



Article High Accuracy and Wide Range Recognition of Micro AR Markers with Dynamic Camera Parameter Control⁺

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Abstract: This paper presents a novel dynamic camera parameter control method for the position and posture estimation of highly miniaturized AR markers (micro AR markers) using a low-cost general camera. The proposed method captures images from the camera at each cycle and detects markers from these images. Subsequently, it performs iterative calculations of the marker's position and posture to converge them to a specified accuracy while dynamically updating the camera's zoom, focus, and other parameter values based on the detected marker's depth distances. For a 10 mm square micro AR marker, the proposed system demonstrated recognition accuracy better than $\pm 1.0\%$ for depth distance and 2.5° for posture angle, with a maximum recognition range of 1.0 m. In addition, the iterative calculation time was 0.7 s for the initial detection of the marker. These experimental results indicate that the proposed method and system can be applied to the precise robotic handling of small objects at a low cost.

Keywords: image recognition; micro AR marker; camera parameter control; iterative recognition



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1. Introduction

In recent years, robots have been used to automate many tasks to improve productivity in manufacturing and other production sites. Real-time object position and posture estimation using image processing is an essential function for autonomous robots that perform object handling in automation. There are various methods for estimating object position and posture using image processing.

Methods using stereo cameras or RGB-D cameras (RGB-D cameras are sensors capable of capturing both color images and the depth distance to objects) can estimate the position, posture, and shape of an object from multiple RGB images or depth images, enabling the handling of general objects without the need to process the handling target. There have been many attempts to estimate the position and posture of objects using machine learning [1–5]. However, in general, the above methods have disadvantages, such as high implementation costs due to the large number of datasets required and the time required for data learning. Therefore, they are not suitable for applications that require low-cost and low-computational resources.

Visual markers are support tools that facilitate object identification and position and posture estimation. Because visual markers use known shape information and image features, they can be used to identify marker IDs and estimate relative positions and postures from a single 2D camera. Although there is the restriction that the marker must be fixed to the target object, this is inexpensive to implement. In addition, various marker projection patterns have been presented for various applications [6–10].

Among visual markers, AR markers have the advantage of easily enabling augmented reality and providing information to users in a more intuitive manner. Most AR markers use the principle of projective transformation to estimate the position and posture of the marker by finding a homogeneous transformation matrix that represents the position and posture of the marker's coordinate system as seen from the camera coordinate system. The open source library ARToolKit markers [11] is a typical example, and this marker technology is used in self-position estimation [12–17] and mapping [18–20] for mobile robots, and is an essential technology in navigation systems.

AR markers can also be used to handle specific objects [21–23]. However, the size and recognition accuracy of AR markers are problematic when handling small objects or objects with complex shapes. Conventional AR markers require a large amount of space to be attached to the target object, and it is undesirable from an aesthetic point of view for the markers to be too conspicuous in a real environment. Several previous studies have attempted to reduce the size of markers or improve their aesthetics. Zhang et al. [24] developed a curved surface marker that can be attached to cylindrical objects as small as 6 mm in diameter, enabling real-time tracking of ultrasound probes. However, these markers can only be recognized at a depth of 30–125 mm from the camera, making them unsuitable for object handling that requires a large workspace. Costanza et al. [25] created a marker that is unobtrusive to users in their living environment with "d-touch", an open source system that allows users to create their own markers based on their aesthetic sense. However, there is no concrete verification of miniaturization or recognition accuracy.

