

Review

# Superconducting Accelerator Magnets Based on High-Temperature Superconducting Bi-2212 Round Wires

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**Abstract:** Superconducting magnets are an invaluable tool for scientific discovery, energy research, and medical diagnosis. To date, virtually all superconducting magnets have been made from two Nb-based low-temperature superconductors (Nb-Ti with a superconducting transition temperature  $T_c$  of 9.2 K and Nb<sub>3</sub>Sn with a  $T_c$  of 18.3 K). The 8.33 T Nb-Ti accelerator dipole magnets of the large hadron collider (LHC) at CERN enabled the discovery of the Higgs Boson and the ongoing search for physics beyond the standard model of high energy physics. The 12 T class Nb<sub>3</sub>Sn magnets are key to the International Thermonuclear Experimental Reactor (ITER) Tokamak and to the high-luminosity upgrade of the LHC that aims to increase the luminosity by a factor of 5–10. In this paper, we discuss opportunities with a high-temperature superconducting material Bi-2212 with a  $T_c$  of 80–92 K for building more powerful magnets for high energy circular colliders. The development of a superconducting accelerator magnet could not succeed without a parallel development of a high performance conductor. We will review triumphs of developing Bi-2212 round wires into a magnet grade conductor and technologies that enable them. Then, we will discuss the challenges associated with constructing a high-field accelerator magnet using Bi-2212 wires, especially those dipoles of 15–20 T class with a significant value for future physics colliders, potential technology paths forward, and progress made so far with subscale magnet development based on racetrack coils and a canted-cosine-theta magnet design that uniquely addresses the mechanical weaknesses of Bi-2212 cables. Additionally, a roadmap being implemented by the US Magnet Development Program for demonstrating high-field Bi-2212 accelerator dipole technologies is presented.

**Keywords:** high-temperature superconducting magnets; HTS; Bi-2212; accelerator magnets

## 1. Introduction

High-field superconducting magnets are a key component in many scientific and medical instruments, including particle accelerators [1], fusion energy reactors [2], magnetic resonance imaging (MRI) scanners, ion beam cancer therapy devices [3], as well as thousands of nuclear magnetic resonance (NMR) spectrometers. So far, virtually all superconducting magnets have been made from two Nb-based low-temperature superconductors (Nb-Ti with a superconducting transition temperature  $T_c$  of 9.2 K and Nb<sub>3</sub>Sn with a  $T_c$  of 18.3 K). Our technical capability of building high-field magnets could be greatly expanded by high- $T_c$  cuprates and iron-based superconducting materials with an upper critical magnetic field ( $\mu_0 H_{c2}$ ) exceeding 50 T at 4 K, much greater than that of Nb-Ti (~14 T at 1.8 K) and Nb<sub>3</sub>Sn (~26–27 T at 1.8 K). For particle colliders, the usefulness of achieving high magnetic fields is readily seen from the simple description of the proton beam energy of proton colliders  $E \propto 0.3 \times B \times R$ , where  $B$  is the field in the dipole magnets (T),  $R$  is the bending radius in the dipole magnets (km) and the particle energy  $E$  in TeV. Coincidentally, magnetic fields of >25 T generated by all superconducting magnets are also desired for condensed matter research [4], fusion energy [5], and NMR [6].

Any conductor for superconducting applications must develop a high critical current density,  $J_c$ , in its long-length form. Only after three decades of arduous conductor development, three high-temperature superconducting (HTS) cuprates (REBa<sub>2</sub>Cu<sub>3</sub>O<sub>x</sub> (REBCO) (RE = rare earth), (Bi, Pb)<sub>2</sub>Sr<sub>2</sub>Ca<sub>2</sub>Cu<sub>3</sub>O<sub>x</sub> (Bi-2223), and Bi<sub>2</sub>Sr<sub>2</sub>CaCu<sub>2</sub>O<sub>x</sub> (Bi-2212)) have been commercially made into practical forms of metal/superconductor composite conductors in lengths suitable for making magnets. They have also been demonstrated to have a high current-carrying capability with the whole wire current density  $J_E$  exceeding 100 A/mm<sup>2</sup> at 4.2 or 1.8 K above 23 T, where the  $J_c$  of Nb<sub>3</sub>Sn wires ceases to be useful. 100 A/mm<sup>2</sup> is a benchmark value for the  $J_E$  of superconducting wires for them to be useful for constructing solenoids. Unlike Nb-Ti and Nb<sub>3</sub>Sn, high  $J_E$  Bi-2223 and REBCO are produced as tapes with a large shape aspect ratio, due to the need to macroscopically texture the conductor to minimize the obstacle of large-angle grain boundaries to the current flow [7,8]. Both Bi-2223 and REBCO tapes have a strong anisotropy of  $T_c$ ,  $\mu_0 H_{c2}$ , and  $J_c$  in magnetic fields. For Bi-2223, there are no high-current cable technologies available for constructing accelerator magnets yet, whereas for REBCO, two cable technologies, Roebel [9–12] and CORC<sup>®</sup> (conductor on round core) [13–15], are being investigated for constructing accelerator magnets with an aligned block concept and a canted-cosine-theta design, respectively. Perspectives on using REBCO coated conductors for constructing accelerator magnets were given by X. Wang [16].

The present paper focuses on Bi-2212, which, similar to Nb-Ti and Nb<sub>3</sub>Sn, is produced in an isotropic, round, multifilamentary form [17] that can be wound or cabled into arbitrary geometries including Rutherford cables, a flat rectangular cable simple and cheap to produce and composed of wires twisted and transposed for stability and high-field quality. Bi-2212 would also enable high-field magnets beyond the present 1 GHz (23.5 T) NMR proton resonance limit of Nb<sub>3</sub>Sn technology. A tremendous progress has been made in developing it for use in high-field magnets since the demonstration of a multifilamentary Bi-2212 round wire by Oxford Instruments, Superconducting Technology (OI-ST, now Bruker OST LLC) in 2005 with a practical  $J_c$  [18,19]. Along the way, wire  $J_c$  in demonstration coils has been increased by several fold and several key challenges have been met, understood, and solved. Key materials challenges and technology breakthroughs in producing a high  $J_c$  in wires will be discussed in Section 3. High critical currents do not by themselves make a competitive conductor technology. Section 2 reviews the complexity of superconducting accelerator magnet technologies. Section 4 provides an overview of the recent progress with subscale magnets based on racetrack coils made from Rutherford cables. Section 5 reviews the challenges beyond achieving a high  $J_c$  in short superconducting wires and questions that remain for constructing an accelerator grade superconducting magnet. Section 6 discusses a canted-cosine-theta magnet concept that presents an ingenious solution to the mechanical weakness of Bi-2212 wires and the challenges associated with its heat treatment control, and the progress of building prototype coils. The paper will conclude with a technical roadmap being implemented at the US Magnet Development Program (MDP) [20], and synergetic developments.

## 2. Superconducting Accelerator Magnets: Complexity and Requirements

The superconducting accelerator magnet technology is complex and its development can take decades. In 1990, a 1 m long, 50 mm bore Nb<sub>3</sub>Sn dipole model built by CERN and ELIN achieved 10.2 T with a few quenches [21]. This success was followed by three decades of intense development including two notable advances, the development of the high  $J_c$  Restacked Rod Process (RRP<sup>®</sup>) Nb<sub>3</sub>Sn conductor by the OI-ST in 2002 [22] and the development of a bladder-and-key shell mechanical structure at Lawrence Berkeley National Lab (LBNL) [23]. In 2019, Nb<sub>3</sub>Sn accelerator magnets produced still exhibit a long quench training and a lack of reproducibility [24–26]. The term training refers to the increase of peak current observed in a magnet when it undergoes a series of tests where the current is ramped up until the magnet quenches.

The widely used superconducting accelerator technology is a two-layer, cosine-theta magnet wound from Rutherford cable in a roman-arch structure [27,28]. The cable carries >5 kA to make

a possible pulsed operation. The first key test of the suitability of superconductors for accelerator magnets is whether the winding current density  $J_w$  can be made sufficiently high ( $>400 \text{ A/mm}^2$ ) for an efficient field generation ( $B \propto J_w \times t$ , here  $t$  is the thickness of the coil winding). This requires a wire  $J_E$  of  $>600 \text{ A/mm}^2$ , a cable with low porosity and thin insulation.

Second, it is important to have mechanical structures to manage the tremendous Lorentz forces that compress cables azimuthally towards the mid-plane of the winding and radially outwards. The 4 T Nb-Ti Tevatron magnet has an outward force of 11.8 kN per meter magnet length. Both forces go up with  $B^2$ . Nb-Ti is ductile. However, Nb<sub>3</sub>Sn, Bi-2212, and REBCO are brittle; the dependence of their superconducting properties on mechanical loads needs to be well understood and ingenious engineering solutions need to be found.

