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Peridynamic Analysis of Marine Composites under Shock Loads by Considering Thermomechanical Coupling Effects

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Abstract: Nowadays, composite materials have been increasingly used in marine structures because of their high performance properties. During their service time, they may be exposed to extreme loading conditions such as underwater explosions. Temperature changes induced by pure mechanical shock loadings cannot to be neglected especially when smart composite materials are employed for condition monitoring of critical systems in a marine structure. Considering this fact, both the thermal loading effect on deformation and the deformation effect on temperature need to be taken into consideration. Consequently, an analysis conducted in a fully coupled thermomechanical manner is necessary. Peridynamics is a newly proposed non-local theory which can predict failures without extra assumptions. Therefore, a fully coupled thermomechanical peridynamic model is developed for laminated composites materials. In this study, numerical analysis of a 13 ply laminated composite subjected to an underwater explosion is conducted by using the developed model. The pressure shocks generated by the underwater explosion are applied on the top surface of the laminate for uniform and non-uniform load distributions. The damage is predicted and compared with existing experimental results. The simulation results obtained from uncoupled case are also provided for comparison. Thus the coupling term effects on crack propagation paths are investigated. Furthermore, the corresponding temperature distributions are also investigated.

Keywords: peridynamics; thermomechanical; composites; shock loads

1. Introduction

Laminated composite materials have many outstanding mechanical, physical, and chemical properties. For example, they are an easily fabricated and cost-effective alternative to some other monolithic materials [1]. Therefore, in recent years, composites have become common materials in marine industries. One application is for the construction of military vessels [2]. Composite materials can provide low-radar signatures for stealth operations. In addition, the low electro-magnetic signature these materials provide can reduce the possibility of detonating magnetic sea mines [3]. However, due to the special working conditions for military vessels, the composite materials may be subjected to some severe environments, such as mechanical shock loads, large temperature variations, and exposures [4]. Hence, the damage level of composites induced by such extreme loading conditions becomes a critical factor with regards to the safety issue in the designation of the vessels. As a result, the failure analyses of composite materials under shock loadings draws a lot of interest, and has been investigated for years.

It is a challenging task to predict damage in composites. Composites can be defined as two or more materials combined to form a single material [5]. For fiber-reinforced laminates, there are mainly four modes of failure: matrix cracking occurs parallel to the fiber; delamination; fiber breakage

in tension, as well as fiber bulking in compression; and penetration due to impact [6]. Therefore, the inhomogeneous nature of composites must be taken into consideration in the analysis, in order to predict the corresponding failure modes. Furthermore, the stacking sequence and thickness also have an important effect on the failure initiation and evolution [7]. In addition to the complexity of the composite material properties, shock loadings, which result in high strain rates, also give rise to additional complexity in the analysis. Large safety factors are typically used in composite structure design to make sure no damage will occur, resulting a conservative solution or over-design [8]. Therefore, a good understanding of the responses of composite materials under shock loadings (i.e., explosions) is necessary for the balance between safety and economy issues.

There are three major methods to investigate the responses of composite materials under explosions: the experimental method, the analytical method, and the numerical simulation method. As to the experiment method, there are two kinds of experimental tests, according to the scale, i.e., a full-scale test and a laboratory-scale test. The full-scale explosive tests can provide important information on survivability, damage tolerance, and failure modes [9]. They are necessary to validate the results of analytical and numerical simulations [10]. In 1989, a 3 m × 3 m composite plate was tested under an underwater blast, to be investigated in full scale [11]. However, the full-scale tests are performed infrequently, due to high costs. For this reason, the explosive test in the laboratory scale is adopted for research. A divergent shock tube was designed to investigate the responses of a clamped test plate under shock loadings [12]. Thus, plane wave fronts and wave parameters were easily controlled and repeated. LeBlanc and Shukla used a tube filled with water to reproduce the underwater explosive loads [13]. Wadley [14] developed another test method to investigate the compressive responses of multilayered lattices during underwater shock loadings. Analytical methods are generally adopted in the initial design state of composite structures, which give relatively faster solutions compared to the other two methods. Rabczuk et al. [15] proposed a simplified method to investigate the effects of fluid–structure interaction in composite structures subjected to dynamic underwater loads. Hoo Fatt and Palla [16] derived analytical solutions for transient response and damage initiation of a composite panel subjected to blast loading. However, analytical solutions are mainly limited to special and simple cases. In contrast, numerical simulation methods can be applied on various types of loadings, complicated geometries of structures, and complex boundary conditions. Kazancı [17] conducted a review of the available numerical achievements regarding the simulation of composite plates under a blast load. The finite element method (FEM) [18], smooth particle hydrodynamics (SPH) [19], and the finite strip method (FSM) [20] have all been applied to model composite materials.

Unlike the FEM, peridynamics (PD) is a new, non-local theory, and utilizes a mesh-free approach [21]. In FEM, partial differential equations are used to predict the motions of a body, which creates non-physical singular stress and strain at discontinuities. As a result, remedies such as the cohesive zone element (CZE) [22] and the extended finite element method (XFEM) [23] are proposed to improve the shortcomings of the FEM. However, additional assumptions are still needed to predict the crack propagation path in these methods. In contrast, PD converts the equation of motion from its traditional partial differential form into an integral form, which remains valid even at discontinuities [24]. Consequently, PD is well-suited for problems involving discontinuities. As to the composite materials, PD has been successfully applied on the failure analyses of composites [7,25–29]. However, the composites are mainly the focus on the mechanical field only. When explosion loads are applied to the test plate, the plate experiences high strain rate stages. Therefore, the coupling effect of deformation on temperature cannot be neglected, which may have an effect on the crack propagation path with the induced temperature changes. Therefore, a fully coupled thermomechanical composite model is necessary for the simulation of thermal and mechanical responses of composites under shock loadings. Here, a fully coupled approach means both the temperature effects on deformation and the deformation effects on temperature are included in the simulation [30]. Oterkus et al. [31] proposed a PD thermal model to simulate the heat conduction in isotropic materials. Then, they generalized

the model to include the coupling effects on both deformation and temperature [32]. Furthermore, the model is developed for composite lamina by considering its directional dependency properties [33]. Based on previous work, the fully coupled thermomechanical laminate model formulated by PD is developed in this paper, including heat conduction and coupling effects in the thickness direction of the composite laminate.

The paper is organized as follows. Firstly, the PD theory is introduced, and some basic concepts are explained. Secondly, a mechanical and thermal model for composite materials is formulated by bond-based PD. Then, the responses of a 13-ply composite plate subjected to an underwater explosion load are studied, by considering the fully coupled thermomechanical effects. The crack propagation evolutions are predicted and compared with uncoupled cases. The predicted temperature distributions are also provided.

2. Peridynamic (PD) Theory

2.1. Basic Concepts in PD Theory

The PD theory which is proposed by Silling and Askari [34] falls into the category of non-local theory. The material points, \mathbf{x} , can interact other material points, i.e., \mathbf{x}' , in a neighbourhood $H_{\mathbf{x}}$. The maximum interaction distance is called horizon and denoted by δ . $H_{\mathbf{x}}$ is called the family of point \mathbf{x} . As shown in Figure 1, the initial relative position vector is denoted as $\xi = \mathbf{x}' - \mathbf{x}$, in the deformed configuration, the positions of material points \mathbf{x} and \mathbf{x}' are represented by \mathbf{y} and \mathbf{y}' , respectively. Hence, the displacements of the points \mathbf{x} and family member \mathbf{x}' are $\mathbf{u}(\mathbf{x}) = \mathbf{y} - \mathbf{x}$ and $\mathbf{u}(\mathbf{x}') = \mathbf{y}' - \mathbf{x}'$, respectively. Consequently, the relative displacement between \mathbf{x} and \mathbf{x}' can be defined as

$$\boldsymbol{\eta} = \mathbf{u}(\mathbf{x}') - \mathbf{u}(\mathbf{x}) = (\mathbf{y}' - \mathbf{y}) - (\mathbf{x}' - \mathbf{x}) \tag{1}$$

The stretch between two points can be defined as

$$s = \frac{|\mathbf{y}' - \mathbf{y}| - |\mathbf{x}' - \mathbf{x}|}{|\mathbf{x}' - \mathbf{x}|} = \frac{|\boldsymbol{\eta} + \xi| - |\xi|}{|\xi|} \tag{2}$$

