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Enhanced Sensing Performance of Electrospun Tin Dioxide Nanofibers Decorated with Cerium Dioxide Nanoparticles for the Detection of Liquefied Petroleum Gas

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Abstract: Tin dioxide (SnO₂) nanofibers and cerium dioxide (CeO₂) nanoparticles were prepared by electrospinning and hydrothermal methods, respectively. The morphology and structure of the synthesized SnO₂/CeO₂ samples were characterized by a variety of methods. The gas-sensing properties of the SnO₂/CeO₂ sensor were investigated for liquefied petroleum gas (LPG) detection at room temperature. Compared with pure SnO₂ nanofibers, the SnO₂/CeO₂ composite sensor showed a much higher response and shorter response time for LPG sensing after doping with CeO₂ nanoparticles. Furthermore, the SnO₂/CeO₂ composite sensor had better resistance to interference from humidity than the pure SnO₂ sensor. The significantly enhanced sensing performance of the SnO₂/CeO₂ composite sensor for LPG can be attributed to the modification with CeO₂ to increase oxygen vacancies and form a heterostructure with SnO₂ nanofibers. Meanwhile, the LPG detection circuit was built to realize real-time concentration display and alarm for practical applications.

Keywords: liquefied petroleum gas sensing; electrospinning method; cerium dioxide doping; gas detection circuit



Citation: Liu, X.; Zhang, J.; Zhang, H.; Chen, C.; Zhang, D. Enhanced Sensing Performance of Electrospun Tin Dioxide Nanofibers Decorated with Cerium Dioxide Nanoparticles for the Detection of Liquefied Petroleum Gas. *Chemosensors* **2022**, *10*, 497. <https://doi.org/10.3390/chemosensors10120497>

Academic Editor: Wei-Lung Tseng

Received: 23 October 2022

Accepted: 22 November 2022

Published: 23 November 2022

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1. Introduction

With the progress of industrialization, people are paying more and more attention to personal health and safety [1]. Liquefied petroleum gas (LPG) is mainly composed of propane, butane, and other alkanes [2]. It can be used as an industrial and civil fuel for kiln roasting, automobile driving, and residential life. It is widely used in daily life and industrial production as an efficient source of combustion energy [3]. The lower explosive limit of liquefied petroleum gas is only 2 vol.% [4]. Since the specific gravity of liquefied petroleum gas is greater than that of air, once it leaks, it is easy for it to gather in low-lying areas and mix with air to reach this concentration [5]. Therefore, for the safety of production and general living, it is necessary to develop liquefied petroleum gas sensors to detect leakages and take further measures in a timely manner.

In view of the good crystal structure and stable chemical properties of SnO₂, it can be used in the fields of batteries, photocatalysis, and sensing [6]. However, the application of pure SnO₂ still has many limitations. For example, detection can only be carried out under high operating temperatures, and it even fails to detect certain gases [7]. To solve these problems, most research groups control the morphology of SnO₂ and introduce dopants based on it [8,9]. Electrospinning is one of the methods used to quickly and directly fabricate nanofibers. Due to its advantages of large specific surface area and high porosity, electrospinning has potential application value in many fields—especially for gas sensors [10,11]. Morais et al. successfully prepared a NO₂ sensor from electrospun WO₃ nanofibers and studied the influence of the temperature and heating rate on the thickness and grain size of the electrospun nanofibers [12]. Ultimately, they found that the WO₃ nanofibers calcined at 500 °C with a heating rate of 10 °C/min performed better in gas sensing. Shingange et al. prepared one-dimensional LaCoO₃ nanofibers by electrospinning

to detect ethanol gas [13]; their results showed a high response of 32.4 to 40 ppm ethanol at the optimal working temperature of 120 °C. This excellent ethanol sensing performance can be attributed to the interconnected porous nanofiber morphology.

In addition to controlling the morphology, forming oxide semiconductor composites is also an effective way to improve the sensing performance [14]. The modification of functional materials can take advantage of the synergistic effect of the two materials to obtain good sensing characteristics [15,16]. Liu et al. synthesized polyaniline-coated Rh-doped hollow SnO₂ nanotubes through electrospinning and in situ polymerization techniques [17]. At room temperature, the sensor had a response value of 13.6 to 100 ppm NH₃. In recent years, rare-earth elements have been used in gas sensors because of their unique characteristics, such as excellent oxygen storage capacity and abundant oxygen vacancy [18,19]. The surface modification of SnO₂ nanofibers through rare-earth elements can improve their sensitivity to the target gas [20]. As a typical n-type semiconductor, CeO₂ is recognized as a promising sensing material for the detection of liquefied petroleum gas, benefiting from the characteristics of its high thermal stability, tunable bandgap, and high diffusion coefficient for oxygen vacancies induced by reversible transition between Ce³⁺ and Ce⁴⁺ oxidation states [21,22]. Yoon et al. modified In₂O₃ by redox conversion between the valence states of CeO₂ to remove the hydroxyl groups on the surface of In₂O₃ to prepare an acetone gas sensor that was resistant to humidity interference [23].

In this study, tin dioxide (SnO₂) nanofibers and cerium dioxide (CeO₂) nanoparticles were prepared by electrospinning and hydrothermal methods, respectively. The composite of tin dioxide nanofibers decorated with cerium dioxide nanoparticles (SnO₂/CeO₂) was used as sensitive nanomaterial for the detection of liquefied petroleum gas (LPG). The nanostructure of the SnO₂/CeO₂ composite was characterized by a variety of methods, such as X-ray diffraction (XRD), X-ray photoelectron spectroscopy (XPS), scanning electron microscopy (SEM), and transmission electron microscopy (TEM). The characterization results verified the synthesis of tin dioxide nanofibers decorated with cerium dioxide nanoparticles. The as-prepared SnO₂/CeO₂ composite sensor showed a much higher response and shorter response time for LPG detection at room temperature, compared with that of the pure SnO₂ nanofibers. Furthermore, the SnO₂/CeO₂ composite sensor demonstrated higher resistance to humidity interference than the pure SnO₂ sensor, as proven by the comparative experiments for LPG detection. In this paper, the significantly enhanced sensing performance of the SnO₂/CeO₂ composite sensor for LPG can be attributed to the modification of CeO₂ to increase oxygen vacancies and form a heterostructure with SnO₂ nanofibers. Meanwhile, the LPG detection circuit was built to realize real-time concentration display and alarm for practical applications.