It is also difficult to consistently achieve the recognition accuracy required for accurate object handling. To solve this problem, Douxchamps et al. [26] improved accuracy and robustness by physically increasing the marker size and using high-density patterns to reduce noise and discretization in marker recognition. This method can recognize markers at a maximum of 0.06–4 ppm; however, the miniaturization of the marker becomes a trade-off issue. Yoon et al. [27] presented a coordinate transformation algorithm to obtain the globally optimal camera posture from local transformations of multiple markers, thus improving the accuracy of pose estimation. Yu et al. [28] presented a robust pose estimation algorithm using multiple AR markers and demonstrated its effectiveness in real-time AR tracking. Hayakawa et al. [29] presented a 3D toothbrush positioning method that recognizes AR markers on each face of a dodecahedron attached to a toothbrush and achieved a motion tracking rate of over 99.5%. However, these methods require multiple markers to achieve high recognition accuracy, which requires a large space to attach them to objects.

There are two methods to improve recognition performance with a single marker while maintaining the marker size: using filters and using circular dots as feature points. The method using a filter [30,31] reduces jitter between frames and stabilizes posture recognition, but does not guarantee accurate recognition. In contrast, Bergamasco et al. [32,33] achieved robustness against occlusion using markers that use the projection characteristics of a circular set of dots and an ellipticity algorithm. In addition to circular dots, Tanaka et al. [34–37] presented an AR marker that uses lenticular lenses or microlens arrays to change the pattern depending on the viewing angle, thereby reducing the posture estimation error and improving robustness against distance and illumination changes. These techniques have dramatically improved the recognition performance of a single marker, thereby enhancing its practicality. Therefore, these techniques are also promising for marker miniaturization but have not yet been demonstrated.

However, even if marker miniaturization and high recognition accuracy can be achieved, a commonly used camera system limits the range of marker recognition, making practical operation difficult. Because the markers are small, they cannot be recognized with high accuracy from an overhead view of the workspace. Conversely, a magnified view narrows the field of view, making it difficult to recognize the surrounding environment necessary for handling. To solve this problem, Toyoura et al. [38] presented a monospectrum marker that enables real-time detection of blurred images, thereby extending the recognition range. However, the recognition of translational positions has an average error of 5 to 10 mm, which does not meet the level of recognition accuracy required for object handling. Another disadvantage is that the system requires a high-performance GPU for real-time detection.

Based on the background described above, this study will develop a prototype micro AR marker of 10 mm per side [39] that is compatible with the high-accuracy recognition method of Tanaka et al. [37], and construct a low-cost and high-accuracy marker recognition system using a general-purpose web camera. The micro AR marker is printed on a glass substrate by photolithography with a high resolution so that the marker image is not easily degraded even when the marker is magnified by a camera. First, we demonstrate that this AR marker inherently has very high accuracy in position and posture recognition despite its ultra-compact size. But, we also reveal the problem of insufficient recognition range for practical use with a conventional camera system. Next, to solve this problem, we present a dynamic camera parameter control method that can maintain high recognition accuracy over a wide field of view and demonstrate its effectiveness through a series of experiments.

This paper is organized as follows. Section 1 describes the background and objectives of this study. Section 2 describes the overall system configuration. Section 3 describes the process of the proposed camera control system, i.e., the algorithm for camera parameter optimization. Section 4 describes the results of the evaluation experiments of the proposed camera control system. Section 5 discusses the results of the evaluation experiments. Finally, Section 6 describes the summary of this paper and future issues.

