

## Article

# Fiber Bragg Grating Sensors for Mainstream Industrial Processes

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**Abstract:** This paper reviews fiber Bragg grating sensing technology with respect to its use in mainstream industrial process applications. A review of the various types of sensors that have been developed for industries such as power generation, water treatment and services, mining, and the oil and gas sector has been performed. A market overview is reported as well as a discussion of some of the factors limiting their penetration into these markets. Furthermore, the author's make recommendations for future work that would potentially provide significant opportunity for the advancement of fiber Bragg grating sensor networks in these mainstream industries.

**Keywords:** fiber Bragg grating; long period grating; process control; industrial control; programmable logic controller; distributed control systems; interrogation

## 1. Introduction

In 2005, Willsch et al. [1] provided a review of fiber optic sensor (FOS) systems in process control, and environmental and structural monitoring. The report highlighted the developments of fiber Bragg grating (FBG) sensing in wind turbine, aerospace, structural health monitoring, and railway transportation applications, as well as improvements in specific chemical sensors and interrogation techniques. In 2011, the same group reviewed FOS with a focus on research and industry in Germany [2]. The review again highlighted the improvements made in FBG technology and its expansion from the laboratory into industrial application through spin-off companies. This is reflective of FBG and other in-fiber grating technologies worldwide.

Nevertheless, penetration of fiber Bragg grating sensors into mainstream industrial processes such as the amenities and services sector, mining, and the oil and gas industry has been extremely limited considering the technology has been developing for over 40 years [3,4]. In fact this has been highlighted many times, not least by Kersey et al. [5] almost 20 years ago, who stated that fiber sensor technology remained in a laboratory-based prototype stage. While there has been some commercial success, this appears to still be the case [4]. There are a number of reasons why their diffusion into these markets has been so slow; from lack of awareness and trust in the technology, to deficiencies in the physical engineering of appropriate transducers for rugged environments, as well as the complexity and cost of FBG sensor networks. Moreover, the lack of FBG sensing and interrogation standards, means the technology has only significantly progressed in niche applications, such as structural health monitoring [6,7] and protection of industrial assets [8], which will not be covered in detail in this review article. An extensive review of fibre based opto-acoustic sensors used in structural health monitoring is given in [9] and a review of optical fibre sensors specifically for physical security applications is provided in [10].

The main focus of researchers over the years with regard to fiber Bragg grating sensing in general, has been to design and produce sensors with increased sensitivity at different wavelengths. For relatively low frequency applications such as the process control industry, this is not the most significant factor. Whereas the correct dynamic range, appropriate packaging and networking capabilities are far more significant issues. Moreover, in certain applications the sensors must be able to withstand extremely high temperatures and pressures and be highly sensitive to acoustic signals [11].

In recent years, there have been significant developments in two of the areas that have constrained the progress of fiber grating technology. Firstly, the issue of temperature and strain isolation has been overcome using various techniques reported in the literature, from simply having collocated sensors that are exposed to the same temperature fluctuations to isolate stress and strain, to more complex methods, such as using tilted or chirped gratings to distinguish between the different measurands [12]. Secondly, simpler interrogation techniques are being utilised such that the optical signal can easily be transposed into the electrical domain, allowing the optical networks to be interfaced seamlessly with electronic systems. In addition, the production of FBGs has improved significantly through draw tower processes and automated manufacturing [13,14].

In this paper, we examine how the fiber Bragg grating market has grown over the past decade and what the predictions are for growth in the industry in the future. We discuss the progression of the different types of fiber Bragg grating sensors that have been developed for potential use in mainstream process control industries from past to present. Moreover, the different interrogation and networking techniques, and their integration with existing control system technology, are reviewed. The paper concludes with recommendations for future work that would potentially provide significant opportunities for the advancement of fiber Bragg grating sensor networks in these mainstream industries. Although some studies referred to in the paper use different types of in-fiber gratings the focus of this review is on FBGs. Moreover, although many sensors have also been reported using polymer optical fibres, this paper primarily examines the use of silica based FBG sensors. A review of polymer optical fiber sensors is given in [15].

## 2. Theory of In-Fiber Bragg Grating Sensors

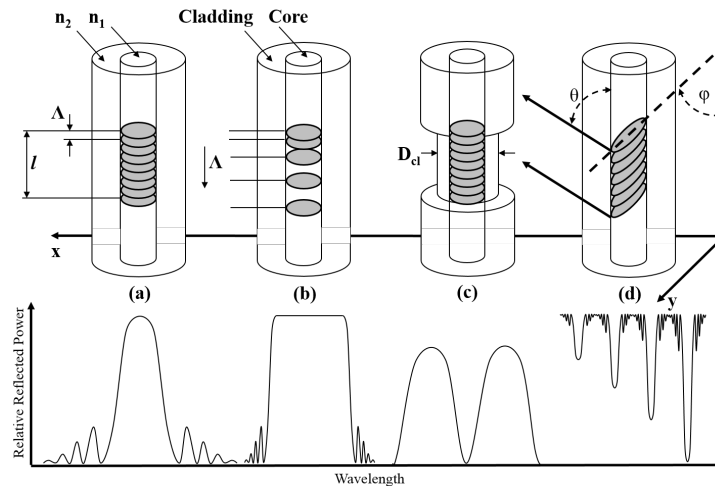
FBGs are spectrally reflective elements which can be created in the core of an optical fiber using a highly energetic light source and a phase mask [16]. This results in an inline optical filter with periodic regions of varying refractive index. The multitude of internal reflections from the periodic interfaces results in a narrow Gaussian waveform being reflected with a specific peak wavelength, known as the Bragg wavelength,  $\lambda_B$ . All other waveforms are transmitted through the FBG. The Bragg wavelength is determined by the product of effective refractive index,  $n_{eff}$  of the grating and the grating period,  $\Lambda$ , as given by;