Third, it is also important to minimize training, and have a reliable circuit protection during quenches in place. A magnet can be easily destroyed by its stored energy, which goes up with  $B^2$ , if the energy is deposited within a small fraction of the superconducting winding. In addition, during quench, a large electrical voltage to ground is generated and therefore a robust insulation is required. HTS conductors offer a potentially training-free superconducting magnet, but also present challenges that need new solutions.

Accelerator magnets operate in cycling mode with various field ramps. The Large Hadron Collider (LHC) main-ring dipole magnet is cycled from injection (0.54 T) to a high field (8.3 T) in a period of 20 min, maintained at high field for 2–10 h for beam collision, and then finally back to low field for another cycle, where it may remain for 20–40 min during which particles are injected. Magnets need to provide great accuracy of the magnetic field seen by particles over the full dynamic range from field injection through collision. The error fields need to be of the order of  $10^{-4}$  of the central bending field for a stable beam behavior, and thus of the order of a few 0.1 mT. To provide field accuracy, it is necessary to control the geometry of the conductor and winding (change of any of dimensions should be constrained to the order of 0.025 mm), and controlling field distortions due to eddy currents that flow between strands during and following a field ramp. In addition, superconductors come with a persistent current that shields superconductor filaments from the external field. Such persistent currents generate spurious fields, especially  $b_3$  (sextupole) at low field. The implication is that the magnetization of the superconductor needs to be minimized. Magnetization scales as  $M \propto J_c \times D_{\text{eff}}$ , where  $D_{\text{eff}}$  is the effective diameter of superconductor filaments, and therefore  $D_{\text{eff}}$  needs to be small (6–7  $\mu\text{m}$  for LHC main dipole wires). The RRP<sup>®</sup> Nb<sub>3</sub>Sn strand selected for the high luminosity LHC (HL-LHC) quadrupole QXF magnets has a  $D_{\text{eff}}$  of 55  $\mu\text{m}$ .

Readers who want to understand superconducting accelerator magnets in depth can study these monographs [29,30] and review articles [1,27,28,31]. We will link the main points discussed briefly above to the status of Bi-2212 technology in the following sections.

### 3. The Development of Bi-2212 into a Magnet-Grade Conductor: Materials Challenges and Breakthroughs

The high- $J_c$ , polycrystalline, silver sheathed, powder-in-tube tapes of Bi-2212 were first demonstrated by Heine et al. [32] in 1989 using a partial melt processing heat treatment, which produces a self-organized, local grain texture [33] beneficial for producing a high  $J_c$ . Using the same technologies in 2005, a high  $J_c$  was demonstrated in a much more desirable multifilamentary round wire form [18,19] by the OI-ST.

The powder-in-tube method provides a convenient and economical fabrication technology that yields versatile wires of various size, filament count and architecture, and aspect ratio. The wires regularly produced by the Bruker OST LLC come with an architecture of  $19 \times 36$ ,  $37 \times 18$  or  $55 \times 18$  (18 bundles, each of which has 55 filaments) for 0.8 mm diameter wires. Filaments are embedded in a silver matrix, which are then again encased with an Ag-0.2 wt% Mg or Ag-Mg-Sb alloy outer sheath. Such wires can be fully twisted, resulting in a hysteresis loss (4 K,  $\pm 3$  T) of 2–3 MJ/m<sup>3</sup> over the superconductor filaments, compared to 1.2–3 MJ/m<sup>3</sup> for Nb<sub>3</sub>Sn, 5.0 MJ/m<sup>3</sup> for Bi-2223, and 320 MJ/m<sup>3</sup>

for REBCO [34]. It can also be rolled into a rectangular form, retaining the isotropic superconducting properties when the aspect ratio is lower than 1.6 [35]. The Ag matrix surrounding the filaments has a very high electrical conductivity as judged by a residual-resistivity ratio (RRR)  $> 100$  and very high thermal conductivity [36,37], despite not surrounding the superconductor filaments with diffusion barriers to prevent superconductor filaments from poisoning the metal matrix such as Cu/Nb-Ti and Cu/Nb<sub>3</sub>Sn wires.

A key to the success of developing high  $J_c$  Bi-2212 wires is the development of a fundamental understanding of what occurs during the heat treatment inside the wire at the microscopic level [38–40]. The heat treatment, so-called partial melt processing, involves heating up the conductor to partially melt filaments (compacted powder) around 885–900 °C in 1 bar pure O<sub>2</sub> or a mixture of O<sub>2</sub>/Ar with an oxygen partial pressure  $p_{O_2} = 1$  bar into a liquid and two solid phases, and then slowly cooling them to form well-connected Bi-2212 grains. The key understanding is that the porosity that occupies about 30% of the filament volume in the as-drawn wires agglomerates into large gas bubbles at high temperatures upon melting [41,42], which also cause filament de-densification in long-length wires [43]. Removing porosity results in a high  $J_c$ , either by a cold-isostatic pressing treatment of as-drawn wires [44], or an overpressure heat treatment (OPHT) that applies an external gas pressure to densify conductors during heat treatment by the creep of silver [45]. The optimized OPHT uses a mix of 98% Ar and 2% O<sub>2</sub> with a total gas pressure at 50 bar (note that the  $p_{O_2}$  is 1 bar); this increases the density of Bi-2212 filaments to  $>95\%$ . The OPHT is similar to the controlled overpressure processing (CT-OP) that underpins the industrial fabrication of long-length, high- $J_c$  Ag/Bi-2223 tapes, sold under the trade name of DI-BSCCO<sup>®</sup> by Sumitomo Electric Industries, Ltd. [46].

Another key to the success of developing high  $J_c$  Bi-2212 wires is the introduction of a chemical combustion vapor condensation (CCVC) method in 2017, which makes possible the production of highly homogeneous, 100–500 nm Bi-2212 precursor powders with good composition control ( $\pm 2\%$  for Ca and  $\pm 1\%$  for others), a low impurity level, and low risk of powder agglomeration. The new powder eclipses the previous melt-cast [47] granulate powder, produced by Nexans LLC and used by the wire industry between 2005 and 2017 [48], raising the  $J_c$  of wires by  $\sim 80\%$  [49,50]. The new powder has the same optimized W521 composition Bi<sub>2.17</sub>Sr<sub>1.94</sub>Ca<sub>0.90</sub>Cu<sub>1.98</sub>O<sub>x</sub> established by the Nexans Superconductors, Germany and the OI-ST [51–53].

Figure 1 presents the  $J_E(B)$  of the 2005 OI-ST wire, a 2015 wire that represents the best of that time, and a 2017 wire that utilizes a new powder technology, in comparison with those of the LHC Nb-Ti wires and the HL-LHC Nb<sub>3</sub>Sn wires. The 2015 and 2017 wires received 50 bar OPHT whereas the 2005 wire was also densified.

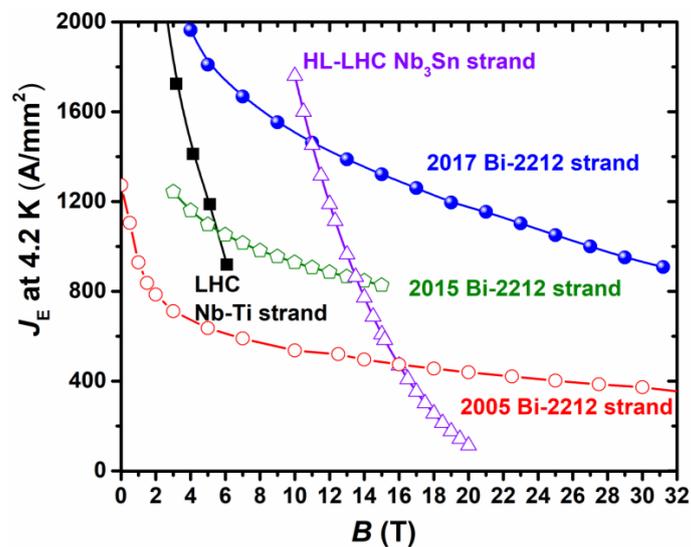


Figure 1. The  $J_E(B)$  of the large hadron collider (LHC) insertion quadrupole Cu/Nb-Ti strand (diameter

= 0.479 mm, Cu/Nb-Ti = 1.678), the high luminosity (HL)-LHC upgrade QXF RRP<sup>®</sup> Nb<sub>3</sub>Sn strand (diameter = 0.85 mm, Cu/non-Cu = 1.20 ± 0.1), and three Bi-2212 wires (Ag:AgMg:Bi-2212 ≈ 2:1:1), best of their time: (1) 2005; data from Miao et al. [18,19], (2) 2015 (PMM151103, diameter = 1.0 mm, 121 × 18 strand, Nexans #87 powder); data from Jiang et al. [48], (3) 2017 (PMM170123, diameter = 0.8 mm, 55 × 18 strand, nGimat LLC (known as Engi-Mat Co. since 2019) LXB-52 powder); data from Jiang et al. [49] and Shen et al. [50].

