



# Article Determination of UV Filters in Waste Sludge Using QuEChERS Method Followed by In-Port Derivatization Coupled with GC–MS/MS

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**Abstract:** UV filters (UVFs) are widely used in personal care and in industrial products for protection against photodegradation. In recent years, their potential toxicological and environmental effects have received growing attention. Due to their excessive use, their residue levels in the environment are gradually increasing and they tend to accumulate on biological wastewater treatment sludge. The utilization of sludge as fertilizer could be one of the main routes of UVF contamination in the environment. Therefore, the development of a reliable and sensitive method of analyzing their trace level residues in waste sludge samples is of great importance. The success of the method largely depends on the sample preparation technique in such complex matrices. This study presents a rapid, sensitive and green analysis method for eight UVFs in sludge samples, selected for their rather low no-observed-effect concentrations (NOEC). For this purpose, the QuEChERS methodology was coupled with in-port derivatization for subsequent detection of the targeted UVFs via GC–MS/MS. The analysis time was substantially shortened using this method, and reagent utilization was also reduced. The method was validated in the sludge samples, and high recovery (66–123%) and low RSD values (<25.6%) were obtained. In addition, major contributing uncertainty sources and expanded uncertainties were determined.

Keywords: UVFs; QuEChERS; in-port derivatization; waste sludge

## 1. Introduction

UVFs are the general name for the chemical group that absorbs ultraviolet light, through which the adverse effects of UV light are eliminated. UVFs can be grouped as inorganic, such as TiO<sub>2</sub> or ZnO [1], and organic, mostly used in personal care products, as well as in plastics, automobile paints and rubber industries to increase resistance towards UV light degradation [2]. These compounds can reach to water bodies through industrial and domestic effluents. Since their utilization in personal care products and industrial applications are widespread, the UVF residue levels in the environment are increasing extensively [3].

Organic UVFs are a wide range of compounds that differ in their structures and properties. These highly persistent compounds in the environment tend to accumulate in water [3–5], suspended particles, soil [6], sediment [7] and sludges [8–10]. Organic UVFs can also accumulate in biota and disrupt the endocrine systems of aquatic organisms by increasing their estrogen-induced cell proliferation [11]. It has been clearly stated that UVFs affect different hormonal targets as well as estrogenic activity in mammals and fish, and are therefore known as endocrine-disrupting chemicals (EDCs) [12,13]. Consequently, one of these compounds has recently been included in the Watch List by The European Water Framework Directive as a future priority pollutant [14]. Although the use of these compounds in cosmetics is legally restricted [15], there is no limit to their concentration in water and sewage sludge matrices. However, studies on the presence of UVFs in waste



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**Copyright:** © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). sludge have revealed that their concentration range from a few to thousands of  $\mu g/g$  in dry mass [16]. The use of this sludge as fertilizer is another concern due to the widespread distribution of UVF residues in agricultural soils and the possible contamination of crops.

Since their concentrations are very low, an appropriate preparation technique must be applied to the samples to isolate and preconcentrate these filters. Current trends in the determination of organic UVFs in environmental water samples based on microextraction techniques have been reviewed [3,17,18]. However, their determination in sludge samples faces difficulties due to the complexity of the matrices and their impact on the environment. To date, one of the techniques used for UVF extraction from sewage sludge comprises liquid–liquid extraction (LLE) followed by solid-phase extraction (SPE) [19–22] where the excessive use of solvent is the main drawback of the method. The other technique is pressurized liquid extraction (PLE), applied alone or coupled with SPE [23–29] or gel permeation chromatography (GPC) [30]. Despite the advantage of using a smaller solvent volume in the PLE technique, special equipment is required to conduct this method.

In the last few decades, method development studies have been devoted to modern sample preparation techniques based on shorter analytical periods and the minimization of organic solvent utilization for a wide range of pollutants. One of these modern techniques, called QuEChERS (which is an acronymic for quick, easy, cheap, effective, rugged and safe) has been well-established to improve laboratory efficiency and throughput. The main advantage of this method is its small quantities of solvent utilization. The method has already been tested for UVFs in human milk [31] and seafood samples [32], followed by liquid chromatography systems coupled with mass detectors (LC-MS) and sludge samples, and then, by detection using gas chromatography (GC–MS) [16,21–23]. LC-MS systems are preferred for the analysis of polar UVFs, and no derivatization step is required in accordance with the physicochemical properties of UVFs [33–36]. GC–MS has been used for rather non-polar and volatile UV filters. Although the GC method provides high separation efficiency, high selectivity and good sensitivity, it displays some disadvantages such as the derivatization step, in which more reagents, greater reaction time and more labor are required. Fortunately, the in-port derivatization technique is a practical and environmentally friendly solution to these issues wherein the reaction takes place in the injection block rather than in an off-line interaction. The analysis time can be substantially reduced using this method and the selectivity can be improved since the technique enables extra purification for the matrix effect.

