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Refined Analysis of RADARSAT-2 Measurements to Discriminate Two Petrogenic Oil-Slick Categories: Seeps versus Spills

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Abstract: Our research focuses on refining the ability to discriminate two petrogenic oil-slick categories: the sea surface expression of naturally-occurring oil seeps and man-made oil spills. For that, a long-term RADARSAT-2 dataset (244 scenes imaged between 2008 and 2012) is analyzed to investigate oil slicks (4562) observed in the Gulf of Mexico (Campeche Bay, Mexico). As the scientific literature on the use of satellite-derived measurements to discriminate the oil-slick category is sparse, our research addresses this gap by extending our previous investigations aimed at discriminating seeps from spills. To reveal hidden traits of the available satellite information and to evaluate an existing Oil-Slick Discrimination Algorithm, distinct processing segments methodically inspect the data at several levels: input data repository, data transformation, attribute selection, and multivariate data analysis. Different attribute selection strategies similarly excel at the seep-spill differentiation. The combination of different Oil-Slick Information Descriptors presents comparable discrimination accuracies. Among 8 non-linear transformations, the Logarithm and Cube Root normalizations disclose the most effective discrimination power of almost 70%. Our refined analysis corroborates and consolidates our earlier findings, providing a firmer basis and useful accuracies of the seep-spill discrimination practice using information acquired with space-borne surveillance systems based on Synthetic Aperture Radars.

Keywords: oil-slick discrimination algorithm; petrogenic oil-slick category; naturally-occurring oil seeps; man-made oil spills; exploratory data analysis; remote sensing; synthetic aperture radar; RADARSAT; Gulf of Mexico; Campeche Bay

1. Introduction

The impact of mineral oil pollution is a widely spread source of environmental concern in various ecosystems [1,2]. The detection of the sea surface expression of oil using space-borne surveillance systems is an extensively studied subject [3–5]. Oil floating on the surface of the ocean can be located, to some extent, with different types of remote sensing sensors—e.g., thermal infrared (AVHRR: Advanced Very High Resolution Radiometer [6]), visible/near infrared (MODIS: Moderate Resolution Imaging Spectroradiometer [7]), etc.—but generally, most attempts concentrate on using

satellite-derived measurements from active microwave-imaging instruments (SAR: Synthetic Aperture Radars [8–10]), e.g., RADARSAT [11,12].

Research projects using SAR measurements to study petrogenic oil slicks usually focus on understanding two major processes: (1) Identification of smoother regions observed at the sea surface with reduced radar backscattering signal, i.e., classification and segmentation for dark spot detection (e.g., [13]); and (2) Differentiation of radar signature of mineral oil slicks from what is commonly referred to as "radar look-alikes" (e.g., [14])—for instance, surface natural oil produced by plants or animals (i.e., biogenic oil films), atmospheric conditions (e.g., low wind and rain cells), oceanographic features (e.g., upwelling regions and internal gravitational waves), etc. [15]. Apart from the scientific effort studying these two processes [16], few investigations are directed at using remote sensing systems to differentiate the mineral oil-slick type—i.e., differences among types of anthropogenic oil slicks observed at the sea surface, for instance: oil slicks formed from heavy versus light oil [17]; or oil slicks from production oil tests (i.e., oil released at the surface of the ocean in the process of evaluating new drilling wells) versus oily water (i.e., oil slicks from leakages occurring during the exploration or production phases) [18].

The available literature covering the subject of identifying oil slicks at the surface of the ocean using space-borne surveillance systems, for the most part, does not address the petrogenic oil-slick category discrimination: telling apart the oil-slick sea surface expression in relation to their source, thus considering oil seeps (i.e., natural oil seepages from a hydrocarbon reservoirs) versus oil spills (i.e., mineral oil spillages from man-made activities) [19–22]. The seep-spill discrimination mostly regards two points of view: economic and environmental. While the former deals with the discovery of new oil exploration frontiers in finding the presence of active petroleum systems, the latter is capable of improving the relationship between the oil- and gas-related industry and environmental organizations (and society as a whole) by reducing any origin uncertainty about the oil slick source (i.e., naturally-occurring seeps versus man-made spills). A third point of view is the one of the remote sensing community, in which if a certain methodology is capable of discriminating oil from oil using microwave measurements acquired from space [19–22], it might be plausible to say that such methodology can also be applied to differentiate oil from look-alike features in SAR imagery. This framework scientifically strengthens the other two points of view.

Notwithstanding the relative neglect of research projects on the use of satellite sensors for the discrimination of the oil-slick category, Carvalho [19] showed it is feasible to use SAR-derived measurements for seep-spill discrimination—see also [20–22]. These authors have used a series of Multivariate Data Analysis Techniques to devise a novel idea to discriminate the oil-slick category while studying seeps and spills observed on the surface of the ocean in the Gulf of Mexico off the Mexican coast in the Campeche Bay region (Figure 1). They have proposed a simple Oil-Slick Discrimination Algorithm based on SAR backscatter signature, i.e., sigma-naught (σ^{o}), beta-naught (σ^{o}), and gamma-naught (σ^{o}) [23–25], along with the geometry, shape, and dimension of the oil slicks. Their best outcome is reached with optimal Overall Accuracies of approximately 70%, based on the oil slicks' areas and perimeters.

We report on analyses to refine the ability to discriminate the petrogenic oil-slick category (seeps versus spills) proposed in our previous investigations [19–22]. Exploiting the same dataset, but with expanded Data Processing Segments, we extend our earlier studies onto a firmer basis. Based on our methodical data mining exercise, we seek to improve the seep-spill discrimination accuracy, as well as to answer three scientific questions:

- 1. Among the several Data Transformation Approaches we tested, which one provides the most accurate oil-slick category discrimination?
- 2. Is there a specific Attribute Selection Process that excels at choosing variables to discriminate seeps from spills?
- 3. Which combination of Oil-Slick Information Descriptors promotes the best discrimination between seeps and spills?

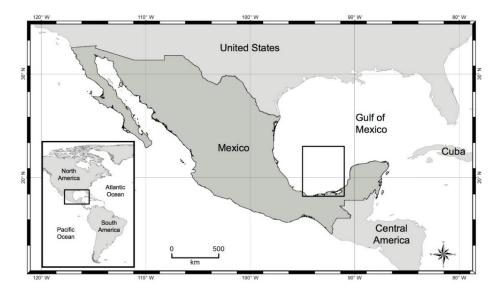


Figure 1. Campeche Bay located off the Mexican coast on the southernmost bight of the Gulf of Mexico. The highlighted region shows the location of the analyzed oil slicks. Courtesy of Adriano Vasconcelos (LabSAR/UFRJ).

2. Methods

We developed a comprehensive Exploratory Data Analysis (EDA) to reveal hidden information contained in the satellite-derived measurements and to refine the analysis to discriminate slicks by category, as proposed in our earlier studies [19–22]. The design of our EDA focuses on a data-driven scheme to investigate possible ways to improve the seep-spill discrimination with the simplest possible analysis and the lowest satellite-imaging cost. The research strategy employed herein is a development of our previous investigations [19–22], and consists of four distinct Data Processing Segments (i.e., A, B, C, and D in Figure 2)—devised in eight individual Phases—separately described in detail and introduced in a complete manner easily enabling replicability of our data mining exercise. A summary of our EDA design is depicted in Figure 2. While in-house Python codes are used to run the oil slick RADARSAT-2 related analyses (i.e., Phases 1–4), PAST (PAleontological STatistics: version 3.20, Oslo, Norway [26]) is used in the implementation of Phases 5–8.

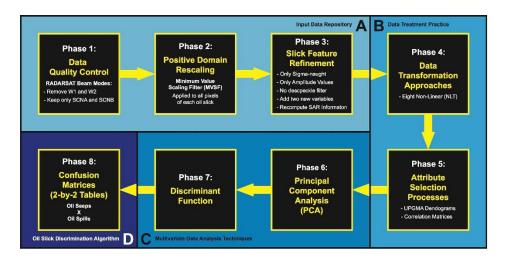


Figure 2. Research strategy developed to refine the ability to discriminate between two petrogenic oil-slick categories (i.e., seeps versus spills), as proposed in our previous studies [19–22]. The proposed Exploratory Data Analysis (EDA) has four distinct Data Processing Segments defined as: (**A**) Input Data Repository (Phases 1–3); (**B**) Data Treatment Practice (Phases 4–5); (**C**) Multivariate Data Analysis Techniques (Phases 6–7); and (**D**) Oil-Slick Discrimination Algorithm (Phase 8).

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A multi-year dataset of RADARSAT-2 scenes imaged between 2008 and 2012 gave rise to the oil slick data archive analyzed in our earlier investigations [19–22]. This data archive consists of polygons representative of oil slicks that had been identified and field validated as seeps and spills by domain experts. For more information about this dataset, see [19–22]. The workable dataset explored herein is defined after fine-tuning this data archive along the 1st Data Processing Segment (Figure 2A: Input Data Repository—Phases 1–3).

2.1. Phase 1: Data Quality Control

The initial oil slick data archive from our previous studies [19–22] is sorted by the satellite scene-imaging configuration (i.e., beam modes determining the acquisition swath width and ground resolution), thus establishing the amount of RADARSAT-2 imagery and the seeps and spills of our workable dataset.