2. Experimental Section

2.1. Materials

Tin(II) dichloride dihydrate (SnCl₂·2H₂O), absolute ethanol (CH₃CH₂OH), N,N-dimethylformamide (DMF), polyvinylpyrrolidone (PVP, M_w = 1,300,000), cerium nitrate hexahydrate [Ce(NO₃)₃·6H₂O], ethylene glycol (EG), and glacial acetic acid (CH₃COOH) were obtained from Sinopharm Chemical Reagent Co. Ltd(Shanghai, China).

2.2. Material Synthesis and Sensor Fabrication

SnO₂ nanofibers were prepared by electrospinning. Firstly, under magnetic stirring at 25 °C for 30 min, 2 mmol of SnCl₂·2H₂O was dissolved in a mixed solution containing 5 mL of ethanol and 5 mL of DMF. Next, 1 g of PVP was added to the above solution, and stirring was continued at 50 °C for 5 h until a viscous transparent precursor solution was formed. Then, the precursor solution was transferred to a syringe connected to a spinneret with an inner diameter of 0.5 mm. During the electrospinning process, the voltage was 15 kV, and the distance between the positive electrode (needle) and the negative electrode (current collector) was 20 cm. The injection speed of the solution was maintained at 0.5 mL/h by using

a peristaltic pump. After electrospinning, the obtained samples were calcined in the air at 500 °C with a heating rate of 1 °C/min for 2 h to remove the organic polymer components.

CeO₂ nanoparticles were prepared via hydrothermal reaction. First, 1 g of Ce(NO₃)₃·6H₂O, 10 mL of deionized (DI) water, and 20 mL of EG were stirred at room temperature to be evenly mixed in a beater. During the stirring process, 1 mL of EG was added by dripping, and 0.8 g of PVP was slowly added into the mixed solution to be completely dissolved. The uniformly mixed solution was transferred to a 50 mL autoclave and treated at 180 °C for 22 h. After the reaction was completed and cooled to room temperature, the obtained powder was filtered, washed twice with ethanol and DI water by centrifugation, and dried at 50 °C to obtain the light gray precursor powder sample. Then, the precursor powder was calcined in a muffle furnace at 500 °C for 2 h to obtain a light yellow CeO₂ hollow sphere powder. For the sensor fabrication, SnO₂ nanofibers and CeO₂ hollow spheres were dispersed in DI water, and then they were spin-coated on an epoxy substrate with a pair of Cu/Ni interdigital electrodes to form a two-layer SnO₂/CeO₂ composite film, as shown in Figure 1. The molar ratio of the SnO₂/CeO₂ composite was determined to be 1:1, which was adopted in subsequent experiments, and the interfinger electrode was mainly composed of a printed circuit board and Cu/Ni electrode (length × width × height: 1 cm × 1 cm × 1 mm). The Cu/Ni electrode spacing and line width were 300 μm.

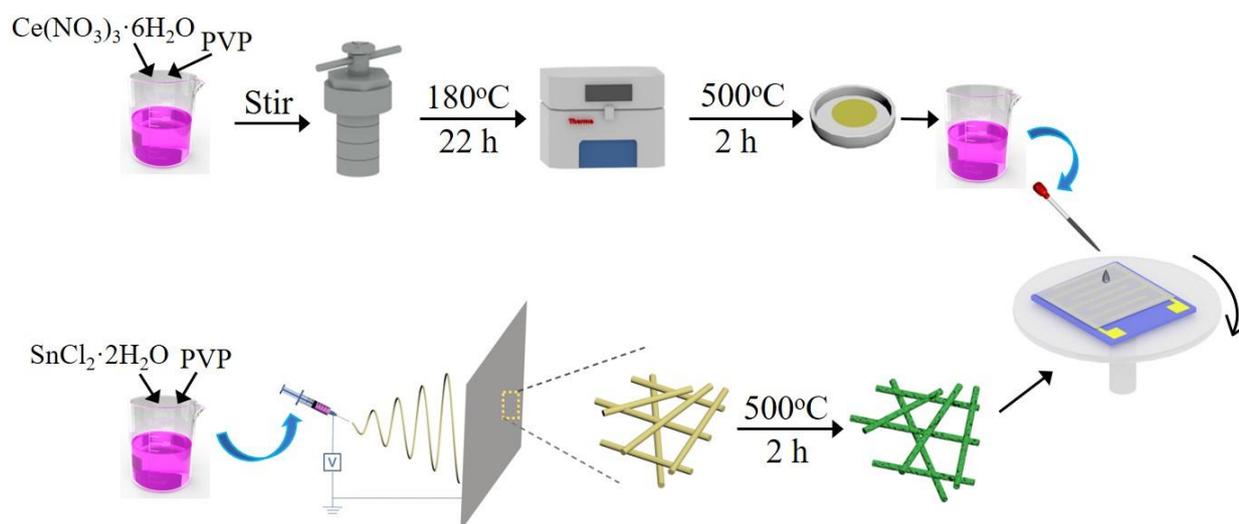


Figure 1. Schematic preparation process of the SnO₂/CeO₂ composite.

2.3. Gas-Sensing Experimental Setup

The temperature and relative humidity of the experimental environment in which the sensor was tested were 25 °C and 47% RH (relative humidity), respectively. The liquefied petroleum gas was composed of propane (25% ± 5%) and isobutane (75% ± 5%). The sensor was placed into a closed gas chamber, into which different volumes of LPG were injected. The Agilent 34470A was used to measure the output electrical signal of the sensor and record the resistance value, which changed with the concentration of the measured gas. The formula for calculating the sensor response value was $S = (R_a - R_g)/R_a \times 100\%$, where R_a is the resistance value of the sensor in air, while R_g is the resistance value of the sensor exposed to a certain concentration of liquefied petroleum gas.

3. Results and Discussion

3.1. Structure Characterization

A Rigaku D/Max 2500PC with Cu K α radiation was used to analyze the crystal planes of pure SnO₂, pure CeO₂, and SnO₂/CeO₂ composites. The X-ray diffraction patterns are shown in Figure 2a. The diffraction angles were scanned in the range of 10–80°. The XRD peaks of SnO₂ at 26.44°, 33.86°, 37.78°, 51.57°, 54.51°, 61.86°, 64.59°, 65.78°, 71.1°, and

78.73° corresponded to the (110), (101), (200), (211), (220), (310), (112), (301), (202), and (321) planes of the tetragonal phase SnO₂ (JCPDS 41-1445), respectively [24,25]. It can be seen from the XRD pattern of CeO₂ that the planes of (111), (200), (220), (311), (400), and (331) are located at 28.68°, 33.16°, 47.37°, 56.33°, 69.56°, and 76.77°, respectively, which is consistent with previous reports (JCPDS 34-0394) [26,27]. The characteristic peaks of CeO₂ and SnO₂ appear in the XRD patterns of the SnO₂/CeO₂ samples, indicating that the composites were successfully prepared.