In the present study, we aimed to detect eight UVFs in sludge samples. Benzophenone-3 (BP-3), 3-benzylidene camphor (3BC), 2-ethyl hexyl-4-(dimethyl amino) benzoate (EDP), 2-ethyl-hexyl-4-trimethoxy cinnamate (EHMC), ethylhexyl salicylate (EHS), homosalate (HMS), isoamyl p-methoxycinnamate (IAMC) and 4-methylbenzylidene camphor (4-MBC) were selected according to their no-observed-effect concentration (NOEC) values. Their chemical structures and NOEC limits are presented in Table 1. Considering the hydrophobicity (logK<sub>ow</sub>: 3.79–6.16) of the analytes, the QuEChERS method was adopted; however, due to the low volatility of these analytes along with their weak acidity (pK<sub>a</sub>: 7.56–8.13), the analytes were derivatized using an in-port silylation technique prior to subsequent quantification using the GC–MS/MS system. To the best of our knowledge, this is the first report in the literature about the combination of QuEChERS with in-port derivatization followed by GC–MS/MS for a wide variety of UVF analyses in waste sludge. This method extensively decreases solvent or chemical consumption and shortens the analysis time compared to off-line derivatization. The method validation parameters, major contributing uncertainty sources and expanded uncertainties were determined.



## 2. Materials and Method

## 2.1. Reagents and Standard Solutions

The chemical standards of 2-ethylhexyl salicylate (EHS), 2-hydroxy-4-methoxybenzophenone (benzophenone-3, BP-3) >98%, 3,3,5-trimethylciclohexylsalicylate (homosalate, HMS) >98%, 4-methylbenzylidene camphor (4-MBC) 99%, 2-ethyl-hexyl-4-trimethoxy cinnamate (EHMC) 99%, and 2-ethyl hexyl-4-(dimethylamino) benzoate (EDP) 99% were obtained from Dr. Ehrenstorfer (Augsburg, Germany). 3-benzylidene camphor (3BC) 99%, isoamyl p-methoxycinnamate (IAMC) and % were acquired from Sigma-Aldrich (St. Louis, MO, USA), Toronto Research Chemicals (Toronto, ON, Canada) and Chemservice (West Chester, PA, USA), respectively.

LC-MS-grade methanol and acetonitrile, GC–MS-grade ethyl acetate (EtAC) and acetone, sodium chloride, sodium sulfate and orthophosphoric acid were purchased from Merck (Darmstadt, Germany). Bis(trimethylsilyl) trifluoroacetamide with 1% trimethylchlorosilane (BSTFA + TMCS; 99:1, v/v) from Macherey-Nagel was used as derivatization reagent. This reagent was stable for only 3 h during analysis. 2-dodecanol, 2-dodecanone, and 1-undecanol

from Sigma were used as extraction solvents. Anhydrous magnesium sulphate (MgSO<sub>4</sub>), primary and secondary amine exchange bonded silica sorbent (PSA) and octadecylsilan (C18) were obtained from Supelco (Bellefonte, PA, USA) for the extraction step.

The stock solutions of individual UVFs (1000  $\mu$ g mL<sup>-1</sup>) and mixtures of UVFs (50  $\mu$ g mL<sup>-1</sup>) were prepared in ethyl acetate to optimize the injection port derivatization conditions in methanol to validate the QuEChERS method. These solutions of 1000  $\mu$ g mL<sup>-1</sup> and 50  $\mu$ g mL<sup>-1</sup> were stable for about 5 months and five days at -20 °C, respectively. The working aqueous solutions were prepared daily from standards in methanol at different concentrations using ultrapure water and environmental water. The sludge samples were collected from a domestic wastewater treatment plant in Izmir, Turkey. Sludges were air-dried and stored in the dark at -20 °C until analysis.

## 2.2. Sample Extraction

The procedure for extracting UVFs from sludge is a modified version of the method reported previously [16]. As shown in Figure 1, a 0.5 g sewage sludge sample was dried at room temperature and a spiked sample was transferred into a conical-bottom 15 mL polypropylene tube containing 10 mL of ACN, vortexed for 2.5 min, and then, left in an ultrasonic bath (J.P. Selecta, Barcelona, Spain) for 15 min. Then, the organic phase was separated via centrifugation at 3500 rpm for 15 min and transferred to a conical-bottom 15 mL polypropylene tube containing 500 mg MgSO<sub>4</sub>, 410 mg C18 and 315 mg PSA. The extract was then vortexed for 2.5 min and centrifuged for 15 min. After the supernatant was transferred to a 10 mL tube, it was evaporated to dryness under  $N_2$  gas. Then, the extract was dissolved in 1000  $\mu$ L EtAC, instead of hexane as performed by Ramos et al. [16], for the in-port derivatization step as previously applied to a surface water sample by our research group [37]. The extract dissolved in EtAC was filtered through a 13 mm, 0.22  $\mu$ m PTFE filter, and then, it was transferred to a 1.5 mL amber vial. Finally, 2 µL of BSTFA and 2  $\mu$ L of extract were derivatized in the injection port using the sandwich technique. In this technique, two aliquots of 2  $\mu$ L BSTFA and 2  $\mu$ L extract in EtAc, separated with an air gap, are drawn into the microsyringe of a PAL autosampler, and then, injected to the GC-MS/MS system.



Figure 1. Schematic illustration of the whole procedure.

## 2.3. GC–MS/MS Analysis

GC–MS/MS analysis was performed using an Agilent 7890 B gas chromatograph coupled with a triple quadrupole mass spectrometer (MS 7000C) and a PAL autosampler (GC Sampler 80). For derivatization, the injection port temperature was held at 70 °C for 3 min, then, increased to 300 °C at a rate of 400 °C min<sup>-1</sup> in splitless mode with a purge-off time of 4.5 min. The oven temperature started at 70 °C for 4 min, increased to 180 °C at 25 °C min<sup>-1</sup>, then, increased to 230 °C at a rate of 5 °C min<sup>-1</sup> and to 300 °C at a rate of 25 °C min<sup>-1</sup>; it was held for 10 min at this temperature. The injector was operated using programmed temperature evaporation (PTV).

