

Article

Derivation of Oscillators from Biquadratic Band Pass Filters Using Circuit Transformations

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Abstract: Network transformations are the techniques to obtain new functional schemes from available circuits. They are systematic methodologies, since each transformation technique can be applied to many circuits to obtain the desired functions or characteristics. A convenient network transformation method, exploiting different circuit transformations, for deriving linear sinusoidal oscillators from biquadratic band pass filters is proposed. This method with generality can be applied to any band pass filter. The oscillation frequency of the new obtained oscillator is identical to the center frequency of the original band pass filter, and the useful properties of the selected band pass filter can be retained. Two examples are illustrated to confirm the feasibility of the proposed approach. The workability of the obtained oscillators is verified with PSPICE simulations.

Keywords: band pass filter; circuit transformation; sinusoidal oscillator; sensitivity

1. Introduction

Sinusoidal oscillators play an essential role in most electronic systems. They find numerous applications in instrumentation, measurement, control and communication systems. New oscillator

circuits based on various active elements have been proposed continuously [1–4]. Most oscillators proposed in the literature have been on an *ad hoc* basis, *i.e.*, a topology is chosen using an arbitrary procedure and is then analyzed. For the design of oscillator circuits, it is useful to follow systematic methodologies to obtain novel circuits. This is beneficial in developing analog tools for circuit design automation. The first systematic synthesis of canonic oscillators using controlled sources was given in [5]. The design of single op-amp single resistance controlled oscillators was reported in [6]. The generation method by using unity gain cells was given in [7]. Generalized synthesis approach for Gm-C oscillators using the signal flow graph approach was given in [8,9]. A systematic state-variable approach to the synthesis of canonic current feedback op-amps-based oscillators was given in [10]. In recent times, the concepts of pathological elements have been proven to be very useful for circuit analysis, transformation and synthesis. Their applications have been presented in the literature [11–14]. By the use of nodal admittance matrix expansion method and pathological elements, the systematic synthesis of the current conveyor-based active RC canonic oscillators was reported in [15,16].

To conveniently derive oscillator circuits, a systematic synthesis method is presented in this paper. By exploiting circuit transformations to the original biquadratic band pass filter, the oscillator circuit can be obtained. It retains some useful properties of the original band pass filter. Two circuit examples are given to demonstrate the feasibility of the proposed method. The workability of the derived oscillators is verified by PSPICE simulation.

2. Description of the Proposed Method

The proposed approach involves the use of complementary and inverse transformations. One can obtain a complementary voltage-mode network by interchanging the input and ground of a circuit [17,18], as shown in Figure 1. The resulting transfer function (TRANSF) T_2 of the obtained circuit would be the complement (COMP) of the original voltage transfer function T_1 ; *i.e.*, $T_2 = 1 - T_1$. According to inverse transformation by interchanging the output norator and the input voltage source of a circuit (with its transfer function $T_3 = Y/U$), the inverse transfer function (INV) can be obtained as $T_3' = 1/T_3 = Y'/U'$, as shown in Figure 2 [12]. The inverse network can also be obtained by interchanging the output pathological current mirror and the input source of a circuit [19]. To obtain a sinusoidal oscillator from the biquadratic band pass filter, the combination of circuit transformations can be exploited, as the stages shown in Tables 1 and 2.

Figure 1. The complementary transformation for voltage-mode a network. (a) Original network; (b) complementary network of (a).

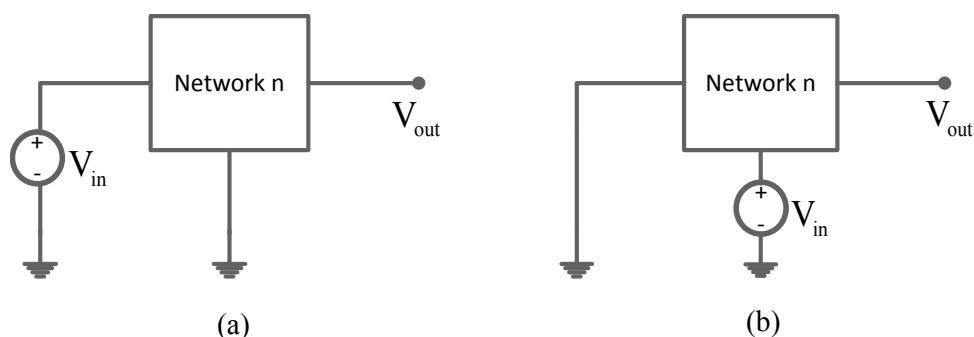


Figure 2. The inverse transformation of a circuit. (a) Original network; (b) inverse network of (a).