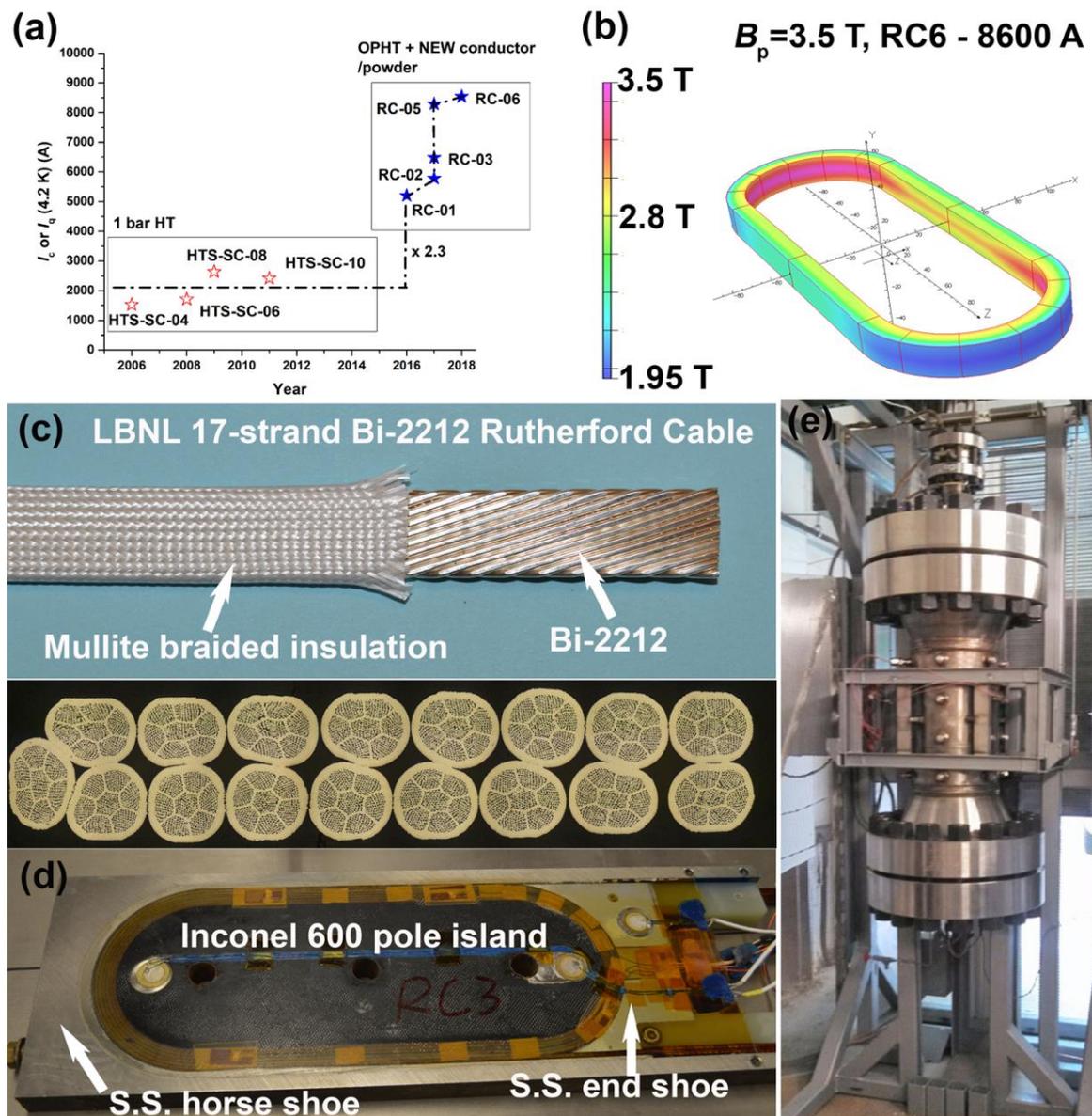
#### 4. Subscale Magnets Based on Racetrack Coils

Racetrack coils offer a fast turn-around platform for testing various technology variants. Subscale magnets based on them were used as an R&D vehicle [54] for developing Nb<sub>3</sub>Sn accelerator magnet technologies at LBNL before the US LARP R&D that successfully developed the cosine-theta Nb<sub>3</sub>Sn quadrupole magnet technology for the HL-LHC upgrade; a notable magnet that belongs to this group is RD3, a 14.7 T magnet tested in 1999 [55].

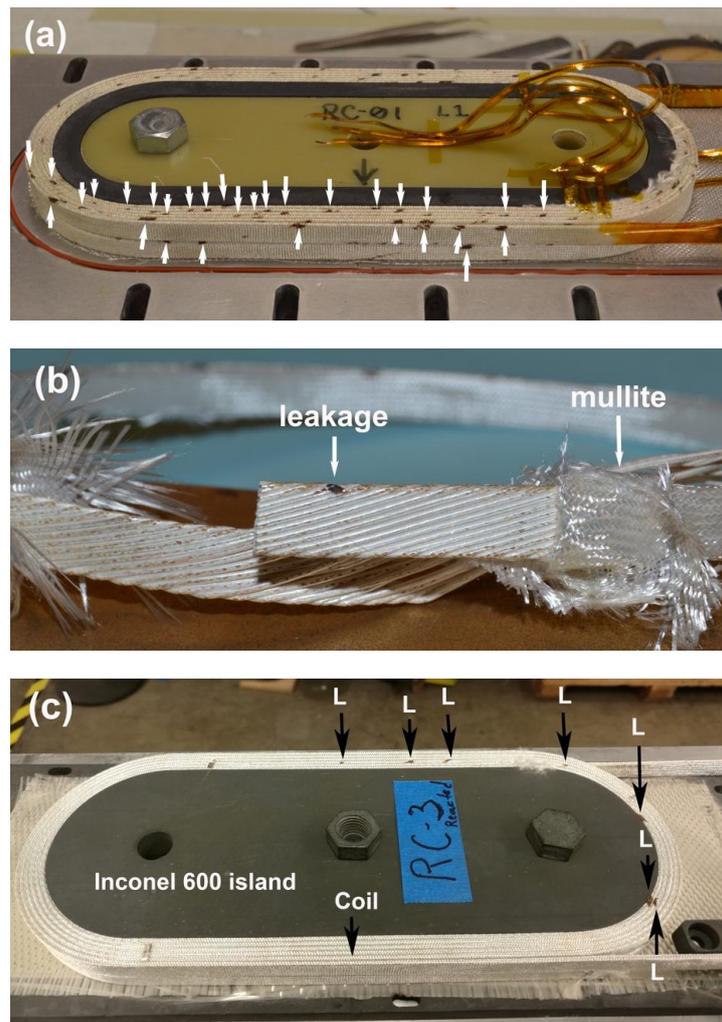
Such an approach was also adopted for Bi-2212. Figure 2 summarizes the performance of the LBNL Bi-2212 racetrack coils (two-layer, six turns/layer, a foot long) since 2006. The HTS-SC series were reacted using the conventional 1 bar heat treatment and its fabrication and performance is described by A. Godeke et al. [56,57]. The introduction of the OPHT in 2016 into the RC series more than doubled the quench current of the coil from ~2.4 to >5 kA [57]. The introduction of the new generation of Bi-2212 wires with the nGimat LLC, Lexington, KY (known as Engi-Mat Co. since 2019) CCVC Bi-2212 nanopowder enabled an improvement of the quench current to 8.6 kA exhibited by RC6 [50].