2.2. Phase 2: Positive Domain Rescaling

The initially available oil slick data archive analyzed in our earlier investigations [19–22] had undergone a linear scaling action (Negative Values Scaling Filter: NVSF) that is comprised of a two-fold procedure applied to individual oil slicks: the subtraction of the minimum negative pixel value within each oil slick from every single pixel of such oil slick, followed by the addition of 1 to every single pixel—the minimum pixel value becomes 1. This brings all pixel values to the positive domain, which is a requirement of data normalization procedures that cannot be applied to negative values, e.g., \log_{10} . The NSVF is applied at the pixel level, i.e., taking into account all pixels of each oil slick to provide a single measure representative of all pixels of such oil slick (see below: Section 2.3.2). Nevertheless, previously, the NVSF was only applied to certain oil slicks: those having at least one negative pixel value—for instance, oil slicks that had spurious negative SAR backscatter signature caused by intrinsic multiplicative random granular speckle noise destructive imprecision in the range-dependent gain calculation [27,28].

Although we also conduct this filtering strategy, we apply it in the present research to all oil slicks. In essence, hereafter, for our purpose, the NVSF is referred to as Minimum Values Scaling Filter (MVSF), such that: PIXpos = (PIX-PIXmin) + 1, in which PIXpos corresponds to the new positive pixel value, PIX is the original pixel value, PIXmin is the minimum pixel value of all pixels of each oil slick. Therefore, this is a dissimilarity between our previous investigations and the current EDA: NVSF versus MVSF. The reason for applying the MVSF to all oil slicks is three-fold: (1) To avoid possible biases caused by gradient differences among oil slicks with and without NVSF; (2) To circumvent the application of despeckle filtering (e.g., Frost Filter: FFrost [29]; see also Phase 3) that eventually would eliminate negative values, but would alter (e.g., smoothing) the SAR backscatter signature values—the lack of such filter is justifiable to preserve the data-driven design of our EDA; and (3) To exploit data transformations that do not accept negative values (see below: Phase 4).

2.3. Phase 3: Slick Feature Refinement

2.3.1. SAR Backscatter Signature

Previously, we explored twelve SAR backscatter signatures: SAR backscatter coefficients corresponding to the radar cross-section (RCS: σ) normalized by the unit area calculated in three different surface planes (i.e., σ^o , β^o , and γ^o [30–34]) computed in four radiometric-calibrated image products—i.e., the amplitude (1st) of the received radar beam and its dimensionless physical quantity form that represents power expressed in dB (2nd), both with (3rd) and without (4th) despeckle filtering (FFrost: 3-by-3 window). However, herein we perform a simplification for a more controlled EDA solely using σ^o given in amplitude without despeckle filtering. As such, from this point onwards, unless otherwise stated, any reference to SAR backscatter signature synonymously refers to this simplification.

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2.3.2. Oil-Slick Information Descriptors

As before [19–22], we start our research analyzing the same ten attributes describing the oil slicks' geometry, shape, and dimension (these are collectively referred to as Size Information Descriptors) derived from two basic morphological features characterizing the oil slicks—i.e., area (Area) and perimeter (Per):

- **AtoP**: Area to Per ratio;
- **PtoA**: Per to Area ratio [35];
- **PtoAnor**: Normalized Per to Area ratio = Per/[(2.(Pi.Area))^{1/2}] [36];
- Complex Index = [Per²]/Area [37];
- **Compact Index** = [4.Pi.Area]/[Per²] [18];
- Shape Index = $[Per/4]/[Area^{1/2}]$ [38];
- Fractal Index = [2.Ln(Per/4)]/[Ln(Area)] [39];
- LEN: Number of pixels of each oil slick polygon.

Analogously, we also exploit the same 36 basic descriptive statistics metrics experimentally explored to characterize the oil slicks' SAR backscatter signature as in our previous investigations [19–22]. These metrics are calculated based on all pixels inside individual oil slick polygons:

- Four central tendency measures: Average (AVG), Median (MED), Mode (MOD), and Mid-mean (MDM: mean of the values between the 2nd and 3rd interquartiles, i.e., it trims off 25% of both ends);
- Six measures of dispersion: Range (RNG), Coefficient of Dispersion (COD: the subtraction of the
 1st interquartile from the 3rd interquartile and the division by their sum), Standard Deviation
 (STD), Variance (VAR), Average Absolute Deviation (AAD: mean of the absolute difference of each
 value to the mean), and Median Absolute Deviation (MAD: median of the absolute difference of
 each value minus the median);
- 24 pair-values of Coefficients of Variation (COV: ratio between STD and AVG [18], such that each of the six dispersion measures are individually divided by the four central tendencies);
- The Minimum (MIN) and Maximum (MAX) pixel values of each oil slick.

Herein we introduce two new variables that describe the distribution patterns of the pixels within each oil slick: Skewness (SKW) and Kurtosis (KUR). As such, this collection of 38 basic descriptive statistics metrics characterizing the oil slick's SAR backscatter signature is henceforth referred to as SAR Information Descriptors. Together, these two types of Oil-Slick Information Descriptors (i.e., Size and SAR) determine the initial number of variables (48) accounted in our workable dataset.

2.4. Phase 4: Data Transformation Approaches

In contrast with our previous investigations [19–22], which implemented only a single non-linear normalization (log_{10}) and one linear standardization (Ranging [40]), we exploit several Non-Linear Transformations (NLTs [41–44]):

- **NLT.0**: No Transformation (x);
- **NLT.1**: Reciprocal (1/x);
- **NLT.2**: Logarithm Base 10 ($log_{10}(x)$);
- **NLT.3**: Napierian Logarithm (Ln(x));
- **NLT.4**: Square Root $(x^{1/2})$;
- **NLT.5**: Square Power (x²);
- **NLT.6**: Cube Root $(x^{1/3})$;
- **NLT.7**: Third Power (x^3) .

In which x corresponds to the actual value of each oil slick variable (i.e., Oil-Slick Information Descriptors—see Phase 3). Half of these (i.e., NLT.1, NLT.2, NLT.3, and NLT.4) do not accept negative values (x). To simplify our analyses, we do not perform linear standardizations.

2.5. Phase 5: Attribute Selection Processes

The processes of selecting relevant attributes deals with the complex matter of reducing dimensionality in the variable-hyperspace domain (see also Phase 6); this generally helps to elucidate the problem solution of numerical ecology assessments and to improve the performance of classification algorithms [42,45]. As such, another difference from our earlier studies is the number of explored attributes: before, we investigated 44 data sub-divisions with 502, 433, 423, 151, 141, 35, 10, and 2 variables [19–22]. Indeed, we considerably reduce these numbers with the SAR backscatter signature simplification (see Phase 3: Section 2.3.1). Additionally, we start with 48 Oil-Slick Information Descriptors (see Phase 3: Section 2.3.2) but use even fewer variables upon the completion of the Attribute Selection Processes (see below: Section 2.5.1).

2.5.1. Unweighted Pair Group Method with Arithmetic Mean (UPGMA)

Two attribute selection strategies (i.e., R-mode) have been performed in our previous investigations [19–22]: UPGMA [42,43,46] and CFS (Correlation-Based Feature Selection [47,48]). Based on our earlier results, we only implement the former as it allows a user-defined strategy to select relevant variables: the choice of the similarity index (Pearson's r correlation coefficient) used in the UPGMA dendrogram as cut-off to form groups of similar variables, i.e., phenon line [49,50]. See also [19–22] for further information about analyses and interpretations of rooted tree UPGMA dendrograms.

Moreover, an imperative distinction from our earlier investigations is that herein we are experimenting the use of a strict cut-off level, i.e., a fixed similarity value of 0.3, in relation to the previous fixed value of 0.5 and varying one ranging around 0.9 [19–22]. The selection of the 0.3 similarity cut-off is enlightened by the Bonferroni Adjustment as the level of minimum significance (p value) for large datasets (n > 100); below this there is no statistically significant correlation and variables are considered different from one another [51].

2.5.2. Histograms and Correlation Matrices

Histograms and correlation matrices assist in the verification of residual inter-variable correlation and to help with the decision of which variables to select on the groups formed on the UPGMA analyses.

2.6. Phase 6: Principal Component Analysis (PCA)

PCAs reduce the large correlated variables set into a smaller set of uncorrelated hypothetical variables—Principal Components (PCs)—containing most of the relevant information of the initial larger set [42,43]. The rotation of the original axes to the new orthogonal coordinate system is implemented in the same manner as our earlier work: square symmetric correlation matrix and 1000 bootstraps [52]. However, the approach to select relevant axes (i.e., PCs) is a departure from our earlier investigations. While, herein we use only the Kaiser Cut, i.e., Kaiser-Guttman criterion (eigenvalues > 1 [53]), previously we explored several PC-selection practices, e.g., Jolliffe, Scree Plot (Knee/Elbow), and a combined strategy using the Scree Plot (broken stick) with Kaiser [54–57].

2.7. Phase 7: Discriminant Function

Discriminant Analysis differs from Clustering Analysis as it is not meant to determine to which group each object belongs [43]. Instead, Discriminant Functions use a priori measured information (Oil-Slick Information Descriptors) and knowledge of the object's (oil slick) group membership (seep or spill), to obtain the maximum discriminating power that minimizes the probability of erroneous discrimination: $[DF(X) = (W_1X_1 + W_2X_2 + ... + W_nX_n) - C_{off}]$; in which DF(X) corresponds to the dependent variable (i.e., Discriminant Function); X_n to the independent variables (i.e., Oil-Slick Information Descriptor value); W_n to the independent variables' weight; and C_{off} to the constant offset [58–61].

