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# Admittance Remodeling Strategy of Grid-Connected Inverter Based on Improving GVF

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**Abstract:** With the continuous enhancement of weak grid characteristics, the negative effects of grid voltage feedforward (GVF) and PLL on grid-connected inverters become more and more serious and are coupled. Therefore, it is difficult to effectively solve the system stability problem by only improving the PLL structure. Firstly, based on an improved phase-locked loop structure (CCF-PLL) with complex coefficient filter and considering the influence of GVF, the output admittance model of a grid-connected inverter is established. Through stability analysis, it is found that conventional GVF leads the total output admittance phase of the inverter, thus reducing the system stability margin under the weak grid. Then, an improved admittance remodeling strategy of the grid-connected inverter is proposed. An all-pass filter is introduced into the GVF loop to correct the phase of the total output admittance of the inverter, and the phase margin is used as the constraint to design the control parameters, which effectively improves the stability of the system under the weak grid. Finally, the simulation results show that, compared with traditional GVF, the proposed strategy can obviously improve the distortion of grid-connected current waveforms and improve system stability.

**Keywords:** grid-connected inverter; grid voltage feedforward; admittance remodeling; all-pass filter



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## 1. Introduction

In remote areas, new energy generation needs to be transported to the load center via long-distance lines, and the power grid exhibits weak grid characteristics with a low short circuit ratio (SCR) [1–3]. In weak grids ( $2 < \text{SCR} < 3$ ), the grid impedance cannot be ignored [4,5], and both traditional synchronous reference frame phase-locked loop (SRF-PLL) and grid voltage feedforward (GVF) introduce negative admittance [6]; resulting in an advanced output admittance phase of the inverter [7,8]; making the system difficult to operate stably due to a decreased stability margin. Therefore, improving the stability of grid-connected inverters under weak grid conditions is particularly important [9].

Regarding grid-connected inverters that only consider the impact of SRF-PLL, the stability of the system under weak grid conditions can be improved by reshaping the inverter admittance through improving the PLL structure [10,11]. The literature [12,13] proposed methods of introducing a second-order low-pass filter to improve the PLL structure and constructing a new type of PLL structure, respectively, to reshape the impedance characteristics of the PLL branch, thereby improving system dynamic performance and phase margin. However, the above strategies can cause the phase of the grid voltage collected by the PLL to lag at the fundamental frequency, causing the grid voltage to be out of sync with the grid current. Therefore, the literature [14,15] proposed a PLL structure with a complex coefficient filter (CCF-PLL), which can improve system dynamic performance and phase margin while ensuring that the phase collected by the PLL does not lag at the fundamental frequency.

GVF control can suppress the background harmonics of the grid voltage and improve the quality of the grid current, and, thus, it has been widely used in grid-connected inverters [16–18]. However, grid voltage feedforward can reduce the adaptability of grid-connected inverter systems to a weak grid [19,20]. The literature [21–23] has pointed out

that the feedforward branch can reduce the stability margin of the grid-connected inverter under weak grid conditions, and may lead to harmonic instability in the grid-connected current. The literature [24,25] has also indicated that the introduction of traditional grid voltage feedforward can cause a significant amplification of background harmonics near the cutoff frequency of the system loop gain, resulting in a significant decrease in the robustness of the inverter under weak grid conditions. The literature [26,27] proposes a phase advance compensation method to increase the phase angle of inverter output impedance, reduce the instability region generated by GVF, and improve the robustness of the system to the impedance changes of the power grid. The literature [28] proposed an improved control strategy based on the combination of phase compensation and multiple resonant controllers. Multiple resonant links were added to GVF branches, and a phase compensator with adaptive parameter adjustment was introduced into the forward path to improve the phase margin and the adaptability of the system.

As can be seen from the above, there are many effective solutions considering only the influence of SRF-PLL on a grid-connected inverter system, among which the method proposed in the literature [14] is, relatively, better. However, with the continuous enhancement of weak grid characteristics, the interaction frequency band between grid impedance and system expands, and the negative effects of GVF and phase-locked loop on grid-connected inverters are intensified and interactive coupling occurs [29,30]. The inverters need to be able to operate stably under the condition of wide-range transformation of grid impedance [31]. In this case, the influence of GVF on inverters cannot be ignored.

Therefore, the control model of a grid-connected inverter using CCF-PLL is established, and the influence of GVF is considered on this basis. The analysis shows that GVF reduces the phase margin of the grid-connected inverter system using CCF-PLL in a weak grid, thus restricting the stable operation of the system. An admittance remodeling strategy based on improved GVF is proposed. An all-pass filter is introduced into the GVF loop to reduce the output admittance phase, improve the phase margin of inverters in a weak grid, and enhance the adaptability of the system to a weak grid.

## 2. Admittance Model and Stability Analysis of Grid-Connected Inverter

### 2.1. Output Admittance Model of Inverter System

Figure 1 shows the control structure of a single-phase LCL grid-connected inverter. The LCL filter consists of inductor  $L_1$ , capacitor  $C_f$  and inductor  $L_2$ .  $i_1$  is the current of  $L_1$ ,  $i_c$  is the current of  $C_f$ ,  $i_g$  is the grid-connected current,  $k_c$  is the  $i_c$  feedback coefficient,  $H_1$  is the  $i_g$  feedback coefficient,  $G_c(s)$  is the proportional resonance controller,  $U_{dc}$  is the ideal DC voltage output of the pre-stage photovoltaic power generation unit,  $u_{pcc}$  is the common-point voltage,  $i_r$  is the  $i_g$  reference value. The phase is synchronized with the  $u_{pcc}$  phase by CCF-PLL, and the amplitude is always the given value  $I_r$ .  $G_c(s)$  is the current controller.  $Z_g$  is the impedance of the power grid. For the analysis of extreme cases,  $Z_g$  is assumed to be pure inductive, denoting  $Z_g = sL_g$ .

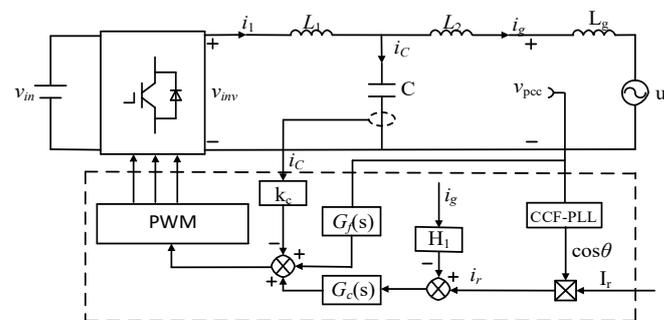
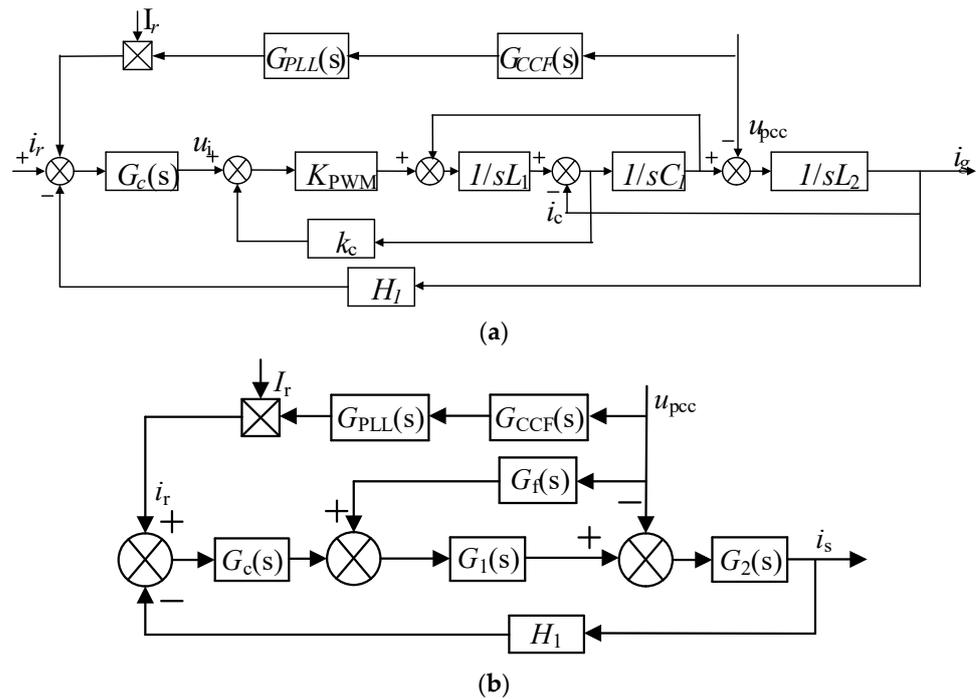


Figure 1. Structure diagram of simple-phase LCL grid connected inverter.