The subscale magnets use a 17-strand (strand of 0.8 mm diameter) Rutherford cable fabricated at LBNL with a typical width of 7.8 mm and a thickness of 1.44 mm. The insulation used for HTS-SC and RC coils is a ceramic yarn (mullite, 2 Al<sub>2</sub>O<sub>3</sub>:SiO<sub>2</sub>) braided insulation, first used by K. Marken et al. [35], and has been found to be a suitable solution. An interesting finding is that OPHT does not entirely remove ceramic leakage in RC coils, clear discolorations where the Bi-2212 liquid leaks through the encasing metal (Ag alloy) at high temperatures and react with surrounding materials such as insulation. The leakage does not result in turn-to-turn or turn-to-ground electrical shorts. The leakage degrades  $J_E$  locally. Most leakage in RC coils was observed at the cable edge. The mechanism of the leakage was identified as the creep rupture of the Ag-Mg sheath due to internal gas by Shen et al. [45] and thus, the leakage was expected to be removed by OPHT. However, the leakage in RC coils suggests a new thermodynamic leakage mechanism. An empirical method of eliminating or reducing ceramic leakage was identified as coating the bare Rutherford cable with a thin layer of TiO<sub>2</sub>-polymer coating insulation [58–60] before applying the mullite sleeve, and its effectiveness was experimentally demonstrated in solenoids produced at the National High Magnetic Field Laboratory (NHMFL) and RC3. Ceramic leakage in RC1 and RC3 are shown in Figure 3. RC coils other than RC3 had no TiO<sub>2</sub> slurry applied, and they show a similar degree of leakage to RC1.

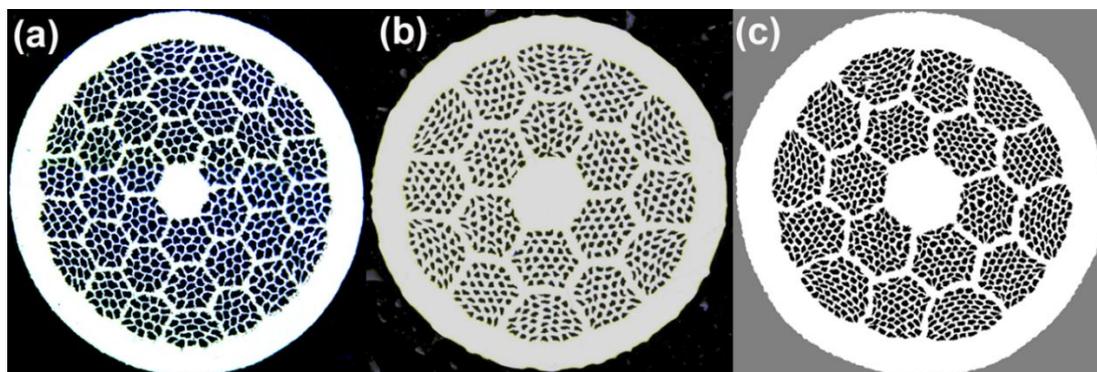
A technology variant the RC program explored is strand, in collaboration with the wire manufacturer (Bruker OST LLC). The three wire architectures tested are shown in Figure 4. The best wire was found to be 55 × 18 for 0.8 mm diameter wires with the nGimat LLC powder.



**Figure 2.** (a) Historical performance of Lawrence Berkeley National Lab (LBNL) two-layer, six turns/layer subscale magnet Bi-2212 racetrack coils. (b) A surface magnetic flux density of Rutherford cable (RC)6 at its quench current of 8600 A. (c) A photo and a cross-section of the braided mullite sleeve insulated, 17-strand Bi-2212 Rutherford cable used. (e) RC3 after impregnation with the NHMFL-mix61 epoxy resin. (d) The 50 bar overpressure heat treatment (OPHT) facility, DELTECH, at the National High Magnetic Field Laboratory (NHMFL) where RC coils were reacted.



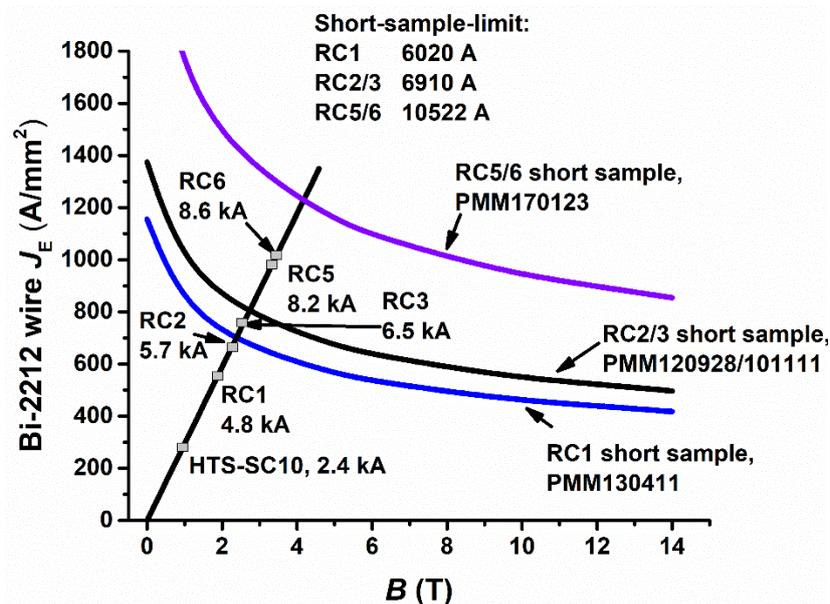
**Figure 3.** Leakage in RC coils after 50 bar OPHT. (a) RC1 whose Bi-2212 cable was insulated with the mullite sleeve only exhibited extensive leakage. Thirty of about 100 leakage spots are labeled with arrows. (b) A typical leakage spot. (c) RC3 whose Bi-2212 cable was coated with a TiO<sub>2</sub> slurry before being insulated with the mullite sleeve showed much reduced leakage. All seven leakage spots found are labeled. L = leakage. Photos reproduced from K. Zhang et al. [57].



**Figure 4.** (a) RC1 wire PMM130411, 19 × 36 architecture, Nexans powder #77; (b) RC2 and RC3 wire PMM101111, 36 × 18 architecture, Nexans powder #77; (c) RC5 and RC6 wire PMM170123, 55 × 18 architecture, nGimat powder LXB-52. The photograph of PMM170123 is a courtesy of J. Jiang of NHMFL.

The RC coil program provides evidence that the heat treatment processing of Bi-2212 coils can be reliably done and provides valuable experience with materials compatibility and selections. During heat treatments, an RC coil was reacted inside an Inconel 600 structure comprised of an island, horseshoe, and endshoe. It was also found that in addition to Inconel 600, the coil can be reacted in direct contact with a Fe-Cr-Al alloy [61] that develops a passivation Alumina layer on its surface, and in close vicinity of C276 and stainless steel 316LN fasteners.

The RC coil program also shows to what degree the short wire  $J_E$  can be achieved in practical coils (Figure 5). The coils exhibiting leakage (RC1, RC2, RC5, RC6) achieved ~80%, ~82.3%, 78%, and 81.7% of short-sample-limit (SSL), respectively. Importantly, note that the short-sample wire  $J_E$  used was the lowest value achieved in short samples (<10 cm) over a peak processing temperature  $T_p$  of  $\pm 5$  °C. Removing leakage in RC3 improves the coil performance to 94% of the SSL. All quenches originated in the high field regions (ramp turns and pole turns) and were not associated with the conductor leakage.



**Figure 5.** The  $J_E(B)$  of strands used in RC1, RC2/3, and RC5/6, their load lines, and the achieved quench current versus their short-sample-limits. Note that the  $J_E$  used is the lowest value achieved in short samples over a peak processing temperature  $T_p$  of  $\pm 5$  °C and therefore smaller than the best  $J_E$  shown in Figure 1 for the strand PMM170123.

The RC coil program proved to be a useful technology development platform. Two new technologies were tested for quench detection, including an acoustic thermometry [62] and stray-capacitance monitoring [63]. It was also used to test impregnation materials. RC coils were impregnated with wax (RC1, RC2), CTD-101K epoxy resin (RC5), and NHMFL mix-61 epoxy resin (RC3 and RC6). They exhibited no quench training [50,57].

In 2019, two racetrack coils (RC7 and RC8, two-layer, eleven-turn/layer, seventeen-strand Rutherford cable) were fabricated from twisted strands PMM180207 (RC1–6 strands were not twisted), assembled into an iron yoke and aluminum alloy shell using the bladder and key technique, and powered up as a common-coil magnet. The magnet (RC7n8) achieved 5.6 kA (77% of the SSL) without training, generating a dipole field of 4.7 T in a gap of 6 mm.

## 5. Magnet Challenges beyond $J_c$

### 5.1. The Ability of Rutherford Cables to Handle Transverse Loads

Bi-2212 is brittle and its superconducting properties are affected by strain. The primary stress that superconducting wires in solenoids experience is hoop stress, a stress along the axis of the wire.