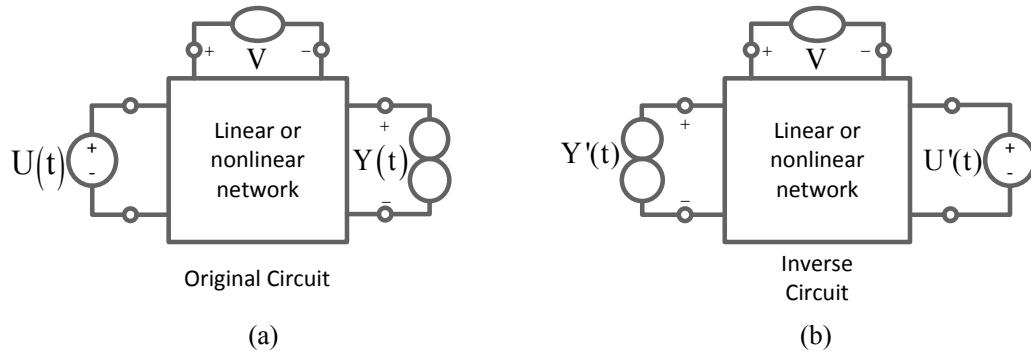


Table 1. The combination of complementary-inverse transformation (TRANSF) for a voltage-mode network. COMP, complement; INV, inverse transfer function.

Procedure	Stage (0)	Stage (1): COMP of (0)	Stage (2): INV of (1)	Stage (3): COMP of (2)
TRANSF	T	1-T	$\frac{1}{1-T}$	$\frac{T}{T-1}$

Table 2. Another combination of complementary-inverse transformation for a voltage-mode network.

Procedure	Stage (0)	Stage (1): INV of (0)	Stage (2): COMP of (1)	Stage (3): INV of (2)
TRANSF	T	1/T	$\frac{T-1}{T}$	$\frac{T}{T-1}$

To describe the synthesis method clearly, a biquadratic voltage-mode band pass filter with its transfer function given by Equation (1) is considered. The pole frequency ω_o and bandwidth (BW) of the filter can be computed as $\omega_o = \sqrt{c}$ and $BW = \omega_o/Q = b$, where Q is the quality factor of the filter. The coefficient b and c are always greater than zero for a stable system.

$$T(s) = \frac{V_0}{V_{in}} = \frac{as}{s^2 + bs + c} \quad (1)$$

Applying the proposed procedure in Tables 1 or 2 to this filter, we obtain its new transfer function as Equation (2).

$$T'(s) = \frac{V_0}{V_{in}} = -\frac{as}{s^2 + (b-a)s + c} \quad (2)$$

Namely, the new filter with $\omega_o = \sqrt{c}$ and $\omega_o/Q = (b-a)$ is derived.

For a positive-feedback system in Figure 3 with a stable amplifier stage $A(s)$ and a frequency-selective network $B(s)$ connected in a positive-feedback loop, the closed-loop gain $A_f(s)$ can be expressed by:

$$A_f(s) = \frac{X_0}{X_{in}} = \frac{A(s)}{1 - A(s)B(s)} \quad (3)$$

If at a specific pole frequency ω_o the loop gain $A(s)B(s)$ is equal to unity, A_f will be infinite. That is, at this frequency, the system defined as an oscillator will have a finite output for zero input signal. Thus, the condition for the feedback loop of Figure 3 to provide sinusoidal oscillations of frequency ω_o is:

$$1 - A(j\omega_o)B(j\omega_o) = 0 \quad (4)$$

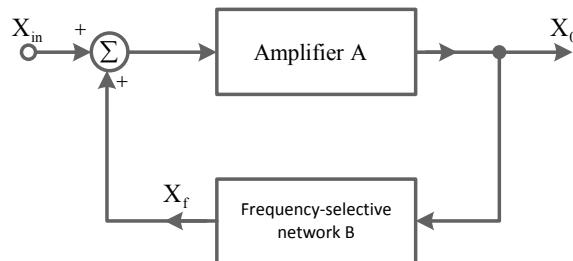
This is known as the Barkhausen criterion. Therefore, a linear oscillator can be synthesized by zeroing the input source of the filter [18]. The obtained characteristic equation of the oscillator can be expressed as Equation (5). The oscillation condition is given by Equation (6) and oscillation frequency can be expressed by $\omega_o = \sqrt{c}$.

$$\Delta(s) = s^2 + (b-a)s + c = 0 \quad (5)$$

$$b - a = 0 \quad (6)$$

In general, Equation (6) can be easily satisfied by selecting suitable passive components of the original band pass filter.