The equation of motion in bond based PD theory is [34]

$$\rho(\mathbf{x})\ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{H_{\mathbf{x}}} \mathbf{f}(\boldsymbol{\zeta}, \boldsymbol{\eta}, t)dV + \mathbf{b}(\mathbf{x}, t) \tag{3}$$

where $\rho(\mathbf{x})$ represents density, V represents volume, $\ddot{\mathbf{u}}(\mathbf{x}, t)$ represents the acceleration, $\mathbf{b}(\mathbf{x}, t)$ represents the body force and $\mathbf{f}(\boldsymbol{\zeta}, \boldsymbol{\eta}, t)$ represents the pairwise PD force. The pairwise PD force can be defined as [32]

$$\mathbf{f}(\boldsymbol{\zeta}, \boldsymbol{\eta}, t) = c(s - \alpha T) \frac{\boldsymbol{\zeta} + \boldsymbol{\eta}}{|\boldsymbol{\zeta} + \boldsymbol{\eta}|} \tag{4}$$

In which α is the linear thermal expansion coefficient of the material, T is the average temperature of point \mathbf{x} and \mathbf{x}' with respect to reference temperature, c is the PD constant. It should be noted that in bond based PD, the pairwise PD forces \mathbf{f} and \mathbf{f}' are forced to be equal in magnitude and parallel in direction. Hence, the Poisson's ratio is forced to be 1/3 in two dimensional (2D) analysis and 1/4 in three dimensional (3D) analysis [21].

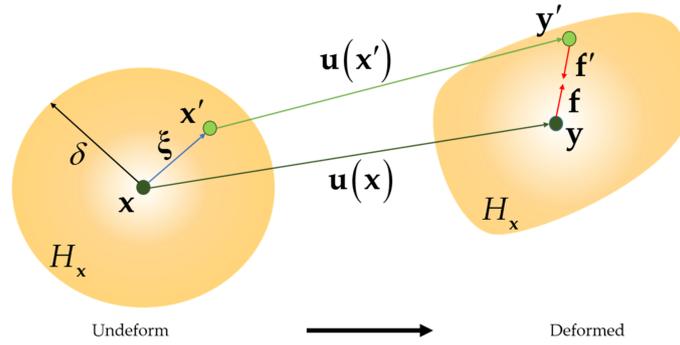


Figure 1. Illustration of PD forces

2.2. PD Mechanical Laminate Model

The PD mechanical model developed by Oterkus and Madenci [21,25] for composite laminates is adopted in this paper. As illustrated in Figure 2, each ply in a laminate is modelled by one-layer PD nodes (shown in blue, red, and yellow colours for different plies). The multi-layer laminate is modelled by assembling the single layer models according to the stacking sequence. For a resin-rich laminate, the properties in the thickness direction are treated as its matrix material properties. Due to the directionally-dependent properties of the laminate, four kinds of PD bonds are defined in the model: in-plane fibre bonds, in-plane matrix bonds, interlayer normal bonds, and interlayer shear bonds. The grid size is represented by Δx and the fibre direction is denoted by Φ .

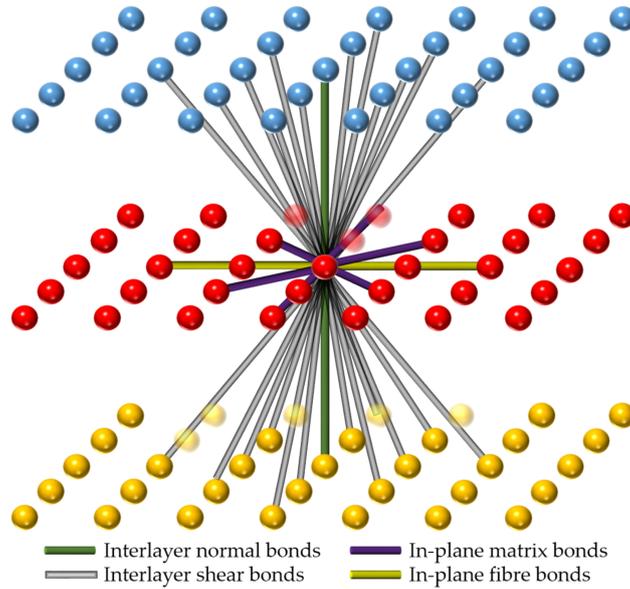


Figure 2. Illustration of PD laminate model for $\delta = 2\Delta x$ and fibre direction, $\Phi = 0$.

The discretized form of the PD equation of motion for a material point \mathbf{x}_k^n in the n layer of a laminate can be written as

$$\begin{aligned} \rho(\mathbf{x}_k^n) \ddot{\mathbf{u}}(\mathbf{x}_k^n, t) = & \sum_{j=1}^N (\mu_f c_f + c_m) (s_{kj}^n - \alpha_\theta T_{kj}^n) \frac{y_j^n - y_k^n}{|y_j^n - y_k^n|} V_j^n \\ & + \sum_{m=n+1, n-1} c_n (s_k^{nm} - \alpha_m T_k^{nm}) \frac{y_k^m - y_k^n}{|y_k^m - y_k^n|} V_k^m + \sum_{m=n+1, n-1} \sum_{j=1}^{N_s} c_s \varphi(\Delta x)^2 \frac{y_j^m - y_k^n}{|y_j^m - y_k^n|} V_j^m \\ & + \mathbf{b}(\mathbf{x}_k^n, t) \end{aligned} \quad (5)$$

The first three terms on the right hand side of Equation (5) represent the PD forces developed by in-plane bonds (including fibre bonds and matrix bonds), interlayer normal bonds, and interlayer shear bonds in sequence. If the bond direction is parallel to the fibre direction, μ_f is equal to 1, otherwise it is 0. c_f , c_m , c_n , and c_s are PD material constants associated with in-plane fiber bonds, in-plane matrix bonds, interlayer normal bonds, and interlayer shear bonds, respectively. The definitions for PD material constants are listed as [21,25,27]

$$c_f = \frac{2E_1(E_1 - E_2)}{\left(E_1 - \frac{1}{9}E_2\right) \left(\sum_{j=1}^{N_f} |\xi_{jk}| V_j\right)} \tag{6}$$

$$c_m = \frac{8E_1E_2}{\left(E_1 - \frac{1}{9}E_2\right) \pi h \delta^3} \tag{7}$$

$$c_n = \frac{E_m}{hV} \tag{8}$$

$$c_s = \frac{2G_m}{\pi h} \frac{1}{(\delta^2 + h^2 \ln(h^2/\delta_s^2))} \tag{9}$$

In the above equations, E_1 and E_2 represent the elastic moduli of a single ply in fiber and transverse directions, respectively. E_m represents the elastic modulus of matrix material and G_m represents the shear modulus of matrix material, h represents the thickness of one ply and Δx represents the spacing between material points on the plane of a ply. It is assumed that a material point interacts with other points in adjacent plies through interlayer normal bonds and interlayer shear bonds. Therefore, the horizon of interlayer normal bond is taken as equal to thickness of one ply, h . δ_s is the horizon of interlayer shear bond determined as $\delta_s = \sqrt{\delta^2 + h^2}$. In Equation (6), N_f represents the total number of family members those connect to the material point with fibre bonds. In Equation (8), the value of V can be calculated as the average volume of material points connected through interlayer normal bonds.

As to the thermal expansion coefficients appeared in Equation (5), the formulation developed in [27] is utilized in the current model as

$$\alpha_\vartheta = \alpha_x \cos^2(\vartheta) + \alpha_y \sin^2(\vartheta) + \alpha_x \alpha_y \cos(\vartheta) \sin(\vartheta) \tag{10}$$

where α_ϑ is the thermal expansion coefficient in the bond direction, ϑ . α_x , α_y and α_{xy} are thermal expansion coefficients of the located ply with respect to the global coordinate system. α_m represents thermal expansion coefficient of matrix material.