The Ag-0.2 wt% Mg outer sheath of commercial Ag/Bi-2212 strands is an oxide-dispersion strengthened alloy for providing strength along the axial direction. For a commercial Ag-0.2 wt% Mg/Ag/Bi-2212 (area ratio AgMg: Ag: Bi-2212 = 0.25: 0.5: 0.25) round wire, the working maximum of tensile axial stress is around 150–160 MPa at 4.2 K, determined using an ITER barrel coil method [64] whereas the irreversible tensile axial strain, beyond which  $J_c$  degrades irreversibly, is between 0.4% and 0.6%, determined using a U-shaped bending spring [65], a 77 K  $I_c$ -tensile strain coupled with in situ X-ray strain measurement [66], a Walter-spring measurement [67,68]. The irreversible  $I_c$  degradation is caused by filament cracks.

The primary stress that cables in accelerator magnets are subjected to is a large transverse load. The  $I_c$  of the Bi-2212 Rutherford cables exhibited a 5% reduction with a transverse stress of ~120 MPa on the wide face of a Rutherford cable and ~160 MPa on the narrow face, measured by D. Dietderich et al. [69] in the early 2000 s on strands of that time. The transverse pressure limits of the modern Bi-2212 Rutherford cables are being investigated at the University of Twente at 4 K and a background field of 11 T.

### 5.2. Heat Treatment of Long-Length Magnets for Predictable High Performance

Heat treating Bi-2212 coils requires careful temperature control. The  $J_c$  of Bi-2212 wires is sensitive to the peak processing heat treatment temperature  $T_p$  ( $\pm 2$  °C is recommended whereas  $\pm 5$  °C is permitted), the time at the maximum processing temperature  $t_p$  ( $t_p < 1$  h is recommended) and other parameters experimentally revealed by Shen et al. [70]. The collective effect of  $T_p$  and  $t_p$  is reflected by a time in the melt  $t_{\text{melt}}$ , where  $t_{\text{melt}}$  is defined as the time that elapses between the melting of Bi-2212 filaments upon heating and the recrystallization of Bi-2212 grains upon cooling [71].

To the first approximation, the coil pack can be approximated by a slab of a material with a volumetric specific heat of  $C_v$  and a thermal conductivity of  $k$ , and a thickness of  $a$ . The distribution of temperature in the slab is parabolic during a linear heat ramp with rate of rise  $dT/dt$ . The depth of the parabolic dip  $\Delta T$  in temperature at the slab center relative to the faces being heated is  $\Delta T = \tau \cdot dT/dt$ , where  $\tau$  is the time constant and a measure of the coil pack to come into equilibrium after a change in the heat program;  $\tau = C_v/k \cdot a^2$ . The temperature distribution is modified by the heat absorption when Bi-2212 filaments melt (heat of fusion, ~46 J/g) right before reaching  $T_p$ . The real coil pack is not a slab with uniform material properties, but rather is comprised of turns of wires or cables separated with insulation materials. An analytical modeling tool of such a Bi-2212 coil pack with the effects of heat of fusion included was provided by the late A. Tollestrup [72], who, based on in situ thermocouple measurements by M. Dalban-Canassey et al. [73], estimated that the time constant for a 10-layer solenoid made from mullite insulated Bi-2212 wires ( $a = 13$  mm, bare wire diameter = 1.03 mm, insulated wire diameter = ~1.30 mm) is about 3 min. By simple approximation, to limit  $\tau < 60$  min,  $a$  needs to be no larger than 62 mm. One has to take this limitation into consideration when designing Bi-2212 accelerator magnets. The RC coil in its reaction tooling has a dimension of  $37 \times 12 \times 3.1$  cm.

### 5.3. Field Quality and Effective Filament Size

The field quality of Bi-2212 accelerator magnets is largely unknown so far. The Bi-2212 wires that Bruker OST LLC has been routinely producing are based on an optimum filament size of 15  $\mu\text{m}$ , with  $19 \times 36$ ,  $37 \times 18$ , and  $55 \times 18$  for 0.8 mm diameter wires,  $85 \times 7$  and  $55 \times 18$  for 1.0 mm wires,  $85 \times 18$  for 1.2 mm wires, and  $121 \times 18$  for 1.4 mm wires [74]. Jiang et al. [48] demonstrated that the filament diameter in unreacted wires (after powder densification) can be reduced to 9  $\mu\text{m}$  without decreasing  $J_c$ . However, filaments bond together during heat treatment and filaments within a bundle are linked together with bridges (Bi-2212 grains) that can carry the supercurrent [40], effectively raising  $D_{\text{eff}}$  to the size of the bundle. For a  $37 \times 18$ , 0.8 mm wire, magnetization measurements with the vibrating sample magnetometer (VSM) by Y. Oz et al. [34] determined that  $D_{\text{eff}}$  is 200  $\mu\text{m}$  for the untwisted wires, and 150  $\mu\text{m}$  for twisted wires with a twist pitch of 25 mm.  $D_{\text{eff}}$  can be effectively reduced by increasing the filament spacing. In a 0.8 mm,  $27 \times 7$  wire (filling factor = 8%), Y. Oz et al. [34] determined that  $D_{\text{eff}}$

drops from  $\sim 150 \mu\text{m}$  for the untwisted wires, to  $\sim 50 \mu\text{m}$  for twisted wires with a twist pitch of 50 mm. However, this reduction in  $D_{\text{eff}}$  is achieved at the expense of the superconductor filling factor and wire  $J_E$ . Unlike Sumitomo's CT-OP Bi-2223 tapes, the OPHT Bi-2212 wires show no evidence of  $J_c$  hysteresis due to the magnetic field increase and decrease.

#### 5.4. Rutherford Cables Optimization and Engineering

The overall compaction factor of Nb-Ti Rutherford cables ranges from 88% to 92.5%; typical values of a narrow edge compaction are in the range of 95% to 103% [75]. The primary concern with Nb-Ti cables is filament breakage. These values drop to  $\sim 85\%$  and  $\sim 90\%$ , respectively, for Nb<sub>3</sub>Sn Rutherford cables. The added risks are shearing the sub-elements of the RRP<sup>®</sup>, Internal-Sn type Nb<sub>3</sub>Sn wires and rupturing the diffusion barriers, causing Sn leakage from filaments into the Cu matrix and degrading the RRR of the surrounding matrix. Bi-2212 Rutherford cables used in the LBNL racetrack coils are non-keystone and have a low overall compaction factor of  $\sim 79\%$ . A question is whether this compaction factor can be increased to 90% or above. The reduction of RRR is not an issue for Bi-2212 wires, a conclusion that can be deduced from the work by Li et al. [36]. An added concern, yet to be evaluated experimentally, is whether increasing the compaction factor above 81% causes too much wire deformation at the edge of the cable that poses the risk of increasing leakage. Bi-2212 Rutherford cables were also fabricated by Barzi et al. [76], at the Fermi National Accelerator Lab using a strand diameter ranging from 0.692 to 1.02 mm with a packing factor from 81% to 86.5%. Barzi et al. [77] also rolled the wire to various thicknesses and did not find any monotonic decrease of the  $J_c$  for three wires produced by the OI-ST up to a deformation of 0.6, measured by  $(d - t)/d$  where  $d$  is the original wire diameter and  $t$  is the wire thickness.

For both Nb<sub>3</sub>Sn and Bi-2212, during heat treatment strands within a cable have ample opportunity to sinter together and develop low inter-strand contact resistances, increasing coupling current losses and field errors. For the HL-LHC upgrade, the coupling is alleviated by including a 316 L stainless steel strip (non-magnetic) as a core to Nb<sub>3</sub>Sn Rutherford cables [78]. A similar method may work with Bi-2212, though an additional issue is managing materials compatibility (core material induced chemical reactions); the core materials attempted so far include MgO papers (nonmagnetic but brittle) [79], and Ni-Cr foils (magnetic) [80]. Such cored Bi-2212 cables have not yet been fabricated into practical magnets.

#### 5.5. Quench Detection and Protection: Is There a New Operation Paradigm?

A vital concern for any HTS magnet is the need to detect a quench so that active protection can be triggered. The greatest danger is localized thermal runaway at unexpected locations. Long quench training of Nb<sub>3</sub>Sn magnets is a cumbersome and costly problem but it seldom risks coil loss. In contrast, failing to detect a quench in a much more stable HTS magnet puts the HTS magnet in great danger because the dissipative zones propagate slowly and overheat quickly. At the very high wire current density of  $1000 \text{ A/mm}^2$  safely demonstrated in these Bi-2212 racetrack magnets, hot spot temperatures can rise at hundreds of K/s, thus making rapid ( $< 10 \text{ ms}$ ) detection and rapid switching of the dump resistor vital to a safe quench without magnet burnout. The state-of-the-art quench detection for Nb-Ti and Nb<sub>3</sub>Sn magnets relies on fast ( $> 10 \text{ k-samples/s}$ ) but low precision (mV resolution) voltage measurements to define a typical threshold in the range of 100 mV to several volts. Due to the fast quench propagation velocities (typically 10 m/s for Nb-Ti and Nb<sub>3</sub>Sn magnets), 100 mV develops across growing normal zones in a negligible 0.1 ms. By contrast, at the typical 1 cm/s quench velocities of HTS conductors, resistive voltages across a localized hot spot increase at less than 0.1 mV within 0.1 ms.