2. System Configuration

2.1. Hardware Configuration

The hardware of the camera control system proposed in this paper consists of three pieces of hardware: an AR marker, a single RGB camera, and a PC as a processing unit. The AR marker used is a micro AR marker of 10 mm per side, which is compatible with the Tanaka et al. [37] high-precision recognition method shown in Figure 1. As shown in Figure 1, this marker is equivalent in size to a USB Type-A. The marker was printed on a glass substrate by photolithography with high resolution so that the marker image was not easily degraded even when viewed under a camera's magnification. The camera captures reference points at the four corners of this marker, and by processing the images arithmetically, as shown in Figure 2, it is possible to estimate the relative position and posture of the marker as seen from the camera with high accuracy. A USB 3.0 webcam was used as the single RGB camera. Table 1 shows the camera performance. The proposed dynamic camera control system requires zoom and focus adjustment functions and a wide diagonal viewing angle. Therefore, a BRIO C1000eR[®] (Logitech International S.A., Lausanne, Switzerland, Figure 3) with digital zoom and focus adjustment functions and a maximum diagonal viewing angle of 90 degrees was used. However, when the camera's diagonal viewing angle was set to 90 degrees, the output image from this camera was highly distorted, which required removal. To prepare the camera calibration data that would serve as a reference for removing the distortion, calibration was performed using OpenCV's camera calibration function [40], with the camera's autofocus function turned on. In addition, for the camera control system described in Section 3.1, calibration was performed with the camera's autofocus function turned off to prepare a set of calibration data for each focus value. A Think-Pad X1 Carbon (i7-6600U 2.6GHz, 16 GB memory, Lenovo, Hong Kong, China) was used as the processing PC.



Figure 1. The 10 mm square micro AR marker prototyped in this study.



Figure 2. Definition of marker position and posture with respect to camera.

Table 1. The camera specifications.

Product name	BRIO C1000eR [®]
Output resolution	1920 × 1080 (FHD)
Frame rate	30 fps
Diagonal FOV	90°
Digital zoom	$1 \times -5 \times$
Size (mm)	$102 \times 27 \times 27$



Figure 3. BRIO C1000eR[®].

2.2. Software Configuration

Figure 4 shows the software configuration of the camera control system proposed in this paper. ROS Melodic was used as the middleware for the development of this study. The software used for AR marker recognition was LEAG-Library from LEAG Solutions Corp. This library is compatible with the high-accuracy recognition method of Tanaka et al. [37]. It also uses OpenCV as an image processing library and uvc-camera as a library for acquiring images from USB cameras. The Relay node relays the AR marker values received from the LEAG Library. It identifies marker IDs and performs type conversion. The Iteration node determines camera parameters such as zoom, focus, and calibration data based on the AR marker values received from the Relay node and provides input to the camera and feedback to the LEAG-Library. It also determines the convergence of the AR marker position and posture and the final AR marker value. Topic communication was used to send and receive AR marker information between nodes. Figure 5 shows the correlation diagram of

topic communication between nodes obtained from the ROS function rqt_graph. The mid node acts as the Relay node shown in Figure 4, passing AR marker values to the iteration node using a topic named tf_mid. Each node is written in C/C++ language for high-speed processing. The cycle of topics delivered from the LEAG Library is approximately 30 Hz, which is the same as the frame rate of the camera.



Figure 5. Correlation diagram of the ROS nodes.

3. Camera Control System

This section describes the dynamic camera control processes that properly adjust the parameters of zoom, focus, and calibration data to determine the position and posture of the AR markers. The three parameters of the zoom, focus, and calibration data are collectively referred to as "camera parameters".

3.1. Marker Recognition Process

As shown in Figure 6, the proposed camera control system consists of two processes: the Scanning process scans the camera's shooting range to detect AR markers; the Iteration process optimizes camera parameters based on the detected AR marker positions to determine the final AR marker position and posture. Here, it is assumed that the AR marker is still present within the camera's shooting range when the camera parameters are changed.

Table 2 shows the camera parameters used in this system and the parameters used to calculate the camera parameters. As will be discussed later in Section 4.4, when recognizing micro AR markers, if the camera zoom function is not used, the size of the AR marker in the image will be very small and the recognition range of the AR marker will be narrow. In addition, when the zoom magnification is large, the recognition accuracy of the position of AR markers in close proximity to the camera is poor. Therefore, it is necessary to dynamically control the zoom value to achieve a wide recognition range. The zoom value *W* is proportional to the depth distance *z* from the camera of the AR marker shown in



Figure 2 and is calculated by Equation (1). The camera magnification n is also proportional to W, as shown in Equation (2).