$$\lambda_B = 2n_{eff}\Lambda \quad (1)$$

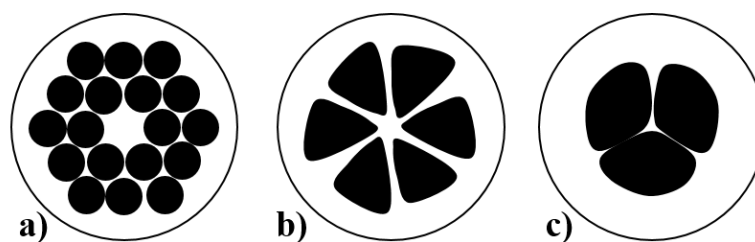
There are essentially three types of gratings which vary in photosensitivity. They are known as type I, II and IIA with the details of each type given in [12]. In addition there are different physical types of gratings such as long period gratings (LPGs), chirped gratings, tilted (blazed) gratings, and micro-structured FBGs. The structure and refractive index profile of some of the different types are shown in Figure 1.

LPGs are similar to standard gratings although they typically have a grating period greater than 100  $\mu\text{m}$ . LPGs cause light from the guided mode to be coupled into the cladding modes, where it is lost due to scattering and absorption, resulting in a number of reflected peak wavelengths; a review of LPG sensors is given in [17,18]. Chirped gratings have a varying grating period which usually causes the reflected spectrum to broaden significantly; as such they are often used as bandpass or edge filters [19,20], or interrogators [21]. In tilted gratings, the grating is at an angle with respect to the optical axis causing the light to be coupled outside of the core of the fiber [22]. Generally tilted gratings are used in optical interrogators as spectrometers [23]. The first microstructured FBG had the cladding

diameter reduced around the FBG so that the evanescent wave could interact with the surrounding medium [24,25]. Nowadays, there are many different types of microstructured fibers with an array of different cross sectional areas which can improve the way the evanescent wave interacts with the medium inside the holes. Examples of some microstructured fibers are shown in Figure 2.



**Figure 1.** Different fiber gratings; (a) standard; (b) chirped; (c) micro-structured; and (d) tilted, with their corresponding reflection/transmission spectra below.



**Figure 2.** Microstructured optical fibers; (a) Hollow core; (b) Grapefruit; and (c) three-hole suspended core.

Essentially all of the different types of gratings produce different reflected and/or transmitted spectrum profiles. The profiles can be manipulated and controlled for a given application.

### 3. Industrial Control Systems and Networking

In industrial applications large arrays of different sensors are typically used forming a distributed sensor network. Where optical fiber sensors are used in process control applications they commonly either convert the optical signal to an electrical signal locally at the sensor, eliminating many of the desired properties of the optical fiber itself as the data is transmitted over copper cables, or use stand alone optical fiber interrogators for data acquisition. Traditional sensor networks use industrial controllers for data acquisition. However, it may be possible to integrate optical fiber sensor networks with standard electronic controllers using a simple optoelectronic interface [26]. A brief description of some of the possible current electronic controllers and networking protocols that may be used in hybrid optical fiber sensor systems is given below. This is by no means a comprehensive or complete list, although it should provide a basis for further discussion regarding some of this issues with respect to integrating optical fiber sensors with current industrial controllers.

### 3.1. Industrial Controllers

Programmable logic controllers (PLCs) and other industrial automation controllers such as distributed control systems (DCSs) are the standard intelligence for instrumentation and control systems utilised in process control. They are used in a wide variety of industries from car manufacturing to building management systems, as well as controlling machinery in large mine sites [27]. PLCs often form the basis of many automated industrial processes and are essentially the heart of a Supervisory Control And Data Acquisition (SCADA) system. A PLC is an industrial computer specifically designed to be connected to input and output cards in order to take in information from a multitude of sensors in industrial processes, and control actuators in response to those inputs as defined by the control logic [28]. For example, a signal corresponding to the pressure of a fluid in a pipeline may be sent to a PLC which then could send a command to the field to stop a pump, sound an alarm, open a valve, or any other action, depending on what is required. Both PLCs and DCSs were originally developed to replace physical relay systems and designed to fulfill certain criteria:

1. Be environmentally rugged ensuring it can operate in an industrial setting;
2. Be programmed relatively easily and maintained by plant operators and technicians;
3. Be reusable.

Nowadays both PLCs and DCSs can perform much more than basic logic operations and are used to perform complex functions as required by any particular process. PLCs are usually preferred over DCSs for smaller systems where a single PLC may be used to control a specific area of a plant, whereas DCSs are usually used for extremely large processes.

### 3.2. Embedded Controllers

Embedded controllers such as Raspberry Pi [29] or Arduino microcontrollers [30] are being used more frequently in very small scale control systems. There are educational kits that are used in high school activities, as well as hobby kits for an array of residential applications, such as home automation and robotics. This increase is because the controllers are extremely low cost, small in size and easily programmed using open source software.

### 3.3. Bus Topologies

Ethernet is one of the most commonly used network protocols that enables communication between computers and other connected devices. With the addition of a router, Ethernet can be used for communication via the internet. The network speed is generally determined by the physical medium used for communication. If fiber optic cables are used bit rates as high as 10Gbit/s are now possible. Industrial processes typically require time specific data transfer, meaning standard Ethernet is not practical as there is no guarantee when the data packet will arrive. However, with the addition of extra protocol layers or by using a master controller Ethernet can be made to be time specific [31].