The quench protection of Nb-Ti and Nb<sub>3</sub>Sn accelerator magnets relies on driving the circuit current to decrease fast enough to limit the amount of energy deposited in the normal zone (the hot spot temperature  $T_{\text{hot spot}} \propto \int_0^{3\cdot\tau} J_m^2 \cdot \rho dt$ , where  $J_m$  is the density of the current that flows in the metal matrix,  $\rho$  the resistivity of the matrix, and  $\tau$  the time constant of the exponential current decay.  $\tau$  can be approximated as  $\tau = L / (R_D + R_i)$ , where  $R_D$  is the value of a dump resistor external to the cryostat

and  $R_i$  an internal coil resistance.) For Nb-Ti and Nb<sub>3</sub>Sn magnets,  $R_i$ , triggered by a strip heater, plays an important role. Again,  $R_i$  is limited by the slow propagation of normal zones in HTS conductors.

Luckily, HTS conductors have a high stability margin. RC coils exhibited no quench training. All quenches occurred in high-field regions and were driven to thermal runaway by index loss  $E \times J$  when conductors approach their critical current.  $E = E_c \cdot (J/J_c)^N$ , where  $E_c$  is the electrical field criterion (1  $\mu$ V/cm) and  $N$  the index that characterizes the superconducting transition. Since  $N$  of Bi-2212 wires is generally less than 30 and there is a strong current sharing in Bi-2212 Rutherford cables, there are clear precursor signals before quenches. Therefore, the quench currents of Bi-2212 magnets can be predicted with an active precise voltage measurement without driving magnets to quench. The stable and predictable operations of Bi-2212 magnets up to a  $J_E$  of 1000 A/mm<sup>2</sup> were demonstrated in RC coils [50]. Such a quench-predictable and quench-training free mode is a new operation paradigm unavailable for Nb-Ti and Nb<sub>3</sub>Sn magnets, where quenches are sudden and driven by transient, tiny disturbances such as epoxy cracking. The implication is that the  $J_w$  and  $J_m$  of HTS only magnets may be no longer quench limited, making coils more compact and simplifying quench protection.

## 6. Canted-Cosine-Theta Accelerator Magnet Design and Technology

In the framework of the US MDP, LBNL is exploring the Bi-2212 accelerator magnet technology. The goal is to “develop and demonstrate an HTS accelerator magnet with a self-field of 5 T or greater with operation in a hybrid LTS/HTS magnet for fields beyond 16 T” [20].

A key challenge when designing a Bi-2212 accelerator magnet is stress management. The canted-cosine-theta (CCT) accelerator magnet design is an interesting and ingenious solution [81,82]. The CCT concept consists of a pair of solenoids tilted in opposite directions to create a field in the bore whose superposed solenoidal components cancel out while the dipole components add up (Figure 6). This configuration provides an intrinsic cosine-theta current distribution resulting in a pure dipole field. Moreover, since the conductor is placed in individual channels separated by “ribs”, the transverse component of the Lorentz force on the conductor is intercepted by the ribs and transferred to the spar (Figure 7). Assuming the mandrel and the conductor are infinitely rigid, the stresses do not build up in the conductor, leading to about an order of magnitude reduction of the stress on the conductor compared to the conventional cosine-theta design. L. Garcia Fajardo et al. [83] showed that a conceptual 3.9 T CCT Bi-2212 insert in a 15 T Nb<sub>3</sub>Sn outsert, with a total field in the bore of 18.9 T, experiences a transverse stress on the cable of less than 35 MPa, when the insert is mechanically decoupled from the outsert. In practice, neither the mandrel nor the conductor are infinitely rigid, and this implies that the mandrel experiences bending under the Lorentz forces, and there is shear stress between the cable and the surface of the channel if the coils are impregnated with an epoxy resin. The same CCT design has also been explored at LBNL for constructing high-field accelerator magnets using REBCO CORC® [14–16], at both LBNL and the Paul Scherer Institute for constructing high-field accelerator magnets using Nb<sub>3</sub>Sn Rutherford cables [84,85], and curved Nb-Ti gantry magnets for ion beam cancer therapy [86,87].

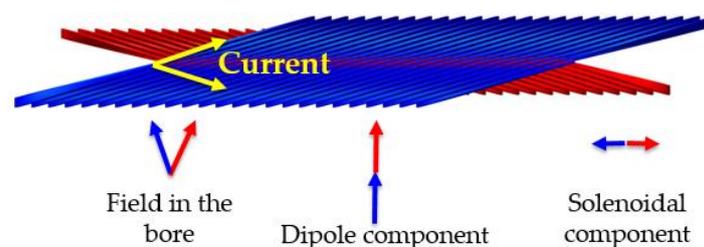
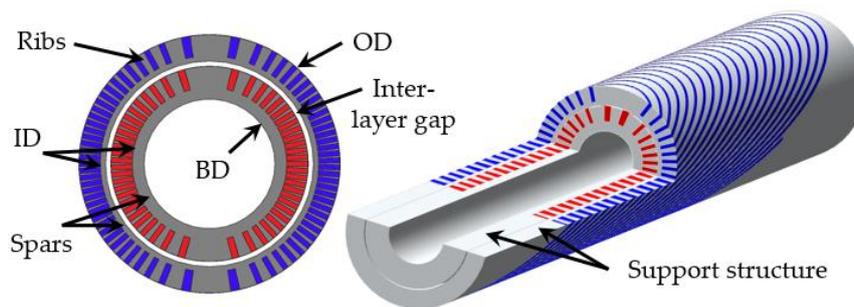


Figure 6. Two-layer CCT concept for dipole magnets.



**Figure 7.** Parts of a two-layer canted-cosine-theta (CCT) magnet. ID—coil winding inner diameter; OD—coil winding outer diameter; BD—bore diameter.

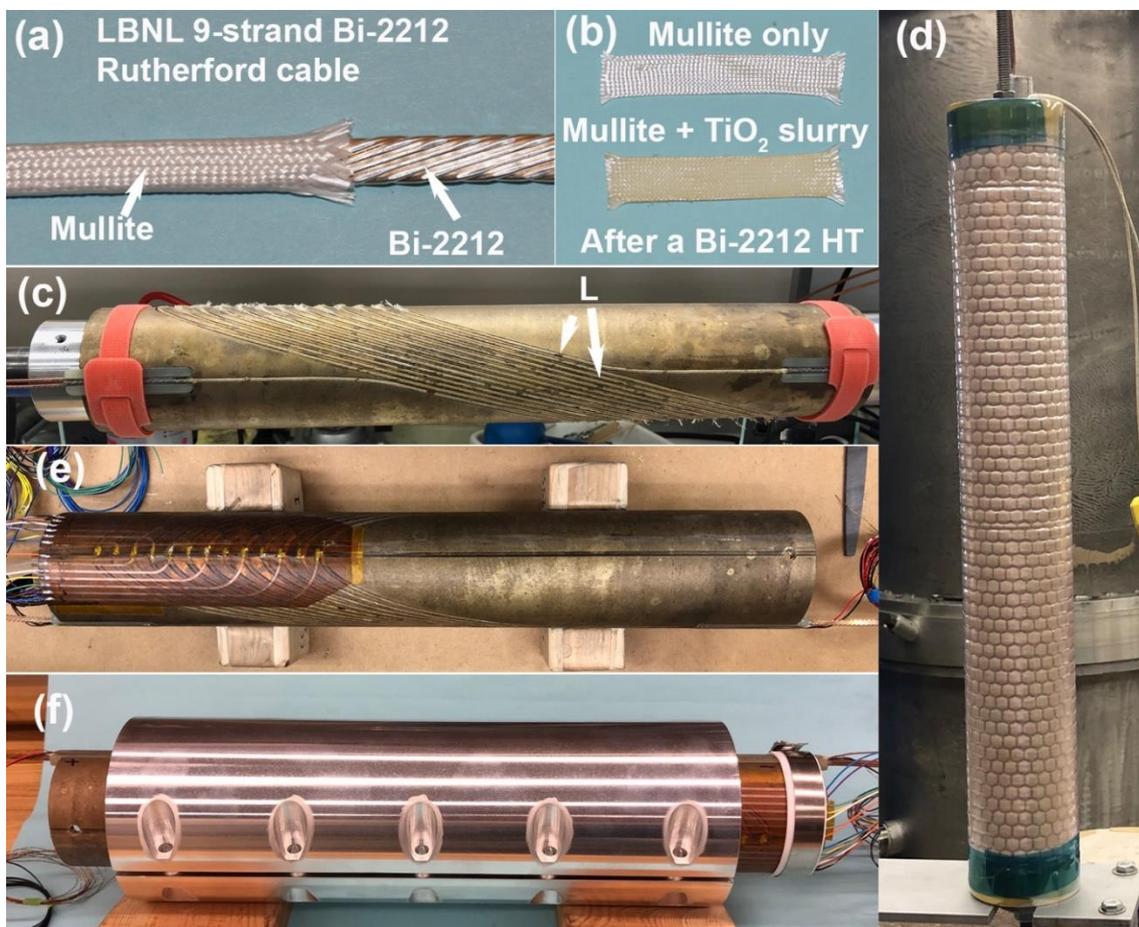
Table 1 lists the subscale Bi-2212 CCT coils that have been fabricated at LBNL. They were designed to answer critical questions: (1) Can high current CCT coils be fabricated with Bi-2212 wires and cables and what fabrication issues need to be solved? (2) What are the quench performance and the field quality of Bi-2212 CCT coils? (3) What are the field generation limit and efficiency of Bi-2212 CCT coils? They were also designed to explore technology variants including conductors, and mandrel and insulation materials. Godeke et al. [88] manufactured coils BIN1 and BIN2 and provided several first insights into mandrel material selection and fabrication issues.