According to Figure 1, the control block diagram of an LCL single-phase grid-connected inverter in a weak grid is established, as shown in Figure 2a.



**Figure 2.** Equivalent control block diagram of simple-phase LCL grid-connected inverter. (a) Without GVF; (b) With GVF.

Figure 2b is the equivalent control block diagram of Figure 2a. In Figure 2b,  $G_f(s)$  is the traditional grid voltage proportional feedforward, and the expression is  $1/k_{pwm}$ .  $G_{PLL}(s)$  is the transfer function of SRF-PLL [8].  $G_{CCF}(s)$  is the transfer function of CCF [24].  $G_c(s)$  is the current controller.  $G_1(s)$  and  $G_2(s)$  are the transfer functions after equivalent transformation in the current loop [32], and their expressions are as follows:

$$\begin{cases} G_1(s) = \frac{k_{pwm}}{L_1 C_f s^2 + k_c k_{pwm} C_f s + 1} \\ G_2(s) = \frac{L_1 C_f s^2 + C_f k_c k_{pwm} s + 1}{L_1 L_2 C_f s^3 + L_2 C_f k_c k_{pwm} s^2 + (L_1 + L_2) s} \end{cases} \quad (1)$$

$$\begin{cases} G_c(s) = k_p + \frac{2k_r \omega_i s}{s^2 + 2k_r \omega_i s + \omega_0^2} \\ G_{PLL}(s) = \frac{0.5[k_{pp}(s - j\omega_0) + k_{pi}]}{(s - j\omega_0)^2 + U_{pcc}[k_{pp}(s - j\omega_0) + k_{pi}]} \\ G_{CCF}(s) = \frac{k_{CCF} \omega_0 (s + j\omega_0)}{s^2 + 2k_{CCF} \omega_0 s + \omega_0^2} \end{cases} \quad (2)$$

where,  $k_{pwm}$  represents the gain of the inverter. While a bipolar sinusoidal pulse width modulation is used for the inverter, the transfer magnitude of the inverter bridge  $k_{pwm}$  can be approximated by  $U_{dc}/2$  [33].  $k_{pp}$  is the proportional coefficient and  $k_{pi}$  is the integral coefficient.  $k_{CCF}$  is an adaptive adjustment coefficient, and, in order to avoid the interaction between CCF and SRF-PLL [14],  $k_{CCF}$  is set to 0.2.

In Figure 2b,  $i_g(s)$  can be derived from the superposition theorem as follows:

$$i_g(s) = \frac{G_c(s)G_1(s)G_2(s)}{1 + G_c(s)G_1(s)G_2(s)H_1} i_r(s) - \frac{G_2(s) * (G_1(s)G_f(s) - 1)}{1 + G_c(s)G_1(s)G_2(s)H_1} u_{pcc}(s) \quad (3)$$

The relationship between  $i_r(s)$  and  $u_{PCC}(s)$  is as follows:

$$i_r(s) = G_{PLL}(s) I_r u_{PCC}(s) \quad (4)$$

Substituting Formula (3) into Formula (2), the grid-connected current can be rewritten as follows:

$$i_g = -\left(\frac{G_2 - G_c G_1 G_2 I_r G_{CCF} G_{PLL} - G_f G_1 G_2}{1 + G_c G_1 G_2 H_1}\right) u_{pcc} \quad (5)$$

According to Formula (5), the equivalent output acceptance model of the inverter side can be established, taking into account CCF-PLL and GVF [34]. At the same time, the Thevenin equivalent model is performed for the power grid side. By connecting the power grid side and the inverter side through PCC, the interactive equivalent circuit of the inverter and the weak power grid can be obtained [35], as shown in Figure 3.

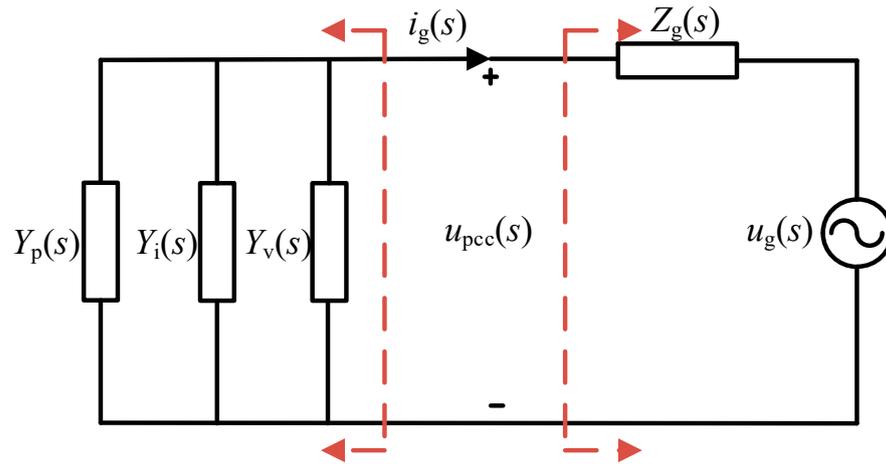


Figure 3. Equivalent circuit for grid-connected system.

In Figure 3,  $Y_p(s)$  represents CCF-PLL admittance,  $Y_i(s)$  represents inverter output admittance, and  $Y_v(s)$  represents GVF admittance, whose expressions are as follows:

$$Y_p(s) = -\frac{G_c G_1 G_2 G_{CCF} G_{PLL} I_r}{1 + G_c G_1 G_2 H_1} \quad (6)$$

$$Y_i(s) = \frac{G_2}{1 + G_c G_1 G_2 H_1} \quad (7)$$

$$Y_v(s) = -\frac{G_1 G_2 G_f}{1 + G_c G_1 G_2 H_1} \quad (8)$$

where,  $k_p$  represents the proportional coefficient,  $k_r$  represents the harmonic coefficient,  $\omega_i$  represents the bandwidth coefficient,  $\omega_0$  represents fundamental frequency angular frequency.

The expression of the total output admittance  $Y_o(s)$  of the inverter system is:

$$Y_o(s) = Y_p(s) + Y_i(s) + Y_v(s) \quad (9)$$

The total output admittance without GVF is denoted as  $Y_{o1}(s)$ , whose expression is  $Y_{o1}(s) = Y_p(s) + Y_i(s)$ .

### 2.2. Stability Analysis

According to Figure 3 and Formula (9), the expression of  $i_g(s)$  can be rewritten as:

$$i_g(s) = -\frac{Y_o(s) u_g(s)}{1 + Y_o(s) / Y_g(s)} \quad (10)$$

where,  $Y_g(s)$  is grid admittance, and the expression is  $1/Z_g(s)$ .

According to the stability criterion based on impedance [36], system stability can be ensured by reasonably designing control parameters so that  $Y_o(s)$  does not contain unstable poles under the strong grid. The stability of the system under a weak grid is determined by  $Y_o(s)/Y_g(s)$ , and the stability condition is as follows: As  $|Y_o(s)| = |Y_g(s)|$ , the phase difference between  $Y_o(s)$  and  $Y_g(s)$  is less than  $180^\circ$ ; that is, the admittance ratio of  $Y_o(s)/Y_g(s)$  phase margin (PM) is greater than  $0^\circ$ . Since the phase of  $Y_g(s)$  is  $-90^\circ$  in all frequency bands, the stability condition can be rewritten as: when, and only when  $|Y_o(s)| = |Y_g(s)|$ , the phase of  $Y_o(s)$  is less than  $90^\circ$ .