Figure 3. A positive-feedback system with a stable amplifier stage, A, and a frequency-selective network, B.



It is known that the grounded nullator and norator will be conducive to lower active sensitivities of a circuit [20]. The proposed oscillator synthesis procedure includes performing inverse transformation and zeroing the input signal source. This will result in the circuit processes grounded nullator and norator (as we add a series nullator-norator pair between the outputted node and the ground and then interchange the inputted signal source with outputted norator to perform inverse transformation). Therefore, an oscillator with lower active sensitivities may be derived. Therefore, the obtained oscillator has identical passive sensitivities and may have improved active sensitivities with respect to the original band pass filter.

3. Application Examples and Discussion

To demonstrate the feasibility of the proposed method, we first consider the voltage-mode low active and passive sensitivities band pass filter modified from the filter circuit in Figure 1 of [21], as redrawn in Figure 4a. Its transfer function is given by Equation (7). By using the transformation in Table 1, the obtained circuit with its transfer function given by Equation (8) is shown in Figure 4b.

A series nullator-norator pair is added during performing the inverse transformation. By zeroing the input signal source, we obtain the oscillator in Figure 5a. The nullator-norator pair in Figure 5a can be realized by a second generation current conveyor (CCII-) [16], as shown in Figure 5b. Taking into account the non-idealities of a current conveyor, namely $I_Z = \pm\alpha I_X$, $V_X = \beta V_Y$, where $\alpha = 1 - e_i$ and e_i denotes the current tracking error, $\beta = 1 - e_v$ and e_v denotes the voltage tracking error of a current conveyor, respectively, the non-ideal characteristic equation of the oscillator is expressed by Equation (9). Its oscillation condition and oscillation frequency ω_o are given by Equations (10) and (11), respectively. The sensitivities of ω_o to active and passive components are given in Equation (12). It is clear that the obtained oscillator has identical passive sensitivities and has improved active sensitivities compared to the original band pass filter [21]. In addition, the oscillation frequency and the oscillation condition are independently adjustable through with R_3 and R_1 . In reality, R_1 must be slightly greater than R_2/α_1 for the startup of oscillation [22].

Figure 4. (a) A CCII-based band pass filter; (b) the obtained filter after applying the transformations in Table 1.