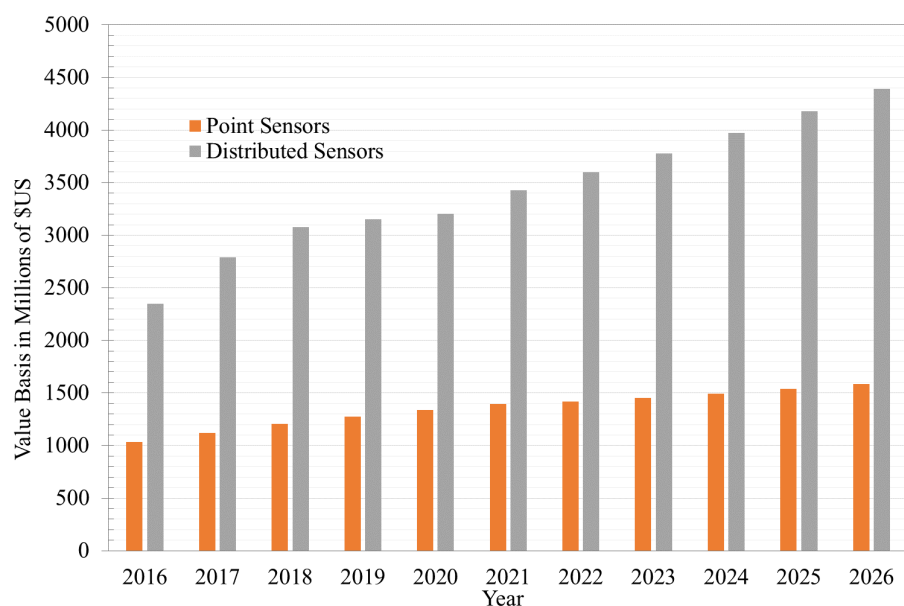
There are many different bus topologies used in industrial control systems including Modbus, controller area network bus (CANbus), Foundation FieldBus, as well as an array of smaller proprietary protocols. The particular standards used in any one process depend on a number of factors, from the size of the plant to the scale of automation required and the PLC manufacturer. A detailed review of the history of fieldbus technologies is given in [32]. Profibus (process-field-bus) is one of the most widely used industrial protocols. Profibus Decentralised Peripheral (DP) is used for high speed communication between industrial equipment such as large drives. The protocol is based on RS485 and can provide an array of diagnostics about each device on the network, communicating at up to 12 Mbit/s. Profibus Process Automation (PA) is used for monitoring remote sensors. The protocol uses Manchester Bus Powered (MBP) transmission and communicates at a rate of 31.25 kbit/s. Even though it has relatively slow data transmission rates Profibus PA is capable of providing power to sensors using over the same cable used for data transmission [33].

Profinet is a type of industrial Ethernet that incorporates the benefits of Profibus and Ethernet [34]. Profinet offers extremely fast data rates with almost no limitation on the number of slave devices and is also time specific. These attributes mean it is an ideal candidate for communication between a PLC and an optoelectronic interface.

## 4. Market Overview

### 4.1. Fiber Optic Sensors

A report released in February 2014 by ElectroniCast, a market and technology forecast consultancy company, states that the global consumption value of FOS will grow from US\$1.89 billion in 2013 to US\$4.33 billion in 2018 resulting in an annual growth rate of 18% [35]. Whereas a similar report released by BCC Research in June 2014 states the same market will grow from US\$1.8 billion in 2013 to US\$2.2 billion in 2018, resulting in a compound annual growth rate (CAGR) of 4.5% [36]. This follows BCC's 2011 report which predicted a growth from US\$1.2 billion in 2011 to US\$2.5 billion in 2017, a CAGR of 10.5% [37]. BCC's latest report released at the beginning of 2017 states that the FOS market will grow from US\$2.0 billion in 2016 to US\$3.2 billion by 2021 at a CAGR of 9.9% [38]. The latest report by ElectroniCast from May 2017 predicts the FOS market will increase at a CAGR of 7.35% from US\$3.38 billion in 2016 to US\$4.82 billion in 2021 and then increase at a CAGR of 4.41% to US\$5.98 billion by 2026, as shown in Figure 3 [39].



**Figure 3.** Global consumption value of fiber optic sensors market forecast. Reproduced with permission from [39], Copyright EletroniCast Consultants, 2017.

The distributed FOS market was \$585 million in 2013 and projected to be US\$1.458 billion in 2018 with one of the major applications being process control, as reported by the Photonics Sensor Consortium in conjunction with Light Wave Venture [40]. Despite some discrepancies in the figures all of the reports predict substantial growth in the FOS market, particularly in intrinsic sensors, those embedded within the fiber.

### 4.2. Automation Industry

The amount of revenue generated from the global process automation market is expected to grow from \$86.1 billion in 2012, to \$124.3 billion in 2018, at an estimated CAGR of 6.05% from 2013 to 2018. Also, the amount of revenue generated from the process instrumentation market is expected to grow

from \$26.5 billion in 2012, to \$36.7 billion in 2018, with a CAGR of 5.07% [41]. Seamlessly integrating FOS into process control industries has the potential to not only tap into these lucrative markets but also boost them further.

## 5. Types of Fiber Bragg Grating Sensors for Mainstream Industries

The most commonly used sensors in process control industries such as power generation, water treatment and services, mining, and oil and gas are; temperature, pressure, level, and flow. FBG sensors have been demonstrated sensing each of these different measurands. The following sections should provide the reader with a comprehensive review of the FBG sensors for the those measurands; however, it is by no means a record of every FBG sensor reported to date.