Separation was performed on 5% phenyl-arylene/95%-dimethylpolysiloxane HP-5MS ( $30 \text{ m} \times 0.25 \text{ mm}$  i.d. 0.25 µm film thickness) supplied by Phenomenex (Torrance, CA, USA). Helium (99.999% purity) was used as the carrier gas at a constant flow of 1 mL min<sup>-1</sup>. In MS/MS analysis, the temperatures of the ion source and the transfer line were 280 and 300 °C, respectively. The multiple reaction monitoring (MRM) technique was applied, and electron ionization (EI) mode was used. The retention times (R<sub>t</sub>) obtained, the optimized MRM transitions and the collision energies (CE) for each UVF are given in Table 2. The bold parent and product ions in the table show the quantification transitions.

| UVFs   | R <sub>t</sub><br>(min) | MW<br>(g mol <sup>-1</sup> ) | Parent Ions<br>( <i>m</i> / <i>z</i> ) | Product Ions<br>( <i>m</i> / <i>z</i> ) | CE<br>(eV) |
|--------|-------------------------|------------------------------|--|---|------------|
|        |                         |                              |  | 149.2                                   | 5          |
| 3-BC   | 14.443                  | 240.35                       | 240.0                                  | 225.1                                   | 9          |
|        |                         |                              |  | 92.10                                   | 12         |
|        |                         |                              |  | 177.0                                   | 15         |
| EHS    | 14.452                  | 250.34                       | 195.0                                  | 159.0                                   | 25         |
|        |                         |                              |  | 75.00                                   | 30         |
|        |                         |                              |  | 177.0                                   | 15         |
| HMS    | 15.610                  | 262.36                       | 195.0                                  | 159.0                                   | 25         |
|        |                         |                              |  | 75.00                                   | 27         |
| IAMC   | 15 727                  | 248 22                       | 178.1                                  | 161.1                                   | 15         |
| IAIVIC | 15.757                  | 240.32                       | 161.0                                  | 161.0 133.0                             | 10         |
| 4 MBC  | 16 120                  | 254.27                       | 254.0                                  | 239.0                                   | 15         |
| 4-MDC  | 10.120                  | 234.37                       | 254.0                                  | 105.0                                   | 25         |
| BP-3   | 16.527                  | 228.25                       | 285.0                                  | 242.0                                   | 25         |
|        |                         |                              | 277.0                                  | 164.9                                   | 10         |
| EDP    | 19.014                  | 277.41                       | 148.0                                  | 104.2                                   | 30         |
|        |                         |                              | 165.0                                  | 148.6                                   | 32         |
|        |                         |                              | 161.0                                  | 133.1                                   | 8          |
| EHMC   | 19.501                  | 290.41                       | 178.0                                  | 133.1                                   | 22         |
|        |                         |                              | 290.0                                  | 178.1                                   | 6          |

Table 2. Experimental GC-MS/MS parameters of UVFs.

#### 2.4. Validation Studies

The matrix match method was used for the calibration curves. In this method, the curves were constructed by subtracting the peak area values of the real sludge sample from the spiked extract and plotting against the concentration of the UV filter added into the real sludge sample.

The linear range, intra-day and inter-day repeatability, Limit of Detection (LOD), Limit of Quantitation (LOQ) and recovery parameters were determined, and measurement uncertainties of the method applied for UVFs were calculated. For the linearity of UVFs, sludge samples were spiked with 40, 80, 200, 600 and 1200 ng g<sup>-1</sup> UVF standards. The extracts were evaporated to dryness under nitrogen gas, and they were diluted to 1000  $\mu$ L using ethyl acetate. The LOQ and LOD were calculated according to S/N = 10 and S/N = 3, respectively. Intra-day and inter-day repeatability studies were performed at low (80 ng g<sup>-1</sup>), medium (300 ng g<sup>-1</sup>), and high (600 ng g<sup>-1</sup>) concentrations, with 3 replicates.

The selected test material was analyzed repeatedly under different conditions such as on different days, using different analysts and different equipment, etc. The total variation in the whole cluster can be represented as the combination of variances (s<sup>2</sup>) between ( $S_{between}$ ) and within groups ( $S_r$ ). The repeatability (intra-day) and intermediate precision (inter-day) values were calculated via ANOVA [38]. The standard deviation of  $S_r$  was calculated by taking the square root of the within-group mean square term, as shown in Equation (1), and the contribution of the grouping factor to the total variation was obtained from Equation (2). In Equations (1) and (2),  $MS_w$  is the within-group mean square term and  $MS_h$  is the between-group mean square term.

Then, intermediate precision  $(S_I)$  was calculated by combining the within-group and between-group variance components, as shown in Equation (3).

$$S_r = \sqrt{MS_w} \tag{1}$$

$$s_{between} = \sqrt{\frac{MS_b - MS_w}{n}} \tag{2}$$

$$S_I = \sqrt{S_r^2 + S_{between}^2} \tag{3}$$

The intra-day (n = 3) and inter-day (n = 2) relative standard deviations (RSD%) of the QuEChERS followed by GC–MS/MS were obtained using spiked solutions of the analytes at different concentration levels. According to the 2015/1787 directive, if the RSD% value of the applied method is less than 25%, the precision of this method is acceptable for organic compounds.

