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# A Fractional Complex Permittivity Model of Media with Dielectric Relaxation

Armando Ciancio 10 and Bruno Felice Filippo Flora 10 2,\*

- Department of Biomedical and Dental Sciences and Morphofunctional Imaging, University of Messina, Via Consolare Valeria c/o A.O.U. Policlinico "G.Martino", I, 98125 Messina, Italy; aciancio@unime.it
- <sup>2</sup> Engineering Office, Via Matteotti, 89044 Locri, Italy
- \* Correspondence: bruno.flora@pecprofessionisti.com

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**Abstract:** In this work, we propose a fractional complex permittivity model of dielectric media with memory. Debye's generalized equation, expressed in terms of the phenomenological coefficients, is replaced with the corresponding differential equation by applying Caputo's fractional derivative. We observe how fractional order depends on the frequency band of excitation energy in accordance with the 2nd Principle of Thermodynamics. The model obtained is validated with respect to the measurements made on the biological tissues and in particular on the human aorta.

Keywords: fractional calculus; fractional ordinary differential equations; media with dielectric relaxation

#### 1. Introduction

The frequency domain response function of a media dielectric, well-known how complex permittivity,  $e(i\omega)$ , one obtains from spectral measurement of electrical displacement field  $d(i\omega)$  respect to applied electric field  $e(i\omega)$ :

$$\epsilon (i\omega) = \frac{d(i\omega)}{e(i\omega)},\tag{1}$$

with  $\omega = 2\pi f$ ,  $i = \sqrt{-1}$ , and f being frequency.

The polarization does not follow instantaneous changes of the applied electric field, so the dielectric material is in a state of non-equilibrium. Dielectric relaxation is a process through which dielectric media reach the state of equilibrium, with one or more time constants in relation to corresponding polarization phenomena. In biological tissues, there are five independent polarization mechanisms corresponding to five dispersion spectrum [1]. Debye [2] has proposed the following complex permittivity to take into account dielectric relaxation corresponding to a linear differential equation of the first order, with constant time  $\tau$ :

$$\epsilon (i\omega) = \epsilon_{\infty} + \frac{\epsilon_s - \epsilon_{\infty}}{(1 + i\omega\tau)}, \tag{2}$$

where  $\epsilon_{\infty}$  is the initial permittivity (high frequency), and  $\epsilon_{s}$  is the static permittivity. Several complex permittivity models have been proposed, which approximate the experimental values sufficiently with respect to a given frequency band and for particular dielectrics. In the following order, the Cole–Cole model [3,4], the Cole–Davidson model [5], and the Havriliak–Negami model [6] are presented:

$$\epsilon (i\omega) = \epsilon_{\infty} + \frac{\epsilon_{s} - \epsilon_{\infty}}{\left[1 + (i\omega\tau)^{1-\alpha}\right]},\tag{3}$$

with  $0 \le \alpha < 1$ ;

$$\epsilon (i\omega) = \epsilon_{\infty} + \frac{\epsilon_{s} - \epsilon_{\infty}}{(1 + i\omega\tau)^{\beta'}}$$
(4)

with  $0 < \beta \le 1$ ;

$$\epsilon (i\omega) = \epsilon_{\infty} + \frac{\epsilon_{s} - \epsilon_{\infty}}{\left[1 + (i\omega\tau)^{1-\alpha}\right]^{\beta}}.$$
 (5)

With reference to the measures of complex permittivity, carried out in [7–10] on the biological tissues, the Cole–Cole model has been proposed to four dispersion spectrum from 10 to 20 GHz:

$$\epsilon(i\omega) = \epsilon_{\infty} + \sum_{n=1}^{4} \left[ \frac{\Delta \epsilon_n}{1 + (i\omega \tau_n)^{1-\alpha_n}} \right] + \frac{\sigma_{dc}}{i\omega \epsilon_0}, \tag{6}$$

where  $\epsilon_0 = 8.8542 \cdot 10^{-12} (F/m)$  is electric permittivity of free space,  $\tau_n$  are time constants and  $\sigma_{dc}$  is conductivity in direct current. In these models (3)–(6), the fractional nature of complex permittivity, due to the presence of the  $\alpha$  parameter how power the time's constant  $\tau$ , is evident. From the thermodynamic point of view, the dielectric relaxation phenomenon has been extensively treated [11–14]. In these works, the use of internal variables called phenomenological coefficients led to Debye's generalized equation with two constants of time:

$$\epsilon_0 \chi^{(2)} \ddot{E} + \chi^{(1)}_{(ED)} \dot{E} + \chi^{(0)}_{(ED)} E = \chi^{(2)} \ddot{D} + \chi^{(1)}_{(DE)} \dot{D} + \chi^{(0)}_{(DE)} D,$$
 (7)