### 5.1. FBG Temperature Sensors

FBGs are inherently sensitive to temperature as outlined in the theory of this paper, and as such the literature for FBG based temperature sensors is extensive. Some of the key findings will be discussed in this paper and summarised in Table 1. In 1990, Morey et al. [42] were the first to show a FBG temperature sensor. They reported a FBG temperature sensitivity of 6.8 pm/°C at a wavelength of 830 nm. Xu et al. [43] reported a FBG temperature sensitivity of 10 pm/°C at a wavelength of 1300 nm, in 1994. The following year, Rao et al. [44] reported a FBG temperature sensitivity of 13 pm/°C at a wavelength of 1550 nm. Since then Dr Rao has published a number of papers on the progress of FBG technology and applications. Not least, in 1997, Rao et al. [45] devised a FBG temperature sensor system for medical applications. They showed that FBGs could be used for profiling the human body during hyperthermia treatment. They achieved a resolution of 0.1 °C and an accuracy of  $\pm 0.2$  °C over a temperature range of 30–60 °C. Recently, Mamidi et al. [46] reported a high temperature FBG sensor with an operating range from 20–550 °C. Interestingly, they also report a low cost intensity based interrogation technique using a LPG as a linear edge filter. The system had a resolution of 0.5 °C. Canning et al. [47] presented a review of 4 different types of temperature sensors using gratings with distinct characteristics. Among these, a high temperature sensor with an operating range of up to 1200 °C, was reported.

One of the main applications for FBG based temperature sensors is in electrical power systems and large generators because of their immunity to electromagnetic interference. A number of studies have been performed and are detailed in [48–54].

Perhaps more significant, with respect to FBG temperature measurements, is the research based on techniques for temperature compensation when using FBGs to detect other measurands. In other words, how is it possible to isolate and distinguish between fluctuations in temperature and strain induced changes. Some of these techniques will be discussed in the following sections.

**Table 1.** Summary of Fiber Bragg Grating Temperature Sensors.

Year	Sensitivity	Resolution	Range	Wavelength	Author
1990	6.8 pm/°C	-	-	850 nm	Morey et. al.
1994	10 pm/°C	-	-	1300 nm	Xu et al.
1995	13 pm/°C	-	-	1550 nm	Rao et. al.
1997	-	0.1/°C	30–60 °C	1550 nm	Rao et. al.
-	-	0.5/°C	20–550 °C	-	Mamidi et. al.
2009	-	-	up to 1200 °C	-	Canning et. al.

### 5.2. FBG Pressure Sensors

Xu et al. [55] reported a FBG pressure sensor in 1993. They showed a wavelength-pressure sensitivity of  $-3$  pm/MPa over a range of 70 MPa. This is the commonly excepted value for the pressure sensitivity of a standard bare FBG. This value is far too low for most sensing applications



and as such the main focus of research groups has been to produce pressure sensors with increased sensitivity. The improvements are detailed in the following paragraphs and summarised in Table 2.

Three years later Xu et al. [55] reported their FBG pressure sensor, the same group improved the pressure sensitivity by a factor of ten, using mechanical amplification, by mounting the FBG in a hollow glass bubble [56]. Liu et al. [57] used a polymer coated FBG for simultaneous pressure and temperature measurements. They reported a sensitivity of  $-80 \text{ pm/MPa}$  and  $88 \text{ pm/}^\circ\text{C}$  at  $1540.2 \text{ nm}$ . By embedding the polymer coated FBG in an aluminium cylinder they later increased the pressure sensitivity of their sensor to  $-5.28 \text{ nm/MPa}$  [58]. A polymer coated FBG embedded in a copper cylinder with improved thermal stability was later reported with a sensitivity of  $-3.77 \text{ nm/MPa}$  at  $1558 \text{ nm}$  [59]. An ultra thin FBG pressure sensor with the FBG orientated perpendicular to a diaphragm which meant the pressure induced a strain along the length of the FBG was subsequently reported by the same group. The effect of the radius and Young's modulus of the diaphragm was examined and a maximum sensitivity of  $7 \text{ nm/MPa}$  was reported [60]. More recently they reported a diaphragm based FBG sensor which uses an L-shaped lever and has a sensitivity of  $0.244 \text{ nm/kPa}$  [61].

An FBG pressure sensor embedded within metal bellows was reported by Song et al. [62]. As the metal bellows had a lower spring rate than the fiber, a sensitivity of  $48 \text{ pm/kPa}$  was reported.

Again using a polymer filled aluminum casing, Ahmad et al. reported a sensitivity of  $-8.7 \text{ nm/MPa}$  [63]. The same group also reported a metal diaphragm based FBG pressure sensor with a sensitivity of  $-1.67 \text{ nm/MPa}$  [64]. Although this was not as sensitive as the polymer based sensors, it could be used in more practical applications as it was more robust and not susceptible to corrosion.

Likewise, Huang et al. [65] reported a pressure sensor with a sensitivity of  $1.57 \text{ pm/KPa}$  across a range from  $0\text{--}1 \text{ MPa}$  using a diaphragm with two FBGs bonded to it. This method effectively eliminated the temperature sensitivity of the sensor, as the relative shift in the wavelengths of the two FBGs was used to determine the associated pressure. Later a Bourdon tube type FBG pressure sensor designed for pipeline leakage detection was reported by the same group [66]. The sensor had a sensitivity of  $1.414 \text{ pm/kPa}$  across a range from  $0\text{--}1 \text{ MPa}$ . Temperature compensation was achieved in the same way as their previous sensor.

Pachava et al. also described a diaphragm type FBG pressure sensor where the FBG is bonded perpendicular to the diaphragm surface with a U-shaped clamp. They report a sensitivity of  $31.67 \text{ nm/MPa}$  [67,68]. Xiong et al. [69] designed, simulated, and tested a similar sensor to that proposed by Pachava et al. which had a sensitivity of  $3.55 \text{ nm/MPa}$ .

Bock et al. [70] reported a tapered long period Bragg grating pressure sensor with a pressure sensitivity of  $51 \text{ pm/MPa}$ , which was significantly greater than a bare standard FBG. LPGs have the potential to have custom designed sensitivities, however, the manufacturing process is usually expensive and time consuming. In their paper, Bock et al. describe a new low cost fabrication technique using a computer assisted precision arc-discharge apparatus.