Figure 6. Flowchart of the proposed method.

$$W = C(z - z_{min}) + W_{min} \tag{1}$$

$$u = \frac{W}{100} \tag{2}$$

As in the data presented in Section 4.3, a fixed-focus camera has a narrow range for recognizing AR markers of only 0.2 m in the depth distance. Thus, we attempted to recognize AR markers using autofocus cameras. However, with this approach, the autofocus tended

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to focus on the background, which often had higher contrast than the markers themselves. As a result, we could not consistently achieve an accurate focus on the small 10 mm markers. Therefore, it was necessary to explicitly control the focus to achieve a wide recognition range. The focus value *F* is also determined by the marker's depth distance *z* using Equation (3). The smaller the focus value, the farther away the camera. The constants α and β used in Equation (3) are constants obtained by measuring the optimum focus value according to the depth distance from the camera in advance and by exponential approximation of the experimental results.

$$F = -\alpha \ln z + \beta \tag{3}$$

Parameter	Symbol	Value
Zoom value	W	Variable (100 \sim 500)
Maximum zoom value	W _{max}	500
Minimum zoom value	W _{min}	100
Depth distance of the AR marker	Z	Variable (m)
Minimum depth distance	z_{min}	0.05 (m)
Conversion coefficient of the zoom value	С	1000 (1/m)
Camera magnification	п	Variable
Focus value	F	Variable (0 \sim 150)
Constants of the focus value	α	42.11
Constants of the focus value	β	4.0
Distortion coefficient matrix	$D_{1 \times 5}$	Determined by calibration
Radial distortion coefficient	k_1, k_2, k_3	
Tangential distortion coefficient	l_1, l_2	
Internal parameter matrix	$I_{3 \times 3}$	Determined by calibration
Focus distance	f_x, f_y	
Optical center	C_x, C_y	
AR marker position	$\boldsymbol{p} = \begin{bmatrix} \boldsymbol{x} & \boldsymbol{y} & \boldsymbol{z} \end{bmatrix}^T$	Iterative output variable
AR marker posture	$\boldsymbol{q} = \begin{bmatrix} \theta & \phi & \psi \end{bmatrix}^T$	Iterative output variable
Threshold of position error	t_p	Arbitrally setting
Threshold of posture error	$\dot{t_q}$	Arbitrally setting

Table 2. Parameters used in the proposed camera control system.

The calibration data also include the distortion coefficient matrix D and the internal parameter matrix I of the camera. The distortion coefficient matrix D refers to the lens distortion and is represented by a 1 × 5 matrix containing the radial distortion coefficients (k_1, k_2, k_3) and tangential distortion coefficients (l_1, l_2) as in Equation (4). The internal parameter matrix I refers to camera-specific parameters and is represented as shown in Equation (5) in a 3 × 3 matrix containing the focus distance (f_x, f_y) and optical center (c_x, c_y) . In this study, 31 calibration data sets for every increment of 5 in the focus value were prepared. The system selects the most appropriate calibration data based on the calculated focus value and applies them to the next recognition process.

$$\boldsymbol{D} = \begin{bmatrix} k_1 & k_2 & l_1 & l_2 & k_3 \end{bmatrix} \tag{4}$$

$$I = \begin{bmatrix} f_x & 0 & c_x \\ 0 & f_y & c_y \\ 0 & 0 & 1 \end{bmatrix}$$
(5)

The two processes shown in Figure 6 are described in detail below.

In the Scanning process, AR markers are initially detected by scanning within the camera's shooting range; the Scanning process follows the steps below.

- The camera parameters are set to the initial values W = 500 and F = 150, with the (1a) zoom at its maximum and the focus at its farthest forward. The reason for these settings is that the zoom value is farther away for a wider recognition range, and the focus value can be processed faster if it is shifted from near to far.
- (1b) Detect AR markers within a single frame of the image output from the camera.
- (1c) If no AR marker is found in the image, the focus value F is reduced by 15 to focus on a more distant point.
- (1d) Repeat steps (1b)–(1c) until AR markers are detected.
- (1e) If an AR marker is detected for the first time, obtain the initial position p_0 and posture q_0 of the AR marker to be given as initial values for the next Iteration process.