In Equation (5) φ represents the shear angle of the diagonal shear bonds, the effect of temperature is included as

$$\varphi = \left[\left(s_{kj}^{nm} - \alpha_m T_{kj}^{nm} \right) - \left(s_{jk}^{nm} - \alpha_m T_{jk}^{nm} \right) \right] \left| \xi_{kj}^{nm} \right| / (2h) \tag{11}$$

where s_{kj}^{nm} is the stretch between nodes \mathbf{x}_k^n and \mathbf{x}_j^m , and T_{kj}^{nm} is the temperature difference between nodes \mathbf{x}_k^n and \mathbf{x}_j^m , with respect to reference temperature. It should be noted that because of the adoption of bond based PD theory, the four material constants existing in a laminate—i.e., E_1 , E_2 , ν_{12} , and G_{12} —reduce to two constants: E_1 and E_2 . The major Poisson’s ratio ν_{12} is limited to 1/3, and the major shear modulus is $G_{12} = \frac{\nu_{12}E_2}{1-\nu_{12}\nu_{21}}$ with $\nu_{12}/E_1 = \nu_{21}/E_2$.

2.3. PD Thermal Laminate Model

PD thermal model was developed in [32] and extended into composite lamina by Oterkus and Madenci [33] as

$$\rho c_v \dot{T}(\mathbf{x}_k^n, t) = \sum_{j=1}^N \left[\left(\mu_f \kappa_f + \kappa_m \right) \frac{\Theta(\mathbf{x}_j^n, t) - \Theta(\mathbf{x}_k^n, t)}{|\xi_{kj}^n|} - \Theta_0 (\mu_f \beta_f + \beta_m) \dot{e}_{kj}^n \right] V_j^n \quad (12)$$

where c_v is the specific heat capacity, $T(\mathbf{x}_k^n, t)$ is the temperature change, $T(\mathbf{x}_k^n, t) = \Theta(\mathbf{x}_k^n, t) - \Theta_0$, $q_b(\mathbf{x}_k^n, t)$ is the volumetric heat source, and \dot{e} is the time rate of the change of stretch, which is defined as $\dot{e} = \frac{\eta + \xi}{|\eta + \xi|} \cdot \dot{\eta}$.

In Equation (12) κ_f and κ_m represent the micro-conductivities associated with in-plane fibre bonds and in-plane matrix bonds. The expressions for these micro-conductivities in PD concept are given as [33]

$$\kappa_f = \frac{2(k_1 - k_2)}{\sum_{j=1}^{N_f} |\xi_{kj}^n| V_j^n} \quad (13)$$

$$\kappa_m = \frac{6k_2}{\pi h \delta^3} \quad (14)$$

where k_1 and k_2 represent the thermal conductivities for fibre and transverse directions in a ply. PD thermal modulus β depends on the PD material bond constant [32,33,35]. β_f and β_m are associated with in-plane fibre bonds and in-plane matrix bonds which can be expressed as

$$\beta_f = \frac{1}{2} c_f \alpha_\vartheta \quad (15)$$

$$\beta_m = \frac{1}{2} c_m \alpha_\vartheta \quad (16)$$

where c_f and c_m represent the PD material bond constant provided in Equations (6) and (7).

In this study, the heat conduction equation given for a lamina is modified to represent a composite laminate by taking into account the interaction between the plies as

$$\begin{aligned} \rho c_v \dot{T}(\mathbf{x}_k^n, t) = & \sum_{j=1}^N \left[\left(\mu_f \kappa_f + \kappa_m \right) \frac{\Theta(\mathbf{x}_j^n, t) - \Theta(\mathbf{x}_k^n, t)}{|\xi_{kj}^n|} - \Theta_0 (\mu_f \beta_f + \beta_m) \dot{e}_{kj}^n \right] V_j^n \\ & + \sum_{m=n+1, n-1} \left[\kappa_n \frac{\Theta(\mathbf{x}_k^m, t) - \Theta(\mathbf{x}_k^n, t)}{|\xi_{kn}^m|} - \Theta_0 \beta_n \dot{e}_k^{nm} \right] V_k^m \\ & + \sum_{j=1}^{N_s} \left[\kappa_n \frac{\Theta(\mathbf{x}_j^m, t) - \Theta(\mathbf{x}_k^n, t)}{|\xi_{kj}^{nm}|} - \Theta_0 \beta_s \dot{e}_{kj}^{nm} \right] V_j^m + \rho q_b(\mathbf{x}_k^n, t) \end{aligned} \quad (17)$$

where κ_n represents the micro-conductivity for both interlayer normal and shear bonds as

$$k_n = \frac{k_m}{2\pi h^3 (\delta_s - h)} \quad (18)$$

where k_m is the thermal conductivity of the matrix material. PD thermal modulus for interlayer normal bonds and interlayer shear bonds can be expressed as

$$\beta_n = \frac{1}{2} c_n \alpha_m \quad (19)$$

$$\beta_s = \frac{1}{2} c_s \alpha_m \quad (20)$$

2.4. Failure Criteria

In classical mechanics, singular stress and strain occur at crack tips, which are non-physical. Therefore, additional assumptions are needed to simulate crack propagation paths. On the contrary, in PD theory, the equation of motion is converted into its non-local form. As a result, failure can be simulated without any additional assumptions [36]. The form of equations in PD theory makes it suitable for failure analysis. The approach to simulate failure in PD theory is simply to break a bond once its stretch is beyond the critical stretch value, s_0 . The PD forces of broken bonds become zero permanently. Because of the existing of four kinds of PD bonds in PD laminate model, different critical stretch values are defined for different types of PD bonds. The definitions of these critical stretch values are listed as [7,25,34]

$$s_{ft} = \frac{\sigma_{1t}}{E_1} \tag{21}$$

$$s_{fc} = \frac{\sigma_{1c}}{E_1} \tag{22}$$

$$s_m = \sqrt{\frac{5G_{IC}}{9K_m\delta}} \tag{23}$$

$$s_n = \sqrt{\frac{2G_{IC}}{hE_m}} \tag{24}$$

$$s_s = \sqrt{\frac{G_{IIC}}{hG_m}} \tag{25}$$

In the above equations, s_{ft} and s_{fc} are critical stretch values of fibre bonds in tension and compression states, respectively. s_m , s_n , and s_s are related with matrix bonds, interlayer normal bonds, and interlayer shear bonds. G_{IC} and G_{IIC} are the critical energy release rates for first and second failure modes, respectively. K_m is the bulk modulus of the matrix material. σ_{1t} and σ_{1c} are longitudinal tension and compression strength properties of a single ply. By applying the above failure criteria, it can be observed that the fibre bonds can fail both in tension and compression. The matrix bonds, interlayer normal bonds, and interlayer shear bonds are only allowed to fail in tension.

A history dependent function, $\mu(\xi, t)$, is introduced to indicate the status of a bond, i.e., being 1 for intact bond and being zero for broken bond. The definitions of parameter, $\mu(\xi, t)$ for different kinds of PD bonds can be defined as

$$\mu_{ff} = \begin{cases} 1, (s - \alpha_\theta T) < s_{ft} \text{ and } (s - \alpha_\theta T) > s_{fc} \\ 0, (s - \alpha_\theta T) \geq s_{ft} \text{ or } (s - \alpha_\theta T) \leq s_{fc} \end{cases} \tag{26}$$

$$\mu_m = \begin{cases} 1, (s - \alpha_\theta T) < s_m \\ 0, (s - \alpha_\theta T) \geq s_m \end{cases} \tag{27}$$

$$\mu_n = \begin{cases} 1, (s - \alpha_m T) < s_n \\ 0, (s - \alpha_m T) \geq s_n \end{cases} \tag{28}$$

$$\mu_s = \begin{cases} 1, \varphi < s_s \\ 0, \varphi \geq s_s \end{cases} \tag{29}$$

where μ_{ff} , μ_m , μ_n , and μ_s are related with fibre, matrix, interlayer normal, and interlayer shear bonds, respectively. Subsequently, a local damage parameter, i.e., the ratio of the number of broken bonds to the number of total bonds, is introduced to represent the damage level of a point, shown as [21]

$$\varphi(\mathbf{x}, t) = 1 - \frac{\int_H \mu(\xi, t) dV}{\int_H dV} \tag{30}$$

3. Numerical Implementation

In this study, the heat conduction equation and the equation of motion are solved simultaneously for each time increment by using explicit time integration.