In 2010 and 2011 Yan et al. [71,72] described their pressure sensor sheet which used FBGs fabricated in photonic crystal fibers (PCFs) which were then embedded in polymer foils. Their initial sheet had 5 FBGs within it whereas their later sheet consisted of 15 FBGs in a mesh layout with a spatial resolution of  $10 \text{ mm}$ . The intention was to develop a large area pressure mat for use in rehabilitation and medical fields. They report a local pressure sensitivity of  $9.08 \text{ pm/kPa}$  and  $265 \text{ pm/kPa}$ , for the small and large sheet, respectively.

A pressure sensor reported by Hsu et al. [73] has a sensitivity of  $28 \text{ pm/MPa}$  and is effectively temperature insensitive. They use a strained FBG and mechanical system that reduces the strain on the FBG as the temperature increases causing the Bragg wavelength to shift in the opposite direction. The result is minimal wavelength shift across a temperature from  $10\text{--}60 \text{ }^\circ\text{C}$ .

Wu et al. [74] described a sensor capable of measuring temperature and hydrostatic pressure simultaneously using a FBG in a standard section of fiber combined with a FBG in a section of grapefruit microstructured fiber. The FBGs showed a similar response to changes in temperature of approximately

11 pm/°C. However, the microstructured FBG was significantly more sensitive to pressure variations having a sensitivity of 13.4 pm/MPa, compared to 4 pm/MPa for the standard FBG.

In 2015 the author's of this review article developed a highly sensitive standard FBG based pressure sensor. The FBG was bonded to a rubber diaphragm and a sensitivity of 0.116 nm/kPa across a range of 15 kPa was reported [75].

Although this paper reviews FBG sensors in silica fibers, a single reference to a FBG pressure sensor incorporated into a polymer fiber is provided to give context to the improved sensitivity that can be obtained using polymer optical fibers. Rajan et al. [76] reported a pressure sensor incorporating a vinyl diaphragm and a polymer FBG. The lower Young's modulus of the polymer FBG resulted in a sensitivity of 1.32 pm/Pa, more than 6 times greater than the most sensitive standard FBG pressure sensor reported to date.

**Table 2.** Summary of Fiber Bragg Grating Pressure Sensors in Order of Sensitivity.

Year	Sensitivity	Range	Wavelength	Author	FBG Type/Novelty
1993	3 pm/MPa	70 MPa	-	Xu et. al.	Standard/bare
1996	0.3 pm/MPa	70 MPa	-	Xu et. al.	Standard/bare
2000	−80 pm/MPa	-	1540.2 nm	Lui et. al.	Polymer coated/temperature and pressure
2001	−5.28 nm/MPa	-	1558 nm	Zhang et. al.	Polymer coated/aluminium cylinder
2007	−3.77 nm/MPa	-	1558 nm	Lui et. al.	Polymer coated/copper cylinder
2007	7 nm/MPa	-	-	Zhang et. al.	Standard/diaphragm
2009	0.244 nm/kPa	-	-	Zhang et. al.	Standard/L-shaped lever
2009	48 pm/kPa	-	-	Song et. al.	Standard/metal bellows
2008	8.7 nm/MPa	-	-	Ahmad et. al.	Standard/polymer filled casing
2009	−1.67 nm/MPa	-	-	Ahmad et. al.	Standard/metal diaphragm
2013	1.57 pm/kPa	0–1 MPa	-	Huang et. al.	Standard/diaphragm
2013	1.414 pm/kPa	0–1 MPa	-	Huang et. al.	Standard/Bourdon tube
2012	31.67 nm/MPa	-	-	Pachava et. al.	Standard/diaphragm
2012	3.55 nm/MPa	-	-	Xiong et. al.	Standard/diaphragm
2007	51 pm/MPa	-	-	Bock et. al.	Long period grating
2010	9.08 pm/kPa	-	-	Yan et. al.	Photonic crystal fiber
2011	265 pm/kPa	-	-	Yan et. al.	Photonic crystal fiber
2006	28 pm/MPa	-	-	Hsu et. al.	Standard/temperature insensitive
2011	13.4 pm/MPa	-	-	Wu et. al.	Microstructured/temperature and Pressure
2015	0.116 nm/kPa	15 kPa	1550 nm	Allwood et. al.	Standard/rubber diaphragm
2013	1.32 pm/Pa	-	-	Rajan et. al.	Polymer fiber/Vinal diaphragm

### 5.3. FBG Level Sensors

Many FBG level sensors are essentially pressure sensors that determine the level of a liquid based on the pressure applied by the liquid, which is proportional to the height of the liquid. As such some research groups have developed liquid level sensors through simple modifications of their pressure sensors. Guo et al. [77] described their temperature-insensitive FBG liquid level sensor which was based on a cantilever beam structure. The particular shape of the structure produced a chirp in the FBG under pressure which was proportional to the height of the liquid. This chirp broadened the reflected spectrum and resulted in a change in optical power when connected to a photodiode. Changes in temperature caused the Bragg wavelength to shift but did not change the received optical intensity. This is a good example of exploiting nonlinear responses from an FBG to isolate different measurands. Likewise Sohn et al. [78] described a similar level sensor which had an FBG embedded in it. Lai et al. [79] also reported a liquid level sensor, whereby a FBG was bonded to a cantilever which is attached to a buoy. The FBG experienced a vertical pressure that compresses it depending on the amount of buoyancy, which corresponds to the level of the liquid. Meng et al. [80] reported a similar simple technique using a cantilever with a float attached to the end. As the liquid caused the float to rise, a strain induced wavelength shift occurred. Dai et al. [81] described their simple technique of measuring liquid level by attaching one end of a FBG to the base of a container and the other end to a float, thus relating the strain to the level of the liquid.