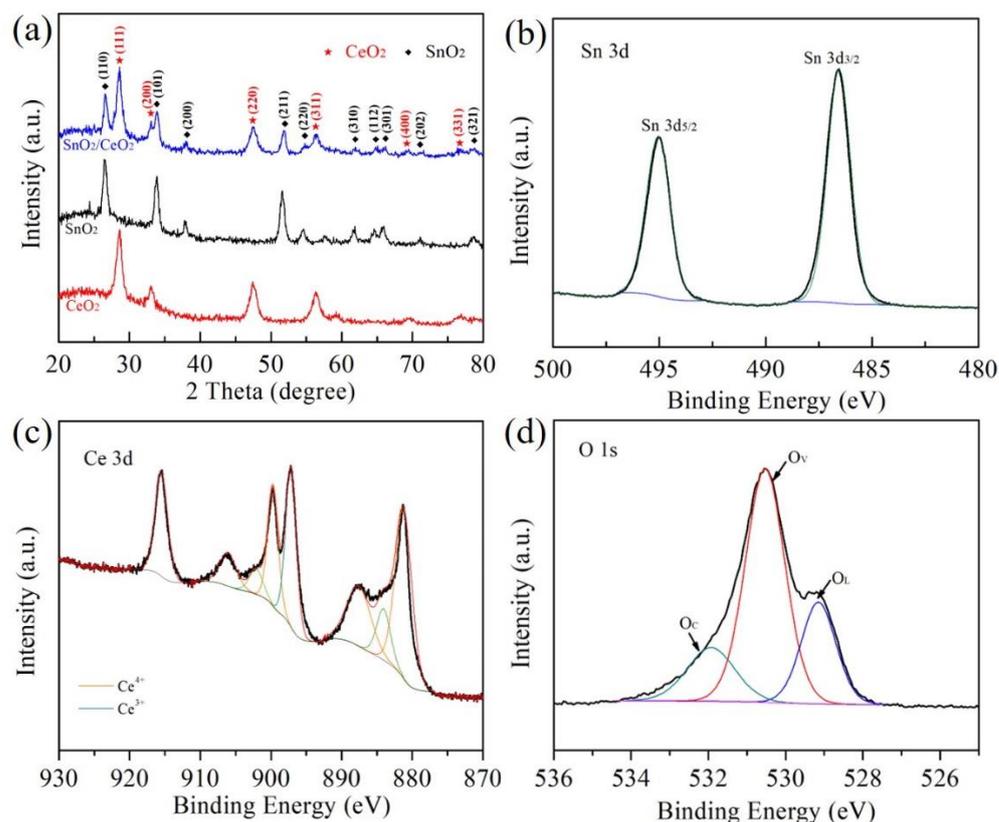


Figure 2. (a) XRD patterns of SnO₂ and SnO₂/CeO₂ composites. XPS spectra of the SnO₂/CeO₂ composite: (b) Sn 3d, (c) Ce 3d, and (d) O 1s.

The elemental composition and chemical state of the SnO₂/CeO₂ composite were further determined by X-ray photoelectron spectroscopy (XPS). Figure 2b shows the spectrum of Sn 3d. The characteristic peaks with binding energies of 486.60 eV and 495.05 eV are attributed to Sn 3d_{3/2} and Sn 3d_{5/2}, respectively [28]. The XPS analysis of Ce 3d is shown in Figure 2c. The peaks located at 881.15, 887.55, 899.75, 906.30, and 915.60 eV correspond to Ce⁴⁺ [29]. The characteristic peaks located at 884.20, 897.15, and 902.15 eV in the spectrum correspond to Ce³⁺, proving the multivalent state of cerium ions in CeO₂ [30]. The three characteristic peaks of the O 1s spectrum in Figure 2d can be attributed to lattice oxygen (O_L), vacancy oxygen (O_V), and adsorbed oxygen (O_C), according to the level of binding energy [31].

After 2 h of calcination at 500 °C, the morphology of single SnO₂ nanofibers was characterized by field-emission scanning electron microscopy (SEM, Hitachi S-4800), as shown in Figure 3a,b. The sample exhibited fibrous morphology, with a diameter of approximately 180 nm. These nanofibers were composed of many small nanoparticles. The network structure of the nanofibers facilitated the diffusion of gas from the surface of the sensing material to the interior. The SEM images of the SnO₂/CeO₂ composite are shown in Figure 3c,d. Compared with the individual SnO₂ nanofibers, agglomerated CeO₂

nanoparticles attached to the surface of SnO₂, indicating that the CeO₂ nanoparticles had successfully decorated the surface of the SnO₂ nanofibers.