Recovery studies to determine the accuracy of the method were carried out by adding the UVF standards to the sewage sludge samples at concentrations of 80, 300 and 600 ng g<sup>-1</sup>. The recovery percentages were calculated from Equation (4) where, Cpre - Ext and Cpost - Ext are the concentrations of sludges in which analytes were added before and after extraction, respectively. *Csample* is the concentration of UVFs in sludges without the addition of the analyte.

$$Recovery \% = \frac{Cpre - Ext - Csample}{Cpost - Ext - Csample} \times 100$$
(4)

The measurement uncertainty is a parameter that was included with the measured result and characterizes the distribution of values that can correspond to the measurand. Knowing the uncertainty means increased confidence in the accuracy of the measurement result. This value is very important in comparing the measurement results of two different methods and deciding whether the results are within the defined limits. Measurement uncertainty consists of many components. Some of these components are derived from the statistical distribution of the results of repeated measurement series to obtain the standard deviations. Combined standard uncertainty (u(c)) is the standard uncertainty that considers contributions from all important uncertainty sources by combining the relevant uncertainty components, and it was calculated as shown in Equation (5). The expanded uncertainty provides the range of an analyte concentration believed to be spread at a higher confidence level. The expanded uncertainty (U) is calculated by multiplying the combined standard uncertainty by "k", which is equal to 2 at 95% confidence level [39]. In this study, the uncertainty sources were defined first; then, the uncertainty of each parameter was determined, and finally, the combined Uc(y) and expanded uncertainties (U) were calculated.

$$u(c) = \sqrt{u_{calibration}^2 + u_{SI}^2 + u_{Recovery}^2}$$
(5)

## 3. Results and Discussion

## 3.1. Optimization Studies

For the extraction of targeted UVFs from sludge samples, the QuEChERS methodology was adopted for the in-port derivatization and the extract obtained was dissolved in 1000  $\mu$ L ethyl acetate (EtAc) instead of hexane. In a previous study carried out in this lab, in-port derivatization conditions were optimized for a wide range of UVFs extracted from surface water via vortex-assisted dispersive liquid–liquid microextraction based on the solidified floating organic droplet (VA-DLLME-SFOD) technique. It was determined that the injection temperature was a statistically significant factor and the optimal temperature was determined to be 260 °C [37]. The effect of injection temperature for the studied UVFs in sludge samples was further studied to see any deviation from the optimal conditions determined. The temperature varied between 260–320 °C, and the peak areas are given in Figure 2.



Figure 2. The effect of injection temperature on peak areas of UVFs.

As can be deduced from the figure, even though the mean peak areas of the UVFs are not substantially different from each other for the studied injection temperatures, a slight decrease was observed for 300 °C. However, this injection temperature was chosen for further studies since the carry-over effect occurred in samples up to 290 °C. The sharp peaks in UVFs with injection port derivatization, after QuEChERS, of the spiked sludge sample were obtained, as shown in Figure 3.

## 3.2. Validation Studies

The linearity and linear range of a method should unequivocally be determined for any analytical method. It is a fact that the lowest concentration of the calibration curve should be very close to the LOQ value for the accurate analysis of analytes with known precision at an LOQ-level concentration. Table 3 depicts the linear equations for the working range of 40–1200 ng g<sup>-1</sup> with correlation coefficients close to unity ( $R^2 > 0.9970$ ).



**Figure 3.** Chromatograms of the UV filters in sewage sludge spiked with UVFs at 300 ng  $g^{-1}$ .

**Table 3.** Analytical merits of the GC–MS/MS method coupled with QuEChERS for UVF determination in sludge samples.

| Analyte     | a *    | b *     | <b>R</b> <sup>2</sup> | LOD (ng $g^{-1}$ ) | LOQ (ng g <sup>-1</sup> ) |
|-------------|--------|---------|-----------------------|--------------------|---------------------------|
| 3-BC        | 30.154 | -591.4  | 0.9991                | 10.1               | 39.6                      |
| EHS         | 888.02 | -23,900 | 0.9987                | 10.0               | 33.3                      |
| HMS         | 515.64 | -11,424 | 0.9984                | 9.90               | 33.0                      |
| IAMC        | 170.2  | -285.3  | 0.9996                | 9.50               | 31.8                      |
| 4-MBC       | 24.748 | -159.2  | 0.9997                | 8.00               | 26.7                      |
| BP-3        | 276.81 | -10,099 | 0.9980                | 4.30               | 14.1                      |
| EDP         | 214.00 | -1290   | 0.9996                | 12.1               | 40.2                      |
| EHMC        | 204.46 | -3367   | 0.9970                | 8.00               | 26.8                      |
| *V - ax + b |        |         |                       |                    |                           |

\* Y = ax + b.

LOQ is defined as the lowest concentration that can be measured with acceptable precision (20% RSD) and accuracy [40–45]. Three different methods are used to determine the LOQ value. The most common approach for LOQ calculation in chromatographic analysis is the signal-to-noise ratio (S/N) [45]. This ratio can be defined as the difference between the height of the analyte peak (signal) and the highest and lowest points of the baseline (noise) in each area around the signal. For LOQ, S/N usually needs to be at least equal to 10. In the second method, a specific calibration curve should be studied using samples containing an analyte in the range of the LOQ. The residual standard deviation of a regression line or the standard deviation of the y-intercepts of regression lines may be used as the standard deviation [39]. The third approach is the concentration corresponding to a response 10 times greater than the SD of the analysis at the minimum concentration [37,41,45].