Figure 4 shows the Bode diagram of  $Y_{o1}(s)$  and  $Y_o(s)$  when  $SCR = 2$ . In this figure, the phase of output admittance of  $Y_{o1}(s)$  in the frequency band of  $f_{min}(133 \text{ Hz}) \sim f_{max}(2375 \text{ Hz})$  is from  $19^\circ \sim 53^\circ$ , the amplitude is about  $-25 \text{ dB}$ , and the PM is  $54.2^\circ$ , indicating that the system is stable. After GVF is added, the phase of the total output admittance  $Y_o(s)$  is advanced in the  $f_{min} \sim f_{max}$  frequency band, and the  $f_1(178 \text{ Hz}) \sim f_2(644 \text{ Hz})$  frequency band is greater than  $90^\circ$ , resulting in a PM of  $-8.8^\circ$  ( $f_c = 439 \text{ Hz}$ ), and the system is unstable. It can be seen that the addition of GVF will affect the phase of the total output admittance of the system, and the influence frequency range is  $f_{min} \sim f_{max}$ , making the phase margin of the CCF-PLL inverter system in a weak grid negative, which seriously affects the stability of the system. Therefore, it is necessary to eliminate the negative effects of GVF.

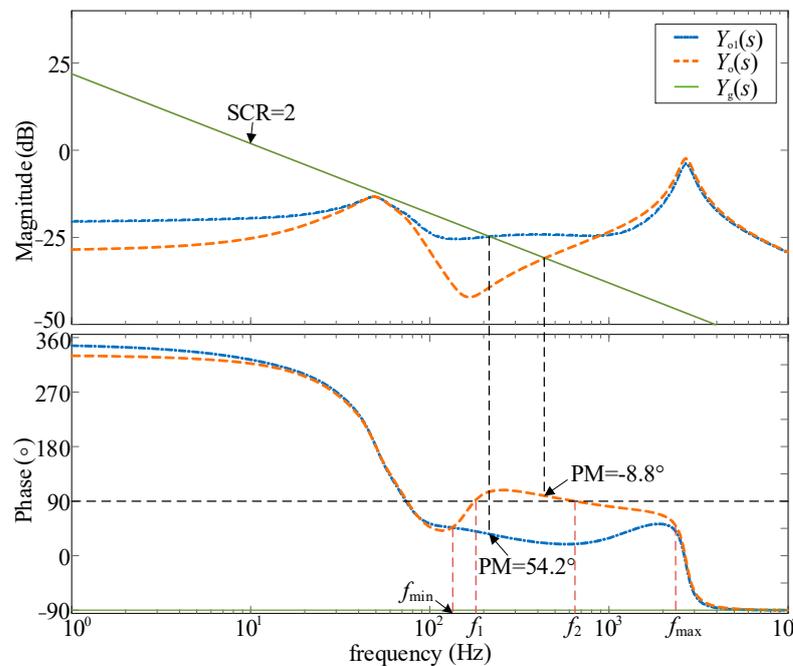


Figure 4. Bode diagram for  $Y_{o1}(s)$  and  $Y_o(s)$ .

### 3. Inverter Admittance Remodeling Strategy Based on Improved GVF

#### 3.1. The Influence of Traditional GVF on System Stability

According to the above analysis, when considering GVF, a CCF-PLL grid-connected inverter system has poor stability under weak grids, so it is necessary to analyze the influence of GVF on system stability on this basis. Figure 5 shows the logarithmic frequency characteristics of  $Y_v(s)$ . It can be seen that its amplitude is about  $-25 \text{ dB}$  in the  $f_{min} \sim f_{max}$  frequency band, and its phase is from  $48.9^\circ \sim 227^\circ$  (the phase at  $f_{min}$  is  $227^\circ$ ). The high phase of  $Y_v(s)$  should be the reason for  $Y_o(s)$  phase advance.

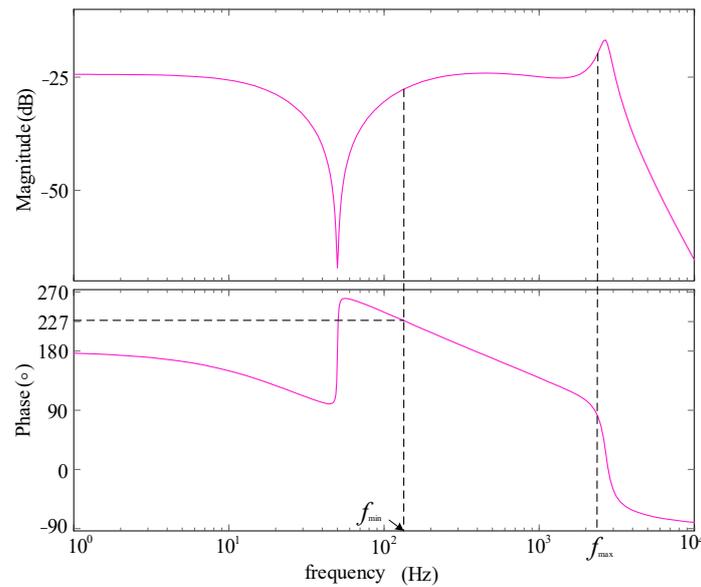


Figure 5. Bode diagram of  $Y_v(s)$ .

In order to further clarify the effect of GVF on  $Y_o(s)$  phase, a phasor diagram in circuit theory is applied to analyze it. By the foregoing, the inside  $f_{min} \sim f_{max}$  spectrum,  $Y_{o1}(s)$  the amplitude of which basically remains the same, and  $Y_v(s)$  have the same amplitude, so for convenience of analysis, it can be assumed  $Y_v(s)$  and  $Y_{o1}(s)$  values are equal; remember  $Y_v(s)$  phase is  $\varphi_v$ ,  $Y_{o1}(s)$  phase is  $\varphi_{o1}$ ,  $Y_o(s)$  phase is  $\varphi_o$ ,  $\varphi_{o1} = \alpha (19^\circ \leq \alpha \leq 53^\circ)$ , to  $Y_{o1}$  phasor for reference. Phasor diagram is as shown in Figure 6, including  $\beta = 60^\circ - \alpha$ .

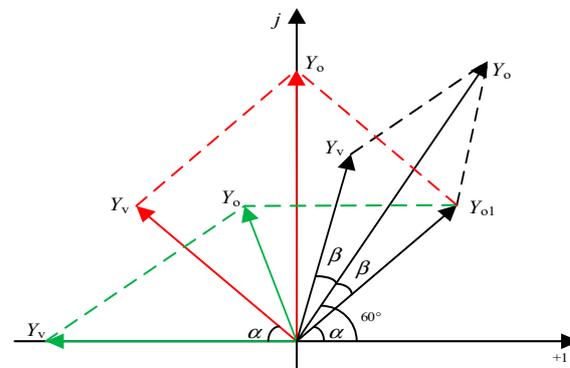


Figure 6. A phasor diagram of  $Y_o(s)$  with  $Y_v(s)$ .

Figure 6, when  $\varphi_v = 180^\circ - \alpha$ ,  $\varphi_o = 90^\circ$ , the critical stability; when  $\varphi_v < 180^\circ - \alpha$ ,  $\varphi_o < 90^\circ$ , satisfy the stability criterion based on impedance, system stability; but when  $\varphi_v > 180^\circ - \alpha$ ,  $\varphi_o > 90^\circ$ , the PM is less than zero, at this time when the system is not stable, the results and analysis results of the Bode diagram are basically identical.