where  $\chi^{(2)}$ ,  $\chi^{(1)}_{(ED)}$ ,  $\chi^{(0)}_{(ED)}$ ,  $\chi^{(1)}_{(DE)}$ ,  $\chi^{(0)}_{(DE)}$ ,  $\chi^{(0)}_{(DE)}$ , are algebraic functions of the phenomenological coefficients. Putting  $\chi^{(2)}=0$  in (7), one obtains Debye's equation. The purpose of this paper is to apply fractional calculus to the phenomenological Equation (7) by obtaining a model of complex permittivity in accordance with experimental values. There are different definitions of fractional derivatives whose application depends on the physical meaning that they represent [15–20]. In [21], Caputo and Fabrizio proposed a direct model of complex permittivity that generalizes the above-mentioned models (3)–(6), using Caputo's fractional derivative. In the fractional model proposed here, it is shown that the possible values of the fractional order  $\alpha$  must be in agreement with those that can assume the phenomenological coefficients in accordance with the 2nd principle of thermodynamics. Compared to [21], the fractional model here obtained derives from Debye's generalized Equation (7). In Section 2, Caputo's fractional derivative is applied to Debye's generalized phenomenological equation. In Section 3, by applying the fractional transformation of Laplace, the fractional model of complex permittivity is obtained. In Section 4, it is shown that the solution obtained by solving a system of four nonlinear equations, whose unknowns are the phenomenological coefficients, conforms with the 2nd principle of thermodynamics, and the fractional model proposed here is valid in accordance with the experimental results.

## 2. Fractional Generalized Debye's Equation

In [11,14], dielectric and magnetic relaxation phenomena are discussed with the aid of the general theory of non-equilibrium thermodynamics. It was shown that a vectorial internal variable, which influences the polarization, gives rise to dielectric relaxation phenomena. If one makes linear this theory and if one neglects cross effects due to electric conduction, heat conduction and viscosity on electric relaxation, the following relaxation equation may be derived:

$$\dot{E} + \chi_{(EP)}^{(0)} E = \chi_{PE}^{(2)} \ddot{P} + \chi_{(PE)}^{(1)} \dot{P} + \chi_{(PE)}^{(0)} P, \tag{8}$$

where

$$\chi_{(EP)}^{(0)} = a_{(P)}^{(1,1)} L_{(P)}^{(1,1)}, \tag{9}$$

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$$\chi_{(PE)}^{(0)} = a_{(P)}^{(0,0)} \left[ a_{(P)}^{(1,1)} - a_{(P)}^{(0,0)} \right] L_{(P)}^{(1,1)}, \tag{10}$$

$$\chi_{(PE)}^{(1)} = a_{(P)}^{(0,0)} \left[ 1 + L_{(P)}^{(0,1)} - L_{(P)}^{(1,0)} \right] + a_{(P)}^{(1,1)} \left[ L_{(P)}^{(0,0)} L_{(P)}^{(1,1)} - L_{(P)}^{(0,1)} L_{(P)}^{(1,0)} \right], \tag{11}$$

$$\chi_{(EP)}^{(2)} = L_{(P)}^{(0,0)},\tag{12}$$

where  $L_{(P)}^{(0,0)}$ ,  $L_{(P)}^{(0,1)}$ ,  $L_{(P)}^{(1,0)}$ ,  $L_{(P)}^{(1,1)}$  are the phenomenological coefficients and  $a_{(P)}^{(0,0)}$ ,  $a_{(P)}^{(1,1)}$  are scalar constants.

Replacing the constitutive equation of *P*:

$$P = D - \epsilon_0 E,\tag{13}$$

in Equation (8), with  $\chi_{PE}^{(2)} \neq 0$ , we obtain:

$$\epsilon_{0} \left\{ \ddot{E} + \frac{(1+\epsilon_{0})\chi_{PE}^{(1)}}{\epsilon_{0}\chi_{PE}^{(2)}} \dot{E} + \frac{\left[\chi_{(EP)}^{(0)} + \chi_{(PE)}^{(0)}\right]}{\epsilon_{0}\chi_{PE}^{(2)}} E \right\} = \ddot{D} + \frac{\chi_{(PE)}^{(1)}}{\chi_{PE}^{(2)}} \dot{D} + \frac{\chi_{(PE)}^{(0)}}{\chi_{PE}^{(2)}} D. \tag{14}$$