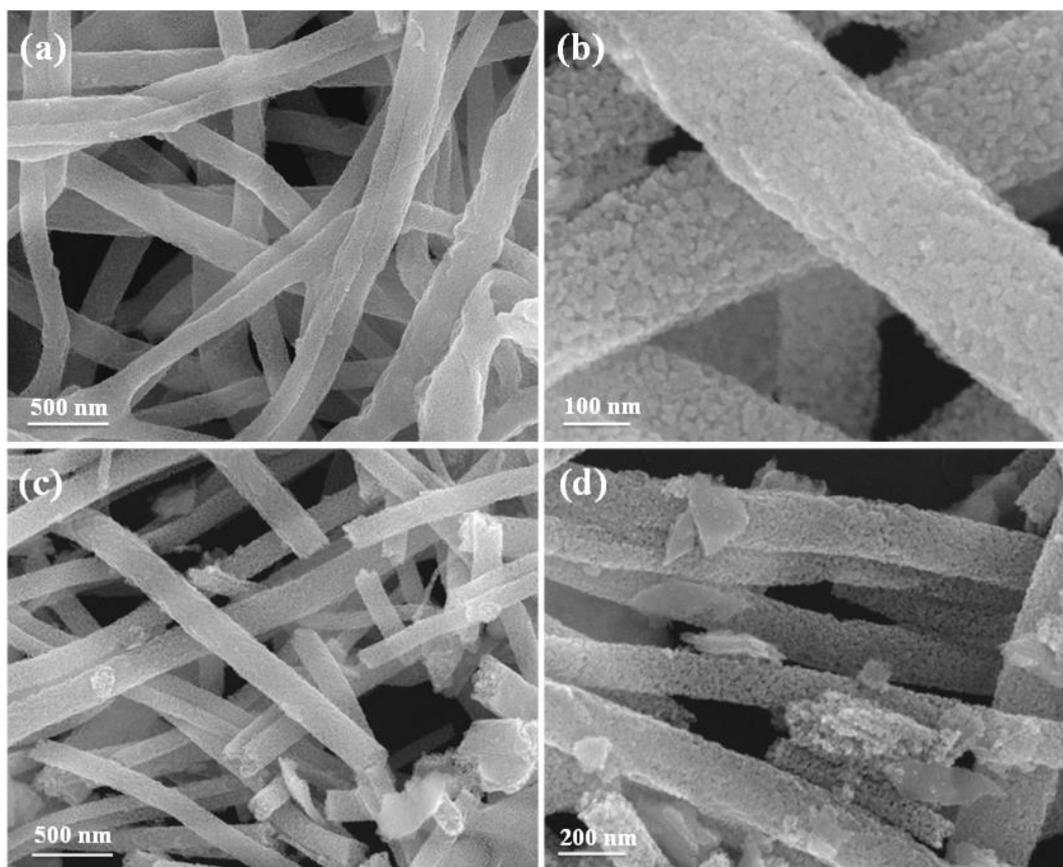


Figure 3. SEM images of (a,b) SnO₂ and (c,d) SnO₂/CeO₂ samples.

The structural characteristics of the SnO₂/CeO₂ composite were further observed by transmission electron microscopy (TEM, JEOL JEM-2100). TEM images of typical nanofibers are shown in Figure 4a,b. It can be seen from Figure 4b that the nanofibers are composed of many nanoparticles. As the calcination removes the polymer, there are pores between adjacent nanoparticles. The crystal lattice corresponding to the (110) plane and the (101) plane of SnO₂ can be seen in the inset of Figure 4b [32]. Figure 4c,d show granular CeO₂ with uniform size distribution. In the TEM images of the SnO₂/CeO₂ composite shown in Figure 4e, the CeO₂ nanoparticles are attached to the surface of the SnO₂ nanofibers. Figure 4f shows a high-resolution image of the SnO₂/CeO₂ composite, which displays the presence of SnO₂ and CeO₂ lattices. The interplanar spacings of 0.33 and 0.31 nm correspond to the spacings of the (110) plane of tetragonal SnO₂ and the (111) plane of CeO₂, respectively [33,34].

3.2. LPG Sensing Properties

The effect of CeO₂ modification on the LPG sensing performance of SnO₂ was investigated. Figure 5a,b show the dynamic response curves of the single SnO₂ sensor and the SnO₂/CeO₂ composite sensor, respectively, toward concentrations of LPG ranging from 500 to 5000 ppm at room temperature. With the increase in the LPG concentration, the responses of both sensors exhibit an upward trend, and it is clear that the sensor based on SnO₂/CeO₂ has a higher response value, which is twice that of the individual SnO₂ sensor. The fitting curves of the response value vs. the concentration are shown in Figure 5c, which can be expressed as $Y = 4.4220x^{0.2034} - 11.5169$ and $Y = 1.7377x^{0.3709} - 10.6888$, respectively. The regression coefficient (R^2) of the SnO₂/CeO₂ composite sensor is 0.98, indicating that

the fitting equation can adequately reflect the relationship between the concentration and the sensor response. Figure 5d shows the response–recovery curves of the SnO₂ sensor and SnO₂/CeO₂ sensor to 2000 ppm LPG. The response time of the SnO₂/CeO₂ sensor (45 s) is shorter than that of the SnO₂ sensor (78 s). However, the recovery time of the SnO₂/CeO₂ sensor is long, indicating that the LPG adsorbed on the surface of the material desorbs slowly in the air. Reasonable solutions should be sought in subsequent research.

