different adsorbents, when applied for the removal of uranium. As can be observed by comparing the relevant data of Tables 5 and 6, the sorption ability of the previously described nanostructured materials was generally substantially higher.

Contract Matarial	nН	Sorption Capacity (mg g ⁻¹)	Reference	
Sordent Material	PII	Cr (VI)		
Manganese oxide coated zeolite	4.0	15	Han et al. (2007) [87]	
Natural sepiolite	3.0	35	Donat (2009) [88]	
Modified clays with titanium oxide		0.6	Humelnicu et al. (2009) [89]	
Magnetite nanoparticles		5	Das et al. (2010) [75]	
Ethylenediamine-modified chitosan		83	Wang et al. (2011) [90]	
Goethite (α -FeOOH)	6.0	34	Yusan et al. (2011) [91]	
Binary iron-manganese oxy-hydroxides (FMHO)	6.5	133	Dimiropoulos et al. (2015) [92]	

Table 6. Comparison of sorption capacities between various sorbents towards the removal of U(VI) ions.

5. Conclusions

The pollution of natural waters caused by toxic metals is a global issue, and various treatment technologies have been developed to remove these inorganic pollutants from water sources (mostly from groundwater). The application of most important novel nanostructured materials was summarized, regarding the removal of arsenic (As(III) and As(V)), chromium ((Cr(III) and Cr(VI)) and uranium (U(VI)) from aqueous systems. As it was shown, the use of nanostructured materials, exhibiting generally higher surface areas and average structural sizes below 100 nm, could be very promising in this direction.

Specifically, in this review, the most certain of the novel and recently applied materials for the removal of certain inorganic pollutants from water sources were summarized, providing their major structure characteristics and application conditions (Table 1), according to relevant recent literature. In particular, the removal of arsenic was examined by the application of hierarchically porous CeO_2 –ZrO₂ nanospheres material, as well as by the incorporation of other metal ions into

the lattice structure of iron(III) oxide, such as the hydrous titanium(IV), the bimetallic mixed oxide (NHITO), and the copper(II) binary oxide nanomaterials.

Of particular interest was the application of graphene and a series of novel composite materials based on graphene oxide (GO), such as graphene oxide-ferric hydroxide $GO/Fe(OH)_3$ composites, magnetite Fe_3O_4 -reduced graphite oxide– MnO_2 and graphene oxide-hydrated zirconium oxide. Among these materials, the iron(III)-copper(II) binary oxide and the Fe_3O_4 -reduced graphite oxide– MnO_2 , showed particularly high adsorption capacity for the case of As(III) in comparison to As(V), especially for the treatment of anaerobic groundwaters, mostly containing As(III), and avoiding the preliminary oxidation step to the pentavalent As form.

Regarding chromium removal, this review referred to the application of nickel oxide nanoparticles, because of their high surface area, and their very promising magnetic cyclodextrin–chitosan/graphene oxide (CCGO) and other composite materials, such as CS-GO, PPy–GO NC, HR-M-GO/Fe₃O₄, GO/PAMAMs. These materials, were found to be very efficient for the adsorption/removal of Cr(VI), but only in the strongly acidic pH area, i.e., at pH values below 5, and therefore, they could find applications for the treatment of acidic wastewaters, avoiding the usually applied preliminary reduction step towards the Cr(III) formation.

Uranium could likely be removed from aqueous solutions by the application of magnetic $Fe_3O_4@SiO_2$ composite particles, as a novel and effective adsorbent material, as well as by the application of several novel and optimum graphene modified composite materials, such as rGO/LDH, GO-ACF, GO-NH₂, COOH-GO, GO-DTPAA, GO-TW, and rGO/Fe₃O₄/TW, showing promising results. However, these materials need to be tested for the treatment of much lower initial concentrations, relevant to drinking water treatment. Furthermore, these materials need to be applied in real natural ground/waters, containing all the commonly found co-existing anions, such as carbonate, phosphates and sulfates, because most of the presented results were obtained using deionized waters (i.e., performing model experiments).

Author Contributions: Data curation, A.K.T.; Writing draft, A.K.T. and I.A.K.; Validation, A.I.Z. and I.A.K.; Visualization, A.K.T., I.A.K. and A.I.Z.; Writing—Review and editing, A.K.T., I.A.K. and A.I.Z.; Supervision, A.I.Z. All authors have read and agreed to the published version of the manuscript.

Funding: This research received no external funding.

Conflicts of Interest: The authors confirm that this article content has no conflict of interest.

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