### 3.2. Improve the GVF Control Strategy

From the analysis of Section 2.1, it is known that, to make the system stable, we must guarantee that within  $f_{min} \sim f_{max}$  spectrum  $\varphi_v < 180^\circ - \alpha$ , but to meet the requirements of  $PM \geq 30^\circ$  ( $\varphi_o \leq 60^\circ$ ), will be expected to make  $\varphi_v \leq \alpha + 2\beta$ . Therefore, an improved control strategy of GVF is proposed, and an all-pass filter is added to the  $G_f(s)$  branch to correct the phase of  $Y_v(s)$  and improve the phase margin of the inverter in the weak grid.

Figure 7 shows the equivalent control block diagram of a grid-connected inverter after improved GVF, where  $G_{AF}(s)$  is the all-pass filter transfer function, and the expression is:

$$G_{AF}(s) = k \frac{1 - as}{1 + as} \tag{11}$$

where,  $k$  is the fixed amplitude gain within the full frequency range, which does not affect the amplitude of improved system,  $k$  is 1, and  $a$  is the phase compensation coefficient [37].

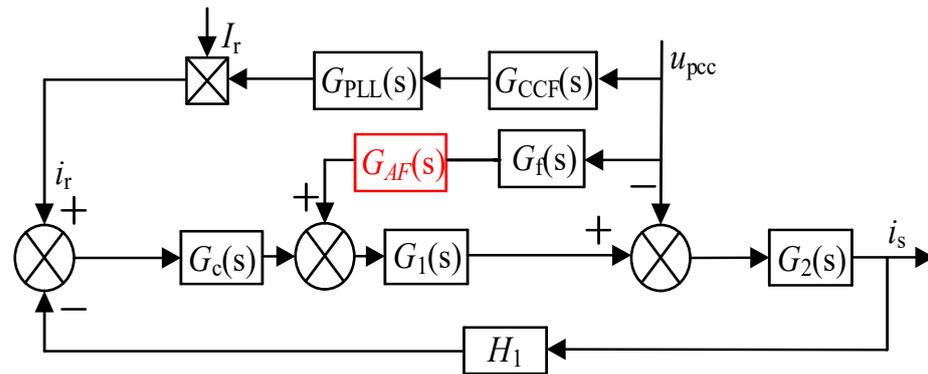


Figure 7. Equivalent control block diagram of grid-connected inverter after improved GVF.

Figure 8 shows the Bode diagram of the all-pass filter with different values of  $a$  under the condition of  $k = 1$ .

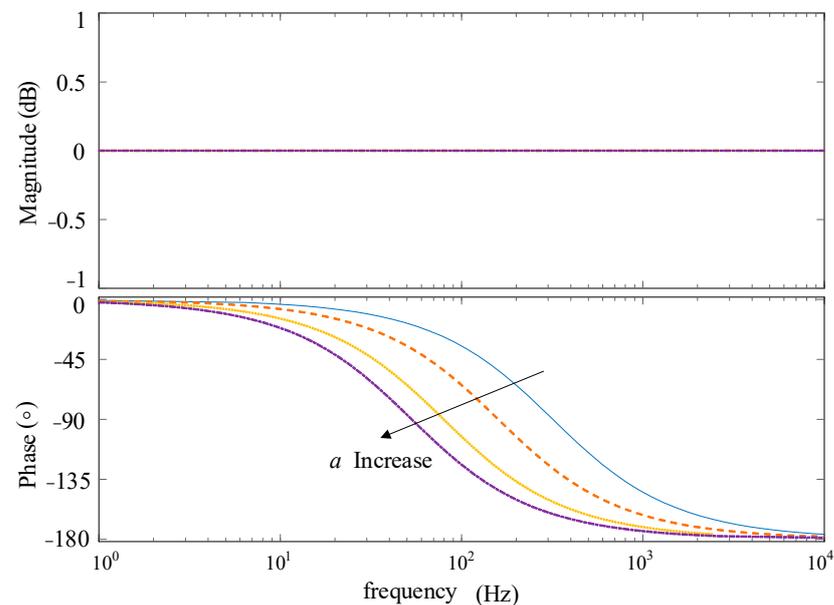


Figure 8. Bode diagram of all-pass filter with different values of  $a$ .

In the above figure, it can be seen that its amplitude in the full frequency range is 0 dB, which can provide 0~180° phase lag compensation in a certain frequency band. Therefore, on the premise of not changing the amplitude, phase correction can be carried out by adjusting the value of parameter  $a$  in a specific frequency band.

$$a = \frac{1 + \sqrt{1 + \tan^2 \theta}}{2\pi f \tan \theta} \tag{12}$$

where,  $f$  to compensate frequency points,  $\theta$  for lag compensation.

In the frequency range where phase lead occurs, the maximum phase of  $Y_v(s)$  at  $f_{min}$  is  $227^\circ$ , and its phase-frequency curve monotonically decreases in the frequency band from  $f_{min}$  to  $f_{max}$ . Therefore, as long as the phase at this point meets the requirements, the phase at other frequencies can also meet the requirements. Make  $f_{min}$  with phase compensation point, then the lag compensation angle  $\theta = (\alpha + 2\beta) - 227^\circ$ . A larger  $\alpha$  corresponds to a smaller value of  $\varphi_v$  that ensures the stability of the system; therefore, for analyzing the worst case, taking  $\alpha = 53^\circ$ , thus  $\beta = 7^\circ$ , the system stability is obtained, and leaving at least  $30^\circ$  phase margin requirements for  $\varphi_v \leq 67^\circ$  or less. It should at least provide  $\theta = 160^\circ$  phase compensation. By substituting  $f_{min} = 133$  Hz and  $\theta = -160^\circ$  into Formula (12),  $a = 0.0068$  can be obtained.

After adding all feedforward links, the expression of voltage feedforward admittance is:

$$Y_{v\_AF}(s) = -\frac{G_1 G_2 G_f G_{AF}}{1 + G_c G_1 G_2 H_1} \frac{k \frac{1-as}{1+as}}{[L_1 L_2 C_f s^3 + L_2 C_f k_c k_{pwm} s^2 + (L_1 + L_2)s] + k_{pwm} G_c H_1} \tag{13}$$

Figure 9 shows the Bode diagram of  $Y_{v\_AF}(s)$ . Compared with Figure 5, it can be seen that the addition of an all-pass filter only changes the phase of  $Y_v(s)$  but does not change its amplitude. The phase of  $Y_{v\_AF}(s)$  at  $f_{min}$  is  $66.7^\circ$ , less than  $67^\circ$ , and the phase in the whole band affected by the GVF phase is less than  $67^\circ$ , meeting the requirement of stability.

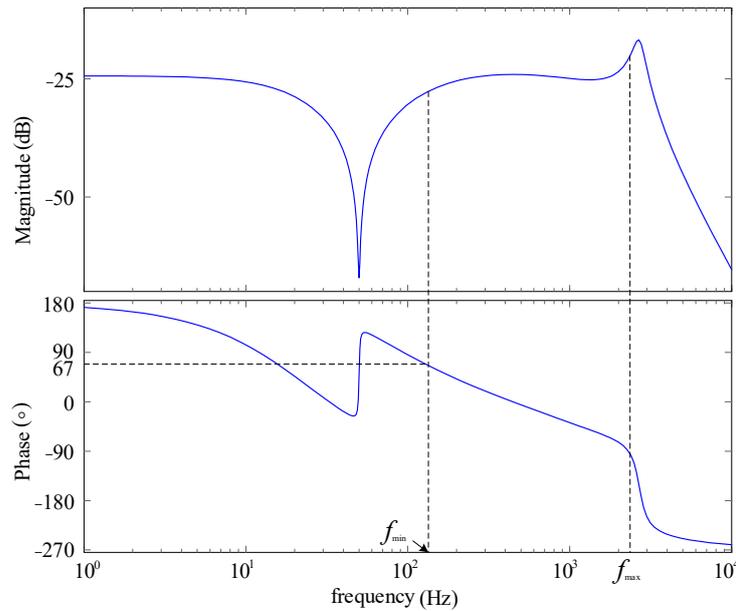


Figure 9. Bode diagram of  $Y_{v\_AF}(s)$ .