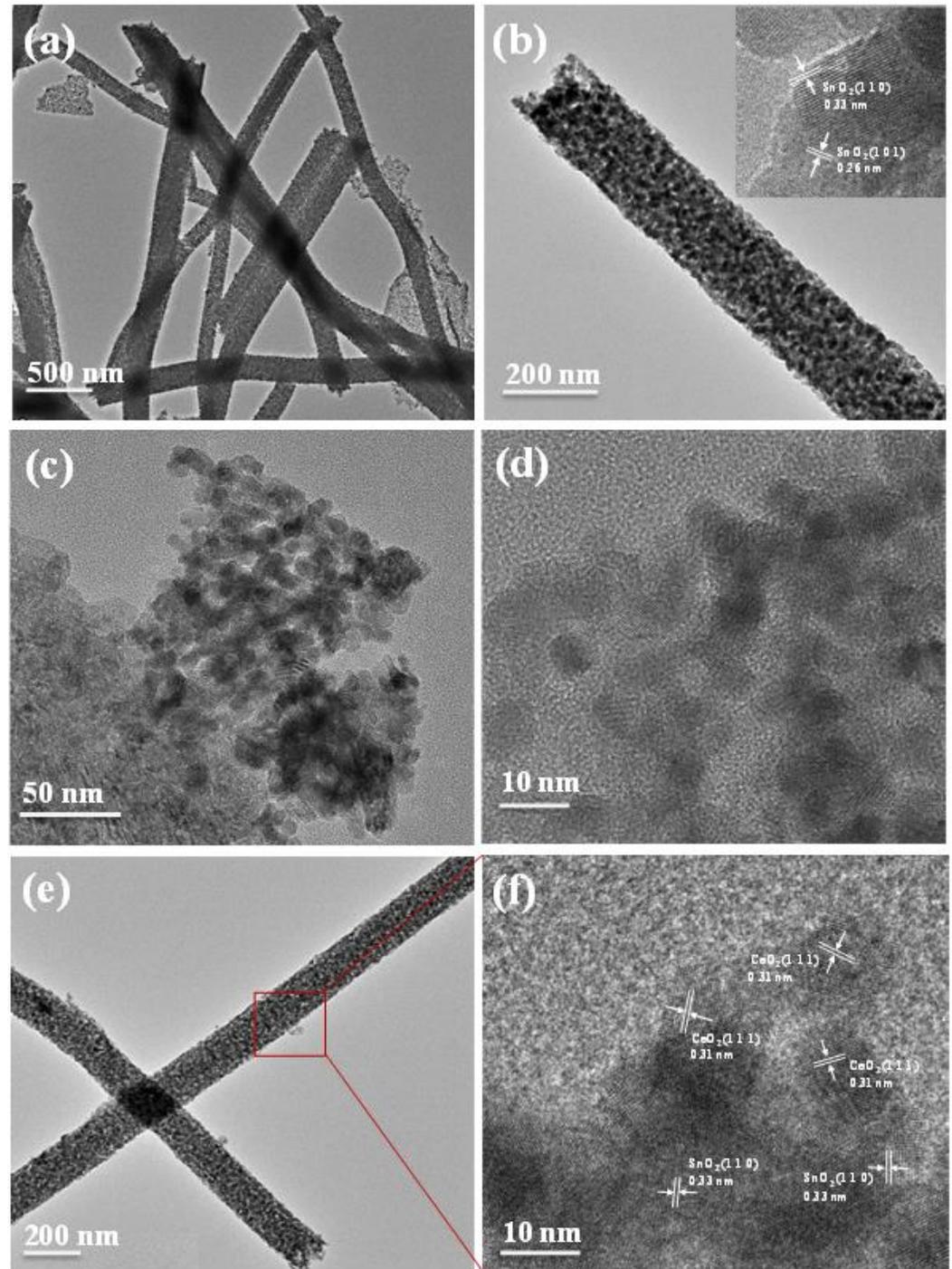


Figure 4. TEM micrographs of (a,b) SnO₂, (c,d) CeO₂, and (e,f) SnO₂/CeO₂.

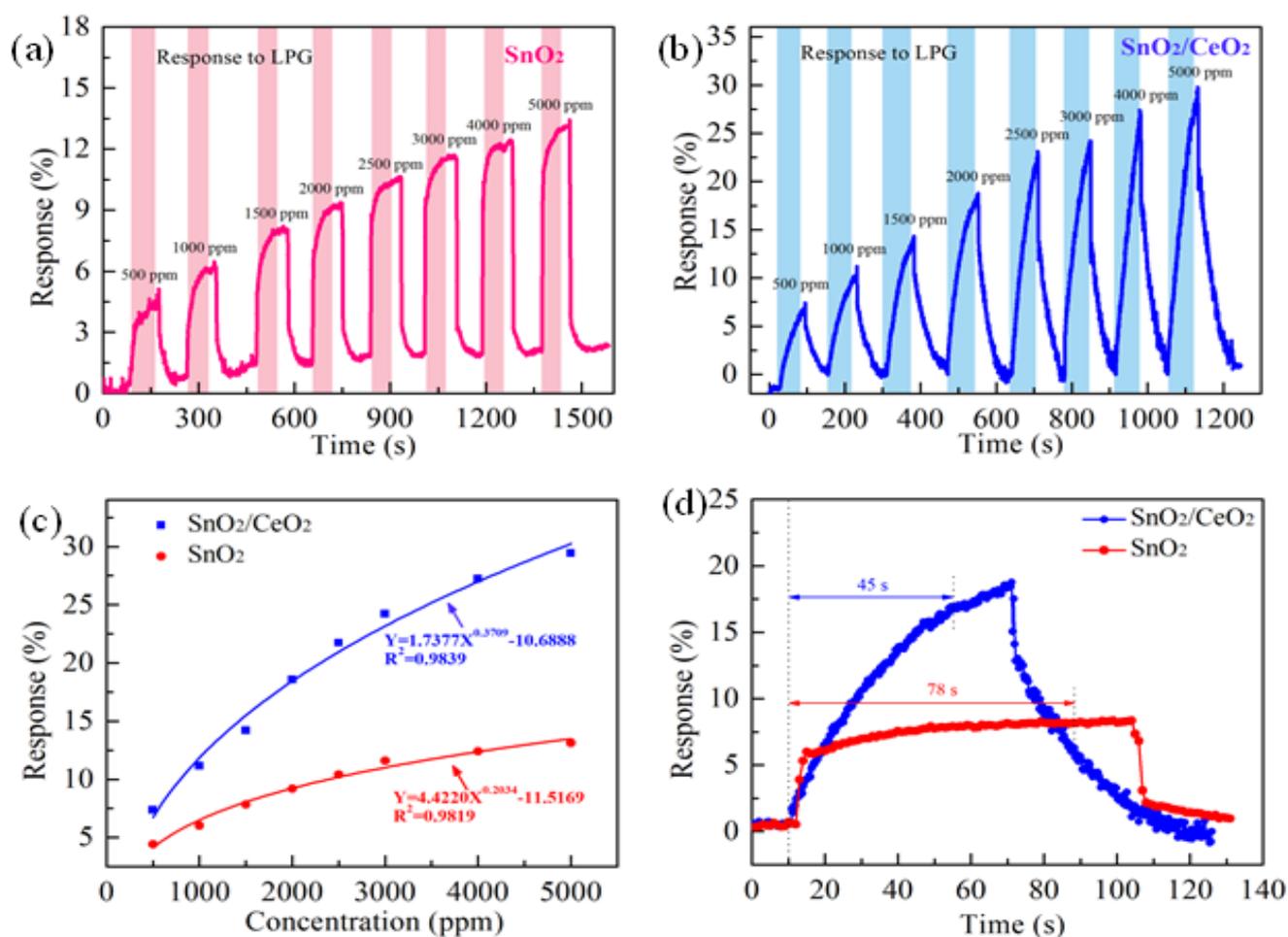


Figure 5. Responses of sensors based on (a) pure SnO₂ and (b) SnO₂/CeO₂ nanocomposite versus LPG concentration in the range of 500–5000 ppm. (c) Response vs. concentration of LPG. (d) Single transient response of pure SnO₂ and SnO₂/CeO₂ nanocomposite.

The response time and recovery time of the SnO₂/CeO₂ sensor at different concentrations are shown in Figure 6a. Figure 6b shows the I–V characteristic curves of the SnO₂ sensor and the SnO₂/CeO₂ sensor. Compared with the pure SnO₂ sensor, the forward current and reverse current of the SnO₂/CeO₂ composite sensor are asymmetric, and the curve is nonlinear, indicating that the SnO₂/CeO₂ sensor has a heterogeneous structure. We can see from the repeatability measurements shown in Figure 6c that the response value did not change significantly in the three test cycles with gas concentrations of 1000 ppm and 3000 ppm. Figure 6d shows the long-term stability results of the SnO₂/CeO₂ sensor. The response of the sensor at 2000 ppm was tested for a month. The fluctuation was small, indicating that the SnO₂/CeO₂ sensor has good commercial potential.