3.1. Problem Description

The bond based PD laminate model is implemented in FORTRAN program to predict the responses of a 13 ply laminate subjected to shock loading which was previously considered by Diyaroglu et al. [37]. Note that, in this study, the temperature changes due to mechanical deformations and their effects on damage evolution are taken into account by solving fully coupled thermomechanical equations whereas thermal effects are ignored in [37]. The composite material properties is provided in Table 1.

Table 1. Material properties of composite [8].

Mechanical Properties		Thermal Properties	
E_1 (GPa)	39.3	α_1 ($\mu\text{m}/\text{m}/\text{K}$)	8.6
E_2 (GPa)	9.7	α_2 ($\mu\text{m}/\text{m}/\text{K}$)	22.1
G_{12} (GPa)	3.32	k_1 (W/mK)	10.4
Poisson's ratio ν_{12}	0.33	k_2 (W/mK)	0.89
ρ (kg/m^3)	1850	c_v (J/(kg · K))	879
E_m (GPa)	3.792	α_m ($\mu\text{m}/\text{m}/\text{K}$)	63
G_m (GPa)	1.422	k_m (W/mK)	0.34
Poisson's ratio ν_m	0.33	Θ_0 (K)	285

Because of the adoption of bond based PD, the major shear modulus changed to be 3.32 GPa according to the constraint on material constants. As illustrated in Figure 3, the 13 ply test plate is in a circle shape with outer radius, $R_{out} = 132.715$ mm and inner radius, $R_{in} = 114.3$ mm. The thickness of each ply in the laminate is same as $h = 0.254$ mm. The region between the inner circle and outer circle is constrained in top and bottom plies, and is left free for other plies. The constraint is implemented by applying six bolts with a radius of $r = 4$ mm. Thus the fixed end allows the specimen to absorb the full energy of the applied load. The stacking sequence is $[0/90/0/90/0/90/0]$ (shown in Figure 3).

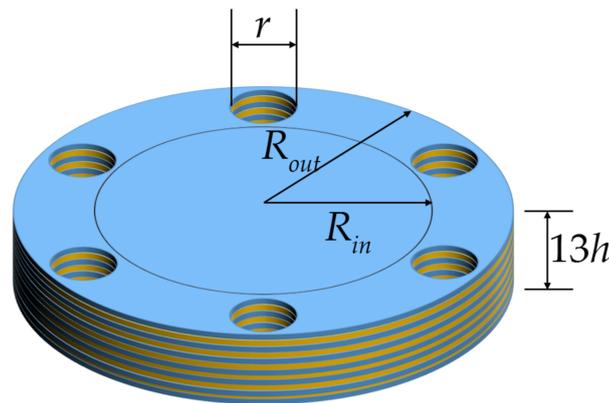


Figure 3. Geometry dimension illustration of the test laminate. (Blue colour represents 0° and yellow colour represents 90° plies).

The PD discretization of one ply is presented in Figure 4. The grid size is $\Delta x = 2.6543 \times 10^{-3}$ m. The horizon size is chosen as $\delta = 3.015\Delta x$. The material points located within the bolt regions are deleted in order to represent the actual shape of the test plate. Based on such discretization, the critical stretch value related with bonds failures can be calculated [7]. The critical energy release rate for

matrix failure is $G_{IC} = 11.85 \times 10^{-3}$ MPa, thus s_m is calculated as $s_m = 1.47 \times 10^{-2}$. The tension and compression strength properties are $\sigma_{1t} = 965$ MPa and $\sigma_{1c} = -883$ MPa. Therefore, the critical stretch value for fibre failure in tension is $s_{ft} = 2.46 \times 10^{-2}$ and in compression is $s_{fc} = -2.25 \times 10^{-2}$. As to the interlayer bonds, the critical stretch values are calculated as $s_n = 7.015 \times 10^{-2}$ with $G_{IC} = 2.73 \times 10^{-3}$ MPa and $s_s = 0.14$ with $G_{IIC} = 7.11 \times 10^{-3}$ MPa. The time step size for an explicit time integration is $\Delta t = 7.69 \times 10^{-8}$ s. The total simulation time is set as 0.3641×10^{-3} s.

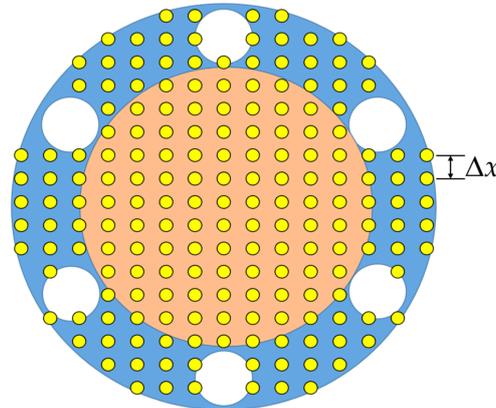


Figure 4. Illustration of PD discretization for one ply (blue colour represents the fixed boundary region and orange colour represents the inner part).

Several dynamic loadings generated by explosions are modelled by using different time-dependent pressure functions. The pressure shock applied in the experiment conducted by LeBlanc and Shukla [8] is utilized here. The charge which is equivalent to 1.32 g TNT is located at 5.25 m away from the test plate. The pressure wave is caused by rapid expansion of explosive gases. The speed of these gases can be approximated as the speed of sound in water [38]. The pressure linearly increases until it reached its peak value, P_{max} , followed by the exponential decay, expressed in Equation (31) and shown in Figure 5. Here P_{max} is set to be 9.65 MPa.

$$P(t) = \begin{cases} P_{max} \times (t/4 \times 10^{-5}) & t < 0.04 \times 10^{-3} \text{ s} \\ P_{max} & 0.04 \times 10^{-3} \text{ s} < t < 0.08 \times 10^{-3} \text{ s} \\ P_{max}e^{-1000(t-0.08)/0.2} & 0.04 \times 10^{-3} \text{ s} < t < 1 \times 10^{-3} \text{ s} \end{cases} \quad (31)$$

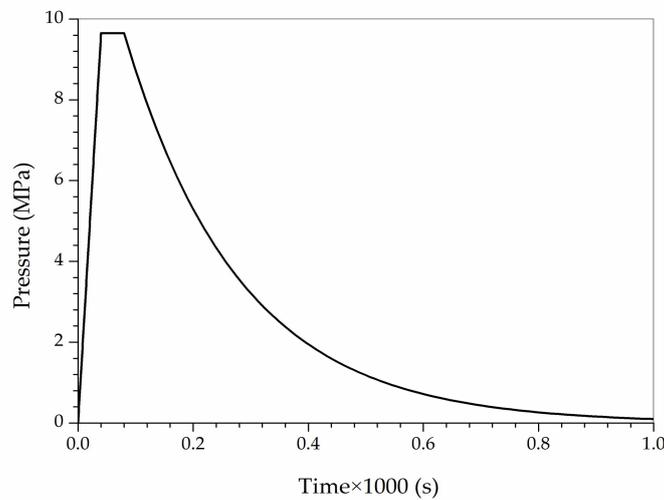


Figure 5. Pressure load distribution for the test plate.

Generally, there are two approaches for modelling the shock load depending on the distance (stand-off distance) between the charge source and the object of interest [17]. The explosion load is assumed to be uniform if the stand-off distance is long enough, which is termed as far-field explosion. On the contrary, the near-field explosion adopts non-uniform load distribution. There are also two approaches to simulate the non-uniform pressure shock loads, i.e., decoupling the load and the structural response and coupling the load and response. In this paper, a non-uniform pressure load simulated and decoupled approach is utilized, i.e., the pressure shock load is in a form of $P(r,t) = P_1(r)P_2(t)$. A non-uniform distribution of shock loading over the plate is simulated by adopting the pressure distribution derived by Turkmen and Mecitoglu [39] as

$$P(r) = -0.0005r^4 + 0.01r^3 - 0.0586r^2 - 0.001r + 1 \tag{32}$$

where r represents the distance from the collective node to the centre of the test plate. The test plate adopted here is slightly larger than the one in [39]. Consequently, the distribution profile is extended by 0.83 cm correspondingly, as illustrated in Figure 6. Finally, the explosion load is defined as

$$P(r,t) = \begin{cases} P(t) \left(-0.0005(r - 0.83)^4 + 0.01(r - 0.83)^3 - 0.0586(r - 0.83)^2 - 0.001(r - 0.83) + 1 \right) & r > 0.83 \text{ cm} \\ P(t) & r < 0.83 \text{ cm} \end{cases} \tag{33}$$