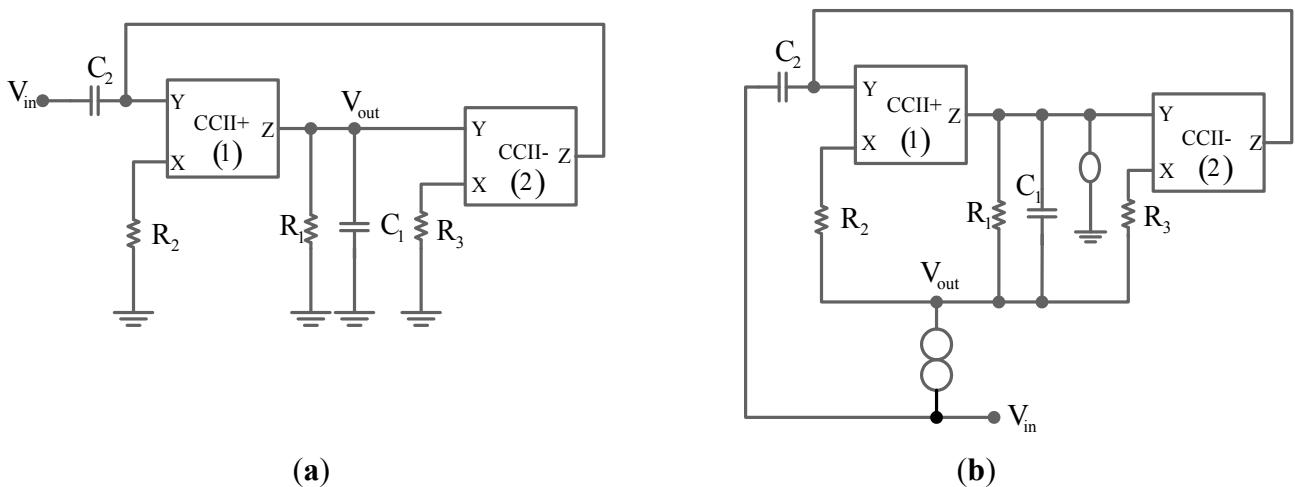
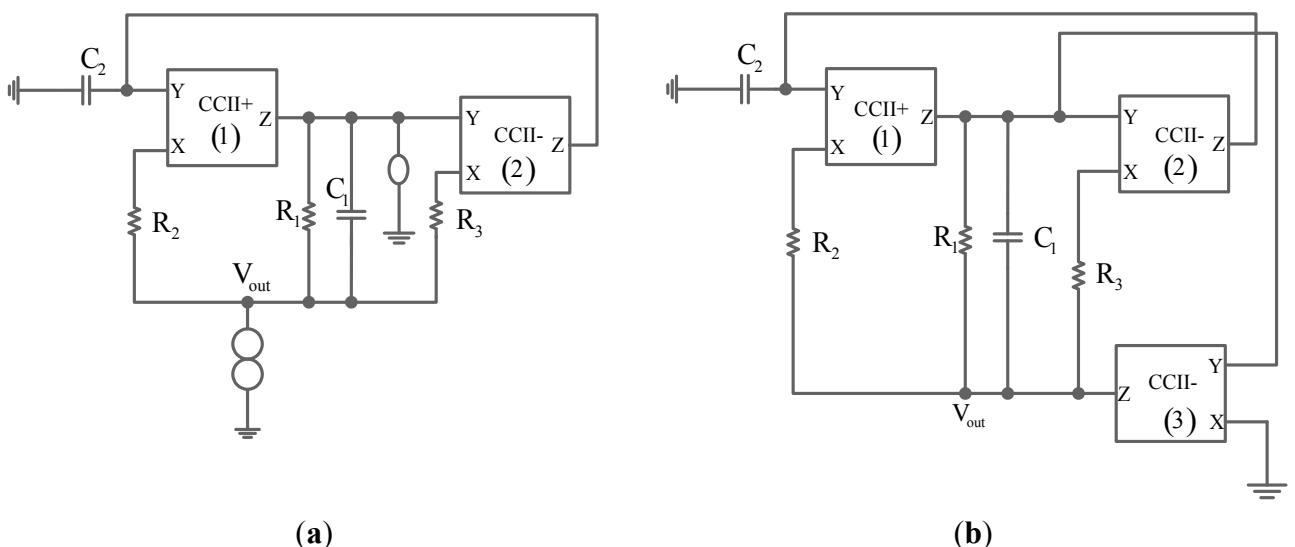


Figure 5. (a) The obtained oscillator; (b) realization of the obtained oscillator in (a).



$$\frac{V_{out}}{V_{in}} = T(s) = \frac{s \left(C_2 / R_2 \right)}{s^2 C_1 C_2 + s \left(C_2 / R_1 \right) + 1 / R_2 R_3} \quad (7)$$

$$T'(s) = -\frac{s \left(C_2 / R_2 \right)}{s^2 C_1 C_2 + \left(\frac{1}{R_1} - \frac{1}{R_2} \right) C_2 s + \frac{1}{R_2 R_3}} \quad (8)$$

$$s^2 C_1 C_2 + s C_2 (G_1 - \alpha_1 G_2) + \alpha_1 \alpha_2 \beta_1 G_2 G_3 = 0 \quad (9)$$

$$G_1 = \alpha_1 G_2 \quad (10)$$

$$\omega_0 = \sqrt{\frac{\alpha_1 \alpha_2 \beta_1 G_2 G_3}{C_1 C_2}} \quad (11)$$

$$S_{\alpha_1, \alpha_2, \beta_1}^{\omega_0} = \frac{1}{2}; S_{\beta_2}^{\omega_0} = 0$$

$$S_{G_2}^{\omega_0} = S_{G_3}^{\omega_0} = -S_{C_1}^{\omega_0} = -S_{C_2}^{\omega_0} = \frac{1}{2}; S_{G_1}^{\omega_0} = 0 \quad (12)$$

The second example considers the single CCII-based voltage-mode band pass filter, which is obtained from [23], as shown in Figure 6a. Using the transformed procedure mentioned in Table 2, the derived circuit with its transfer function shown in Equation (13) is given by Figure 6b. Figure 7a shows the derived oscillator by grounding the input source of the circuit in Figure 6b. The nullator and norator in Figure 7a can be realized by a CCII-, as shown in Figure 7b. The characteristic equation of the obtained oscillator can be expressed by Equation (14). The oscillation condition and the oscillation frequency can be respectively given by Equations (15) and (16) with $R_2 = R_3 = R$ and $C_1 = C_2 = C$. It can be found that the oscillation condition and oscillation frequency are orthogonal adjustable. It must be noted that R_1 must be slightly less than $R/3$ for the startup of oscillation.