According to the above algorithm, the scanning takes a maximum of 11 frames of images before the AR marker is detected. Since the frame rate of the camera used is 30 fps, the maximum scanning time is theoretically about 0.33 s. In reality, however, even if the AR marker was at the farthest point within the recognition range, the scanning time was only about 0.3 s. This is because the AR marker could be detected even when the focus position was in front of the AR marker, and detection was possible from the tenth frame of the image.

In the *Iteration process*, the camera parameters are optimized to determine the final marker position p_d and posture q_d with enhanced accuracy; the *Iteration process* follows the steps below.

- Receive the initial recognition values p_0 and q_0 of the AR marker from the *Scanning* (2a) process.
- (2b) Update the camera parameters based on the recognized depth distance z of the AR marker.
- (2c) Get the next recognition values p_k and q_k with the updated camera parameters.
- (2d) Calculate the absolute error value between p_{k-1} and p_k , and between q_{k-1} and q_k . If the error values are larger than the thresholds t_p and t_q , repeat steps (2b)–(2c).
- (2e) If the absolute error values calculated in step (2d) are smaller than the thresholds t_p and t_q , the latest p_k and q_k are output as the final recognition values p_d and q_d .

Software algorithms of the aforementioned two processes are described in Algorithms 1 and 2.

Algorithm 1 Scannig Process

Input: RGB image
Output: p_0 , q_0
Initialization:
1: $W \leftarrow 500, F \leftarrow 150, D, I \leftarrow Autofocus values$
2: Get RGB image
Loop Process:
3: while AR marker is not detected in RGB image do
4: $F \leftarrow F - 15$
5: Get RGB image
6: if AR marker is initially detected then
7: p_0 , $q_0 \leftarrow$ Position, Posture of detected marker
8: $W \leftarrow C(z - z_{min}) + W_{min}$
9: $F \leftarrow -\alpha \ln z + \beta$
10: $D, I \leftarrow$ select ones from dataset of pre-defined data according to the focus value
11: Break
12: end if
13: Get RGB image
14: end while
15: Go to Iteration Process

Algorithm 2 Iteration Process

Input: RGB image **Output:** p_d , q_d Loop Process: 1: while $|p_k - p_{k-1}| >= t_p \& |q_k - q_{k-1}| >= t_q \text{ do}$ 2: $p_{k-1}, q_{k-1} \leftarrow p_k, q_k$ $W \leftarrow C(z - z_{min}) + W_{min}$ 3: 4: $F \leftarrow -\alpha \ln z + \beta$ $D, I \leftarrow$ select ones from dataset of pre-defined data according to the focus value F 5: 6: Get RGB image 7: if AR marker is detected then p_k , $q_k \leftarrow$ Position, Posture of detected marker 8: 9: if $|p_k - p_{k-1}| < t_p \& |q_k - q_{k-1}| < t_q$ then 10: $p_d, q_d \leftarrow p_k, q_k$ Break 11: end if 12: 13: end if 14: end while

3.2. Dynamic Camera Parameter Controller

Figure 7 shows a block diagram of the system for updating the camera parameter optimization shown in the *Iteration process* in Figure 6. The values p_d and q_d are the final output of the marker's position and posture. The Iterator judges whether the recognized position and posture converge to an accuracy within set thresholds, as in Equations (6) and (7).

$$|\boldsymbol{p}_k - \boldsymbol{p}_{k-1}| < t_p \tag{6}$$

$$|\boldsymbol{q}_k - \boldsymbol{q}_{k-1}| < t_p \tag{7}$$

The Iterator also calculates the marker's depth distance z for updating the camera parameters, which considers the magnification of the image due to zooming. When the image is magnified by a factor of n by zooming, the "apparent" depth distance z' becomes 1/n of the real value z. Therefore, the zoom value W is input to the LEAG Library to recognize the real marker position with compensation of the apparent depth distance z', as shown in Equation (8).

$$z = z' \times n = z' \times \frac{W}{100} \tag{8}$$

After the depth distance z is calculated, the zoom value W and focus value F are updated by Equations (1) and (3), respectively. In addition, the lens distortion coefficients D and the internal parameter matrix I are appropriately selected from the calibration data list based on the focus value F.