Furthermore, we considered the influence of humidity on gas detection. Figure 7a shows that as the humidity increases, the resistance of the SnO₂ sensor and the SnO₂/CeO₂ sensor will decrease. Figure 7b shows a comparison chart of the ratio of R_{a-wet} to R_{a-dry} of the SnO₂ sensor and SnO₂/CeO₂ sensor. To explore the ability of the sensor to resist the influence of humidity, we switched the sensor in the air environment with a given humidity to a gas environment with the same humidity. Figure 7c plots the response values of the SnO₂/CeO₂ composite sensor to 500 ppm, 1000 ppm, and 2000 ppm LPG under different levels of humidity. Figure 7d shows a comparison chart of the ratio of S_{wet} to S_{dry} of the SnO₂ sensor and the SnO₂/CeO₂ sensor. The ability of the SnO₂/CeO₂ sensor to resist the influence of humidity was more effective than that of the single SnO₂ sensor.

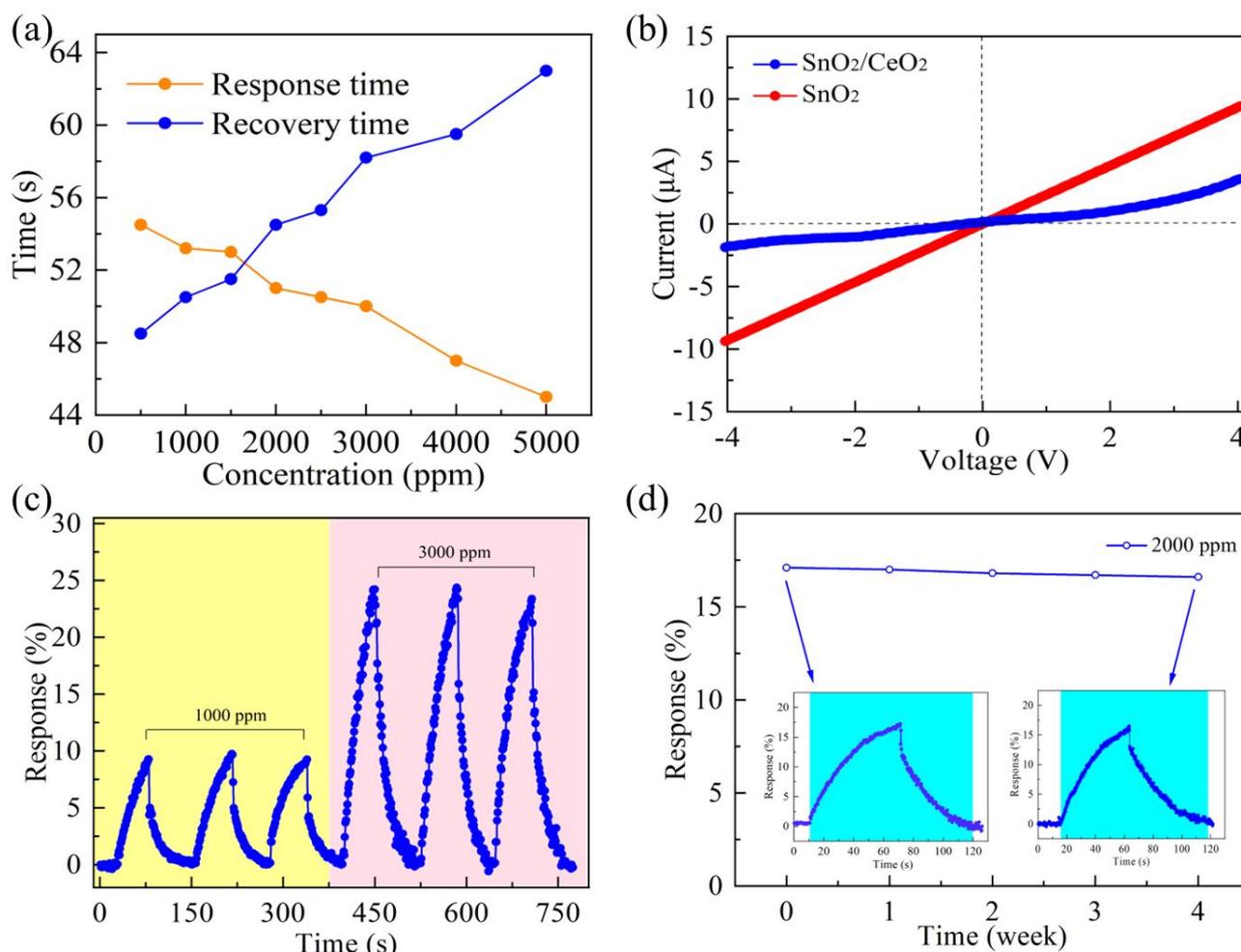


Figure 6. (a) Response vs. recovery time of the SnO₂/CeO₂ composite sensor. (b) Current–voltage curves of the SnO₂ and SnO₂/CeO₂ composite sensors. (c) Reproducibility of the SnO₂/CeO₂ sensor toward 1000 and 3000 ppm LPG. (d) Long-term stability of the SnO₂/CeO₂ composite sensor upon exposure to 2000 ppm LPG.

A real-time gas detection circuit was built by using the microcontroller to apply the SnO₂/CeO₂ gas sensor for the detection of LPG. A TL431 chip was used to generate a steady voltage as reference for the bleeder circuit and the analog/digital converter chip of the TLC549. The output voltage of the sensor was amplified after the voltage follower and filtering circuit, and then it was converted to a digital signal by using the TLC54, as shown in Figure 8. The terminal realizes real-time detection and concentration visualization of LPG through an LCD display. When the concentration exceeds the safe value, an alarm prompt appears immediately on the display interface, and the buzzer begins to sound. This provides a feasible scheme for the safety monitoring of LPG and promotes the development of industrial safety.

3.3. LPG Sensing Mechanism

The sensing performance of the semiconductor gas sensor is related to the oxygen-adsorption capacity of the gas-sensitive film [35,36]. The electronic gain and loss of oxygen leads to the transfer of electrons in the sensitive film, changing the output electrical parameters of the sensor. As shown in Figure 9a, the oxygen molecules adsorbed on the surface of the SnO₂/CeO₂ composite can capture electrons from the conduction band and form oxygen ions on the surface of the material, resulting in a decrease in the electron concentration [37]. When the SnO₂/CeO₂ sensor is exposed to LPG, the adsorbed oxygen

ions react with propane molecules and isobutane molecules to release electrons to the conduction band of the material, as shown in Figure 9b [38]. Therefore, the conductivity of the SnO₂/CeO₂ gas sensor will increase, resulting in a decrease in the sensor's resistance.