The use of uncorrelated attributes (selected PCs from Phase 6), or at least with the lowest possible degree of dependence (UPGMA selected variables from Phase 5), is a pressing need for Discriminant Functions [62], and as such, this concerns a crucial development of the current EDA from our previous investigations [19–22]: herein, we are not only using the PCA scores (PCs) as input to the Discriminant Functions, we are also testing the use of UPGMA dendrogram selected variables (see Phase 5: Section 2.5.1) without passing through the PCA.

2.8. Phase 8: Confusion Matrices (2-by-2 Tables)

The Oil-Slick Discrimination Algorithm accuracy is reported based on the Discriminant Function results by means of the complete understanding of adapted 2-by-2 Tables (Confusion Matrices: CMs). See also [19–22,63–65] for information on how to analyze and to better interpret 2-by-2 Tables. The conjunct interpretation of five metrics [66] is essential to fully evaluate the algorithm's effectiveness. Table 1 gives a picture of these metrics that are color-coded for clarity:

- **CM.1**: Overall Accuracy (shown in Green);
- CM.2: Producer's Accuracy (i.e., Sensitivity and Specificity—shown in Yellow);
- CM.2: Commission Error (i.e., False Negative and False Positive);
- CM.3: User's Accuracy (i.e., Positive and Negative Predictive Values—shown in Purple);
- CM.3: Omission Error (i.e., Inverse of the Positive and Negative Predictive Values).

Table 1. Adapted 2-by-2 Tables (Confusion Matrix: CM [19–22,63–65]) illustrating the various metrics explored to evaluate the Oil-Slick Discrimination Algorithm accuracy, i.e., Discriminant Function (DF) results.

	1.1	DF Oil Seep	DF Oil Spill	Total Real				
	ep Real	Α	В	A+B				
	ill Real	С	D	C+D				
Tota	al DF	A+C	B+D	A+B+C+D				
				(A+D) *				
				(A+B+C+D)				
	.2**	DF Oil Seep	DF Oil Spill	Total Real				
	ep Real	A/(A+B)	B/(A+B)	100%				
Oil Spi	ill Real	C/(C+D)	C/(C+D)	100%				
	.3**	DF Oil Seep	DF Oil Spill					
	ep Real	A/(A+C)	B/(B+D)					
	ill Real	C/(A+C)	D/(B+D)					
Tota	al DF	100%	100%					
		ber of Samples						
	A = Oil Seeps: Correct Identification							
	B = Oil Seeps: Miss-Identification							
CM.1	C =	Oil Spills: Miss-I	dentification					
	D =	D = Oil Spills: Correct Identification						
	A+B	A+B+C+D = Oil Slicks (i.e. 4,562)						
	* Ov	eral Accuracy						
	Produc	er's A/(A+B) =	Sensitivity					
		C/(C+D) =						
CM.2	Comiss	ion B/(A+B) =	False Negative					
CM.Z	Error		False Positive					
			Oil Seeps (i.e.					
			Oil Spills (i.e. :					
	User's		Positive Predictiv					
	Accura		Negative Predicti					
см.з	Omissi		Inverse of the Po					
0.1.5	Error		Inverse of the Ne	eg. Predict. Val.				
	l		DF Oil Seeps					
		B+D =	DF Oil Spills					

^{**} Values given in pecentage.

3. Results and Discussion

3.1. Phase 1: Data Quality Control

The initially available oil slick data archive is composed of 4,916 oil slick polygons—2021 oil seeps (41%) and 2895 oil spills (59%)—imaged with 277 RADARSAT-2 scenes (Table 2 I), all of which are 16-bit and VV polarized [19–22]. These include two different RADARSAT beam modes—Wide [W1 and W2: 354 oil slicks (7%)] and ScanSAR Narrow [SCNA and SCNB: 4562 oil slicks (93%)]—that own two fundamental imaging differences: (1) W1 and W2 are Single Beam Modes (i.e., a strip-map SAR mode

with certain imaging aspects constant along the entire scene), whereas SCNA and SCNB are ScanSAR Modes (i.e., combine two or more of the Single Beam Modes) [67]; the latter provides larger area coverage: swath width of 300 km—almost twice that of W1 and W2: 170 km and 150 km, respectively; and (2) Wide has a finer ground resolution of 25 m, which is $\frac{1}{4}$ of the ScanSAR Narrow one: 50 m.

Table 2. Number (and percentage) of explored oil slicks (seeps and spills) and satellite images.

Oil Category	I: Previous Work	II: Our Reseach	III: Difference
Oil Seeps	2,021 (41%)	1,994 (44%)	-27 (-1%)
Oil Spills	2,895 (59%)	2,568 (56%)	-327 (-11%)
Oil Slicks	4,916 (18%)*	4,562 (13%)*	-354 (-7%)
RADARSAT-2 scenes	277	244	-33 (-12%)

- I: Initially available oil slick data archive [19-20].
- II: Our workable dataset, i.e. large collection of oil slick polygons imaged with RADARSAT-2 scenes of the two ScanSAR Narrow beam modes: SCNA and SCNB.
- III: Removal of RADARSAT-2 beam mode (Wide: W1 and W2) dunig Phase 1 (Data Quality Control).
 - * Difference between oil spills and oil seeps.

Regarding their specification differences, eventual inaccuracies may be introduced to beam mode cross-comparisons. Notwithstanding that W1 and W2 provide better delineation of smaller oil slicks with their finer ground resolution, only SCNA and SCNB are kept in our analysis as these represent more than 90% of the available scenes. Furthermore, the ScanSAR Narrow swath width is more appropriate for monitoring applications requiring large-scale coverage such as the one that gave rise to the initially available oil slick data archive [19–22]. In fact, the lower scene cost of using ScanSAR Narrow to monitor larger ocean regions is rather preferable than the smaller area coverage of the Wide images.

Consequently, our workable dataset is composed of the collection of oil slick polygons imaged with the two ScanSAR Narrow beam modes: 4562 oil slicks—1994 oil seeps (44%) and 2568 oil spills (56%)—Table 2 II. Despite the fact that our EDA has 7% (354) fewer oil slicks than our previous study [19–22], representing about 1% (27) fewer seeps and approximately 11% (327) fewer spills (Table 2 III), such data reduction results in a more balanced dataset as compared to the one explored in our previous investigations, i.e., a smaller difference between the number of analyzed spills and seeps: 13% instead of 18% (Table 2: I–II). Indeed, this provides a firmer basis in the oil-slick category discrimination. Moreover, the oil slick polygons imaged with SCNA and SCNB come from 244 RADARSAT-2 scenes imaged between 2008 and 2012—12% (33) fewer images than our earlier investigations (Table 2).

3.2. Phase 2: Positive Domain Rescaling

As the MVSF is applied at the pixel level to all oil slicks in our workable dataset (Table 2 II: 4562), it affects the values of the 38 SAR Information Descriptors but not of the 10 Size Information Descriptors (see Phase 3: Section 2.3.2). The latter is independent of the MVSF application as they are derived from and include the two basic morphological oil slick features: Area and Perimeter.

3.3. Phase 3: Slick Feature Refinement

The consequence of MVSF (see Phase 2) is two-fold: (1) the SAR Information Descriptors are not the same as in our previous investigations and need to be recomputed for all analyzed oil slicks; (2) MIN loses its meaning as its value for all oil slicks becomes 1; accordingly, it is not pursued in our analysis.

3.4. Phase 4: Data Transformation Approaches

Although the NLTs can be independently applied to each attribute, for consistency, during our EDA, all-numeric variables uniformly undergo the same column-wise transformation. Because three Oil-Slick

Information Descriptors—i.e., Fractal, SKW, and KUR—have values that range from negative to positive, they are not used on half of the NLTs that require only positive values: NLT.1; NLT.2; NLT.3; and NLT.4.

3.5. Phase 5: Attribute Selection Processes

Histograms show that the distribution of some Size Information Descriptors is the same as others, sometimes being inverted independent of NLT, meaning that there is no new information revealed. As a result, only one of these variables is selected, for instance: (1) AtoP and PtoA have equal but inverted distributions; (2) PtoAnor, Complex, Compact, and Shape, also have equal distribution but Compact is inverted from the three other. Of these variables, we only keep PtoA and Compact, as Area and Perimeter appear in opposition in their formula: PtoA has area in the denominator, as opposed to Compact, which has area in the numerator; the contrary holds true for the perimeter (see Phase 3: Section 2.3.2).

3.5.1. Unweighted Pair Group Method with Arithmetic Mean (UPGMA)

The combined analysis of dendrograms and correlation matrices show that the 24 COV pair-values have a strong intra-correlation, as well as that they are highly correlated with most of the other variables; hence, they are not further explored. Therefore, out of the 48 initial Oil-Slick Information Descriptors (see Phase 3: Section 2.3.2), only 19 remain for further analyses—Size (6): Area, Per, PtoA, Compact, Fractal, and LEN; and SAR (13): AVG, MED, MOD, MDM, RNG, COD, STD, VAR, AAD, MAD, MAX, SKW, and KUR. However, only half of the NLTs (NLT.0, NLT.5, NLT.6, and NLT.7) utilize these 19 variables; the other half (NLT.1, NLT.2, NLT.3, and NLT.4) explores three fewer Oil-Slick Information Descriptors, i.e., only 16 variables (see Phase 4: Section 3.4).