The LOD and LOQ values were calculated based on the S/N = 3 approach and S/N = 10, respectively. The LOQ values calculated using this method were found to be in agreement with previous studies on the analysis of UVFs in sludge [17,24,26]. In-port derivatization provides lower detection limits by converting polar analytes to more volatile compounds, as reported earlier [46–48]. For most of the compounds, the LOQ is close to or less than the lowest concentration level of the calibration curve. The RSD% values obtained in this study are below 25% as seen in Table 4.

| UVFs - | Intra                 | -Day RSD% (a            | n = 3)                 | Inter-Day RSD% ( $n = 2$ ) |                         |                        |  |
|--------|-----------------------|-------------------------|------------------------|----------------------------|-------------------------|------------------------|--|
|        | 80 ng g <sup>-1</sup> | $300 \text{ ng g}^{-1}$ | 600 ng g <sup>-1</sup> | $80~ng~g^{-1}$             | $300 \text{ ng g}^{-1}$ | 600 ng g <sup>-1</sup> |  |
| 3-BC   | 4.3                   | 8.7                     | 3.2                    | 10.8                       | 9.1                     | 7.1                    |  |
| EHS    | 9.9                   | 9.7                     | 17.2                   | 10.9                       | 10.9                    | 19.3                   |  |
| HMS    | 13.1                  | 12.1                    | 21.9                   | 19.8                       | 13.7                    | 25.6                   |  |
| IAMC   | 5.2                   | 8.2                     | 3.4                    | 15.1                       | 17.9                    | 19.8                   |  |
| 4-MBC  | 4.0                   | 8.1                     | 3.2                    | 10.1                       | 10.7                    | 7.2                    |  |
| BP-3   | 16.2                  | 11.6                    | 13.6                   | 17.7                       | 13.7                    | 15.5                   |  |
| EDP    | 4.9                   | 11.2                    | 2.3                    | 15.0                       | 14.4                    | 15.4                   |  |
| EHMC   | 9.2                   | 12.9                    | 3.4                    | 22.6                       | 15.9                    | 18.8                   |  |

**Table 4.** Intra-day (n = 3) and inter-day (n = 2) relative standard deviations (RSD%) calculated for the UVFs.

The recoveries were in the range of 66%–23% as depicted in Table 5. Although, the recoveries are almost the same as the results obtained in other studies [17,24,26,31], our method provides certain advantages such as the lack of special apparatus and comparatively shorter analysis times.

|       | % Recovery $\pm$ RSD ( <i>n</i> = 3) |                        |                        |  |  |  |  |
|-------|--------------------------------------|------------------------|------------------------|--|--|--|--|
| UVFs  | 80 ng g <sup>-1</sup>                | 300 ng g <sup>-1</sup> | 600 ng g <sup>-1</sup> |  |  |  |  |
| 3-BC  | $115\pm4.49$                         | $93\pm10.1$            | $98\pm4.03$            |  |  |  |  |
| EHS   | $113\pm 6.83$                        | $98\pm10.2$            | $96\pm7.34$            |  |  |  |  |
| HMS   | $87\pm11.1$                          | $109 \pm 12.5$         | $104\pm25.8$           |  |  |  |  |
| IAMC  | $121\pm2.70$                         | $118\pm8.80$           | $113\pm4.70$           |  |  |  |  |
| 4-MBC | $97\pm2.35$                          | $75\pm9.12$            | $66\pm3.05$            |  |  |  |  |
| BP-3  | $88\pm18.1$                          | $87\pm14.9$            | $66 \pm 14.7$          |  |  |  |  |
| EDP   | $106\pm2.25$                         | $103\pm12.1$           | $103\pm3.21$           |  |  |  |  |
| EHMC  | $123\pm7.49$                         | $108 \pm 14.4$         | $107\pm4.43$           |  |  |  |  |

 Table 5. Recoveries of UVFs from sludge samples spiked with different concentrations.

## 3.3. Measurement Uncertainty

Here, the main uncertainty components such as  $u_{calibration}$ ,  $u_{SI}$  and  $u_{Recovery}$  were calculated for the analysis of two different UVF concentrations, as given in Table 6. The uncertainty of the QuEChERS-GC–MS/MS method for UVFs is between 13.2–47.4% at a concentration of 300 ng g<sup>-1</sup> and between 6.9–43.6% at a concentration of 600 ng g<sup>-1</sup>, which are quite satisfactory in such a complex matrix. Uncertainties regarding the recovery and calibration curve were the largest source contributing to measurement uncertainty.