**Table 1.** Summary of Bi-2212 CCT coils fabricated at LBNL. “654” means the 654-aluminum bronze whereas “954” refers to the 954-aluminum bronze. The central core of the “6 + 1” cable used for BIN2IL is a Bi-2212 strand as well. The 50 bar OPHT was performed at NHMFL. The BIN2IL quench current data is a courtesy of Dr. Xiaorong Wang of LBNL and the field quality data of BIN5aOL is a courtesy of Dr. Xiaorong Wang of LBNL and Dr. Cory Myers of the Ohio State University.

Coil (Year)	Conductor	Mandrel	Insulation	Heat Treatment	Performance
BIN1 (2014)	Single strand	Inconel 600	Mullite sleeves	1 bar HT	Extensive leakage $I_q \sim 1.477$ kA at 4.3 K, Peak field $B_p$ on conductor = 0.48 T, $B_1 = 0.29$ T in the bore. Significant deformation after reaction. Not manufactured.
BIN2IL (2014)	6 + 1 round cable	654	Mullite sleeves	1 bar HT	
BIN3	-	-	-	-	Electrically shorted to mandrel after winding. Not reacted.
BIN4 (2017)	9-strand Rutherford cable	954	Mullite sleeves	-	Bore diameter = 51.5 mm. SSL = 6.48 kA. $I_q \sim 4.02$ kA at 4.2 K, $B_p$ on conductor = 1.3 T, $B_1 = 0.71$ T in the bore, $b_3 = 1000$ units and about 30 units at $r = 13$ mm due to persistent currents at $I = 1$ kA. Small deformation after reaction. Epoxy impregnated.
BIN5aOL (2018)	Same as above	954	TiO <sub>2</sub> slurry on mullite sleeves	OPHT	Transferred to a Bluestone 3D-printed mandrel after reaction. $I_q \sim 3.1$ kA at 4.2 K.
BIN5bOL (2018)	Same as above	954	TiO <sub>2</sub> slurry on mullite sleeve	OPHT with Inconel 600 strongback	
BIN5c (2020)	Same as above	954	TiO <sub>2</sub> slurry on cable, and on mullite sleeve	OPHT	In fabrication. SSL = 5.85 kA. $B_{bore} = 2.4$ T.
BIN6 (2021)	17-strand Rutherford cable	954	Same as above	OPHT	In design. SSL = 9 kA, $B_{bore} = 5$ T. Bore = 50 mm. OD = 100 mm.

The development of BIN1 to BIN5 has provided a better understanding of fabrication processes of Bi-2212 CCT coils. The insulation for Bi-2212 CCT coils was also improved. BIN4 used a 9-strand Rutherford cable in Al-bronze 954 mandrel. The cable was insulated with mullite ( $2 \text{Al}_2\text{O}_3 + \text{SiO}_2$ ) braided sleeve, which is prone to damages during winding and whose wear and tear during insertion of cables into the CCT grooves creates electrical shorts between the conductor and the mandrel. Learning from this experience, the approach for the next prototype, BIN5aOL and BIN5bOL, was to paint the cable with the  $\text{TiO}_2$ —polymer slurry [59] on top of the mullite during the winding process, removing electrical shorts. This work is described in L. Garcia Fajardo et al. [89]. The 654 mandrels (BIN2IL) were found to deform significantly. The 954 mandrels were found to have minimum deformation.

The fabrication process of the BIN5aOL is shown in Figure 8; it is rather straightforward. Note that the BIN5aOL only achieved about 62% of the SSL and it shows a large  $b_3$  (Table 1); the reasons are being investigated and will be published elsewhere. A potential cause for the relatively low performance is that the BIN5aOL mandrel was not pre-oxidized and therefore the oxygen partial pressure was changed locally during heat treatment. Since BIN5c, all mandrels were pre-oxidized.



**Figure 8.** Production and test of the coil BIN5aOL. (a) The cable. (b) A piece of mullite sleeve, and a piece of mullite sleeve painted with the  $\text{TiO}_2$  slurry after a Bi-2212 heat treatment. (c) Coil after reaction exhibiting minimal deformation as well as some leakages (black discolorations). L = leakage. (d) Coil being impregnated with an epoxy resin using a vacuum bag method. (e) Coil after the vacuum impregnation. (f) Coil before the 4.2 K test. It is installed inside an aluminum alloy shell.

Note that because the CCT design allows coils to be reacted by a single layer and with minimum reactional tools (in the case of the BIN5aOL, only a layer of a ceramic cloth and a layer of an Inconel 600 cloth were added), the thickness of the coil pack is essentially the width of the Rutherford cable

used plus the spar thickness and, in this case, no larger than 50 mm. Therefore, recalling the discussion in Section 5.2, the heat treatment is manageable.

Nevertheless, the CCT design becomes a challenging approach when designing Bi-2212 insert magnets for a hybrid LTS/HTS magnet. The main challenges are described below.

### 6.1. Constraints in the Transverse Dimension

**Bore diameter (BD), outer diameter (OD), and spar thickness:** A bore aperture of 50 mm is considered by the US-MDP directive as the nominal aperture for future practical insert magnets. Moreover, the OD of the insert is constrained by the BD of the outsert magnet. From here, there are two possible scenarios: Having the insert and the outsert mechanically coupled or decoupled. In a dipole magnet, the azimuthal forces are directed towards the midplane. In the CCT concept, the spars provide transverse stiffness to the support structure; the thicker the spars, the less the layers bend transversely. This is particularly important if the insert is mechanically decoupled from the outsert, because the spars should be thick enough to support the Lorentz forces from the insert coils. If mechanically coupled, the outsert coils contribute to support the deflection of the insert, and the transverse dimension of the insert can be smaller. However, more complicated interactions take place since the outsert contributes to the load on the insert.

**Midplane rib thickness:** The individual turns are contained in channels separated by ribs. Therefore, much of the cross-section of the magnet is occupied by mandrel material. This makes the  $J_W$  in the cross-section of the CCT coils smaller than in cosine-theta coils of equivalent size, i.e., the cross-sectional efficiency of the CCT coil is dependent on the thickness of the ribs at the midplane and there is a limit on how thin the ribs can be machined depending on the mandrel material. There have been studies that aim to increase the efficiency of the CCT coils by removing the ribs in the midplane, and using a keystone cable with a keystone angle such that the turns touch completely in the midplane [83]. Since the forces in the midplane are radial, the stress would not build up on the turns and the ribs are not needed in the midplane to transfer the forces to the spar. However, this approach has not yet been demonstrated.

**Coil inner diameter (ID):** It was shown by L. Garcia Farardo et al. [83] that in small diameter CCT coils the efficiency is lower. This directly affects the design of CCT insert coils since they have to be small in order to fit inside the outsert magnet.