In 2002, Fukuchi et al. [82] described a Bourdon tube based water level sensor. An FBG was attached to the end of the Bourdon tube so that an increase in pressure caused by increased water level would increase the strain on the FBF. Sengupta et al. [83] reported a very similar hydrostatic pressure sensor used for measuring liquid level. Their design was also based on a Bourdon tube with two FBGs attached to its free end. The change in hydrostatic pressure induces a strain in one of the FBGs and not the other, meaning it is effectively temperature insensitive. In 2016, Ameen et al. [84] developed a FBG level and temperature sensor which utilised a graphene diaphragm that deformed under hydrostatic pressure. The sensitivity of the sensor reduced as the number of graphene sheets was increased.

There has been some reported techniques for direct liquid level sensing. Khaliq et al. [85] and James et al. [86] described similar LPG level sensors. The ratio of the amount of the FBG immersed in the liquid to that exposed to air produced a change in transmitted intensity. Yun et al. [87] reported an etched FBG liquid level sensor. Etching the cladding from the FBG increases its response to changes in refractive index. Again the ratio of the amount of the FBG immersed in the liquid to that exposed to air produced a change in intensity. Similarly, Mou et al. [88–90] demonstrated a semi-immersed FBG that exploited the difference in refractive index of the liquid and air. Their sensor however, used a tilted fiber Bragg grating (TFBG), rather than an etched FBG or a LPG. Recently Gu et al. [91] demonstrated a similar technique using a TFBG inscribed in a thin core section of a fiber. Their results show high sensitivity and immunity to temperature changes.

#### 5.4. FBG Flow Sensors

Recently, there have been a number of studies performed using FBGs as flow sensors. As with all FBG transducers, FBG flow sensors either manipulate strain or temperature induced wavelength shift to determine the flow rate. Some research groups, such as Zhan et al. [92], have developed flow sensors that act in a similar way to the level sensors, in that a cantilever is used as the basis of the sensor. The force created by the flow of a fluid causes the cantilever to deflect which in turn changes the induces a strain on the FBG. Lu and Chen [93] also used this technique and reported a flow meter with a resolution of  $58.1 \text{ cm}^3/\text{s}$  in the forward direction and  $166 \text{ cm}^3/\text{s}$  in the backward direction. Yao et al. [94] also used this method although they used two FBGs, one attached to either side of the cantilever for temperature compensation. Other gas flow sensors exploit the changes in temperature, by coating the FBG and adapting the principles of conventional hot-wire-anemometers. That is, monitoring the temperature change as a function of gas flow around the sensor [95]. Cashdollar and Chen [96], and Caldas et al. [97,98] reported a gas flow meter using this technique, by coating a FBG with silver. Chashdollar and Chen [96] demonstrated a FBG heated with a laser diode and nitrogen gas blown on to it. The results showed that the change in temperature of the FBG, and hence the shift in Bragg wavelength, related to the gas flow rate. Caldas et al. [97,98] used a hybrid LPG and FBG setup with 1480 nm light launched into the fiber. They presented a working air flow meter with a resolution of 0.8 m/s.

Rodriguez-Cobo et al. [99] proposed a novel FBG flow sensor. They demonstrated an arc-shaped plastic flow transducer with two FBG attached to it. The air flow caused one FBG to stretch and the other to compress. Salgado et al. [100] use two strain sensor FBGs to measure the change in circumference and length of a PVC pipe which they correlated with the flow rate of the fluid in the pipe. Jiang and Gao [101] report a dual FBG flow sensor using an elastomer transducer with a specifically designed shape to maximize the impact of the fluid flow.

Zamarreno et al. [102] demonstrated a multiplexed  $8 \times 8$  FBG array for measuring flow rate, followed by a  $16 \times 16$  FBG array capable of measuring fluid turbulence [103]. The FBG array was orientated perpendicular to the pipe, producing a two dimensional map of the fluid flow. The results showed different patterns for different flow rates.

### 5.5. Additional FBG Sensors

Over the years there have been many papers published on the use of FBGs as chemical sensors, from Meltz et al. [104] in 1991 to Lu et al. [105] in 2009. Most techniques are based on the interaction of hydrogels or polymers that swell in the presence of specific chemicals or the interaction of the evanescent field with different chemicals. When an FBG is immersed in a hydrogel it causes the FBG to expand as the hydrogel swells [106]. Cong et al. [107] specifically show a salinity sensor using this method. Frazao et al. [108] reported an etched FBG for salinity measurement through evanescent field interaction. Furthermore, the group demonstrated the use of their sensor for simultaneous measurement of salinity and temperature in a large scale, fully integrated, environmental monitoring system.

FBGs have become the basis of a number of more exotic sensors such as magnetic field sensors, accelerometers, and tilt sensors, etc. An example of some of these sensors is given below. Madhav et al. [109] demonstrated that a FBG bonded to a piece of nickel can act as a magnetic field sensor. A magnetic field induces a strain on the nickel which is detected by the FBG. Zhu and Shum [110] report a FBG accelerometer in which a FBG attached to a cantilever is deflected depending on the magnitude of the applied acceleration. Guan et al. [111] describe a FBG tilt sensor. Four FBG sensors are attached to four arms that are perpendicular to a pendulum. Each FBG is strained equally when the pendulum is vertical; when the pendulum is tilted each FBG experiences a strain. The system can detect the magnitude and direction of the inclination with respect to the horizontal direction.

## 6. FBG Multiplexing and Interrogation Techniques

One of the main advantages of FBG sensors is their ability to be easily multiplexed through time division multiplexing (TDM) and wavelength division multiplexing (WDM). There are many different multiplexing architectures for quasi distributed sensor systems such as serial bus, dual bus, star, tree and mesh. Each of these architectures are detailed in [112]. Which architecture is the most appropriate depends on the requirements of the application, such as the number of sensors in a system, and also on cost.