**Table 6.** Expanded uncertainties of QuEChERS followed by the in-port derivatization method for studied UVFs.

| UV Filter | Description  | Value (ng g <sup><math>-1</math></sup> )x |                    | Standard Uncertainty <i>u</i> ( <i>x</i> ) |                            | Relative Standard<br>Uncertainty <i>u</i> ( <i>x</i> ) |  |
|-----------|--|---|--------------------|--|----------------------------|--|--|
|           |  | 300                                       | 600                | 300  | 600                        | 300  | 600  |
| EHS       | Repeatability<br>Bias (recovery)<br>Calibration<br>u(c)<br>Expanded $U(x)$ | 1<br>0.8700<br>300                        | 1<br>0.9948<br>600 | 0.0559<br>0.0336<br>14.855                 | 0.0860<br>0.0582<br>15.075 | 0.0559<br>0.0385<br>0.0495<br>0.0841<br>0.1681         | 0.0860<br>0.0585<br>0.0251<br>0.1070<br>0.2139 |

| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | UV Filter | Description           | Value (1 | ng g $^{-1}$ )x | Standard Un | certainty <i>u</i> ( <i>x</i> ) | Relative Standard<br>Uncertainty <i>u</i> ( <i>x</i> ) |         |
|---|-----------|-----------------------|----------|-----------------|-------------|---------------------------------|--|---------|
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           |                       | 300      | 600             | 300         | 600                             | 300  | 600     |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Repeatability         | 1        | 1               | 0.0696      | 0.1267                          | 0.0696   | 0.12673 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Bias (recovery)       | 0.8367   | 0.9183          | 0.1719      | 0.0939                          | 0.2054   | 0.1022  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | HMS       | Calibration           | 300      | 600             | 16.826      | 17.0757                         | 0.0561   | 0.0284  |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   |           | и(с)                  |          |                 |             |                                 | 0.2241   | 0.1653  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.4481   | 0.3306  |
| Bias (recovery) $0.9064$ $0.9294$ $0.0361$ $0.0268$ $0.0398$ $0.0288$ 3-BCCalibration $300$ $600$ $12.634$ $12.822$ $0.0421$ $0.0214$ $u(c)$ $0.0767$ $0.0403$ Expanded $U(x)$ $0.1534$ $0.0805$ Repeatability11 $0.0473$ $0.0198$ $0.0473$ $0.0198$ Bias (recovery) $0.9653$ $0.9527$ $0.0677$ $0.0756$ $0.0702$ $0.0793$ IAMCCalibration $300$ $600$ $8.2934$ $8.2934$ $0.0276$ $0.0138$ $u(c)$ $0.0890$ $0.829$ Expanded $U(x)$ $0.0890$ $0.829$ Expanded $U(x)$ $0.1780$ $0.1658$ Bias (recovery) $0.6423$ $0.6257$ $0.0262$ $0.0167$ $0.0408$ $0.0266$ 4-MBCCalibration $300$ $600$ $6.834$ $6.7825$ $0.0223$ $0.0113$ $u(c)$ $0.0667$ $0.0343$ Bias (recovery) $0.8426$ $0.6435$ $0.0507$ $0.0342$ $0.0602$ $0.0531$ BP-3Calibration $300$ $600$ $18.7049$ $18.9821$ $0.0645$ $0.0135$ BP-3Calibration $300$ $600$ $14.1641$ $14.3741$ $0.0472$ $0.0240$ Bias (recovery) $0.8690$ $0.9033$ $0.0477$ $0.0505$ $0.0548$ |           | Repeatability         | 1        | 1               | 0.0502      | 0.0182                          | 0.0502   | 0.0182  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |           | Bias (recovery)       | 0.9064   | 0.9294          | 0.0361      | 0.0268                          | 0.0398   | 0.0288  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | 3-BC      | Calibration           | 300      | 600             | 12.634      | 12.822                          | 0.0421   | 0.0214  |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   |           | и(с)                  |          |                 |             |                                 | 0.0767   | 0.0403  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.1534   | 0.0805  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Repeatability         | 1        | 1               | 0.0473      | 0.0198                          | 0.0473   | 0.0198  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Bias (recovery)       | 0.9653   | 0.9527          | 0.0677      | 0.0756                          | 0.0702   | 0.0793  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | IAMC      | Calibration           | 300      | 600             | 8.2934      | 8.2934                          | 0.0276   | 0.0138  |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   |           | и(с)                  |          |                 |             |                                 | 0.0890   | 0.0829  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.1780   | 0.1658  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Repeatability         | 1.0000   | 1               | 0.0465      | 0.0185                          | 0.0465   | 0.0185  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |           | Bias (recovery)       | 0.6423   | 0.6257          | 0.0262      | 0.0167                          | 0.0408   | 0.0266  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | 4-MBC     | Calibration           | 300      | 600             | 6.6834      | 6.7825                          | 0.0223   | 0.0113  |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $   |           | и(с)                  |          |                 |             |                                 | 0.0657   | 0.0343  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.1315   | 0.0687  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Repeatability         | 1        | 1               | 0.0670      | 0.0784                          | 0.0670   | 0.0784  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  |           | Bias (recovery)       | 0.8426   | 0.6435          | 0.0507      | 0.0342                          | 0.0602   | 0.0531  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | BP-3      | Calibration           | 300      | 600             | 18.7049     | 18.9821                         | 0.0623   | 0.0316  |
| Expanded $U(x)$ 0.21910.1997Repeatability110.06450.0135Bias (recovery)0.86900.90330.04770.05050.05480.0559EDPCalibration30060014.164114.37410.04720.0240 $u(c)$ 0.09700.06230.19390.1246  |           | и(с)                  |          |                 |             |                                 | 0.1096   | 0.0998  |
| Repeatability110.06450.01350.06450.0135Bias (recovery)0.86900.90330.04770.05050.05480.0559EDPCalibration30060014.164114.37410.04720.0240 $u(c)$ 0.09700.06230.19390.1246  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.2191   | 0.1997  |
| Bias (recovery) $0.8690$ $0.9033$ $0.0477$ $0.0505$ $0.0548$ $0.0559$ EDPCalibration $300$ $600$ $14.1641$ $14.3741$ $0.0472$ $0.0240$ $u(c)$ Expanded $U(x)$ $0.0970$ $0.0623$ Expanded $U(x)$ $0.1246$  |           | Repeatability         | 1        | 1               | 0.0645      | 0.0135                          | 0.0645   | 0.0135  |
| EDPCalibration30060014.164114.3741 $0.0472$ $0.0240$ $u(c)$ 0.09700.0623Expanded $U(x)$ 0.19390.1246  |           | Bias (recovery)       | 0.8690   | 0.9033          | 0.0477      | 0.0505                          | 0.0548   | 0.0559  |
| u(c)0.09700.0623Expanded $U(x)$ 0.19390.1246  | EDP       | Calibration           | 300      | 600             | 14.1641     | 14.3741                         | 0.0472   | 0.0240  |
| Expanded <i>U</i> ( <i>x</i> ) 0.1939 0.1246  |           | и(с)                  |          |                 |             |                                 | 0.0970   | 0.0623  |
|   |           | Expanded $U(x)$       |          |                 |             |                                 | 0.1939   | 0.1246  |
| Repeatability 1 1 0.0747 0.0193 0.0747 0.0193   |           | Repeatability         | 1        | 1               | 0.0747      | 0.0193                          | 0.0747   | 0.0193  |
| Bias (recovery) 0.7552 56,847 0.1589 1.2119 0.2104 0.2132   |           | Bias (recovery)       | 0.7552   | 56,847          | 0.1589      | 1.2119                          | 0.2104   | 0.2132  |
| EHMC         Calibration         300         600         23.9792         24.3341         0.0799         0.0406  | EHMC      | Calibration           | 300      | 600             | 23.9792     | 24.3341                         | 0.0799   | 0.0406  |
| u(c) 0.2371 0.2179  |           | <i>u</i> ( <i>c</i> ) |          |                 |             |                                 | 0.2371   | 0.2179  |
| Expanded <i>U</i> ( <i>x</i> ) 0.4743 0.4357  |           | Expanded $U(x)$       |          |                 |             |                                 | 0.4743   | 0.4357  |