**Number of layers and gaps between them:** In order to cancel the solenoidal field, at least two CCT layers are needed. Therefore, a CCT magnet should be composed of an even number of layers that have to be assembled together after the heat treatment. The design of practical CCT magnets should account for a gap between layers sufficiently large for assembly purposes. In previous Nb<sub>3</sub>Sn and Bi-2212 CCT coils that follow the wind-and-react process, distortion of the Al-bronze mandrels during the heat treatment has been observed [88], especially in Bi-2212 coils that undergo heat treatment at temperatures close to the melting point of the mandrel material. This has to be taken into account in the design of the inter-layer gap. The larger the number of layers, the more space is needed for assembling the layers. Therefore, for an insert magnet it is better to have only two layers, thus, a wider Rutherford cable is needed.

**Conductor grading:** With the CCT approach, different conductor sizes can be used in the different layers in order to reduce the  $I_c$  margin. However, the Bi-2212 critical surface becomes relatively flat beyond 4 T. In an insert magnet with only two layers, grading becomes impractical.

From these considerations, the transverse space between the BD and the OD is mainly occupied by mandrel material (spars and ribs), and the higher the field needed in the insert, the more structural material is needed to manage the Lorentz forces. In addition, with the required space between layers needed to assemble them, there is little space left for the conductor to meet the high field requirements. Hence, practical Bi-2212 inserts rely on the continuous development of the Bi-2212 conductor with an improved  $J_E$ .

## 6.2. Constraints in the Longitudinal Dimension

Currently, the length of a Bi-2212 CCT magnet that can be heat treated is limited. The homogeneity zone of the 50 bar OPHT furnace, called DELTECH, at the NHMFL is 45 cm long with 14 cm diameter. The 2.4 T dipole BIN5 magnet has an OD of 63.5 mm, a tilt angle of 15°, and 13 turns in each layer to achieve a conductor region length of 0.36 m, with no straight section.

## 7. A Roadmap and Synergetic Developments

### 7.1. A US Magnet Development Program Roadmap

Within 2020–2022, the US MDP will pursue the following R&D plan:

- Build high-field Bi-2212 CCT magnets at LBNL. (1) Build 2.4 T dipole magnets using the BIN5 design. These short models serve as a fast turnaround R&D vehicle for testing technology variants. (2) Build a 5 T dipole demonstration magnet (BIN6 in Table 1) to meet the US MDP R&D goal. It has 48 turns per layer and uses 64 m of cable. It has a straight section of 11 mm and uses 5 kg of the Bi-2212 conductor. (3) Perform hybrid magnet tests. The first experiment is to test the 2.4 T BIN5 inside the Nb<sub>3</sub>Sn CCT5, an 8 T, 1 m long CCT dipole magnet that is immediately available with a bore of 90 mm. The second experiment is to test the BIN6 inside a new 11 T, 120 mm bore Nb<sub>3</sub>Sn dipole magnet being developed by the US MDP and available in 2022; the target total dipole field in the bore is >14 T. The goal of these tests are to (a) examine whether the magnet can survive mechanical stresses at 9 T and then ~14 T, (b) determine whether the Bi-2212 CCT magnets will remain quench training free, (c) examine the impacts of electromagnetic coupling and the degree of mechanical interactions between two magnets on quench detection and protection (e.g., flux jumps in Nb<sub>3</sub>Sn may induce voltages spikes in HTS). Such tests will run with two separate electrical power circuits, and (4) measure and model field quality.
- Explore a stress-management cosine-theta (SMCT) concept for both Nb<sub>3</sub>Sn [90] and Bi-2212 [91] at the Fermilab. Similar to the CCT design, the SMCT design, proposed by Zlobin et al. [90,91], also transfers the Lorentz forces of the coil to an internal structure, thus limiting the transverse load to Rutherford cables. The program is still being developed. The proposal [91] is to test a two-layer SMCT Bi-2212 coil inside either a dipole mirror structure HFDM with a background field provided by two-layer Nb<sub>3</sub>Sn coils or a MDPCT structure with a background field provided by four-layer Nb<sub>3</sub>Sn coils. Powering the Bi-2212 insert and Nb<sub>3</sub>Sn outsert independently could produce a dipole field of 12.5–13.5 T in the HFDM structure and 18–19 T in the MDPCT structure. As the first step of the program, powering the Bi-2212 and Nb<sub>3</sub>Sn coils in the series would still produce a dipole field of 9.5 and 12 T in the HFDM and MDPCT structures, respectively.
- Develop a new OPHT facility at the NHMFL. The coils that have been reacted so far have used the DELTECH OPHT furnace at the NHMFL (Figure 2d) that has a heat treatment zone of 45 cm and a diameter of 14 cm. NHMFL/FSU is constructing a larger 50 bar OPHT furnace, RENEGADE, with a homogeneity zone of 1 m long and 0.25 m in diameter. The furnace is expected to be commissioned in 2020.
- Explore a Rutherford cable based high-field solenoid concept at the NHMFL. Compared to a single-strand magnet, Rutherford cable-based solenoids have the benefits of reduced risks against point defects in a long length strand, improved stability, and easier quench protection. The program leverages on a new NHMFL test facility with a 14 T solenoid with a bore of 161 mm and an independent power supply circuit of 7.2 kA. The first step is to demonstrate the feasibility of stress management and quench protection with an insert made from a 9 m long Rutherford cable used in the CCT BIN5aOL and BIN5bOL; the insert generates 2.7 T in a background field of 14 T. If successful, the technologies developed can be extended to generate a total field of 25–30 T.
- Continue the wire R&D collaboration between the US MDP and wire and powder industry to continue the parallel development of the Bi-2212 conductor. The targeted wire  $J_E$  in coils, or the

smallest  $J_E$  achieved in a  $T_p$  of  $\pm 5$  °C is 1000 A/mm<sup>2</sup> at 4.2 K and 20 T, ~35% higher than the  $J_E$  value of the strand PMM170123 shown in Figure 5, and ~15% lower than the best  $J_E$  value of the strand PMM170123 shown in Figure 1.

Beyond 2022, the research is expected to transition to develop series-connected, >16 T hybrid dipole magnets. Putting Nb<sub>3</sub>Sn and HTS electrically in a series has many advantages, such as having a single power circuit and possibly facilitating the magnet protection.

### 7.2. Bi-2212 for >25 T User Magnets and 1.3 GHz NMR Spectrometers

Bi-2212 presents a feasible path to developing commercial, user-friendly 25–30 T solenoid systems. Bi-2212 is a round wire with a flexible diameter and current-carrying capability. Bi-2212 inserts can be placed in electrical series with the background Nb-Ti and Nb<sub>3</sub>Sn magnets, so that the quench protection of such a system can be much simpler. The NHMFL is leading the development of Bi-2212 solenoid technologies with industrial partners including Cryomagnetics, Inc. and Oxford Instruments. More than a dozen coils have been successfully constructed, reaching a peak field of 33.8 T operating a background field of 31.2 T [17]. Much understanding has been obtained in regard to OPHT [92,93], insulation materials [94], persistent superconducting joint [95], quench protection [96], and maintaining a precise winding [97] to preserve the ppb level field homogeneity required by the NMR magnets. A new mechanically reinforced strand with an axial stress limit of greater than 300 MPa has also been developed in collaboration with the Solid Material Solutions, LLC [98].

## 8. Conclusions

Bi-2212, a high-field superconducting material, has become a magnet-grade conductor. High critical current density, long length, industrially produced Bi-2212 wires have been demonstrated, with record  $J_E$  of 1000 A/mm<sup>2</sup> at 4.2 K and 27 T achieved [49,50]. A Bi-2212 high-field accelerator magnet technology is also emerging. Many elements of a successful magnet technology were demonstrated with LBNL's racetrack coil subscale magnets with Rutherford cables, including the overpressure heat treatment, insulation materials, leakage control techniques, and quench performance. A CCT magnet design is capable of addressing the weakness of the mechanical properties of Bi-2212 wires, and its fabrication issues have been explored through prototype coils. Both subscale magnets based on Bi-2212 racetrack coils and Bi-2212 CCT magnets have consistently demonstrated predictable and training free behavior. Such demonstration is still at low fields (<6 T), and the next steps within US MDP are to confirm this potential at high magnetic fields with hybrid HTS/Nb<sub>3</sub>Sn magnet tests (the background field will be provided by a 90 mm bore, 8 T CCT5 Nb<sub>3</sub>Sn dipole magnet and a planned 120 mm bore, 11 T US MDP Nb<sub>3</sub>Sn dipole magnet). The US MDP roadmap for the next three years will aim to demonstrate Bi-2212 CCT technologies at >14.1 T at 4.2 K and explore the potential of building >16 T dipole magnets.

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