$$T'(s) = \frac{V'_{out}}{V_{in}} = -\frac{\left(C_2 / R_1 \right) s}{s^2 C_1 C_2 + \left(\frac{C_1}{R_3} + C_2 \left(\frac{1}{R_2} + \frac{1}{R_3} \right) - \frac{C_2}{R_1} \right) s + \frac{1}{R_2 R_3}} \quad (13)$$

$$s^2 C_1 C_2 + \left(\frac{C_1}{R_3} + C_2 \left(\frac{1}{R_2} + \frac{1}{R_3} \right) - \frac{C_2}{R_1} \right) s + \frac{1}{R_2 R_3} = 0 \quad (14)$$

$$R_1 = \frac{R_2 R_3 C_2}{R_3 C_2 + R_2 (C_1 + C_2)} = \frac{R}{3} \quad (15)$$

$$\omega_o = \frac{1}{\sqrt{C_1 C_2 R_2 R_3}} = \frac{1}{RC} \quad (16)$$

Figure 6. (a) A CCII-based band pass filter; (b) the obtained filter after applying the transformations in Table 2.

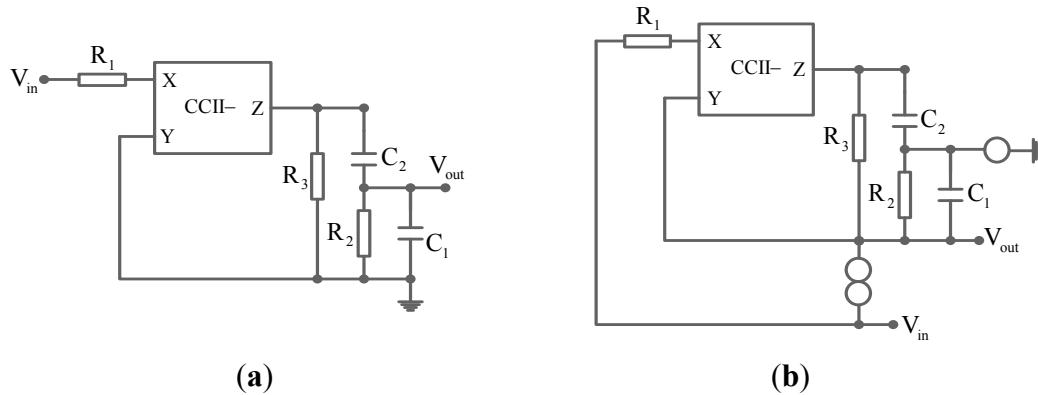
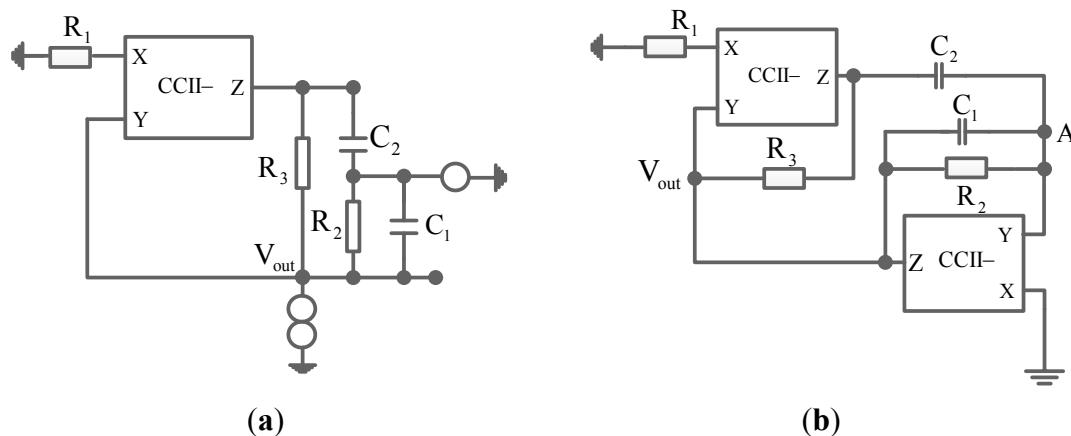


Figure 7. (a) Grounding input of Figure 6b; (b) realization of the obtained oscillator in (a).