Figure 7. Block diagram of the camera parameter optimization.

4. Experimental Evaluation

4.1. Experimental Setup

Figure 8 shows the experimental setup. Figure 8a shows the definition of the coordinates of the AR marker: the depth distance *z* and the rotation angle ϕ , which are treated in the experiments in Sections 4.3–4.5. Figure 8b shows a scene of the actual experimental setup. The actual distances and angles were measured using a measuring tape and a protractor with the AR marker fixed to a rotating stand. To maintain consistent experimental conditions for each trial, we established an environment with a solid-colored wall as the marker background and placed the lighting in the same position. Furthermore, for camera parameters not dynamically controlled using our method, such as focus and zoom, we employed fixed parameters.



Figure 8. Experimental setup: (**a**) definition of the AR marker position and angles. (**b**) scene of the experiment.

4.2. Experimental Conditions

In all experiments, measurements were taken five times for each condition, and the average value was recorded for each condition. Note that the values were recorded only when the marker's ID was correctly recognized five times in a row.

The accuracy of the marker's translational position recognition is evaluated at the error rate relative to the true value. When the measured value is M and the true value is T, the error rate is defined by Equation (9). On the other hand, the accuracy of posture recognition is evaluated by the error between M and T.

$$Error \ rate = \frac{M-T}{T} \times 100 \ (\%) \tag{9}$$

4.3. Recognition Performance Using Fixed Camera Parameters

Prior to the evaluation of the proposed method, the recognition range and recognition accuracy were examined with camera parameters fixed at specific values. The zoom value W and focus value F were set to three patterns: (1) W = 100, F = 100; (2) W = 500, F = 50; (3) W = 500, F = 0. The distortion coefficient matrix D and internal parameter matrix I were calibrated with the camera's autofocus function turned on. The micro AR marker was placed at a rotation angle $\phi = 40^{\circ}$ to the camera for the most stable recognition.

Figure 9 shows the recognition range and error rate for the marker's depth distance z for each of the fixed parameter conditions. Under the conditions of this experiment, the recognition range was very narrow, with a maximum of only 0.2 m in the depth direction. Recognition accuracy also tends to significantly deteriorate, especially at short distances, which cannot be acceptable for precise navigation and object handling. This is largely

because a fixed focus value is used, which results in various out-of-focus areas. Therefore, it is necessary to expand the recognition range to properly control the camera focus and calibration data according to the marker's depth distance.



Figure 9. Recognition error rate of marker depth distance (*z*) with fixed camera parameters.

4.4. Recognition Performance Using Dynamic Focus Control

Next, we investigated the performance improvement in position recognition using the dynamic focus control given by Equation (3). In this experiment, the zoom values *W* were set to five constant values: 100, 200, 300, 400, and 500. The focus value *F* was sequentially computed according to the recognized values of depth distance *z*. The camera calibration data *D* and *I* are determined on the basis of the calculated focus values. During the experiment, the micro AR marker was placed at a rotation angle $\phi = 40^{\circ}$ to the camera for the most stable recognition.