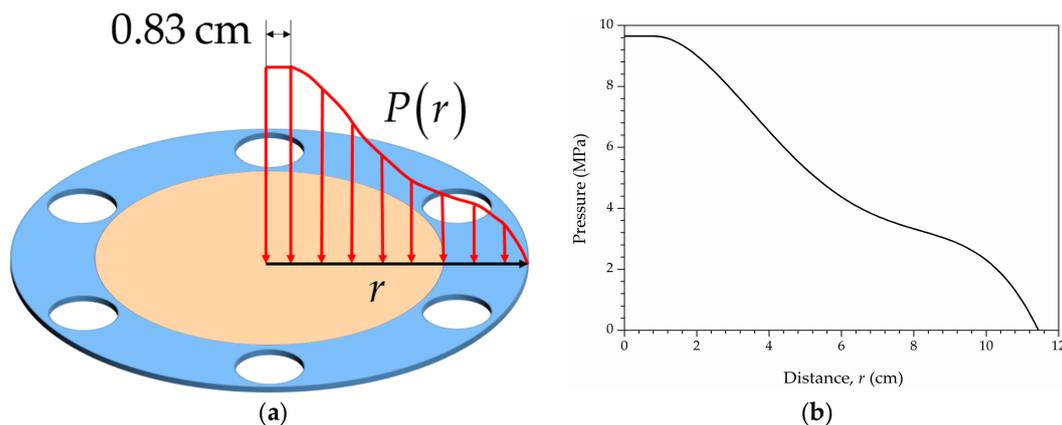


Figure 6. (a) Illustration of non-uniform pressure distribution over the top ply and (b) pressure profile.

3.2. Numerical Results

3.2.1. Subjected to Uniform Pressure Loading

First, the test laminate is subjected to uniform pressure load, $P(t)$ without allowing failure. The regions between the inner circle and outer circle are fixed in three dimensions for all plies. During the simulation, the central points in each ply experience the same vertical (z) displacement evolutions. Therefore, the vertical displacement evolution of the central point on the top ply is plotted in Figure 7a. It can be observed that the test plate firstly deforms in the negative z direction, then it will recover to some extent with velocity in positive z direction. The largest deformation occurs at approximately 3700 time steps, corresponding to 0.28453×10^{-3} s. The vertical displacement distribution over the top ply at 0.28453×10^{-3} s is shown in Figure 7b.

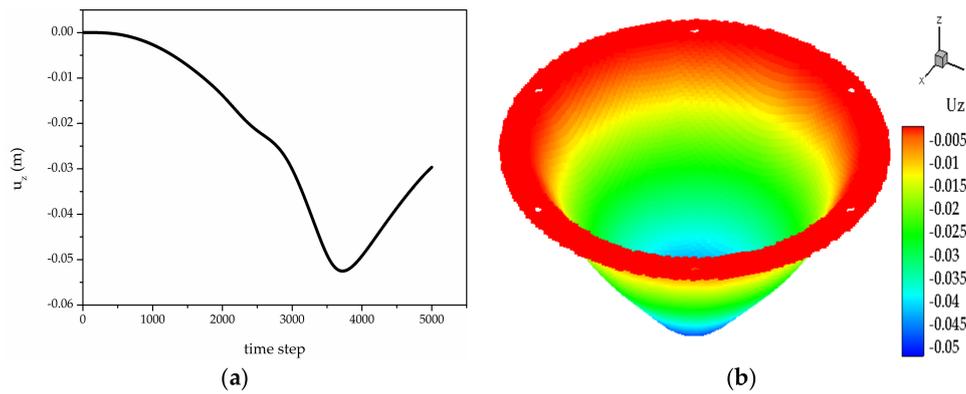


Figure 7. (a) Variation of the displacement in z direction of the central point as a function of time; (b) Vertical displacement distribution for the top ply at 0.28453×10^{-3} s.

Fully coupled thermomechanical simulation under the uniform pressure load $P(t)$, i.e., far field explosion, is also investigated for further comparison. The crack propagations and temperature change distributions at 0.1538×10^{-3} s are provided in Figure 8 for top ply, Figure 9 for middle ply, and Figure 10 for bottom ply. It can be inferred from the matrix damage plots that all the plies in the laminate experience the tear failure near the constraint boundary condition. Furthermore, the damage region in the bottom ply is larger than the top ply, indicating a combination of tension failure mode and tear failure mode. As to the temperature distribution, the temperature increases near cracks are observed for all plies, which are more obvious in the top ply provided in Figure 8b. Temperature drop is also observed in tension state, which is obvious in the bottom ply provided in Figure 10b.

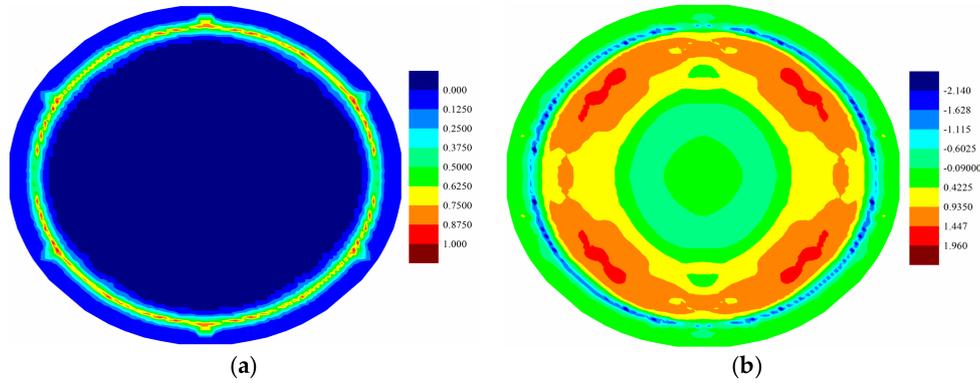


Figure 8. (a) Matrix damage and (b) temperature change distribution (K) of top ply at 0.1538×10^{-3} s.

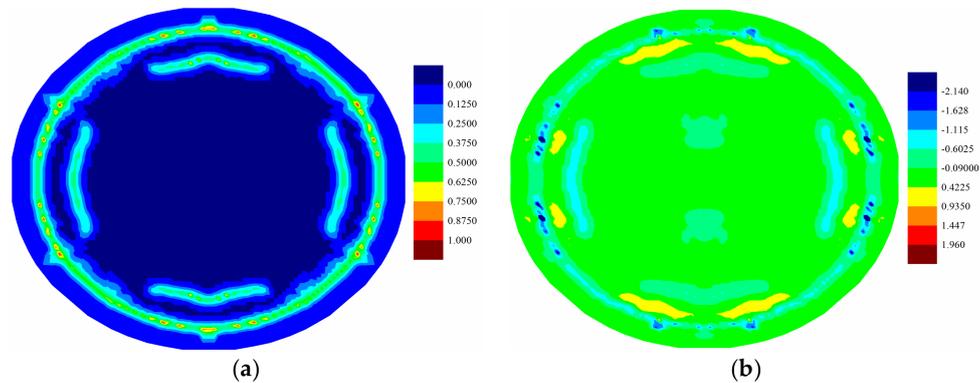


Figure 9. (a) Matrix damage and (b) temperature change distribution (K) of middle (7th) ply at 0.1538×10^{-3} s.

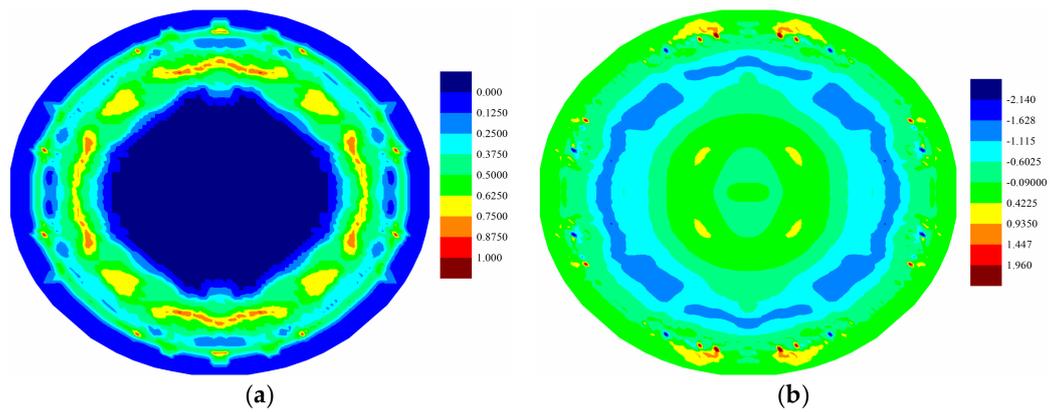


Figure 10. (a) Matrix damage and (b) temperature change distribution (K) of bottom ply at 0.1538×10^{-3} s.