## Table 6. Cont.

#### 3.4. Comparison with Other Methods

The recovery values obtained for all analytes are similar to those of studies with laborious and expensive techniques. In some studies, recovery values at a single concentration were determined [21,22,27,36], while in others, recovery values at different concentrations were investigated [16,19,23,33]. Our results indicated that for 4-MBC, only at a high concentration (600 ng g<sup>-1</sup>) was the recovery value lower than that of the reported ones. Fortunately, good recovery values were obtained at lower concentrations. In addition, to the best of our knowledge, method validation for the analysis of 3-BC, EHS, HMS and IAMC in sludge was attained successfully. Analytes (EHS, HMS, BP-3) were derivatized using the in-port derivatization technique, which is fast, reliable and eco-friendly without being affected by the complexity of the matrix.

The LOD values of the selected UVFs in the spiked sludge sample ranged from 8 ng  $g^{-1}$  to 12.1 ng  $g^{-1}$ . These limits are quite successful when compared to other studies (Table 7). The LOD values obtained for UVFs were lower than previous studies for 4-MBC, EHMC [23,27], BP-3 [23,36] and EDP [16]. On the other hand, the LOD values for 4-MBC [21,22,33], EHMC [16,21,22], BP-3 [19,27,33] and EDP [23] were higher.