The information from each sensor must be separated and interpreted, which requires an interrogator system to interrogate many FBGs connected in series. Initially, FBG interrogators were large, complex and expensive units, however, since the late nineties, a number of different groups have attempted to minimise and simplify them without loss of functionality.

In 1998, Fallen et al. [113] report a simple passive system that can simultaneously interrogate several FBG sensors. Half of the reflected light is incident on a ramped grating and the other half is sent to a reference arm. As the ramped grating has a large bandwidth, each reflected signal from multiple FBGs in series would be reflected off different parts of the ramped FBG.

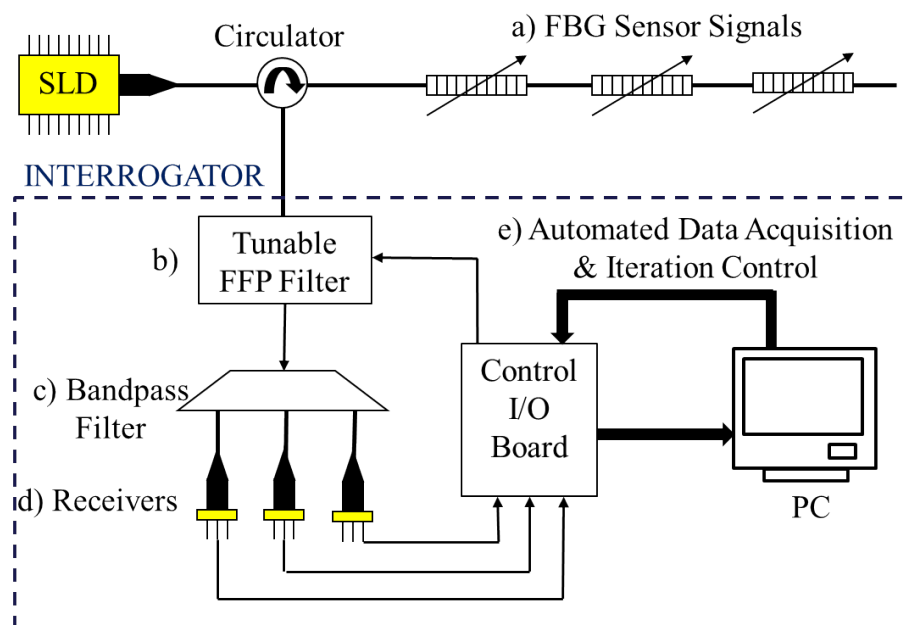
In a similar way, Chtcherbakov et al. [21] present an active interrogation system using a chirped FBG. However, instead of receiving a change in intensity, the signal is converted into a phase change and de-multiplexed using an arrayed-waveguide grating; then the signals are sent to separate detectors.

Ye et al. [114] demonstrate an active interrogation method using polarisation maintaining (PM) fibers, whereby the reflected signals from multiple FBGs firstly pass through a Fabry-Perot filter, separating the different wavelengths, and secondly, pass through a polarisation splitter, which are then sent to two different detectors. The advantages associated with this method are such that the transverse strain measurements are inherently temperature independent, and as there are two separate detectors, there is no limitation on the measurable strain due to the gap between the two Bragg wavelengths decreasing below the normal achievable resolution.

Another active interrogation system shown by Abad et al. [115] uses a two stage de-modulation similar to that of Ye et al. [114], except they use a LPG rather than a chirped grating for separating the wavelengths and then phase delay the signals using a delay line. This method only requires the use of a single detector as the relative phase difference is not affected by unwanted power fluctuations.

A portable, robust FBG interrogation system was proposed by Roths et al. [116] in 2005. The technique uses a tunable FBG that is stretched by a piezo-electric transducer (PZT) and a saw-tooth voltage signal, which acts as an analyser. This approach has significant merit, as it addresses the issue of reducing the complexity and cost associated with interrogator systems. Unfortunately, the system requires fairly extensive calibration and data acquisition software to correct non-linearities associated with the PZT.

Beccherelli et al. [117] report an intensity based interrogation method using an integrated optical filter. Here they use a tunable liquid crystal polymer that can select a specific wavelength depending on the voltage. Again, they present their work as a simple inexpensive option. Likewise, Tsai et al. [118] use an intensity based tunable system incorporating a fiber Fabry-Perot (FFP) filter that is controlled by a voltage from a control I/O board. The FFP filter is tuned with an incremental step of 0.02 V, which corresponds to a resolution of 5 pm in wavelength. The network architecture is shown in Figure 4.



**Figure 4.** FBG Network architecture showing principle operation of interrogator. Reproduced with permission from [118], Copyright IEEE Photonics Technology Letters, 2008.

Orr and Niewczas [119] report a polarization-switching FBG interrogator for simultaneous measurement of magnetic field strength and temperature. The system uses a polarisation beam splitter and a fast optical switch to select which polarised signal is sent to the Mach-Zehnder interferometer. The interrogation involves comparing reflections from both left and right circularly polarised light. In this way, any common noise or drift can be easily cancelled out. As the magnetic field strength is determined from the angle of polarisation, any other measurand that causes a wavelength shift, i.e., temperature, pressure, etc., can be measured simultaneously. While this active technique appears to be effective, the setup is expensive because of its complexity.

Due to the increase in use of FBG networks over the last decade, a number of different commercial interrogator systems have emerged [120]. However, the technology is still relatively new, meaning many of the products on the market do not live up to the manufacturer's claims or customer's expectations, for a number of different reasons including system failure and inaccurate measurements. Furthermore, the lack of a robust measuring system is not only due to problems associated with the interrogator itself, but also with the interrogator software and the complexity of the sensors. In addition, it is worth noting that all of the commercial interrogators available are large expensive

units. A detailed comparison of the performance of the HBM, Insensys, and Smart Fibres products is given in [120].