Moreover, it can be found that the oscillator in Figure 7b possesses an electrically controllable function of the oscillation condition by using a controlled current conveyor (CCCI- τ) to realize the CCII- and R_1 . It is known that the ground node of a nullor-based oscillator can be chosen arbitrarily without affecting the characteristic equation [24]. Therefore, the grounded capacitor oscillator can be obtained by selecting Node A in Figure 7b as the ground. In addition, more oscillators can be obtained by applying adjoint network theorem or RC-CR transformation.

It must be noted that the proposed method can be applied to any band pass filters, so it has better generality compared to the transformed method in [25], which can only be applied to the filters with specific configuration and cascadable property. Furthermore, since the oscillation frequency of the synthesized oscillator is identical to the center frequency of the original band pass filter, one can obtain high-performance oscillators by choosing the suitable band pass filters for transformation. For example, the aforementioned band pass filters with low-sensitivity or electronically adjustability can be selected to obtain useful oscillators. Furthermore, current-mode linear oscillators can also be derived according to the proposed method, because the complementary and inverse transformations can be applied to current-mode circuits.

4. Simulation Results

To verify the theoretical prediction of the proposed method, PSPICE simulations were performed for the obtained linear oscillators in Figures 5b and 7b. The CCII+ and CCII- were realized by current feedback operational amplifier (AD844) ICs [26,27]. The macromodels of AD844 were employed for the simulations with a DC supply of ± 15 V. For the circuit in Figure 5b, we chose $C_1 = C_2 = C = 0.1 \mu\text{F}$ and $R_2 = R_3 = 1.6 \text{k}\Omega$. As shown in Figure 8, the oscillation eventually died out with $R_1 = 1.6 \text{k}\Omega$, and the circuit produced a pure sinusoidal waveform with $R_1 = 1.68 \text{k}\Omega$. Figure 9 shows the oscillation frequency for various values of C . It confirms the independently tunability of the oscillation frequency. For the oscillator in Figure 7b, we choose $C_1 = C_2 = 27 \text{nF}$ and $R_2 = R_3 = 3.3 \text{k}\Omega$. Figure 10 shows the outputted waveforms with $R_1 = 1.07 \text{k}\Omega$ and $R_1 = 1.1 \text{k}\Omega$. All of the simulation results are consistent with our prediction in Section 3.

Figure 8. The output waveforms for the oscillator in Figure 4b with different oscillation conditions.

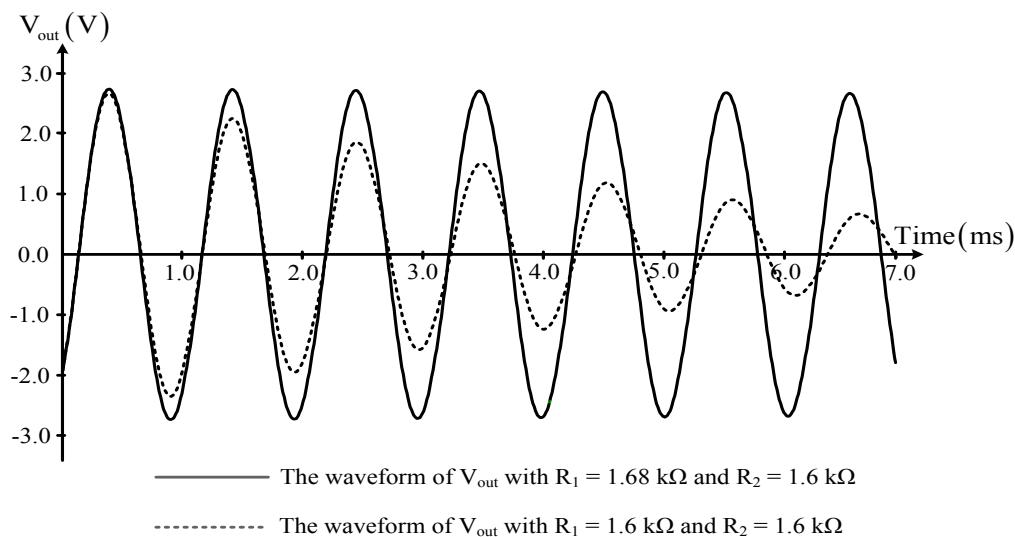


Figure 9. Theoretical and simulation results, varying values of C .