Figure 10 shows the recognition range and error rate of the marker's depth distance z obtained in this experiment. The recognizable range of markers varies depending on the zoom value W. Naturally, the larger the zoom value, the farther away the marker can be recognized. At the maximum zoom value (W = 500), the AR markers can be recognized from the minimum distance $z_{min} = 0.05$ m to the maximum distance z = 1.05 m in the depth direction. Compared to Figure 9, the recognition range is expanded by adjusting the camera focus. However, when the zoom value W is large, the recognition error rate worsens at close distances. This is thought to be because the marker area in the image is considerably larger because of zooming at close distances, making it more susceptible to lens distortion. On the other hand, the recognition accuracy at close distances is good with small values of W. According to the experimental results, proper control of the zoom value W and the focus value F is necessary to ensure high recognition accuracy over the entire range.



Figure 10. Recognition error rate of marker depth distance (*z*) using dynamic focus control with constant zoom values (*W*).

4.5. Recognition Performance Using Dynamic Control of Both Focus and Zoom (Proposed Method)

After understanding the results of the two experiments described above, we investigated and evaluated the recognition performance of the micro AR marker using dynamic control of both focus and zoom values, i.e., applying the proposed camera control method.

Table 3 shows the initial values of the camera parameters and the threshold values t_p and t_q used to determine the convergence of the iterative calculations. The initial zoom value was set to the maximum value (W = 500), which has the widest recognition range, as shown in Figure 10. The initial focus value was set at the closest distance from the camera (F = 150) so that the scanning process was performed from near to far points from the camera. The threshold values t_p and t_q for convergence judgment were set as absolute errors. In addition, the initial values of the camera calibration data D and I were measured with the autofocus function turned on, as described in Section 2.1.

Table 3. Initial camera parameter values and error thresholds.

Parameter	Symbol	Value
Zoom value	W	500
Focus value	F	150
Threshold of the position error	t_{p}	1.0 (mm)
Threshold of the posture error	t_q'	0.01 (deg)

4.5.1. Performance of Translational Position Recognition

First, the precision and accuracy of the marker's translational position recognition are examined. The evaluation experiment was conducted by measuring the marker's depth distance *z* under three conditions of the marker's rotation angle: $\phi = 0^{\circ}, 30^{\circ}, 60^{\circ}$. To focus on the performance of the position measurement in this experiment, the convergence judgment of the marker's posture *q* was not performed; only the convergence judgment of the marker's position *p* was performed.

Figure 11 shows the recognition error rate of the marker's depth distance *z*. The error rate is within ±1% for the entire range in which AR markers can be recognized. Compared with the recognition accuracy with focus value control (see Figure 10), the proposed method achieved significant performance improvement. Furthermore, the variation in recognition error rates is not biased toward either positive or negative values, indicating that the accuracy of position estimation is high when using this method. The range of recognition distance becomes smaller at $\phi = 60^\circ$, but the recognition accuracy has not deteriorated as long as the marker position can be recognized.



Figure 11. Recognition error rate of depth distance (*z*) with proposed camera control for different marker angles (ϕ).

The behavior of iterative calculations during marker position recognition was also investigated. Figure 12 shows the iteration time required for the convergence of position recognition in this experiment. According to the results, the iteration time is within 0.7 s, indicating that the AR marker at an unknown location can be recognized quickly with high accuracy. In addition, as the depth distance *z* increases, the iteration time tends to increase. Because the threshold value for the position convergence t_p is set to a constant value of 1.0 mm, independent of the depth distance, the convergence accuracy becomes relatively high at large distances.

In relation to the iteration time, Figure 13 shows the convergence of the recognized values of depth distance z by iterative calculations for five experimental trials. In this experiment, the true values of the marker's depth distance were set to (a) z = 1.0 m, (b) z = 0.5 m, and (c) z = 0.1 m with a rotation angle of $\phi = 40^{\circ}$. According to the results, although the number of convergence calculations tends to increase at large depth distances, recognition with the specified absolute accuracy (1.0 mm) is achieved over the entire range of recognizable depth distances. Note that the first detected values of z were larger than the true value in all cases. This is because the focus position is not perfectly adjusted to the marker immediately after scanning, and the AR marker is recognized as smaller than its actual size in the blurred image.