3.2.2. Subjected to Uniform Non-Uniform Pressure Load

In this section, the test laminate is subjected to non-uniform pressure load $P(r, t)$, i.e., near field explosion. The matrix damage and temperature distribution in deformed shape are provided in Figure 11. Matrix damage predictions at 0.28453×10^{-3} s and 0.3461×10^{-3} s obtained from coupled and uncoupled cases are shown in Figures 12–17.

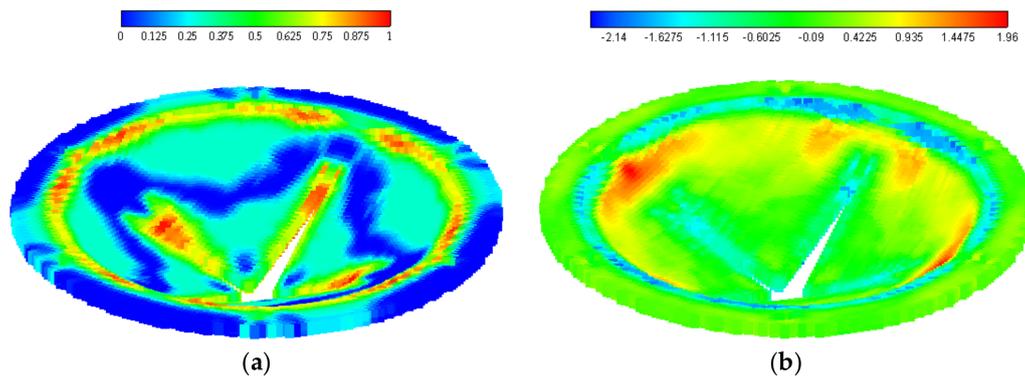


Figure 11. (a) Matrix damage and (b) temperature change distribution (K) of the laminate at 0.3461×10^{-3} s.

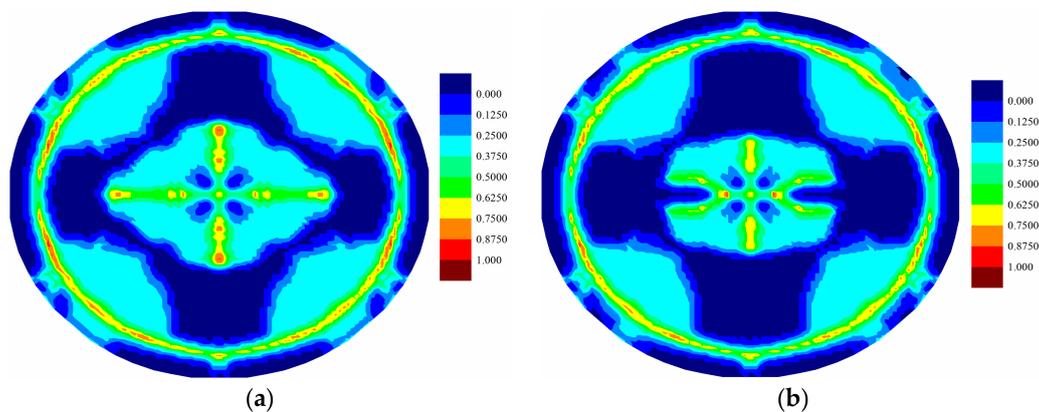


Figure 12. Matrix damage comparison of top ply for (a) coupled case and (b) uncoupled case at 0.28453×10^{-3} s.

For the fully coupled simulation case, by comparing the damage of the plies at different times, it is obvious that the damaged zone gets larger as time progresses. The damage patterns are different for

each ply when compared at the same time. The cracks mainly occur near the clamped boundary region for the top ply, indicating a tear failure mode. On the other hand, the central part experiences the largest level of damage for the bottom ply, indicating a tension failure mode. Consequently, the different force states give rise to the different level of damages. However, for all plies, the crack propagations present a cross-shaped pattern. It can be explained that the fiber direction of each ply is either zero or 90 degrees. The matrix damage occurs parallel to the fiber direction. For a ply with fiber direction being zero, the matrix crack will occur along the horizontal direction. However, the fiber directions for its adjacent plies are 90 degrees. Hence, the matrix crack will also occur in the vertical direction due to the contribution of the interlayer bonds. Consequently, the final cracks are in cross shapes. The damages present highest levels near the central vertical lines for all plies. This phenomenon is also observed in the experiment [13], as shown in Figure 18. As it can be seen in Figures 8–10, there are damages around the bolt holes and these damages were also observed in experiments [13] as it can be seen in Figure 18.

As shown in Figures 12–17, different damage patterns are observed for coupled and uncoupled cases. As the time progresses, temperature change increases and the differences in damage plots become more obvious. Considering the small temperature changes induced by the applied pressure shock, the coupling term effect on damage is significant. It can be inferred that the difference in damage due to coupling effect will become more significant with larger strain rates. Temperature decreases where there is local tension and as a result local compression is created due to temperature drop which reduces the extent of damage observed by the uncoupled cases (Figures 12–17).

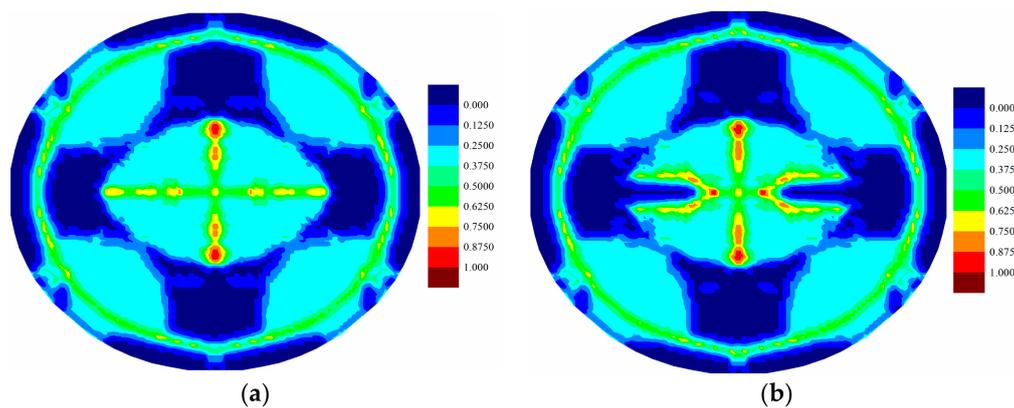


Figure 13. Matrix damage comparison of middle (7th) ply for (a) coupled case and (b) uncoupled case at 0.28453×10^{-3} s.

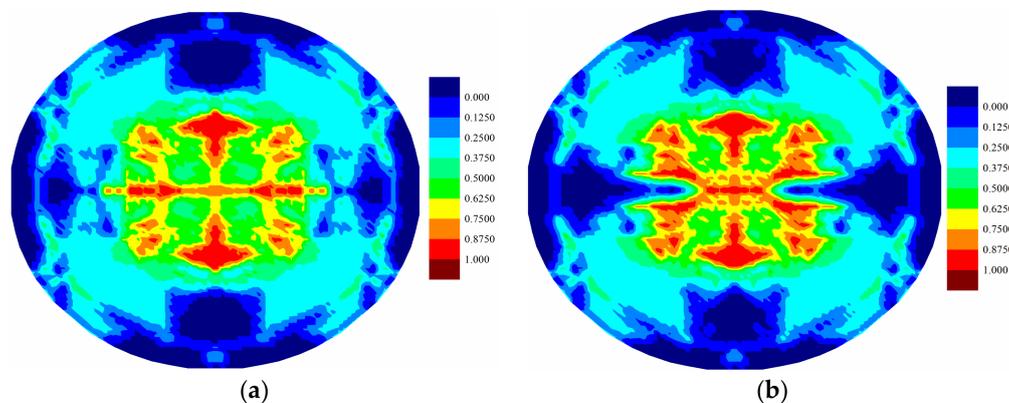


Figure 14. Matrix damage comparison of bottom ply for (a) coupled case and (b) uncoupled case at 0.28453×10^{-3} s.