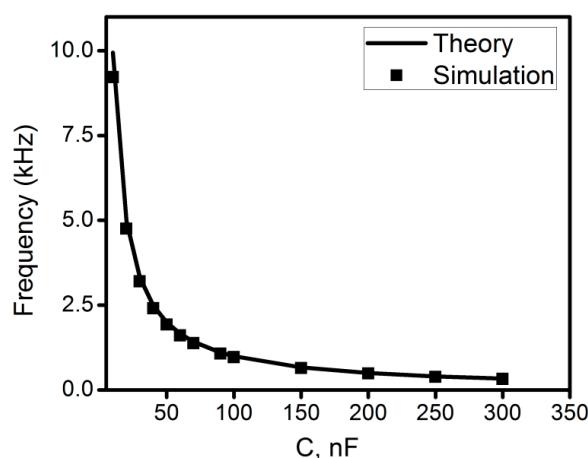
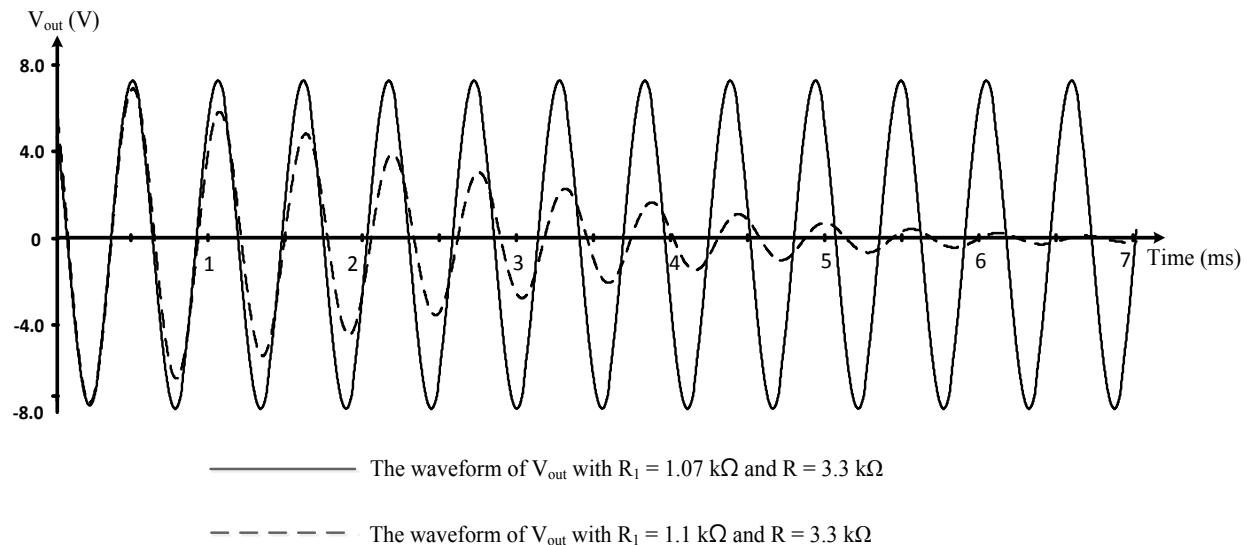


Figure 10. The output waveforms for the oscillator in Figure 6 with different oscillation conditions.



5. Conclusions

In this article, a simple and convenient approach to obtain new linear oscillators from biquadratic band pass filters is presented. The proposed method can be applied to any band pass filters, and the derived oscillators retain some useful properties of the original band pass filters. The practicability of the proposed method is illustrated by two circuits. PSPICE simulation results validate the workability of the obtained oscillators.

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Author Contributions

Huu-Duy Tran and Quoc-Minh Nguyen conceived and designed the theoretical verifications; the optimization ideas were provided by Li-Te Yin and Chih-Yi Liu; Hung-Yu Wang and Huu-Duy Tran analyzed the data and wrote the paper.

Conflicts of Interest

The authors declare no conflict of interest.

References

- Lee, C.T.; Wang, H.Y. Minimum realization for FTFN-based SRCO. *Electron. Lett.* **2001**, *37*, 1207–1208.