Figure 3 depicts eight UPGMA dendrograms (one for each of the analyzed NLT), in which it is possible to observe a number of differences, as well as resemblances, between them; mostly regarding inter-variable correlations. An evident characteristic of the two Logarithm functions (NLT.2: Log_{10} ; and NLT.3: Ln) is that their dendrograms are equal; the same holds true for their correlation matrices that are also identical.

Prior to the uncorrelated variables selection, we have to identify the groups of correlated variables. The process of defining and/or interpreting groups in UPGMA dendrograms is quite subjective [43], but, at first glance, the global picture of Figure 3 clearly reveals how equivalent are the groups between the several NLTs; these are color-coded for clarity. In the visual analysis of Figure 3, one can note that variables tend to group based on their main characteristics, following the Oil-Slick Information Descriptor features, such that:

- **Green**: Measures of central tendency (AVG, MED, MOD, and MDM);
- Blue: Dispersion measures (RNG, COD, STD, VAR, AAD, and MAD);
- Grey: Metrics of pixel distribution (SKW and KUR);
- Yellow: Basic morphological features (Area and Per) and LEN;
- **Red**: Ratios derived from the morphological features (PtoA, Compact, and Fractal).

An advanced analysis of the UPGMA dendrograms shown in Figure 3 discloses that:

- The three morphological ratios (Red group) are not correlated with any other variable (similarity close to or equal to zero)—PtoA and Compact form an uncorrelated group, and Fractal usually stands alone; the exception is in NLT.0 where Compact is the one by itself;
- The two groups of SAR Information Descriptor, i.e., Green (central tendency) and Blue (dispersion), generally form a larger group—Geen + Blue—the exception is in NLT.7;
- The Grey group (pixel distribution metrics) is usually correlated with the Yellow group (basic morphological features)—Grey + Yellow group—the exception is in NLT.7 where it groups with the Green group (measures of central tendency);
- RNG is an exception in three NLTs (NLT.0, NLT.6, and NLT.7) as it correlates with the central tendency variables (Green group);
- MAX groups among the central tendency variables (Green group) except in NLT.4.

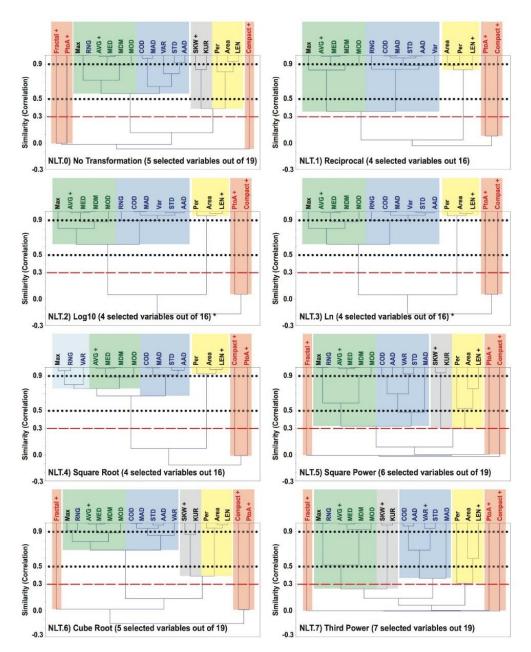


Figure 3. Rooted tree dendrograms (Unweighted Pair Group Method with Arithmetic Mean: UPGMA—see Phase 5: Sections 2.5.1 and 3.5.1) of the several Non-Linear Transformations (NLTs—see Phase 4: Section 2.4). While the horizontal red dashed line represents the phenon line exploited herein to form groups of variables, i.e., similarity value of 0.3 (i.e., Pearson's r correlation coefficient), the two horizontal black dotted lines correspond to the more relaxed thresholds reported in our previous investigations [19–22]. The various color-colored boxes indicate the main groups of variable (see Phase 3: Section 2.3.2). Size Information Descriptors: Yellow [basic morphological oil slick features, i.e., area (Area) and perimeter (Per), and the number of pixels (LEN)] and Red [three ratios derived from the morphological features]. SAR Information Descriptors: Green [measures of central tendency, i.e., average (AVG), median (MED), mode (MOD), and mid-mean (MDM); an exception is the maximum pixel value (MAX)], Blue [dispersion measures, i.e., range (RNG), coefficient of dispersion (COD), standard deviation (STD), variance (VAR); average absolute deviation (AAD), and median absolute deviation (MAD)], and Grey [metrics of the pixel distribution: skewness (SKW) and kurtosis (KUR)]. Selected variables are indicated (+); see also Table 3. * Same outcome: NLT.2 = NLT.3.

The phenon line, represented by the horizontal red dashed line in Figure 3 (i.e., 0.3 Pearson's r correlation coefficient) defines the actual groups from which we select one variable of each—groups are formed when this cut-off line crosses a vertical line (i.e., branch or edge) [49,50]. In fact, the groups formed in this manner match the preliminary visual analysis of the dendrograms:

- Three groups are observed (Green + Blue, Yellow, and one Red) when 16 variables are analyzed, i.e., NLT.1, NLT.2, and NLT.3—NLT.4 is an exception;
- Four other groups are also formed (Green + Blue, Grey + Yellow, and two Red ones) when 19 variables are accounted for, i.e., NLT.0, NLT.5, NLT.6—NLT.7 is an exception;
- Three other groups are formed in NLT.4 (16 variables) in which VAR, RNG, and MAX cluster together forming an extra assemblage (Light Blue)—Light Blue + Green + Blue, Yellow, and one Red;
- Six groups are formed in NLT.7 (19 variables): Green, Grey, Blue, Yellow, and two Red ones.

One should pay close attention to the two Red groups, as from them, three variables are selected—e.g., NLT.0 (Fractal, PtoA, and Compact)—because such variables have no correlation.

The number of selected variables ranges between 4 and 7 variables, depending on the NLT (Table 3), such that:

- **AVG** is selected from the Green + Blue group to maintain the simplest possible analysis;
- VAR is selected when the Blue group is alone (only in NLT.7) to keep it simple as possible;
- **SKW** is preferable from the Grey group as it measures asymmetry;
- LEN is selected from the Yellow group as Area and Perimeter are both present in the ratios;
- The three morphological ratios (Red group: PtoA, Compact, and Fractal) are always selected when present.

Atribute Selection Processes (Phase 5) based on the analyses of dendrograms (UPGMA: Unweighted Pair Group Method with Arithmetic Mean) The color-coding relates to the outcomes of the rooted tree UPGMA dendrograms (see Figure 3) The @ denoted the selected variables. The - denotes the variables that are not accounted for (see Phase 4). 19 16 16 16 16 19 2) Area¹ 3) Per¹ 4) PtoA Perimeter to Area Ratio 5) **Compact** Compact Index = [4.Pi.Area[/[Per²] Fractal Index = [2.ln(Per/4)]/[ln(Area)] 7) **MAX** Maximum 9) **MED** Median 10) MOD Mode 11) MDM 12) RNG Coefficient of Dispersi (n=6)14) **VAR** 15) **STD** Standard Deviation 16) AAD4 Average Absolute Deviation 17) MAD⁵ Median Absolute Deviation 18) **SKW**⁶ (n=2) Pixel 19) KUR⁶

Table 3. Summary of the Attribute Selection Processes (Phase 5).

- Same outcome: NLT.2=NLT.3
- $^{1}\,$ Best oil slick discrimination variables (i.e. Area and Perimeter) reported in our previous studies [19-22].
- MDM = Mean of the values between the 2nd and 3rd interquartiles (i.e. trims off 25% of both ends).
- ³ COD = Subtract the 1st interquartile from the 3rd interquartile and divide by their sum.
- AAD = Mean of the absolute difference of each value minus the mean.
- MAD = Median of the absolute difference of each value minus the median
- ⁶ The two new introduced variables (i.e. SKW and KUR) in relation to [19-22].

3.6. Phase 6: Principal Component Analysis (PCA)

The scatterplots show a large overlap between seeps and spills, but their centroids are somehow distinctively independent of NLT. When all variables (16 or 19) are directly input to the PCA, the cumulative variance of the selected PCs (3 to 7) ranges between 80 to 90% for all NLTs. However, when the input is the UPGMA selected variables (4 to 7), the PC-selection (2 to 4 PCs) shows a much lower cumulative variance: from 52% to 70%; the exceptions are the Logarithm functions (NLT.2: Log₁₀; and NLT.3: Ln) with 99.5% (2 PCs). Table 4 reports the number of selected PCs and their cumulative variance per NLT.

Table 4. Outcome of the Principal Component Analysis (PCA: Phase 6) showing the number of selected Principal Components (PCs) and cumulative variance.