After improving the grid voltage feedforward, the total output admittance of the inverter system can be expressed as:

$$Y_{o\_AF}(s) = Y_p(s) + Y_i(s) + Y_{v\_AF}(s) \tag{14}$$

Figure 10 shows the Bode diagram of  $Y_{o\_AF}(s)$  with different SCR values. By comparison with  $Y_o(s)$  in Figure 4, it can be seen that the phase of total output admittance  $Y_o(s)$  in the frequency band affected by GVF is reduced after the proposed control strategy is added. The phase margin of the system increases from  $-8.8^\circ$ ,  $-4.1^\circ$ ,  $3.2^\circ$  and  $7.9^\circ$  to  $34.2^\circ$ ,  $45.6^\circ$ ,  $67.2^\circ$  and  $84^\circ$  when the SCR is 2, 3, 6, and 10, respectively, which greatly improves the stability of the system.

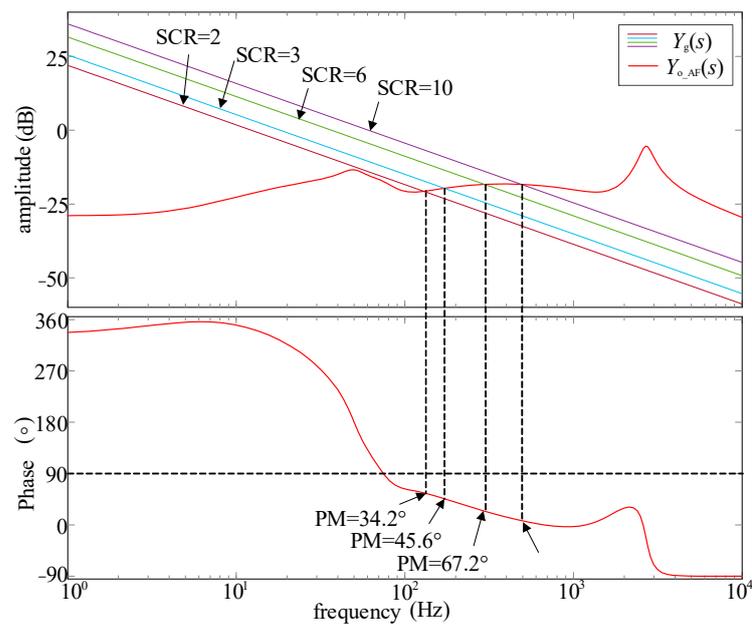


Figure 10. The Bode diagram of  $Y_{o\_AF}(s)$ .

### 4. Simulation and Experimental Results

#### 4.1. Simulated Analysis

In order to verify the correctness of the above theoretical analysis and the effectiveness of the proposed strategy, a single-phase LCL grid-connected inverter model was built based on MATLAB/simulink simulation software. The system simulation parameters are shown in Table 1. The simulation model of a single-phase LCL grid-connected inverter system is shown in Figure 11.

Table 1. Grid-connected inverter simulation parameters.

Parameter	Value	Parameter	Value
$v_g/V$	220	$k_p$	0.55
$v_{in}/V$	400	$k_r$	75
$L_1/mH$	2	$\omega_i$	$\pi$
$L_2/mH$	0.5	$k_{pp}$	0.833
$C_f/\mu F$	8	$k_{pi}$	107.88
$k_c$	0.1	$H_1$	0.15

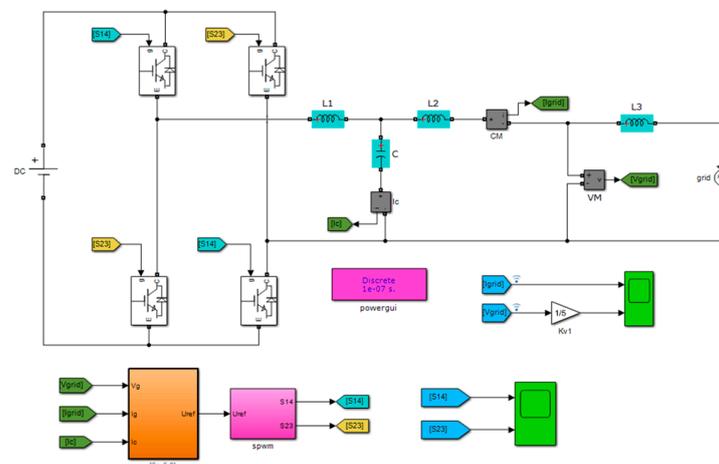


Figure 11. The simulation model of single-phase LCL grid-connected inverter system.

Firstly, the stability of the inverter system before and after adding GVF is compared. Figure 12 shows the grid-connected current waveform when  $SCR = 2 (L_g = 12.8 \text{ mH})$ . When no GVF is added before  $t = 0.12 \text{ s}$ , no oscillation distortion occurs in the grid-connected current. When  $t = 0.12 \text{ s}$  and GVF is added, the grid-connected current oscillates obviously. This indicates that the stability of the grid-connected inverter using CCF-PLL is better without GVF in weak power grids, but becomes unstable after introducing GVF, due to grid current oscillations.

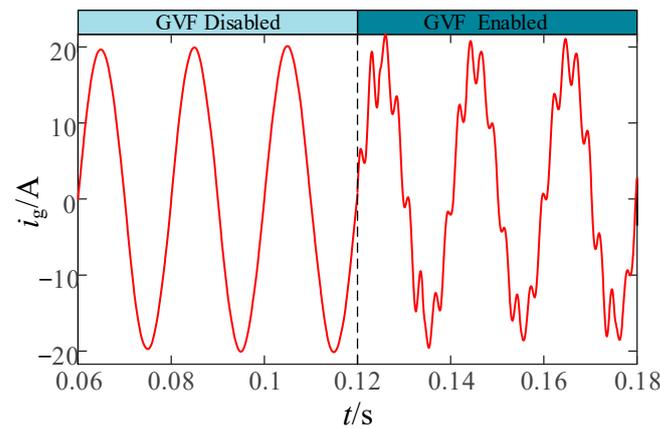


Figure 12. The  $i_g(t)$  waveform before and after adding GVF.

According to Figure 4, it is found that traditional GVF results in a phase margin of  $-8.8^\circ$  for the inverter system at  $SCR = 2$ , indicating system instability. As shown in Figure 13, after adding traditional GVF, the grid-connected current  $i_g(t)$  exhibits distortion and instability when  $SCR = 3.1 (L_g = 8.28 \text{ mH})$ . As the grid impedance increases, the distortion phenomenon of the current waveform becomes more severe when  $SCR = 2$ . The results show that traditional GVF can reduce the stability margin of the grid-connected inverter system using CCF-PLL in a weak grid, and aggravate the system’s instability with the increase in grid impedance.