2. Horng, J.W. Current differencing buffered amplifiers based single resistance controlled quadrature oscillator employing grounded capacitors. *IEICE Trans. Fundam. Electron. Commun. Comput. Sci.* **2002**, *E85-A*, 1416–1419.
3. Horng, J.W.; Hou, C.L.; Chang, C.M.; Cheng, S.T. Current or/and voltage-mode quadrature oscillators with grounded capacitors and resistors using FDCCIIIs. *WSEAS Trans. Circuits Syst.* **2008**, *7*, 129–138.
4. Nandi, R.; Sanyal, S.K.; Bandyopadhyay, T.K. Single CFA-based integrator, differentiator, filter, and sinusoid oscillator. *IEEE Trans. Instrum. Meas.* **2009**, *58*, 2557–2564.
5. Bhattacharyya, B.B.; Sundaramurthy, M.; Swamy, M.N.S. Systematic generation of canonic sinusoidal RC active oscillators. *IEE Proc.* **1981**, *128*, 114–126.
6. Boutin, N. On the identification and design of single amplifier single resistance controlled oscillators. *IEEE Trans. Circuits Syst.* **1984**, *31*, 1046–1049.
7. Gupta, S.S.; Senani, R. New single resistance controlled oscillator configurations using unity gain cells. *Analog Integr. Circ. Sig. Process.* **2006**, *46*, 111–119.
8. Tao, Y.; Fidler, J.K. Electronically tunable dual-OTA second-order sinusoidal oscillators/filters with non-interacting controls: A systematic synthesis approach. *IEEE Trans. Circuits Syst. I* **2000**, *47*, 117–129.
9. Linares-Barranco, B.; Rodriguez-Vazquez, A.; Sanchez-Sinencio, E.; Huertas, J.L. Generation, design and tuning of OTA-C high frequency sinusoidal oscillators. *IEE Proc.* **1992**, *139*, 557–568.
10. Senani, R.; Gupta, S.S. Synthesis of single-resistance controlled oscillators using CFOAs: Simple state variable approach. *IEE Proc. Circuits Devices Syst.* **1997**, *144*, 104–106.
11. Kumar, P.; Senani, R. Bibliography on nullors and their applications in circuit analysis, synthesis and design. *Analog Integr. Circ. Sig. Process.* **2002**, *33*, 65–76.
12. Leuciuc, A. Using nullors for realisation of inverse transfer functions and characteristics. *Electron. Lett.* **1997**, *33*, 949–951.
13. Sanchez-Lopez, C.; Fernandez, F.V.; Tlelo-Cuautle, E.; Tan, S.X.D. Pathological element-based active device models and their application to symbolic analysis. *IEEE Trans. Circuits Syst. I* **2011**, *58*, 1382–1395.
14. Saad, R.A.; Soliman, A.M. A new approach for using the pathological mirror elements in the ideal representation of active devices. *Int. J. Circuit Theory Appl.* **2010**, *38*, 148–178.
15. Haigh, D.G. A method of transformation from symbolic transfer function to active-RC circuit by admittance matrix expansion. *IEEE Trans. Circuits Syst. I* **2006**, *53*, 2715–2728.
16. Soliman, A.M. Generation of current conveyor based oscillators using nodal admittance matrix expansion. *Analog Integr. Circ. Sig. Process.* **2010**, *65*, 43–59.
17. Hilberman, D. Input and ground as complements in active filters. *IEEE Trans. Circuit Theory* **1973**, *CT-20*, 540–547.
18. Sedra, A.S.; Smith, K.C. *Microelectronic Circuits*, 6th ed.; Oxford University Press: Princeton, NJ, USA, 2011.
19. Wang, H.Y.; Lee, C.T.; Huang, C.Y. Characteristic investigation of new pathological elements. *Analog Integr. Circ. Sig. Process.* **2005**, *44*, 95–102.
20. Ozoguz, S.; Acar, C.; Toker, A.; Gunes, E.O. Derivation of low-sensitivity current-mode CCII-based filters. *IEE Proc. Circuits Devices Syst.* **2001**, *148*, 115–120.

21. Horng, J.W. Novel universal voltage-mode biquad filter with three inputs and one output using only two current conveyors. *Int. J. Electron.* **1996**, *80*, 543–546.
22. Rybin, Y.K. Barkhausen criterion for pulse oscillators. *Int. J. Electron.* **2012**, *99*, 1547–1556.
23. Chen, H.P. Single CCII-based voltage-mode universal filter. *Analog Integr. Circ. Sig. Process.* **2010**, *62*, 259–262.
24. Senani, R. On equivalent forms of single-Op-Amp sinusoidal RC oscillators. *IEEE Trans. Circuits Syst. I* **1994**, *41*, 617–624.
25. Valkenburg, M.E.V. *Analog Filter Design*; Holt, Rinehart and Winston: New York, NY, USA, 1981.
26. *AD844 Datasheet*; Analog Devices: Norwood, MA, USA, 2009.
27. Senani, R.; Bhaskar, D.R.; Singh, A.K.; Singh, V.K. *Current Feedback Operational Amplifiers and Their Application*; Springer: Berlin/Heidelberg, Germany, 2013.

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