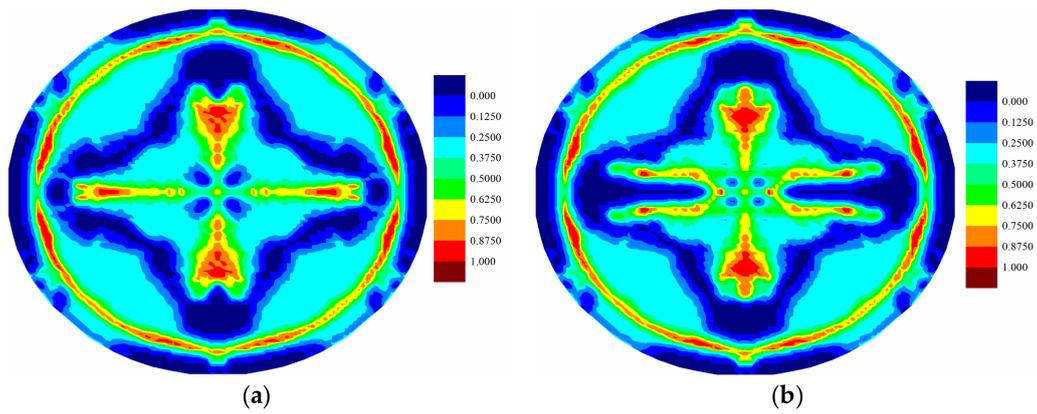


Figure 15. Matrix damage comparison of top ply for (a) coupled case and (b) uncoupled case at 0.3461×10^{-3} s.

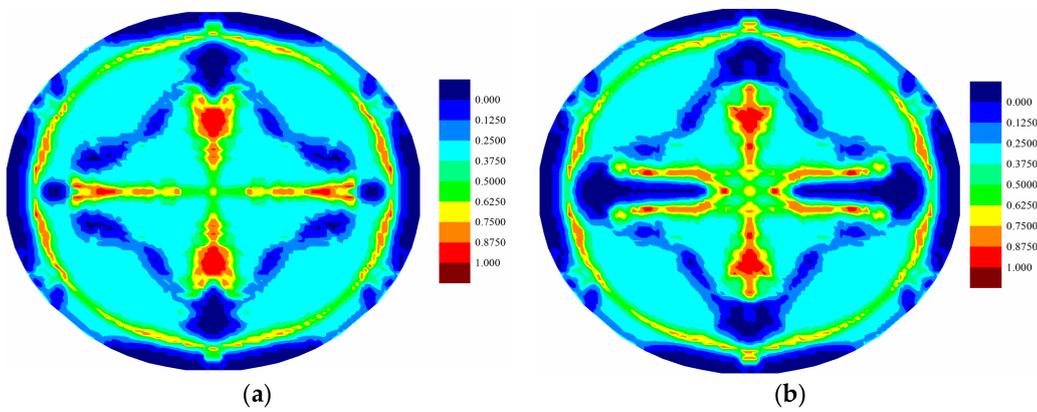


Figure 16. Matrix damage comparison of middle (7th) ply for (a) coupled case and (b) uncoupled case at 0.3461×10^{-3} s.

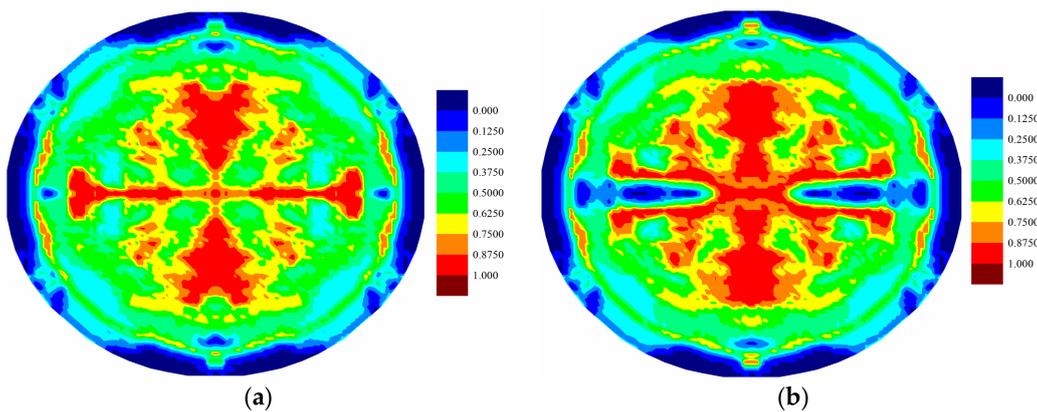


Figure 17. Matrix damage comparison of bottom ply for (a) coupled case and (b) uncoupled case at 0.3461×10^{-3} s.



Figure 18. Material damage during test [13].

The extent of damage in interlayer shear bonds was also investigated, and only slight differences were observed in the top few plies between the coupled and uncoupled cases (Figure 19). The middle ply experienced the most severe damage, as shown in Figure 20. Thus, it can be inferred that the interlayer shear bond damages occur mainly in the middle plies of the test laminate. Hence, it can be concluded that there is delamination failure in the middle plies.

Temperature changes induced by the applied pressure shock loading are presented for different plies in Figures 21–23. It is observed that as the loading increased, the temperature changes of PD nodes increased. For all plies, the temperature change profiles all have similar patterns as the corresponding crack damage patterns. As shown in Figures 21–23, there is a temperature rise where there is local compression, and there is a temperature drop where there is local tension, as explained in [21]. In the top ply, most of the region was under compression and a temperature rise was observed; on the other hand, the bottom ply was mostly under tension, and a consequent temperature drop was observed, as shown in Figure 23. In the cracked surfaces, temperature drops were observed because of the local tension; however, temperature rise was observed near the crack tips. Thus, the crack propagation paths do have effects on the temperature distributions.

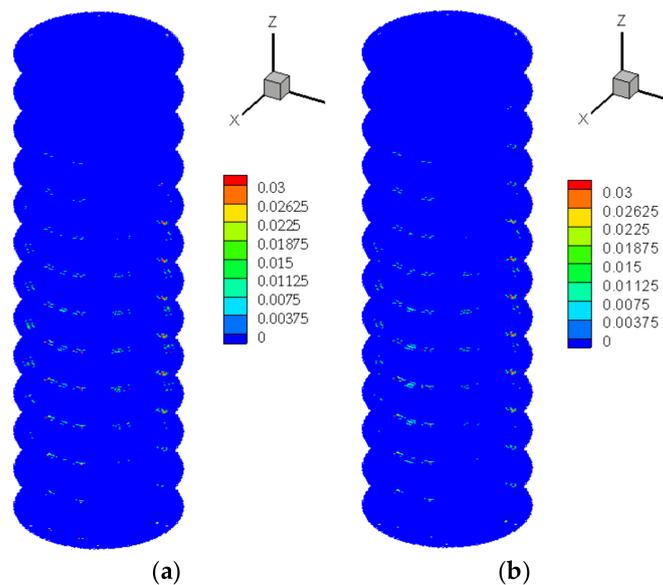


Figure 19. Interlayer shear damage comparison for (a) coupled case and (b) uncoupled case at 0.3461×10^{-3} s.

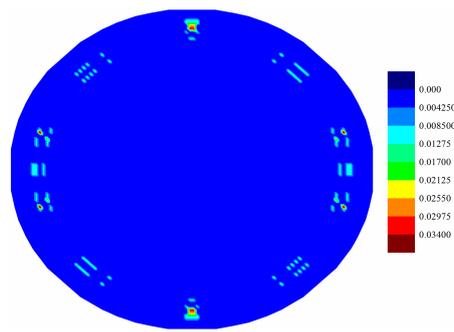


Figure 20. Interlayer shear damage of middle ply in coupled case at 0.3461×10^{-3} s.