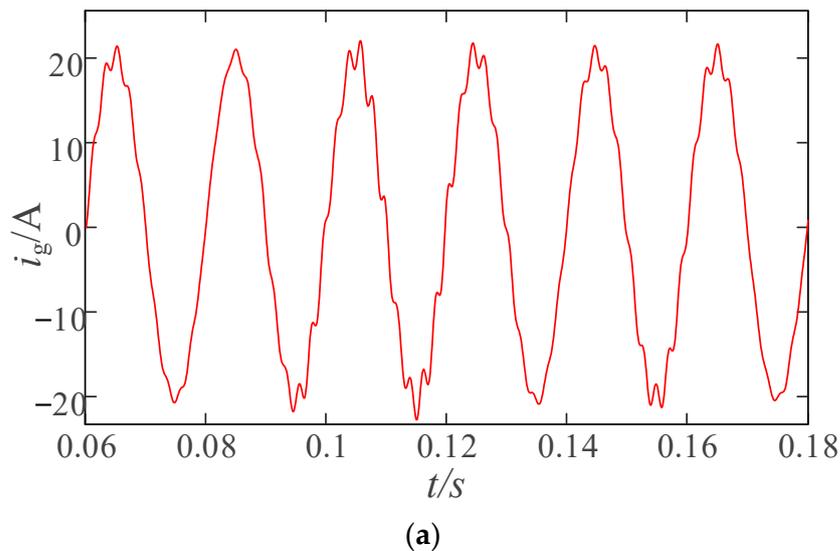
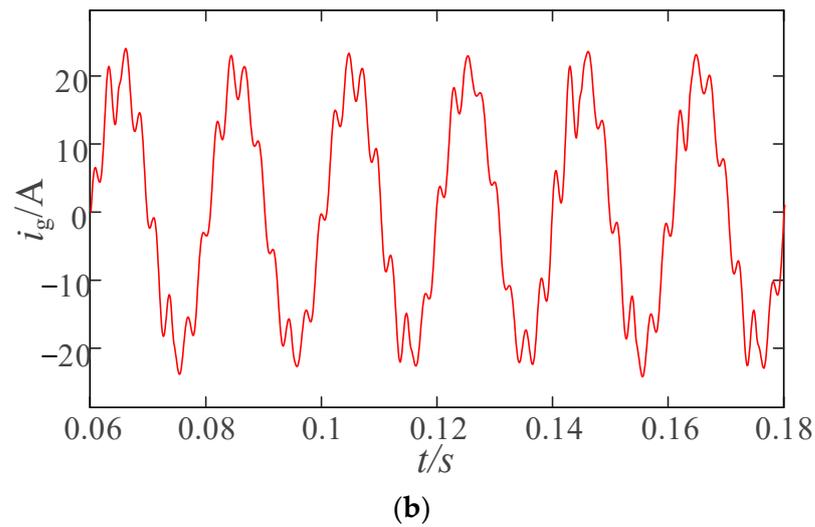
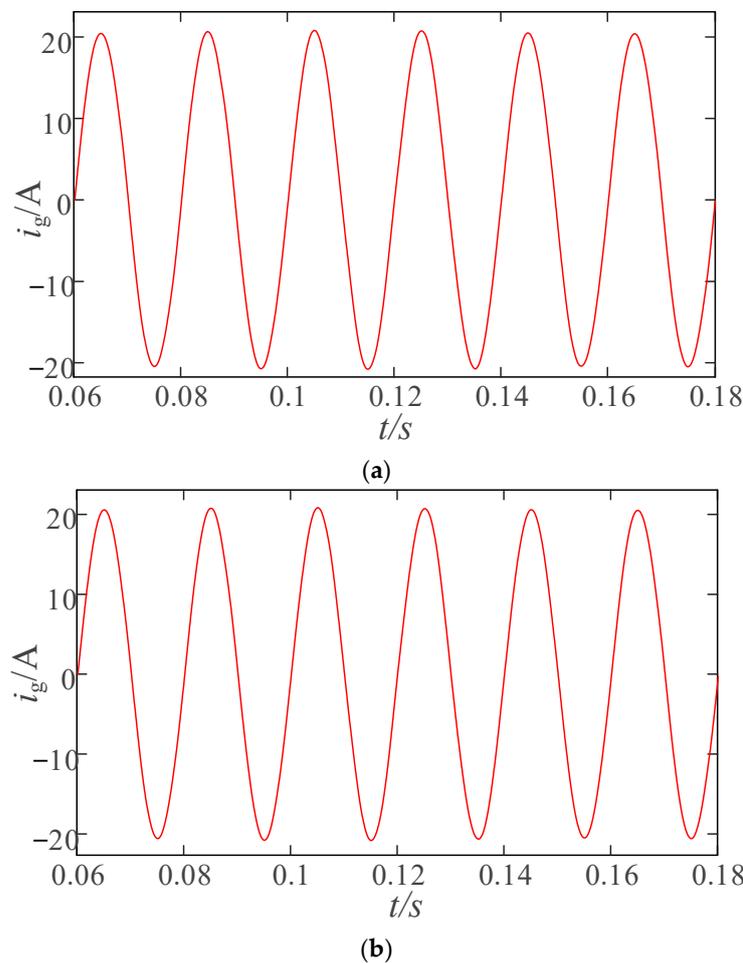


Figure 13. Cont.



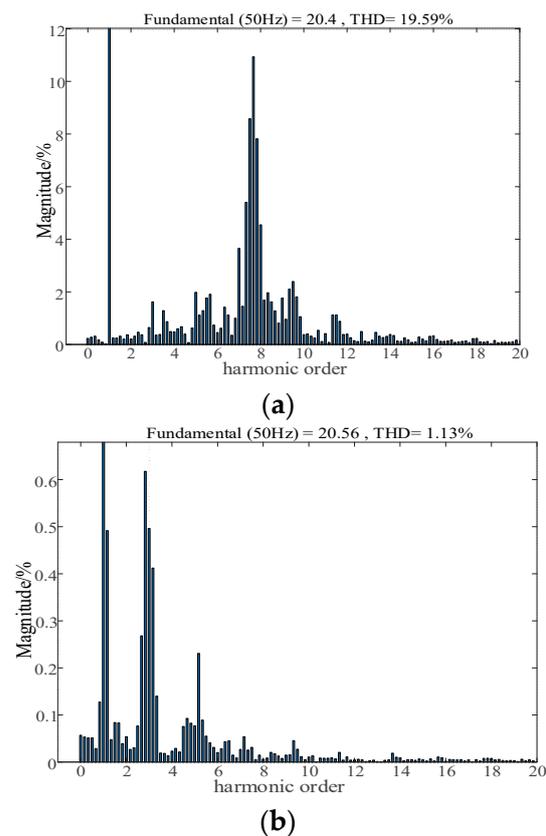
**Figure 13.** Waveform of  $i_g(t)$  adding traditional GVF. (a) SCR = 3.1. (b) SCR = 2.

Figure 10 shows that the improved GVF makes the phase margin of the inverter system  $34.2^\circ$  when SCR = 2, and the system is stable. As shown in Figure 14, after adding the improved GVF, the distortion phenomenon of a grid-connected current waveform is significantly improved. By comparing the simulation results in Figures 12 and 13, it can be seen that the proposed improved GVF strategy effectively improves the adaptability of the grid-connected inverter system to a weak power grid.



**Figure 14.** Waveform of  $i_g(t)$  when improving GVF is added. (a) SCR = 3.1. (b) SCR = 2.

In addition, FFT analysis was conducted on  $i_g(t)$  before and after the improved GVF under  $SCR = 2$ . As shown in Figure 15, the THD before improvement is 19.59%; there are a large number of harmonics in a grid-connected current, and the largest component of harmonics is mainly concentrated in the frequency band  $f_1(178\text{ Hz})\sim f_2(644\text{ Hz})$  whose  $Y_o(s)$  phase is greater than  $90^\circ$ ; which is consistent with the theoretical analysis in Section 2.1. After the improvement, the THD is 1.13%, and the harmonic distortion rate of a grid-connected current is reduced by 94.2%, which greatly reduces the harmonic content in  $f_1\sim f_2$  bands and improves the stability of the system. The results show that the proposed strategy can ensure the stable operation of the grid-connected inverter when the grid impedance is large.