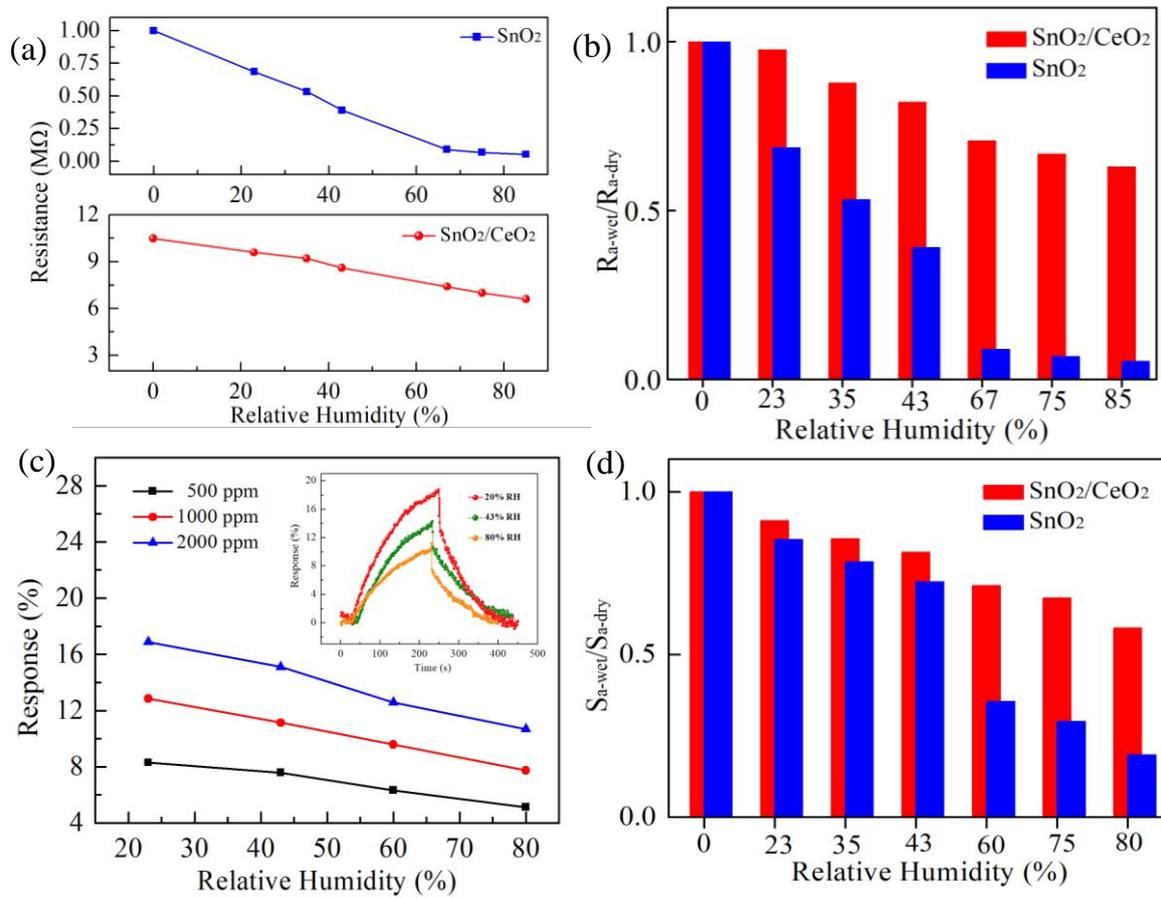


Figure 7. (a) The effect of relative humidity on the base resistance of the SnO₂ and SnO₂/CeO₂ composite, and (b) the R_{a-wet}/R_{a-dry} values of the SnO₂ and SnO₂/CeO₂ composite. (c) The effect of relative humidity on the response of the SnO₂/CeO₂ composite, and (d) the S_{a-wet}/S_{a-dry} values of the SnO₂/CeO₂ composite.

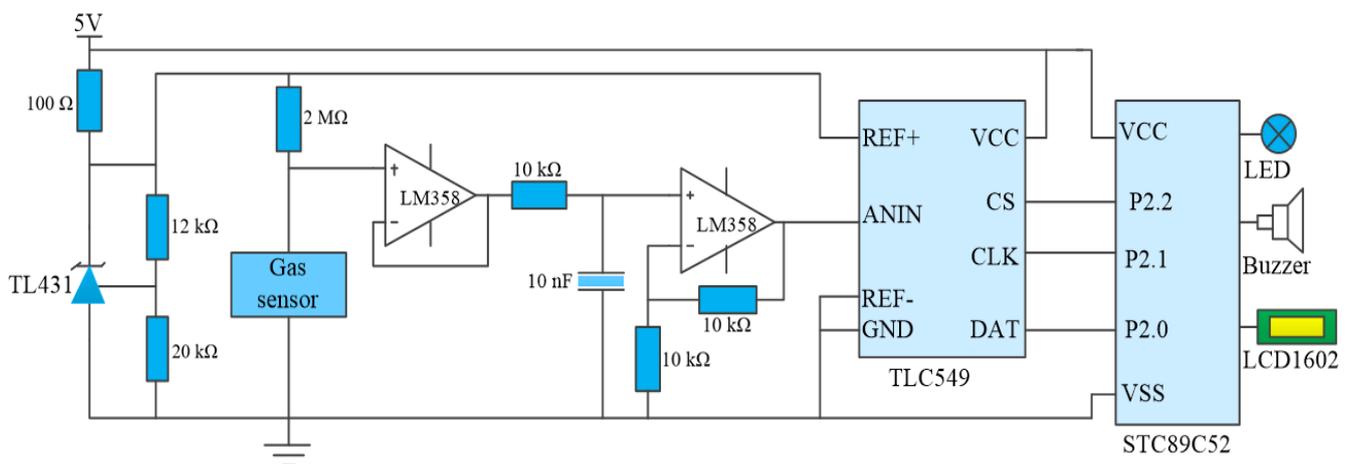


Figure 8. Block diagram of the integrated circuit alarm system.