| UV Filters | Extraction<br>Method | Instrumental<br>Method | LOD (ng g <sup>-1</sup> ) | Recovery (%)   | RSD%       | References |
|------------|----------------------|------------------------|---------------------------|----------------|------------|------------|
| 4-MBC      |                      |                        | 12                        | 102            | 16–10      |            |
| OC         |                      |                        | 18                        | 70             | 4–9        |            |
| EHMC       |                      |                        | 19                        | 90             | 5-10       |            |
| ODP        | DIE                  | LIPLC MS/MS            | 0.2                       | 85             | 7          | [27]       |
| BP-3       | ILL                  | 01 LC-1013/1013        | 1.0                       | 70             | 5–9        | [27]       |
| BP-1       |                      |                        | 60                        | 30             | 9–14       |            |
| 4HB        |                      |                        | 5.0                       | 95             | 4–11       |            |
| 4DHB       |                      |                        | 5.0                       | 96             | 3–6        |            |
| EHS        |                      |                        | 17 *                      | 95-101         | 7          |            |
| HMS        |                      |                        | 34 *                      | 78–96          | 5–6        |            |
| IAMC       |                      |                        | 34 *                      | 80-107         | 4–6        |            |
| BP-3       |                      | CC MS                  | 61 *                      | 89-106         | 6–11       | [22]       |
| 4-MBC      | ILE + JIE            | GC-IVI5                | 26 *                      | 79–86          | 4–5        | [23]       |
| EDP        |                      |                        | 22 *                      | 88–93          | 6–7        |            |
| EHMC       |                      |                        | 24 *                      | 73–90          | 5          |            |
| OC         |                      |                        | 33 *                      | 84-85          | 5-12       |            |
| BP-1       |                      |                        | 2.5 *                     | $74\pm9$       | 9          |            |
| BP-2       |                      |                        | 2.5 *                     | $99 \pm 11$    | 11         |            |
| BP-3,      | PLE                  | LC-MS/MS               | 25 *                      | $104\pm14$     | 14         | [36]       |
| BP-4       |                      |                        | 5 *                       | $114\pm28$     | 28         |            |
| PBSA       |                      |                        | 5 *                       | $118\pm19$     | 19         |            |
| BP-1,      |                      |                        | 0.41                      |                |            |            |
| BP-2       |                      |                        | 0.67                      |                |            |            |
| BP-3       |                      |                        | 0.67                      |                |            |            |
| BP-8       |                      |                        | 0.41                      | 20.2.11/       | 0.1.1.10.0 | [10]       |
| 1H-BT      | LLE + SPE            | LC-MS/MS               | 0.67                      | 38.3-116       | 3.14-13.8  | [19]       |
| 5Me-1H-BT  |                      |                        | 0.67                      |                |            |            |
| TBHPBT     |                      |                        | 0.1                       |                |            |            |
| 4-OH-HB    |                      |                        | 0.41                      |                |            |            |
| 4-MBC      |                      |                        | 4                         | 94.6           | 13.1       |            |
| EHMC       | LLE-SPE              | GC-MS                  | 3                         | 101.2          | 10.5       | [21]       |
| OC         |                      |                        | 6                         | 87.5           | 7.5        |            |
| 4-MBC      |                      |                        | 4                         | 95             | 2          |            |
| EHMC       | LLE-SPE              | GC-MS                  | 3                         | 101            | 13         | [22]       |
| OC         |                      |                        | 6                         | 87             | 7          | []         |
| BP         |                      |                        | 0.3                       | 63_82          | 0.1_1.0    |            |
| BP-3       | OuEChERS             | LIPLC-MS/MS            | 0.3                       | 60-86          | 0.1-1.0    | [33]       |
| 4-MBC      | QUECHERO             |                        | 0.6                       | 86-95          | 0.1-6.0    | [00]       |
|            |                      |                        | 20                        | 00 101         | 2 (        |            |
|            |                      |                        | 20                        | 92-101         | 2-0        |            |
| 4-IVIDC    | OWECHERS             | CC MS /MS              | 29<br>21                  | 80-08<br>80 86 | 2-7        | [16]       |
|            | QUECHERS             | GC-1015/1015           | 51                        | 02-00          | 1-2        | [10]       |
| OC         |                      |                        | 5                         | 81_9 <i>/</i>  | 1-5<br>3-5 |            |
|            |                      |                        | 0                         | 81-94          | 5-5        |            |
| 3-BC       |                      |                        | 10.1                      | 93–115         | 3.2–10.8   |            |
| EHS        |                      |                        | 10.0                      | 96-113         | 9.7–19.3   |            |
| HMS        |                      |                        | 9.90                      | 87-109         | 12.1-25.6  |            |
| IAMC       | QuEChERS             | GC-MS/MS               | 9.5                       | 113-121        | 3.4-19.8   | This study |
| 4-MBC      | -                    |                        | 8.00                      | 66-97          | 3.2-10.7   | 5          |
| BP3        |                      |                        | 4.30                      | 66-88          | 13.6–16.2  |            |
| EDP        |                      |                        | 12.1                      | 103-106        | 2.3-15.4   |            |
| EHMC       |                      |                        | 8.00                      | 107-123        | 3.4-22.6   |            |

 Table 7. Comparison of QuEChERS method with previous microextraction studies in sludge samples.

1H-BT: 1H-benzotriazole, 5Me-1H-BT: 5-methyl-1H-benzotriazole, TBHPBT: 2-(5-t-butyl-2-hydroxyphenyl) benzotriazole, 4-OH-HB: 4-hydroxy benzophenone. \* LOQ values.

The developed method was applied to sludge samples collected from a domestic wastewater treatment plant. The concentrations of UV filters were found to be 66.9, 161.9, 54.5, <LOQ and 79.9 ng g<sup>-1</sup> for EHS, HMS, BP-3, EDP and EHMC, respectively. These results indicate that even in domestic wastewater sludge, high concentrations of UVFs could be found, and the sludge used for soil conditioning or fertilization purposes could raise environmental concerns.

## 4. Conclusions

In this study, eight different UVFs were extracted from sludge samples using a wellestablished QuEChERS methodology, and then, in-port derivatization was applied for more polar and less volatile analytes. The method combining QuEChERS and in-port derivatization, which ensures extra sensitivity, was shown to be accurate, reproducible and sensitive. This method also provided substantially reduced analysis time and solvent or chemical consumption compared to off-line derivatization. Method validation resulted in high recovery of UVFs (66–123%), meaning good accuracy; moreover, low inter-day RSD% (10.1–25.6) indicates high precision, and low values of LOD (<2.1 ng  $g^{-1}$ ) and LOQ (<40 ng  $g^{-1}$ ) show the sensitivity of the analysis for a matrix as complex as waste sludge. This study can be extended to the analysis of UVF degradation metabolites in sludge samples using QuEChERS with in-port derivatization followed by GC–MS/MS.

**Author Contributions:** C.Y. carried out the experiments, evaluation of results and preparation of the manuscript. F.N.E. and I.K. guided the experiments, edited the manuscript and evaluated the results. H.E. designed the experiments and guided the analysis. Research Assistant S.C.T. contributed to the analysis and experiments. All authors have read and agreed to the published version of the manuscript.

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