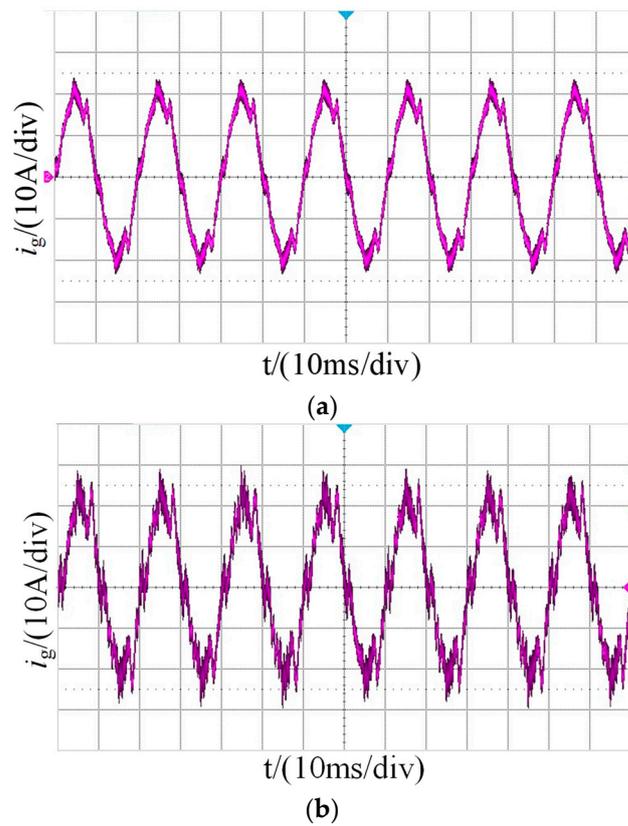


**Figure 15.** THD analysis before and after improving GVF. (a) After improving GVF. (b) Before improving GVF.

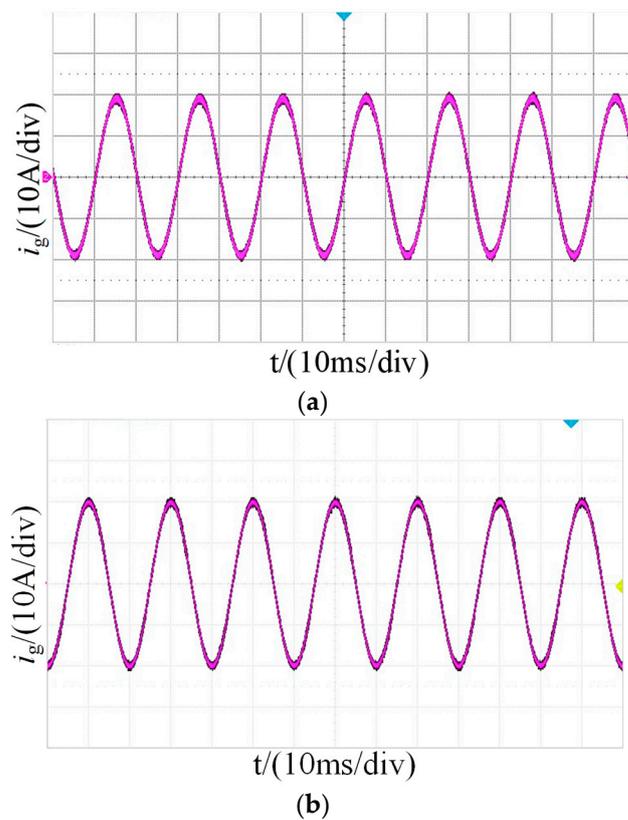
#### 4.2. Experiment Results

In order to verify the effectiveness of the admittance remodeling strategy of the proposed grid-connected inverter with improved grid voltage feedforward, a single-phase LCL grid-connected inverter model was constructed based on the MT1000 power electronic real-time controller, and the experimental parameters were given in Table 1.

The experimental waveform of a grid current with traditional GVF added is shown in Figure 16. Due to the insufficient system phase margin, the grid current waveform is significantly distorted and contains a large amount of harmonics, resulting in system instability. Figure 17 shows the experimental waveform of a grid current with improved GVF added. After adopting the control strategy with improved GVF, the system has sufficient phase margin, and the grid current waveform is free of significant distortion with a significant reduction in harmonics, leading to an improvement in system stability. The experimental results are consistent with the simulation results.



**Figure 16.** Experimental waveform of  $i_g(t)$  before adding improvement GVF. (a)  $SCR = 3.1$ . (b)  $SCR = 2$ .



**Figure 17.** Experimental waveform of  $i_g(t)$  after adding improvement GVF. (a)  $SCR = 3.1$ . (b)  $SCR = 2$ .

## 5. Conclusions

Through analysis, it was found that conventional GVF makes the total output admittance of a CCF-PLL inverter system phase advance in the middle frequency band, even exceeding  $90^\circ$ , which makes the phase margin negative and seriously affects the stability of the system. Therefore, an improved admittance remodeling strategy of GVF is proposed; and an all-pass filter added to the GVF loop to correct the phase of GVF admittance, so that the phase of the total output admittance of the inverter can meet the stability requirements under a weak grid; and improve the stability of a grid-connected inverter under a weak grid.

Shortcomings: It only improves the system stability problem under the condition of a weak grid. However, under the condition of an extremely weak grid with  $SCR < 2$ , the intercept frequency may appear in the low frequency band; and, after improvement, the phase of total output admittance in the low frequency band is still greater than  $90^\circ$ ; so there may be instability phenomena. This problem needs to be further optimized in follow-up studies.

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## References

1. Wu, W.; Liu, Y.; He, Y.; Chung, H.S.H.; Liserre, M.; Blaabjerg, F. Damping methods for resonances caused by LCL-filter-based current controlled grid-tied power inverters: An overview. *IEEE Trans. Ind. Electron.* **2017**, *64*, 7402–7413. [[CrossRef](#)]
2. Yu, L.; Sun, H.; Zhao, B.; Xu, S.; Zhang, J.; Li, Z. Shiyun Short Circuit Ratio Index Analysis and Critical Short Circuit Ratio Calculation of Renewable Energy Grid-connected System. *CSEE* **2022**, *42*, 919–929.
3. Chen, X.; Zhang, Y.; Wang, S.; Chen, J.; Gong, C. Impedance-phased dynamic control method for grid-connected inverters in a weak grid. *IEEE Trans. Power Electron.* **2016**, *32*, 274–283. [[CrossRef](#)]
4. Li, M.; Zhang, X.; Guo, Z.; Wang, J.; Wang, Y.; Lib, F.; Zhao, W. The Control Strategy for the Grid-Connected Inverter through Impedance Reshaping in q-Axis and its Stability Analysis Under a Weak Grid. *IEEE J. Emerg. Sel. Top. Power Electron.* **2020**, *9*, 3229–3242. [[CrossRef](#)]
5. Huanhai, X.; Wei, D.; Xiaoming, Y.; Deqiang, G.; Kang, W.; Huan, X. Generalized Short Circuit Ratio for Multi Power Electronic Based Devices Infeed to Power Systems. *CSEE* **2016**, *36*, 6013–6027.
6. Fang, T.; Zhang, H.; Wu, H.; Zhang, Y. Robustness Enhancement of Coping with Dual Factors for Grid-Connected Inverter in Weak Grid Based on Synthesis-Admittance-Phasor Scheme. *IEEE Trans. Ind. Electron.* **2022**, *14*, 754–769. [[CrossRef](#)]
7. Du, Y.; Sun, Q.; Yang, X.; Cui, L.; Zhang, J.; Wang, F. Adaptive Virtual Impedance of Grid-Tied Inverters to Enhance the Stability in a Weak Grid. *J. Electr. Eng. Technol.* **2019**, *14*, 1235–1246. [[CrossRef](#)]
8. Xu, J.; Qian, Q.; Zhang, B.; Xie, S. Harmonics and stability analysis of single-phase grid-connected inverters in distributed power generation systems considering phase-locked loop impact. *IEEE Trans. Sustain. Energy* **2019**, *10*, 1470–1480. [[CrossRef](#)]
9. Ali, Z.; Christofides, N.; Hadjidemetriou, L.; Kyriakides, E. Multi-functional distributed generation control scheme for improving the grid power quality. *IET Power Electron.* **2019**, *12*, 30–43. [[CrossRef](#)]
10. Fang, J.; Li, X.; Li, H.; Tang, Y. Stability Improvement for Three-Phase Grid-Connected Converters Through Impedance Reshaping in Quadrature-Axis. *IEEE Trans. Power Electron.* **2018**, *33*, 8365–8375. [[CrossRef](#)]
11. Xu, J.; Qian, Q.; Xie, S.; Zhang, B. Grid-voltage feedforward based control for grid-connected LCL-filtered inverter with high robustness and low grid current distortion in weak grid. In Proceedings of the 2016 IEEE Applied Power Electronics Conference and Exposition, IEEE, Long Beach, CA, USA, 20–24 March 2016; pp. 1919–1925.
12. Guo, X.; Guerrero, J.M. Abc-frame complex-coefficient filter and controller based current harmonic elimination strategy for three-phase grid connected inverter. *Mod. Power Syst. Clean Energy* **2016**, *4*, 87–93. [[CrossRef](#)]
13. Lee, K.J.; Lee, J.P.; Shin, D.; Yoo, D.W.; Kim, H.J. A novel grid synchronization PLL method based on adaptive low-pass notch filter for grid-connected PCS. *IEEE Trans. Ind. Electron.* **2013**, *61*, 292–301. [[CrossRef](#)]
14. Tu, C.; Gao, J.; Li, Q. Research on adaptability of grid-connected inverter with complex coefficient-filter structure phase locked loop to weak grid. *Trans. Electrotech. Soc.* **2020**, *35*, 2632–2642.
15. Lin, Z.; Chen, Z.; Yajuan, L.; Bin, L.; Jinhong, L.; Bao, X. Phase-reshaping strategy for enhancing grid-connected inverter robustness to grid impedance. *IET Power Electron.* **2018**, *11*, 1434–1443. [[CrossRef](#)]