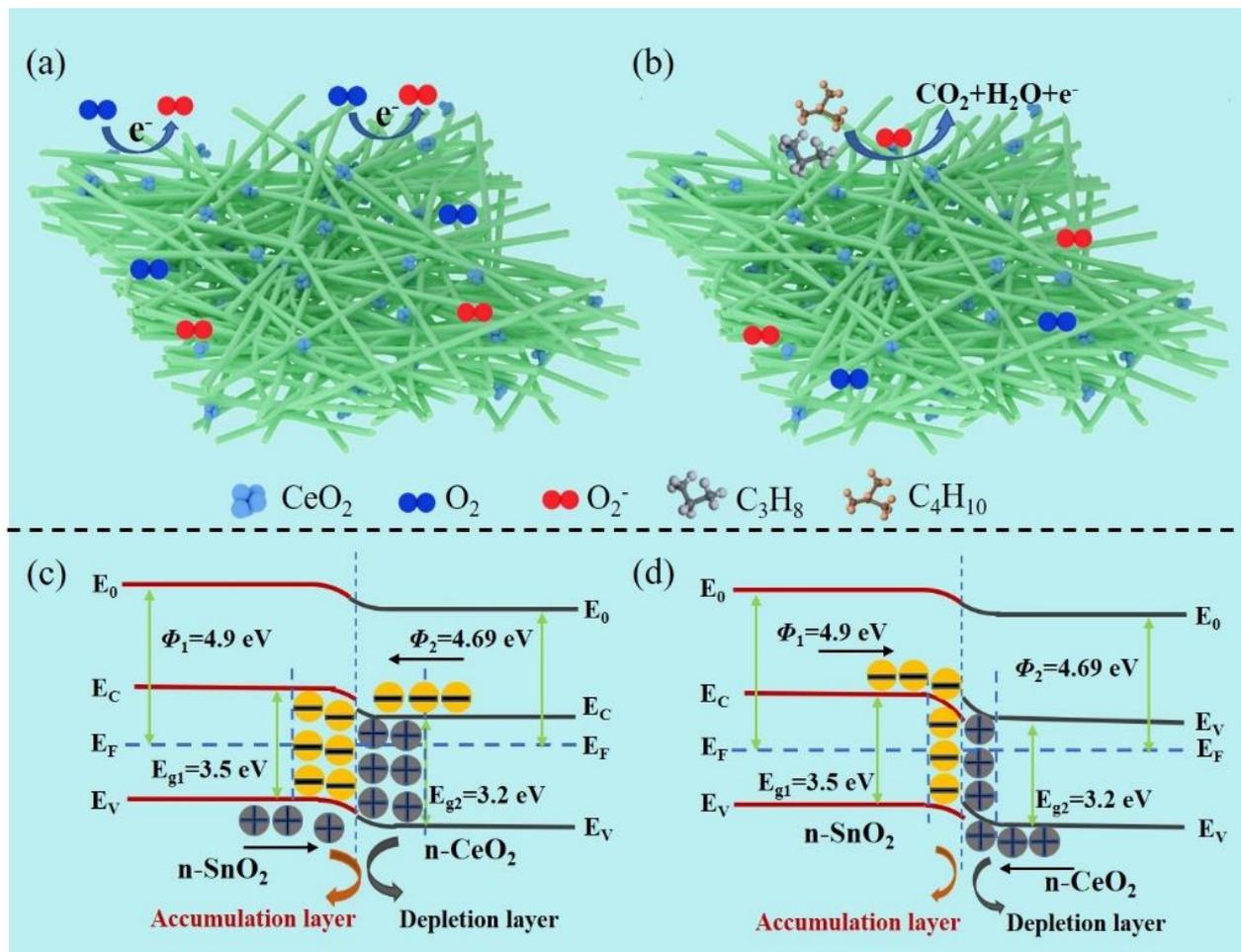
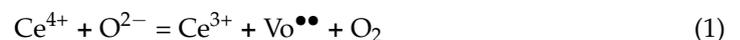


Figure 9. Schematic of the LPG sensing mechanism for the SnO₂/CeO₂ sensor exposed to (a) air and (b) LPG. Energy band structure diagrams of the SnO₂/CeO₂ composite in (c) air and (d) LPG atmospheres.

The enhanced response of the SnO₂ sensor modified with CeO₂ may be attributed to the following reasons: First, a heterojunction is formed between CeO₂ and SnO₂. Since the work function of CeO₂ is 4.69 eV—less than the 4.9 eV of SnO₂—the electrons will migrate from CeO₂ to SnO₂, forming an electron depletion layer at the CeO₂ interface and an electron accumulation layer at the SnO₂ interface, as shown in Figure 9c [39,40]. The formation of the heterojunction leads to an increase in chemically adsorbed oxygen and the capture of more electrons [41,42]. Compared with pure SnO₂, the formation of the higher barrier between the two semiconductor oxides leads to an increase in the base resistance value. When the SnO₂/CeO₂ gas sensor is transferred to the LPG atmosphere, more electrons captured by the oxygen are released back into the conduction band [43]. As the electron concentration becomes higher, the balance of the Fermi level of the composite is destroyed. Some electrons are injected into CeO₂ from SnO₂, resulting in a decrease in the barrier height, as shown in Figure 9d [44].

Secondly, the XPS characterization results show that Ce³⁺ and Ce⁴⁺ coexist in the SnO₂/CeO₂ composite. Some studies report that the redox reaction between Ce⁴⁺ and Ce³⁺ in CeO₂ can generate oxygen defects. The reaction equation is as follows [45–48]:



where Vo^{••} represents the oxygen vacancy with two negative charges as the electron donor. Increased oxygen vacancies in composites modified with CeO₂ induce stronger oxygen adsorption and lead to enhanced gas sensitivity [49–51].

Thirdly, cerium oxide is widely used in automobile exhaust catalysts because it has good stability. It can absorb and release oxygen under oxidation and reduction reactions, allowing more electrons to be easily captured and released from the conduction band, which leads to a higher response [52].

4. Conclusions

In conclusion, the SnO₂/CeO₂ composite was fully characterized for the preparation of LPG sensors. The gas-sensing properties of the SnO₂/CeO₂ sensor were investigated for LPG detection at room temperature. The SnO₂/CeO₂ composite sensor showed a much higher response and shorter response time for LPG sensing after doping with CeO₂ nanoparticles. In addition, the SnO₂/CeO₂ composite sensor had higher resistance to humidity interference than the pure SnO₂ sensor. The enhanced gas-sensing performance of SnO₂/CeO₂ composites can be attributed to the fact that CeO₂, with abundant oxygen vacancies, provides more active sites for gas sensing and the formation of heterostructures between SnO₂ and CeO₂.

Author Contributions: Conceptualization, D.Z. and X.L.; methodology, D.Z.; validation, J.Z., H.Z. and X.L.; formal analysis, C.C.; investigation, J.Z.; data curation, J.Z.; writing—original draft preparation, J.Z.; writing—review and editing, D.Z. and X.L. All authors have read and agreed to the published version of the manuscript.

Funding: This work was supported by the National Natural Science Foundation of China (51777215) and the Original Innovation Special Project of Science and Technology Plan of Qingdao West Coast New Area (2020-85).

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: Not applicable.

Conflicts of Interest: The authors declare no competing financial interests.

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