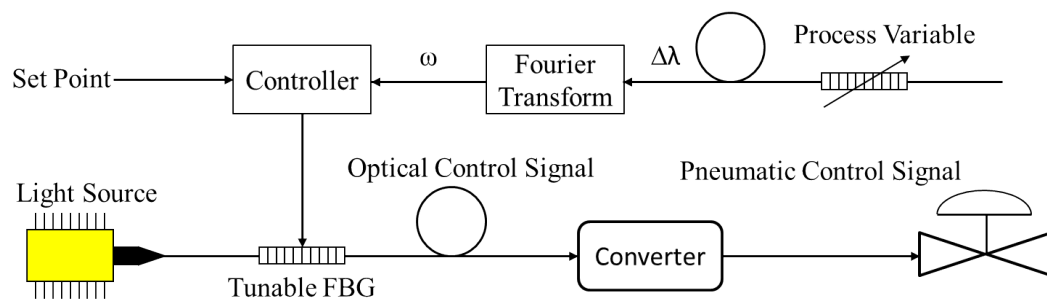
## 7. Optical Actuation and All Optical Control Systems

An entirely optical control system would be highly advantageous in certain applications. They have the potential to exceed current sensitivity and communication speeds as well as having all the advantages associated with optical systems and none of the drawbacks of electrical systems.

The goal is to create a control loop where the process variable is both detected and modulated in the optical domain, in addition to the controller providing feedback optically, with the final component being actuated via an opto-pneumatic or opto-electric converter. While steps have been made toward achieving this goal, to date a practical complete system has not been realised and currently the best solution is to have minimal electronic signal conversion.

In 1990, Hockaday and Waters [121] demonstrated a technique for direct optical to mechanical actuation. Their method uses lasers to heat a pneumatic or hydraulic fluid causing it to deviate from a central path. The deflection was a result of optical modulation of the fluid viscosity. The deflected jet of fluid produced a direct differential pressure signal that can be controlled without the need of any electronic signal. The differential pressure was used to actuate a valve.

In 2003, Mohamed Mahmoud [122] discussed the potential of an all optical control system (AOCS) incorporating FBGs. FBGs enable the process variable to be transmitted, modulated, and received on a single fiber optic cable and “mimics the two wire 4–20 mA electronic signal of an electronic process control loop”. He describes how FBGs can be used to measure many different process variables such as temperature, strain, and flow, and illustrates an AOCS shown in Figure 5, where the process variable is converted into a frequency via a fast Fourier transform, and then the controller uses a PZT to tune another FBG to provide an optical output. It is stated that the proposed system would need an opto-pneumatic or opto-electric converter to provide actuation. The actuation could then be performed by a technique based on Hockaday and Waters system [121] or by using a photovoltaic power converter [123].



**Figure 5.** Schematic of an All Optical Control System (AOCS). Reproduced with permission from [122], Copyright IEEE, 2003.

Photovoltaic power converters (PPCs) are essentially miniature solar cells designed to be responsive to specific wavelengths and connected directly to an optical fiber. GaAs photovoltaic power converters have conversion efficiencies as high as 55% [124] and can produce up to 0.5 W of electrical power. Although only GaAs based PPCs are commercially manufactured, research has shown that both Silicon and Germanium PPCs could be a viable solution for longer wavelength power conversion, having optical to electrical power conversion efficiencies as high as 50% [123]. Furthermore, it has been demonstrated that communication, sensing and power signals can be simultaneously sent over the same fiber without any interference or loss of signal strengths [125].

## 8. Interfacing and Networking FBGs

Ping et al. [126,127] report a networked FOS system based on the IEEE1451 standard for smart transducer interfaces for sensors and actuators. In their study, a GaAs chip is used as a temperature sensor and connected to a smart transducer interface module (STIM). The STIM is then connected to a PC or PLC, which acts as a virtual network capable application processor (NCAP), via a CAN bus interface module.

While the work performed by Kunzler et al. [128,129] is predominantly based on their FBG interrogation technique, their FSIM acts as a smart sensor node, having additional functionality such as signal conditioning, data processing, and a bus output locally on-board. Hence, the FSIM is connected to a network of other devices using Ethernet.

## 9. The Future of FBG Sensing in Industry

In order for FOS networks to penetrate into mainstream industrial processes two things must happen. Firstly, appropriate transducers must be developed that satisfy a number of criteria:

- Be environmentally rugged;
- Have appropriate sensitivity;
- Have the correct dynamic range;
- Be easily replaceable without disrupting the network;
- Adhere to engineering standards, either existing or new.

Secondly, FOS networks should be seamlessly integrated with existing control system architectures. Standalone FOS interrogators are expensive and require knowledge of optical engineering. FOS have the potential to replace all of the downstream I/O components from a PLC or DCS in certain applications. However, in the interim, integrating an array of fiber sensors into an existing control system would be a logical first step. A fiber system could be connected to a PLC through a simple interface module such that the PLC and operators perceive the FOS as standard electronic sensors. This would eliminate the need for additional training and therefore reduce costs and would allow confidence in optical fiber sensing to build up, enabling the use of fiber sensors to become standard engineering practice in mainstream industrial processes. Further, this would pave the way for almost entirely optical control systems of the future.

In addition, interfacing FOS with low cost embedded controllers may have the potential to form smart hybrid systems such as those containing wireless sensor networks and FOS networks. Moreover, the information from the FOS could be sent over a wireless network as proposed in [130].

## 10. Conclusions

In conclusion, a review of FBG sensing technology with respect to their use in mainstream industrial process applications has been performed. The review has focused on the types of sensors that have been developed for industries such as power generation, water treatment and services, mining, and the oil and gas sector. A market overview was reported, as well as a discussion of some of the factors limiting their penetration into these markets. Furthermore, the author has made recommendations for future work that would potentially provide significant opportunity for the advancement of FBG sensor networks in these mainstream industries.

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