16. Lin, Z.; Ruan, X.; Wu, L.; Zhang, H.; Li, W. Multi resonant Component-Based Grid-Voltage-Weighted Feedforward Scheme for Grid-Connected Inverter to Suppress the Injected Grid Current Harmonics under Weak Grid. *IEEE Trans. Power Electron.* **2020**, *9*, 9784–9793. [[CrossRef](#)]
17. Yan, Q.; Wu, X.; Yuan, X.; Geng, Y. An improved grid-voltage feedforward strategy for high-power three-phase grid-connected inverters based on the simplified repetitive predictor. *IEEE Trans. Power Electron.* **2016**, *31*, 3880–3897. [[CrossRef](#)]
18. Xu, J.; Xie, S.; Zhang, B.; Qian, Q. Robust grid current control with impedance-phase shaping for LCL-filtered inverters in weak and distorted grid. *IEEE Trans. Power Electron.* **2018**, *33*, 10240–10250. [[CrossRef](#)]
19. Wang, X.; Qin, K.; Ruan, X.; Pan, D.; He, Y.; Liu, F. A robust grid-voltage feedforward scheme to improve adaptability of grid-connected inverter to weak grid condition. *IEEE Trans. Power Electron.* **2020**, *36*, 2384–2395. [[CrossRef](#)]
20. Yang, S.; Tong, X.; Yin, J.; Wang, H.; Deng, Y.; Liu, L. BPF-based grid voltage feedforward control of grid-connected converters for improving robust stability. *J. Power Electron.* **2017**, *17*, 432–441. [[CrossRef](#)]
21. Xu, J.; Xie, S.; Qian, Q.; Zhang, B. Adaptive feedforward algorithm without grid impedance estimation for inverters to suppress grid current instabilities and harmonics due to grid impedance and grid voltage distortion. *IEEE Trans. Ind. Electron.* **2017**, *64*, 7574–7586. [[CrossRef](#)]
22. Khajeh, K.G.; Farajizadeh, F.; Solatalkaran, D. A full-feedforward technique to mitigate the grid distortion effect on parallel grid-tied inverters. *IEEE Trans. Power Electron.* **2022**, *37*, 8404–8419. [[CrossRef](#)]
23. Xu, J.; Xie, S.; Tang, T. Improved control strategy with grid-voltage feedforward for LCL-filter-based inverter connected to weak grid. *IET Power Electron.* **2014**, *7*, 2660–2671. [[CrossRef](#)]
24. Gao, J.; Tu, C.; Guo, Q.; Xiao, F.; Jiang, F.L.; Lu, B. Impedance Reshaping Control Method to Improve Weak Grid Stability of Grid-Connected Inverters. In Proceedings of the IECON 2020 the 46th Annual Conference of the IEEE Industrial Electronics Society, Singapore, 19–21 October 2020; pp. 1342–1346.
25. Li, X.; Fang, J.; Tang, Y.; Wu, X. Robust design of LCL filters for single-current-loop-controlled grid-connected power converters with unit PCC voltage feedforward. *IEEE J. Emerg. Sel. Top. Power Electron.* **2017**, *6*, 54–72. [[CrossRef](#)]
26. Chen, B.; Zeng, C.B.; Miao, H.; Hong, C. Improved voltage feedforward method for improving robust stability of grid-connected inverters in weak grids. *J. Electr. Power Sci. Technol.* **2021**, *36*, 118–124.
27. Zeng, C.; Wang, H.; Li, S.; Miao, H. Grid-voltage-feedback active damping with lead compensation for LCL-type inverter connected to weak grid. *IEEE Access* **2021**, *9*, 106813–106823. [[CrossRef](#)]
28. Wang, H.; Zeng, C.; Miao, H. A phase compensation algorithm of a grid-connected inverter based on a feedforward multi-resonant grid voltage. *Power Syst. Prot. Control* **2021**, *49*, 81–89.
29. Wang, G.; Du, X.; Shi, Y.; Yang, Y.; Sun, P.; Li, G. Effects on oscillation mechanism and design of grid-voltage feedforward in grid-tied converter under weak grid. *IET Power Electron.* **2019**, *12*, 1094–1101. [[CrossRef](#)]
30. Xie, Z.; Chen, Y.; Wu, W.; Gong, W.; Guerrero, J.M. Stability enhancing voltage feed-forward inverter control method to reduce the effects of phase-locked loop and grid impedance. *IEEE J. Emerg. Sel. Top. Power Electron.* **2020**, *9*, 3000–3009. [[CrossRef](#)]
31. Pang, B.; Li, F.; Dai, H.; Nian, H. High Frequency Resonance Damping method for voltage source converter based on voltage feedforward control. *Energies* **2020**, *13*, 1591. [[CrossRef](#)]
32. Yang, D.; Ruan, X.; Wu, H. Impedance shaping of the grid-connected inverter with LCL filter to improve its adaptability to the weak grid condition. *IEEE Trans. Power Electron.* **2014**, *29*, 5795–5805. [[CrossRef](#)]
33. Xia, W.; Kang, J. Stability of LCL-filtered grid-connected inverters with capacitor current feedback active damping considering controller time delays. *J. Mod. Power Syst. Clean Energy* **2017**, *5*, 584–598. [[CrossRef](#)]
34. Zhu, K.; Sun, P.; Zhou, L.; Du, X.; Luo, Q. Frequency-Division Virtual Impedance Shaping Control Method for Grid-Connected Inverters in a Weak and Distorted Grid. *IEEE Trans. Power Electron.* **2020**, *35*, 8116–8129. [[CrossRef](#)]
35. Wang, H.; Chen, Y.; Wu, W.; Liao, S.; Wang, Z.; Li, G.; Guo, J. Impedance Reshaping Control Strategy for Improving Resonance Suppression Performance of a Series-Compensated Grid-Connected System. *Energies* **2021**, *14*, 2844. [[CrossRef](#)]
36. Sun, J. Impedance-based stability criterion for grid-connected inverters. *IEEE Trans. Power Electron.* **2011**, *26*, 3075–3078. [[CrossRef](#)]
37. Xue, T.; Sun, P.; Xu, Z.; Luo, Q. Feedforward phase compensation method of LCL grid-connected inverter based on all-pass filter in weak grid. *IET Power Electron.* **2020**, *13*, 4407–4416. [[CrossRef](#)]

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