	All Variables ^{4,5}	All Variables ^{4,6}	Separate Analysis ^{4,7}	Separate Analysis ^{4,7}	Separate Analysis ^{4,7}
Principal Components Analysis (PCA: Phase 6) showing the selected Principal Components (PCs) based on the Kaiser Cut	UPGMA Variable Selection: No ³	UPGMA Variable Selection: Yes ³	Area and Perimeter ⁺	PtoA and Compact	Average and Skewness
	²(n) PCs %%	² (n) PCs %%	²(n) PCs %%	²(n) PCs %%	² (n) PCs %%
NLT.0) No Transformation [x]	19 5 80.49%	5 3 69.13%*	2 2 100% (92.21% =)	2 2 100% (52.33% =)	2 2 100% (67.98% ⁼)
NLT.1) Reciprocal [1/x]	16 8 82.42%	4 2 59.95%*			
NLT.2)1 Logarithm Base 10: [Log ₁₀ (x)]	16 3 90.08%	4 2 99.50%	2 2 100% (97.87% =)	2 2 100% (52.76%=))
NLT.3)1 Logarithm Napierian: [Ln(x)]	16 3 90.08%	4 2 99.50%			
NLT.4) Square Root [x1/2]	16 4 90.07%	4 2 68.35%*			
NLT.5) Square Power [x2]	19 6 80.00%	6 4 70.61%*			
NLT.6) Cube Root [x1/3]	19 4 85.05%	5 2 52.32%*	2 2 100% (97.44% =)	2 2 100% (50.47%=)) 2 2 100% (66.27% ⁼)
NLT.7) Third Power [x ³]	19 7 81.46%	7 4 59.93%*			
 Same outcome: NLT.3=NLT.4 Number of input variables. See Figure 3 (UPGMA Dendogra 	ame)				
⁴ See Figure 4.	1113).				
⁵ See Table 5.					
⁶ See Table 6.					
⁷ See Table 7.					
%% Cumulative variance of the sele					
* Low cumulative variance in the					
 Cumulative variance of the 1st Best oil slick discrimination vari 		earlier investigations	[19-22].		

3.7. Phase 7: Discriminant Function

As we are comparing the results of using the score values of the selected PCs versus the use of actual values of the Oil-Slick Information Descriptors, both directly input to the Discriminant Analysis, four different Discriminant Function sets are analyzed per NLT:

- Set.1: No UPGMA variable selection, i.e., all variables (16 or 19), without PCA;
- Set.2: No UPGMA variable selection, i.e., all variables (16 or 19), with PCA (3 to 7 PCs);
- **Set.3:** UPGMA selected variables (4 to 7) without PCA;
- **Set.4:** UPGMA selected variables (4 to 7) with PCA (2 to 4 PCs).

Figure 4 portrays the scheme defining these four input dataset versions for each NLT (8x). Another improvement from our earlier studies is that besides exploring the seep-spill discrimination capabilities of using the PC-scores and values of the variables, as well as the sole use of Area with Perimeter as before [19–22], we also test a separate analysis with a pair of Size Information Descriptors (PtoA with Compact) and with a pair of SAR Information Descriptors (AVG with SKW)—see Figure 4. These are chosen based on the interpretation of the UPGMA dendrograms (Phase 5: Section 3.5.1—see also Figure 3). Although the histograms of the Discriminant Functions' axes show that seep and spill properties overlap, independent of NLT, their centroids are separate.

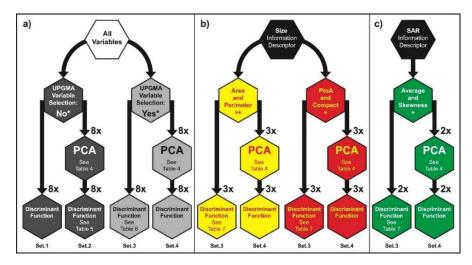


Figure 4. Discriminant Functions explored to discriminate oil seeps from oil spills: (a) All variables; (b) Separate analysis of Size Information Descriptors (Area with Perimeter and PtoA with Compact); and c) Separate analysis of SAR Information Descriptors (AVG with SKW). The four input dataset versions are shown: all variables (16 or 19—see Phase 5: Section 3.5.1; Figure 3 and Table 3) without (Set.1) and with (Set.2) PCA (Principal Component Analysis—see Phase 6), UPGMA (Unweighted Pair Group Method with Arithmetic Mean—see Phase 5: Section 2.5.1) attribute selection (i.e., 4 to 7 variables—see Phase 5: Section 3.5.1; Figure 3 and Table 3) without (Set.3) and with (Set.4) PCA. 8× refers to the several Non-Linear Transformations (NLT—see Phase 4: Section 2.4); 3x to the best NLT: NLT.0, NLT.2, and NLT.6; and 2× to NLT.0 and NLT.6. * See Figure 3. ** See [19–22].

3.8. Phase 8: Confusion Matrices (2-by-2 Tables)

Each NLT is evaluated with the four input dataset versions (Figure 4), and usually, Set.1 presents the highest discrimination power. However, these variables (16 or 19) are strongly correlated (Figure 3) and do not fulfill a Discriminant Functions requirement to use independent, or the least as correlated as possible, attributes [62]. The second best discrimination accuracy occurs with Set.2, which is closely followed by Set.3. The lowest observed accuracies are from Set.4, as the selected PCs have a very low cumulative variance in the selected PCs; the exceptions are the Logarithm functions (NLT.2: Log_{10} ; and NLT.3: Ln—see Table 4).

The global analysis of all 32 Data Transformation Approaches combinations (i.e., eight NLTs versus four input dataset versions) demonstrates the Logarithm functions (NLT.2: Log₁₀; and NLT.3: Ln) and Cube Root (NLT.6) as the most effective NLTs in supporting an accurate Oil-Slick Discrimination Algorithm. The Confusion Matrices evaluating the results of the Discriminant Functions for the several NLTs are shown on the color-coded Table 5 (Pink) and Table 6 (Red): Set.2 and Set.3, respectively. In the examination of these two tables that report the accuracy of the Oil-Slick Discrimination Algorithm, if taking the Log₁₀ (NLT.2), for example, one can find that:

- CM.1: Overall Accuracies ranging about 69%;
- CM.2: Producer's Accuracy, i.e., Sensitivities (65%) or Specificities (71%);
- CM.2: Commission Error, i.e., False Negative (35%) and False Positive (29%);
- CM.3: User's Accuracy, i.e., Positive (64%) and Negative (73%) Predictive Values;
- CM.3: Omission Error, i.e., Inverse of the Positive (36%) and Negative (27%) Predictive Values.

From Tables 5 and 6, one verifies the successful, and similar, results of the Cube Root (NLT.6) in comparison to the Logarithm functions (NLT.2 and NLT.3). Additionally, the cross-comparison of the results from Set.2 (Table 5) and Set.3 (Table 6) indicates that these two attribute selection strategies—i.e., 1) no UPGMA variable selection with PCA; and 2) UPGMA selected variables without PCA—promote comparable seep-spill discrimination accuracies.

A careful analysis of Table 5 (Set.2) discloses that the preferred lowest rate of False Negatives (20.4%) and Inverse of the Positive Predictive Values (23.3%) are observed in NLT.1 (Reciprocal); however, their counterparts, i.e., False Positives (48.0%) and Inverse of the Negative Predictive Values (43.7%), have undesirable high values among all NLTs. As its Overall Accuracy is reasonable (64.07%), this is an example that one needs to look into the conjunct interpretation of the five main metrics shown in Table 1 [19–22,63–65]. Similarly, the cautious analysis of Table 6 (Set.3) reveals that an ideal low rate of False Negatives (11.7%) and Inverse of the Positive Predictive Values (21.8%) are observed in NLT.5 (Square Power), but on the other hand, their counterparts, i.e., False Positives (67.5%) and Inverse of the Negative Predictive Values (49.6%), have unwanted high values. In this case, its Overall Accuracy is quite low (56.90%) though.

When considering the separate analysis of the Oil-Slick Information Descriptors (i.e., Size and SAR), Set.3 and Set.4 (see Figure 4: without PCA and with PCA, respectively) present the same result—these are shown in Table 7. The foremost outcome revealed in Table 7 is that the sole use of SAR Information Descriptors (AVG with SKW) is not as effective as using only Size Information Descriptors (Area with Perimeter and PtoA with Compact). Table 7 also discloses that these two pairs of Size Information Descriptors have the same results in the Logarithm function (NLT.2), and in fact, these results present superior discrimination power than in the other two analyzed NLTs, i.e., NLT.0 (No Transformation) and NLT.6 (Cube Root). Slightly better Overall Accuracies are achieved when using Area with Perimeter than PtoA with Compact; however, one should note that the False Negatives of the former pair are much higher than those of using the second pair: 67.7% against 21.0% (NLT.0), and 43.4% against 28.9% (NLT.6).

We can also evaluate the results of using several variables (Tables 5 and 6) against the use of individual pairs of attributes, i.e. the separate analysis of Size and SAR Information Descriptors (Table 7). If one compares the outcomes of NLT.2 (Log_{10}) in Tables 5–7, it is possible to notice that the sole use of the two Size Information Descriptor pairs (Table 7) has equivalent results as the ones from the other two attribute selection strategies, i.e., no UPGMA variable selection with PCA (Set.2: Table 5) versus UPGMA selected variables without PCA (Set.3: Table 6).