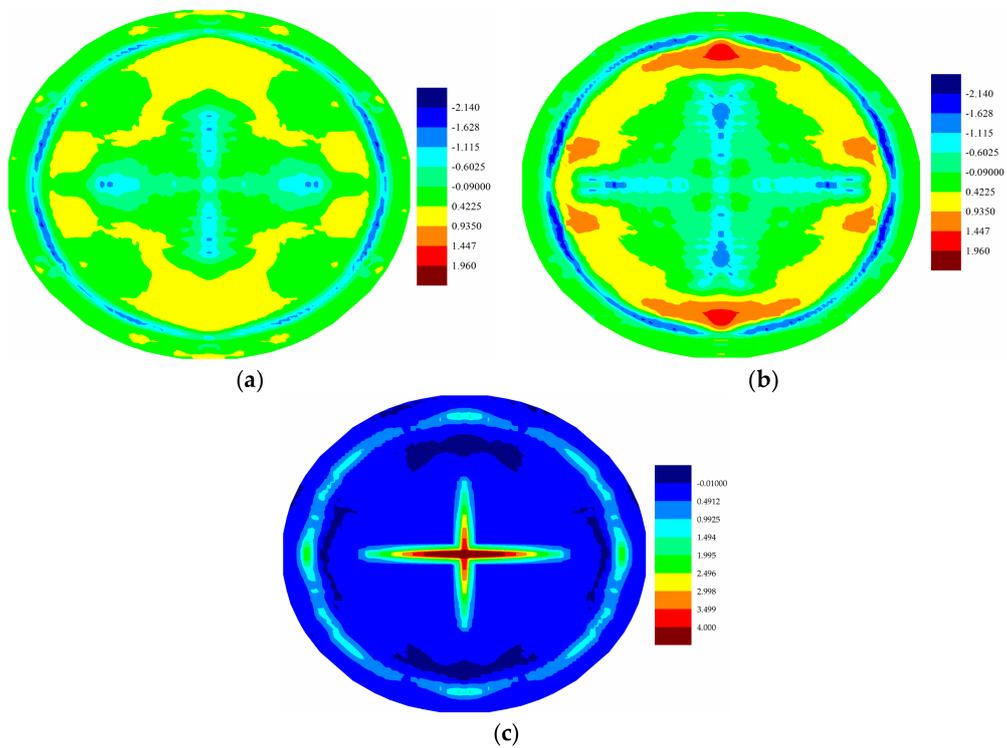


Figure 21. (a) Distribution of temperature change (K) of top ply at 0.28453×10^{-3} s; (b) Distribution of temperature change (K) of top ply at 0.3461×10^{-3} s; (c) Maximum stretch distribution of top ply at 0.3461×10^{-3} s.

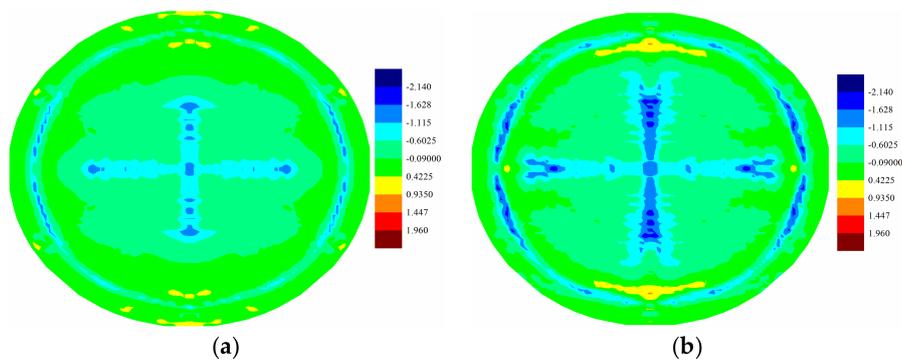


Figure 22. Cont.

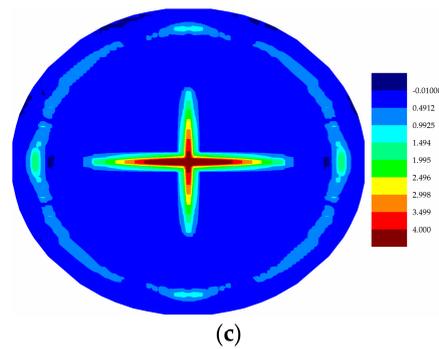


Figure 22. (a) Distribution of temperature change (K) of middle ply at 0.28453×10^{-3} s; (b) Distribution of temperature change (K) of middle ply at 0.3461×10^{-3} s; (c) Maximum stretch distribution of middle ply at 0.3461×10^{-3} s.

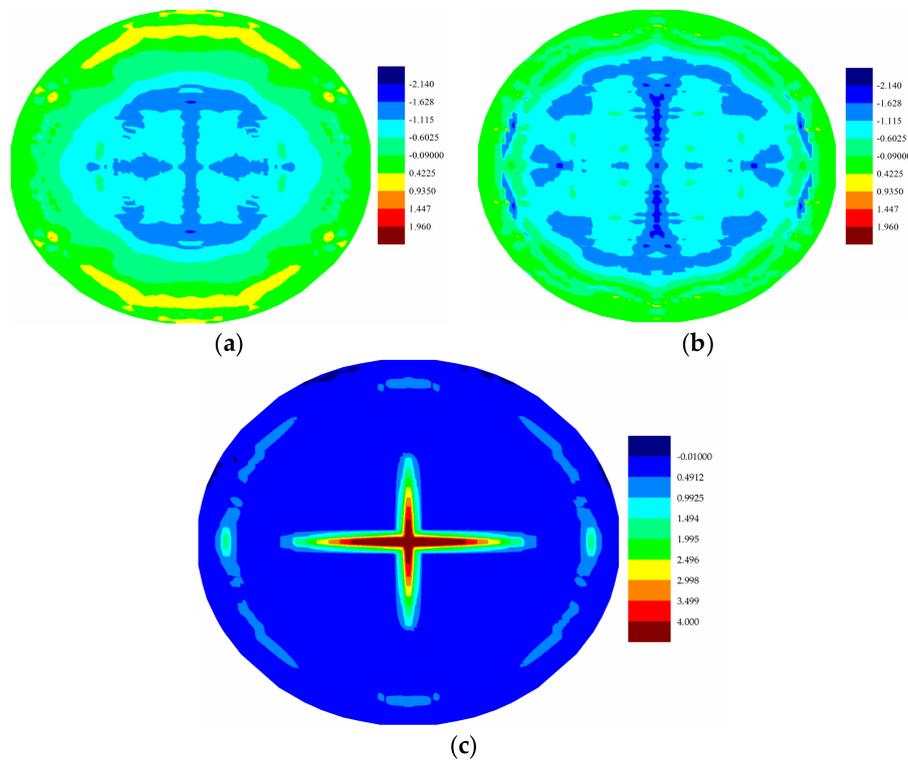


Figure 23. (a) Distribution of temperature change (K) of bottom ply at 0.28453×10^{-3} s; (b) Distribution of temperature change (K) of bottom ply at 0.3461×10^{-3} s; (c) Maximum stretch distribution of bottom ply at 0.3461×10^{-3} s.

4. Conclusions

In this paper, a bond-based PD laminate model was applied to predict the responses of a 13-ply composite under a pressure shock loading. Both the deformation effect on the temperature field and the temperature effect on deformation were taken into consideration in the generalized PD model. Hence, the simulation was conducted by considering fully coupled thermomechanical effects. Firstly, the matrix damages of the laminate were predicted at different simulation times. It was observed that each ply within the laminate experienced a different level of matrix crack. Then, the breakages of the interlayer shear bonds were investigated. The delamination failure occurred mainly in the middle part of the laminate. The PD-predicted damage pattern agrees well with the experimental result. Furthermore, the temperature change evolution induced by the applied mechanical pressure

shock was also simulated. The temperature distributions presented similar patterns with the crack propagations. Finally, the crack propagation patterns were compared for coupled and uncoupled cases. Results showed that the coupling term has an effect on crack propagation pattern. The developed model can be used for predicting more realistic crack patterns. In conclusion, the PD theory is able to predict both thermal and mechanical responses of marine composites under shock loadings.

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