Figure 12. Iteration time of the depth distance (*z*) to converge with the proposed camera control for different marker angles (ϕ).



Figure 13. Cont.



Figure 13. Convergence of the depth distance (*z*) measurement values to true values by iteration: (**a**) z = 1.0 m; (**b**) z = 0.5 m; (**c**) z = 0.1 m.

4.5.2. Performance of Posture Recognition

Next, the precision and accuracy of the marker's posture recognition are examined. The evaluation experiment was conducted by measuring the marker's rotation angle ϕ under three depth distance conditions: z = 0.05, 0.55, 1.05 m. To focus on the performance of the posture measurement in this experiment, the convergence judgment of the marker's position p was not performed; only the convergence judgment of the marker's posture q was performed.

As an experimental result, Figure 14 shows the recognition error of the marker's rotation angle ϕ at each condition. When the marker angle is in the range of 20° to 65°, accurate recognition within an error of $\pm 1^{\circ}$ is achieved. On the other hand, in the range where the marker angle is smaller than 20°, the recognition error is as large as 2.5° at maximum. This is due to the characteristic of AR markers that deteriorates recognition accuracy at angles near the frontal direction of the camera.

In addition, Figure 15 shows the iteration time required for the convergence of posture recognition in this experiment. According to the result, the iteration time is within 0.6 s, resulting in fast convergence of the recognized value of ϕ within the specified iteration accuracy ($t_q = 0.05^\circ$) over the entire recognizable angular range. It can also be seen that the larger the depth distance *z*, the longer it takes to converge the recognized value of the marker angle ϕ .



Figure 14. Recognition error of marker angle (ϕ) with the proposed camera control for different depth distances (*z*).



Figure 15. Iteration time of marker angle (ϕ) with the proposed camera control for different depth distances (*z*).

5. Discussion

Using the proposed dynamic camera control system, a 10 mm square micro AR marker can be recognized with an accuracy better than $\pm 1.0\%$ for depth distance and 2.5° for rotation angle. The depth recognition range is 1.0 m, which is five times greater than the range with fixed camera parameters. In the most recent relevant study, Inoue et al. [41] proposed an AR marker pose estimation system using a 64 mm × 64 mm AR marker, in which the recognition accuracy was 4% in the depth direction and 3.9° in the rotation angle. The depth recognition range was $0.1 \sim 0.7$ m. Compared with the state-of-the-art research described above, the proposed method in this study achieves significantly better performance in terms of marker size, recognition accuracy, and recognition range.

Regarding the iteration time, the proposed system requires a maximum of 0.6–0.7 s for convergence of recognition values for both position and posture. For application to object tracking in a robotic manipulation system, the iteration time can be significantly reduced, except for the initial detection. This is because the previous marker recognition value and the kinematic information of the robot arm can be used to efficiently determine the initial values of the camera parameters at the next recognition.

However, the recognition performance of the proposed system depends on the hardware specifications. A camera with higher zoom magnification capabilities, including an optical zoom, can further expand the recognition range. Iteration time also depends on the computational resources. Considering the low-cost implementation, this study uses a normal laptop PC without a GPU. However, the real-time performance of the system can be further improved using an industrial camera with a high frame rate and a GPU-accelerated processor.

6. Conclusions

In this paper, a dynamic camera parameter control method was proposed for the accurate and precise recognition of micro AR markers. In this system, the detected position and posture of the marker are converged to a specified accuracy through iterative calculations by updating the camera parameters. Evaluation experiments have shown the significant superiority of the proposed system in recognition performance over existing methods.

In future work, we aim to utilize the proposed recognition method for position estimation of small or transparent objects using micro AR markers. Subsequently, we plan to apply this technology in various domains, such as constructing a laboratory automation framework and automating tasks related to object organization and tidying. Ultimately, we intend to implement a robotic arm-based object handling system.

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