4. Conclusions

Our research addresses a gap in our scientific knowledge regarding the discrimination of the oil-slick category, i.e., sea surface expression of oil seeps versus oil spills observed in Campeche Bay (Figure 1). We report on analyses to refine the ability of using SAR-derived measurements for this task, thus addressing expanded Data Processing Segments (A, B, C, and D in Figure 2) as compared to our previous investigations [19–22]. A firmer basis to discriminate slicks by category has been established with the specific data-driven design of our Exploratory Data Analysis (EDA). An innovative strategy to select uncorrelated attributes based on the Bonferroni Adjustment (i.e., Pearson's r correlation coefficient of 0.3 [51]) has been successfully implemented using rooted tree dendrograms (Unweighted Pair Group Method with Arithmetic Mean: UPGMA—see Figure 3). We investigate several Non-Linear Transformations (NLTs—see Phase 4: Data Transformation Approaches) and various strategies to select uncorrelated attributes: we tested more than 32 combinations of Data Transformation Approaches, i.e., eight NLTs versus four input dataset versions (see Set.1, Set.2, Set.3, and Set.4 in Phase 7: Discriminant Function—Figure 4).

Table 5. Confusion Matrices (CMs) expressing the results of the Discrimination Functions (DFs) of the Oil-Slick Discrimination Algorithm from Set.2—i.e., all variables (16 or 19—see Phase 5: Section 3.5.1—Figure 3 and Table 3) without the dendrogram selection (no UPGMA: Unweighted Pair Group Method with Arithmetic Mean) but with the application of the PCA (Principal Component Analysis—see Phase 6: Section 3.6—Table 4). Note that NLT.2 and NLT.3 have the same outcome.

014.4	DE 011 C	DE 011 0-111	Total Book	011.4	55.011.0	DE 011 C-111	T-1-1-D1
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1,331	663	1,994	Oil Seep Real	1588	406	1994
Oil Spill Real	980	1,588	2,568	Oil Spill Real	1233	1335	2568
Total DF	2,311	2,251	4,562	Total DF	2821	1741	4562
NLT.0: N	lo Transformat	ion (x)	2,919	NLT.1	l: Reciprocal (1	./x)	2,923
CM 2	DE Oil Coop	DE Oil Caill	63.99%	CM 2	DE Oil Coop	DE Oil Cail	64.07%
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	79.6%	DF Oil Spill	Total Real
Oil Seep Real	66.8% 38.2%	33.2% 61.8%	100.0% 100.0%	Oil Seep Real Oil Spill Real	48.0%	20.4% 52.0%	100.0% 100.0%
Oil Spill Real CM.3	DF Oil Seep	DF Oil Spill	UPGMA:	CM.3	DF Oil Seep	DF Oil Spill	UPGMA:
Oil Seep Real	57.6%	29.5%	No	Oil Seep Real	56.3%	23.3%	No
Oil Spill Real	42.4%	70.5%	PCA:	Oil Spill Real	43.7%	76.7%	PCA:
Total DF	100.0%	100.0%	Yes	Total DF	100.0%	100.0%	Yes
Total Di	200.070	100.070	100	Total Di	100.070	100.070	103
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1299	695	1994	Oil Seep Real	1299	695	1994
Oil Spill Real	734	1834	2568	Oil Spill Real	734	1834	2568
Total DF	2033	2529	4562	Total DF	2033	2529	4562
NIT 2. Logs	rithm Base 10	(log (v))	3,133	NIT 2: Non	ierian Logarith	(I (×))	3,133
NET.2. Loga	ilitiliii base 10	(10g ₁₀ (x))	68.68%	NET.3. Nap	ieriali Logaritii	iii (Eii(X))	68.68%
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	65.1%	34.9%	100.0%	Oil Seep Real	65.1%	34.9%	100.0%
Oil Spill Real	28.6%	71.4%	100.0%	Oil Spill Real	28.6%	71.4%	100.0%
СМ.3	DF Oil Seep	DF Oil Spill	UPGMA:	СМ.3	DF Oil Seep	DF Oil Spill	UPGMA:
Oil Seep Real	63.9%	27.5%	No	Oil Seep Real	63.9%	27.5%	No
Oil Spill Real	36.1%	72.5%	PCA:	Oil Spill Real	36.1%	72.5%	PCA:
Total DF	100.0%	100.0%	Yes	Total DF	100.0%	100.0%	Yes
CM 1	DE Oil Seen	DE Oil Spill	Total Peal	CM 1	DE Oil Seen	DE Oil Spill	Total Boal
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1269	725	1994	Oil Seep Real	1100	894	1994
Oil Seep Real Oil Spill Real	1269 723	725 1845	1994 2568	Oil Seep Real Oil Spill Real	1100 1100	894 1468	1994 2568
Oil Seep Real Oil Spill Real Total DF	1269 723 1992	725 1845 2570	1994 2568 4562	Oil Seep Real Oil Spill Real Total DF	1100 1100 2200	894 1468 2362	1994 2568 4562
Oil Seep Real Oil Spill Real Total DF	1269 723	725 1845 2570	1994 2568	Oil Seep Real Oil Spill Real Total DF	1100 1100	894 1468 2362	1994 2568
Oil Seep Real Oil Spill Real Total DF	1269 723 1992	725 1845 2570	1994 2568 4562 3,114	Oil Seep Real Oil Spill Real Total DF	1100 1100 2200	894 1468 2362	1994 2568 4562 2,568
Oil Seep Real Oil Spill Real Total DF	1269 723 1992 : Square Root (725 1845 2570 x ^{1/2})	1994 2568 4562 3,114 68.26%	Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power	894 1468 2362 (x ²)	1994 2568 4562 2,568 56.29%
Oil Seep Real Oil Spill Real Total DF NLT.4:	1269 723 1992 : Square Root (725 1845 2570 x ^{1/2})	1994 2568 4562 3,114 68.26% Total Real	Oil Seep Real Oil Spill Real Total DF NLT.5:	1100 1100 2200 Square Power	894 1468 2362 (x ²) DF Oil Spill	1994 2568 4562 2,568 56.29% Total Real
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real	1269 723 1992 : Square Root (DF Oil Seep 63.6%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4%	1994 2568 4562 3,114 68.26% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real	1100 1100 2200 Square Power DF Oil Seep 55.2%	894 1468 2362 (x ²) DF Oil Spill 44.8%	1994 2568 4562 2,568 56.29% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real	1269 723 1992 : Square Root (DF Oil Seep 63.6% 28.2%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8%	1994 2568 4562 3,114 68.26% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2%	1994 2568 4562 2,568 56.29% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill	1994 2568 4562 3,114 68.26% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill	1994 2568 4562 2,568 56.29% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2%	1994 2568 4562 3,114 68.26% Total Real 100.0% 100.0% UPGMA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8%	1994 2568 4562 2,568 56.29% Total Real 100.0% 100.0% UPGMA: No
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Sepill Real Total DF	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0%	1994 2568 4562 3,114 68.26% Total Real 100.0% 100.0% UPGMA: No PCA: Yes	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 50.0%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0%	1994 2568 4562 2,568 56.29% Total Real 100.0% 100.0% UPGMA: No PCA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0%	1994 2568 4562 3,114 68.26% Total Real 100.0% 100.0% UPGMA: No PCA: Yes	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 5: Cube Root (x	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 5: Cube Root (x DF Oil Seep 63.7%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep 28.1%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill 71.9%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real Total DF	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 5: Cube Root (DF Oil Seep 63.7% 26.8%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604 x ^{1/3}) DF Oil Spill 36.3% 73.2%	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill 71.9% 82.4%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real	1269 723 1992 Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 5: Cube Root (DF Oil Seep 63.7%	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep 28.1% 17.6%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill 71.9%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real Total DF	1269 723 1992 E Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 E Cube Root (DF Oil Seep 63.7% 26.8% DF Oil Seep 63.7% 26.8% DF Oil Seep	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604 x ^{1/3}) DF Oil Spill 36.3% 73.2% DF Oil Spill	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real 100.0% UPGMA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep 28.1% 17.6% DF Oil Seep 55.4%	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill 71.9% 82.4% DF Oil Spill	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real 100.0% UPGMA:
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real Total DF	1269 723 1992 E Square Root (DF Oil Seep 63.6% 28.2% DF Oil Seep 63.7% 36.3% 100.0% DF Oil Seep 1270 688 1958 5: Cube Root (DF Oil Seep 63.7% 26.8% DF Oil Seep	725 1845 2570 x ^{1/2}) DF Oil Spill 36.4% 71.8% DF Oil Spill 28.2% 71.8% 100.0% DF Oil Spill 724 1880 2604 (1/3) DF Oil Spill 36.3% 73.2% DF Oil Spill 27.8%	1994 2568 4562 3,114 68.26% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 3,150 69.05% Total Real 100.0% UPGMA:	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF	1100 1100 2200 Square Power DF Oil Seep 55.2% 42.8% DF Oil Seep 50.0% 100.0% DF Oil Seep 560 451 1011 Third Power DF Oil Seep 28.1% 17.6% DF Oil Seep	894 1468 2362 (x²) DF Oil Spill 44.8% 57.2% DF Oil Spill 37.8% 62.2% 100.0% DF Oil Spill 1434 2117 3551 (x³) DF Oil Spill 71.9% 82.4% DF Oil Spill 40.4%	1994 2568 4562 2,568 56.29% Total Real 100.0% UPGMA: No PCA: Yes Total Real 1994 2568 4562 2,677 58.68% Total Real 100.0% UPGMA: No

Table 6. Confusion Matrices (CMs) expressing the results of the Discrimination Functions (DFs) of the Oil-Slick Discrimination Algorithm from Set.3—i.e., with the UPGMA (Unweighted Pair Group Method with Arithmetic Mean—see Phase 5: Section 2.5.1) attribute selection (i.e., 4 to 7 variables—see Phase 5: Section 3.5.1; Figure 3 and Table 3) and without the application of the PCA (Principal Component Analysis—see Phase 6). Note that NLT.2 and NLT.3 have the same outcome.

CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1,570	424	1,994	Oil Seep Real	1454	540	1994
Oil Spill Real	1,224	1,344	2,568	Oil Spill Real	987	1581	2568
Total DF	2,794	1,768	4,562	Total DF	2441	2121	4562
Total Di	2,734	1,700	2,914	lotal Bi	2441	2121	3,035
NLT.0: N	lo Transformat	ion (x)	63.88%	NLT.:	l: Reciprocal (1/x)	66.53%
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	78.7%	21.3%	100.0%	Oil Seep Real	72.9%	27.1%	100.0%
Oil Spill Real	47.7%	52.3%	100.0%	Oil Spill Real	38.4%	61.6%	100.0%
CM.3	DF Oil Seep	DF Oil Spill	UPGMA:	CM.3	DF Oil Seep	DF Oil Spill	UPGMA:
Oil Seep Real	56.2%	24.0%	Yes	Oil Seep Real	59.6%	25.5%	Yes
Oil Spill Real	43.8%	76.0%	PCA:	Oil Spill Real	40.4%	74.5%	PCA:
				Total DF			
Total DF	100.0%	100.0%	No	Total DF	100.0%	100.0%	No
CM.1	DE Oil Soon	DE Oil Cail	Total Real	CM.1	DE Oil Soon	DE Oil Caill	Total Real
	DF Oil Seep	DF Oil Spill			DF Oil Seep	DF Oil Spill	1994
Oil Seep Real	1296	698	1994	Oil Seep Real	1296	698	
Oil Spill Real	739	1829	2568	Oil Spill Real	739	1829	2568
Total DF	2035	2527	4562	Total DF	2035	2527	4562
NLT.2: Loga	rithm Base 10	(log ₁₀ (x))	3,125 68.50%	NLT.3: Nap	ierian Logarith	ım (Ln(x))	3,125 68.50 %
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	65.0%	35.0%	100.0%	Oil Seep Real	65.0%	35.0%	100.0%
Oil Spill Real	28.8%	71.2%	100.0%	Oil Spill Real	28.8%	71.2%	100.0%
CM.3	DF Oil Seep	DF Oil Spill	UPGMA:	CM.3	DF Oil Seep	DF Oil Spill	UPGMA:
					63.7%		
Oil Seep Real	63.7%	27.6%	Yes	Oil Seep Real		27.6%	Yes
Oil Spill Real	36.3%	72.4%	PCA:	Oil Spill Real	36.3%	72.4%	PCA:
Total DF	100.0%	100.0%	No	Total DF	100.0%	100.0%	No
CM.1	DF Oil Seen	DE Oil Snill	Total Real	CM.1	DE Oil Seen	DF Oil Snill	Total Real
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1426	568	1994	Oil Seep Real	1761	233	1994
Oil Seep Real Oil Spill Real	1426 947	568 1621	1994 2568	Oil Seep Real Oil Spill Real	1761 1733	233 835	1994 2568
Oil Seep Real	1426	568	1994 2568 4562	Oil Seep Real	1761	233	1994 2568 4562
Oil Seep Real Oil Spill Real Total DF	1426 947	568 1621 2189	1994 2568 4562 3,047	Oil Seep Real Oil Spill Real Total DF	1761 1733	233 835 1068	1994 2568 4562 2,596
Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (568 1621 2189 x ^{1/2})	1994 2568 4562	Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe	233 835 1068 r (x ²)	1994 2568 4562
Oil Seep Real Oil Spill Real Total DF NLT.4:	1426 947 2373	568 1621 2189	1994 2568 4562 3,047 66.79%	Oil Seep Real Oil Spill Real Total DF NLT.5:	1761 1733 3494	233 835 1068	1994 2568 4562 2,596 56.90%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real	1426 947 2373 Square Root (DF Oil Seep 71.5%	568 1621 2189 x ^{1/2}) DF Oil Spill	1994 2568 4562 3,047 66.79% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3%	233 835 1068 r (x²) DF Oil Spill 11.7%	1994 2568 4562 2,596 56.90% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real	1761 1733 3494 Square Powe	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5%	1994 2568 4562 2,596 56.90% Total Real
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill	1994 2568 4562 2,596 56.90% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0% UPGMA: Yes	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8%	1994 2568 4562 2,596 56.90% Total Real 100.0% 100.0% UPGMA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0% UPGMA: Yes PCA:	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2%	1994 2568 4562 2,596 56.90% Total Real 100.0% 100.0% UPGMA: Yes PCA:
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0% UPGMA: Yes	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8%	1994 2568 4562 2,596 56.90% Total Real 100.0% 100.0% UPGMA: Yes
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0% UPGMA: Yes PCA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2%	1994 2568 4562 2,596 56.90% Total Real 100.0% 100.0% UPGMA: Yes PCA: No
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1%	1994 2568 4562 3,047 66.79% Total Real 100.0% 100.0% UPGMA: Yes PCA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2% 100.0%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 587	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2% 100.0%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 587 1711	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2% 100.0%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264	568 1621 2189 x ^{1/2}) DF Oil Spill 28,5% 63.1% DF Oil Spill 25,9% 74.1% 100.0% DF Oil Spill 587 1711 2298	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 100.0% DF Oil Spill 1102 1773 2875	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857	568 1621 2189 x ^{1/2}) DF Oil Spill 28,5% 63.1% DF Oil Spill 25,9% 74.1% 100.0% DF Oil Spill 587 1711 2298	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0%	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 100.0% DF Oil Spill 1102 1773 2875	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264	568 1621 2189 x ^{1/2}) DF Oil Spill 28,5% 63.1% DF Oil Spill 25,9% 74.1% 100.0% DF Oil Spill 587 1711 2298	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 100.0% DF Oil Spill 1102 1773 2875	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 587 1711 2298	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 100.0% DF Oil Spill 1102 1773 2875 (x³)	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2	1426 947 2373 2 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264 5: Cube Root (x	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 587 1711 2298	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real	Oil Seep Real Oil Spill Real Total DF NLT.5 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687 Third Power	233 835 1068 r (x²) DF Oil Spill 11.7% 32.5% DF Oil Spill 21.8% 78.2% 100.0% DF Oil Spill 1102 1773 2875 (x³) DF Oil Spill	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real	1426 947 2373 2 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264 5: Cube Root (x DF Oil Seep 70.6%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 2298 1//3) DF Oil Spill 29.4%	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687 Third Power DF Oil Seep 44.7%	233 835 1068 r (x²) DF Oil Spill 21.8% 78.2% 100.0% DF Oil Spill 1102 1773 2875 (x³) DF Oil Spill 55.3%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 2 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264 5: Cube Root (x DF Oil Seep 70.6% 33.4%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 2298 1//3) DF Oil Spill 29.4% 66.6%	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687 Third Power DF Oil Seep 44.7% 31.0%	233 835 1068 r (x²) DF Oil Spill 21.8% 78.2% 100.0% DF Oil Spill 1102 1773 2875 (x³) DF Oil Spill 55.3% 69.0%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real Total DF	1426 947 2373 2 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264 5: Cube Root (x DF Oil Seep 70.6% 33.4% DF Oil Seep	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 587 1711 2298 1 ^{1/3}) DF Oil Spill 29.4% 66.6% DF Oil Spill	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.5 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687 Third Power DF Oil Seep 44.7% 31.0% DF Oil Seep	233 835 1068 r (x²) DF Oil Spill 21.8% 78.2% 100.0% DF Oil Spill 1102 1773 2875 (x³) DF Oil Spill 55.3% 69.0% DF Oil Spill	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.4: CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF NLT.6 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Oil Seep Real Oil Spill Real	1426 947 2373 2 Square Root (DF Oil Seep 71.5% 36.9% DF Oil Seep 60.1% 39.9% 100.0% DF Oil Seep 1407 857 2264 5: Cube Root (x DF Oil Seep 70.6% 33.4% DF Oil Seep 62.1%	568 1621 2189 x ^{1/2}) DF Oil Spill 28.5% 63.1% DF Oil Spill 25.9% 74.1% 100.0% DF Oil Spill 2298 1711 2298 14/3) DF Oil Spill 29.4% 66.6% DF Oil Spill 25.5%	1994 2568 4562 3,047 66.79% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 3,118 68.35% Total Real 100.0% 100.0% UPGMA:	Oil Seep Real Oil Spill Real Total DF NLT.5 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real Total DF CM.1 Oil Seep Real Oil Spill Real Total DF CM.2 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Total DF NLT.7 CM.2 Oil Seep Real Oil Spill Real Oil Seep Real Oil Seep Real Oil Seep Real Oil Seep Real	1761 1733 3494 Square Powe DF Oil Seep 88.3% 67.5% DF Oil Seep 50.4% 49.6% 100.0% DF Oil Seep 892 795 1687 Third Power DF Oil Seep 44.7% 31.0% DF Oil Seep 52.9%	233 835 1068 r (x²) DF Oil Spill 21.8% 78.2% 100.0% DF Oil Spill 1102 1773 2875 (x³) DF Oil Spill 55.3% 69.0% DF Oil Spill 38.3%	1994 2568 4562 2,596 56.90% Total Real 100.0% UPGMA: Yes PCA: No Total Real 1994 2568 4562 2,665 58.42% Total Real 100.0% UPGMA: Yes

Table 7. Confusion Matrices (CMs) expressing the results of the Discrimination Functions (DFs) of the separate analysis of the Oil-Slick Discrimination Algorithm (see Phase 3: Section 2.3.2): Size Information Descriptors: Area with Perimeter (shown in Orange) and PtoA with Compact (Shown in Blue); and SAR Information Descriptors: AVG with SKW (shown in Black). See also Figure 4.

CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	645	1349	1994	Oil Seep Real	1575	419	1994
Oil Spill Real	206	2362	2568	Oil Spill Real	1230	1338	2568
Total DF	851	3711	4562	Total DF	2805	1757	4562
NLT.0: N	lo Transformati	on (x)	3,007 65.91%	NLT.0: N	lo Transformat	ion (x)	2,913 63.85%
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	32.3%	67.7%	100.0%	Oil Seep Real	79.0%	21.0%	100.0%
Oil Spill Real	8.0%	92.0%	100.0%	Oil Spill Real	47.9%	52.1%	100.0%
CM.3	DF Oil Seep	DF Oil Spill	Area	СМ.3	DF Oil Seep	DF Oil Spill	AtoP
Oil Seep Real	75.8%	36.4%	and	Oil Seep Real	56.1%	23.8%	and
Oil Spill Real	24.2%	63.6%	Perimeter	Oil Spill Real	43.9%	76.2%	Compact
Total DF	100.0%	100.0%		Total DF	100.0%	100.0%	
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1288	706	1994	Oil Seep Real	1288	706	1994
Oil Spill Real	727	1841	2568	Oil Spill Real	727	1841	2568
Total DF	2015	2547	4562	Total DF	2015	2547	4562
NLT.2: Loga	rithm Base 10	(log ₁₀ (x))	3,129 68.59%	NLT.2: Loga	rithm Base 10	(log ₁₀ (x))	3,129 68.59%
CM.2	DF Oil Seep	DF Oil Spill	Total Real	CM.2	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	64.6%	35.4%	100.0%	Oil Seep Real	64.6%	35.4%	100.0%
Oil Spill Real	28.3%	71.7%	100.0%	Oil Spill Real	28.3%	71.7%	100.0%
CM.3	DF Oil Seep	DF Oil Spill		CM.3	DF Oil Seep	DF Oil Spill	
Oil Seep Real	63.9%	27.7%	Area	Oil Seep Real	63.9%	27.7%	AtoP
Oil Spill Real	36.1%	72.3%	and Perimeter	Oil Spill Real	36.1%	72.3%	and Compact
Total DF	100.0%	100.0%	r crimitates	Total DF	100.0%	100.0%	Compact
•							
CM.1	DF Oil Seep	DF Oil Spill	Total Real	CM.1	DF Oil Seep	DF Oil Spill	Total Real
Oil Seep Real	1128	866	1994	Oil Seep Real	1417	577	1994
Oil Seep Real Oil Spill Real	1128 566	866 2002	1994 2568	Oil Seep Real Oil Spill Real	1417 901	577 1667	1994 2568
Oil Seep Real	1128	866	1994 2568 4562	Oil Seep Real	1417	577	1994 2568 4562
Oil Seep Real Oil Spill Real Total DF	1128 566	866 2002 2868	1994 2568	Oil Seep Real Oil Spill Real Total DF	1417 901	577 1667 2244	1994 2568
Oil Seep Real Oil Spill Real Total DF NLT. CM.2	1128 566 1694	866 2002 2868	1994 2568 4562 3,130	Oil Seep Real Oil Spill Real Total DF NLT. CM.2	1417 901 2318	577 1667 2244	1994 2568 4562 3,084
Oil Seep Real Oil Spill Real Total DF	1128 566 1694 5: Cube Root (x	866 2002 2868	1994 2568 4562 3,130 68.61%	Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real	1417 901 2318 5: Cube Root (x	577 1667 2244	1994 2568 4562 3,084 67.60%
Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real	1128 566 1694 5: Cube Root (x DF Oil Seep 56.6% 22.0%	866 2002 2868 ^{1/3}) DF Oil Spill 43.4% 78.0%	1994 2568 4562 3,130 68.61% Total Real	Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real	1417 901 2318 5: Cube Root (x DF Oil Seep 71.1% 35.1%	577 1667 2244 1/3) DF Oil Spill 28.9% 64.9%	1994 2568 4562 3,084 67.60% Total Real
Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3	1128 566 1694 5: Cube Root (x DF Oil Seep 56.6% 22.0% DF Oil Seep	866 2002 2868 ^{1/3}) DF Oil Spill 43.4%	1994 2568 4562 3,130 68.61% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3	1417 901 2318 5: Cube Root (x DF Oil Seep 71.1% 35.1% DF Oil Seep	577 1667 2244 1 ^{1/3}) DF Oil Spill 28.9 %	1994 2568 4562 3,084 67.60% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1128 566 1694 5: Cube Root (x DF Oil Seep 56.6% 22.0% DF Oil Seep 66.6%	866 2002 2868 1/3) DF Oil Spill 43.4% 78.0% DF Oil Spill 30.2%	1994 2568 4562 3,130 68.61% Total Real 100.0%	Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1417 901 2318 5: Cube Root (x DF Oil Seep 71.1% 35.1% DF Oil Seep 61.1%	577 1667 2244 1/3) DF Oil Spill 28.9% 64.9% DF Oil Spill 25.7%	1994 2568 4562 3,084 67.60% Total Real 100.0%
Oil Seep Real Oil Spill Real Total DF NLT.0 CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1128 566 1694 5: Cube Root (x DF Oil Seep 56.6% 22.0% DF Oil Seep 66.6% 33.4%	866 2002 2868 1/3) DF Oil Spill 43.4% 78.0% DF Oil Spill 30.2% 69.8%	1994 2568 4562 3,130 68.61% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT.(CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real Oil Spill Real	1417 901 2318 5: Cube Root (x DF Oil Seep 71.1% 35.1% DF Oil Seep 61.1% 38.9%	577 1667 2244 1/3) DF Oil Spill 28.9% 64.9% DF Oil Spill 25.7% 74.3%	1994 2568 4562 3,084 67.60% Total Real 100.0% 100.0%
Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1128 566 1694 5: Cube Root (x DF Oil Seep 56.6% 22.0% DF Oil Seep 66.6%	866 2002 2868 1/3) DF Oil Spill 43.4% 78.0% DF Oil Spill 30.2%	1994 2568 4562 3,130 68.61% Total Real 100.0% 100.0%	Oil Seep Real Oil Spill Real Total DF NLT. CM.2 Oil Seep Real Oil Spill Real CM.3 Oil Seep Real	1417 901 2318 5: Cube Root (x DF Oil Seep 71.1% 35.1% DF Oil Seep 61.1%	577 1667 2244 1/3) DF Oil Spill 28.9% 64.9% DF Oil Spill 25.7%	1994 2568 4562 3,084 67.60% Total Real 100.0% AtoP
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Based on our comprehensive approach to find a simple way to discriminate seeps from spills, we are able to answer the three scientific questions:

- 1. The two Logarithm functions (NLT.2: Log₁₀; and NLT.3: Ln) and Cube Root (NLT.6) have the most accurate seep-spill discrimination among the eight Data Transformation Approaches tested.
- 2. Of the different strategies tested for selecting relevant attributes (i.e., four input dataset versions—see Phase 7: Section 3.7), two (Set.2 and Set.3) have comparable discrimination power with Overall Accuracies of almost 70%; however, the sole use of UPGMA dendrograms (i.e., Set.3) excels at selecting uncorrelated variables as it provides a simpler form avoiding the implementation of additional Multivariate Data Analysis Techniques (i.e., PCA). This is clearly observed in an inspection of Table 6 (Set.3) and in a comparison with Table 5 [Set.2: the use of all variables (see Phase 5: Section 3.5.1—Figure 3 and Table 3) without the dendrogram selection (i.e., no UPGMA) but with the application of the PCA (see Phase 6: Section 3.6—Table 4)].
- 3. The use of a collection of variables from two attribute selection strategies, i.e., Set.2 [no UPGMA with PCA (19 or 16 attributes but with 3 to 7 PCs—Table 5)] and Set.3 [UPGMA and no PCA (4 to 7 variables—Table 6)] is equally capable of discriminating seeps from spills. However, these are comparable to the sole use of the two Size Information Descriptor pairs (Area with Perimeter and PtoA with Compact) that outperform the SAR Information Descriptor pair (AVG with SKW)—see Table 7.

Our EDA also demonstrates that using simple and low-cost RADARSAT-2 beam modes (SCNA and SCNB), one can achieve useful seep-spill discrimination accuracies, thus supporting new products for the RADARSAT Constellation Mission (RCM): RADARSAT-2 Mode Selection for Maritime Surveillance (R2MS2).

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