Putting

$$\chi_{ED}^{(0)} = \chi_{(EP)}^{(0)} + \chi_{(PE)}^{(0)},\tag{15}$$

$$\chi_{ED}^{(1)} = (1 + \epsilon_0) \, \chi_{PE}^{(1)},\tag{16}$$

$$\chi_{(DE)}^{(0)} = \chi_{(PE)}^{(0)},\tag{17}$$

$$\chi_{(DE)}^{(1)} = \chi_{(PE)'}^{(1)} \tag{18}$$

$$\chi^{(2)} = \chi_{PF}^{(2)} \tag{19}$$

one obtains Equation (7) in the form:

$$\epsilon_0 (\ddot{E} + A_1 \dot{E} + A_0 E) = \ddot{D} + C_1 \dot{D} + C_0 D,$$
 (20)

where

$$A_0 = \frac{\chi_{ED}^{(0)}}{\epsilon_0 \chi^{(2)}}, \ A_1 = \frac{\chi_{ED}^{(1)}}{\epsilon_0 \chi^{(2)}}, \tag{21}$$

$$C_0 = \frac{\chi_{DE}^{(0)}}{\chi^{(2)}}, C_1 = \frac{\chi_{DE}^{(1)}}{\chi^{(2)}}.$$
 (22)

By applying Caputo's fractional derivative, one obtains:

$$\epsilon_{0}\left\{{}^{c}D_{t}^{(\alpha)}\left\{{}^{c}D_{t}^{(\alpha)}\left[E\left(t\right)\right]\right\}+A_{1}^{c}D_{t}^{(\alpha)}\left[E\left(t\right)\right]+A_{0}E\left(t\right)\right\}=\ {}^{c}D_{t}^{(\alpha)}\left\{{}^{c}D_{t}^{(\alpha)}\left[D\left(t\right)\right]\right\}+C_{1}\ {}^{c}D_{t}^{(\alpha)}\left[D\left(t\right)\right]+C_{0}D\left(t\right). \tag{23}$$

Caputo's fractional derivative of order  $\alpha$  (here  $\alpha$  has a signified different from than indicated in Equations (3)–(6) is:

$${}^{c}D_{t}^{(\alpha)}\left[\phi\left(t\right)\right] = \frac{M\left(\alpha\right)}{\Gamma\left(1-\alpha\right)} \int_{0}^{t} \frac{\dot{\phi}\left(t\right)}{\left(t-\tau\right)^{\alpha}} d\tau,\tag{24}$$

where  $\Gamma(1-\alpha)$  is

$$\Gamma(1-\alpha) = \int_{0}^{\infty} \nu^{-\alpha} e^{-\nu} d\nu, \tag{25}$$

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with  $0 \le M(\alpha) \le 1$  for  $\alpha \in (0,1)$ . Equation (23) is the fractional equation corresponding to Debye's generalized Equation (14). Caputo's fractional derivative coincides, at less than one multiplicative factor  $\frac{M(\alpha)}{\Gamma(1-\alpha)}$ , with the convolution operator:

$$\Phi\left(\nu\right) = \int_{0}^{\nu} \frac{\dot{\phi}\left(\tau\right)}{\left(\nu - \tau\right)^{\alpha}} d\tau = \dot{\phi}\left(t\right) * t^{-\alpha}.$$
 (26)

This property is utilized to determine the Laplace's transform of the fractional derivative:

$$LT\left\{\Phi\left(\nu\right)\right\} = LT\left\{\dot{\phi}\left(t\right)\right\}LT\left\{t^{-\alpha}\right\},\tag{27}$$

where

$$LT\left\{\phi\left(\nu\right)\right\} = \int_{0}^{\infty} \phi\left(\nu\right) e^{-s\nu} d\nu,\tag{28}$$

and, assuming  $\phi(0) = 0$ ,

$$LT\left\{\dot{\phi}\left(\nu\right)\right\} = \int_{0}^{\infty} \dot{\phi}\left(\nu\right) e^{-s\nu} d\nu = sLT\left\{\phi\left(\nu\right)\right\},\tag{29}$$

with  $s = a + i\omega$  and  $a \in \mathbb{R}^+ \cup 0$ . If a = 0, then  $LT \{ \circ \}$  is coincident with the Fourier's transform  $FT \{ \circ \}$ . From Equation (29), Equation (27) becomes:

$$LT \left\{ \Phi \left( \nu \right) \right\} = LT \left\{ \phi \left( t \right) \right\} sLT \left\{ t^{-\alpha} \right\} = LT \left\{ \phi \left( t \right) \right\} s \int\limits_{0}^{\infty} t^{-\alpha} e^{-st} dt$$

$$= s^{\alpha} LT \left\{ \phi \left( t \right) \right\} \int\limits_{0}^{\infty} \left( st \right)^{-\alpha} e^{-st} d \left( st \right) = s^{\alpha} LT \left\{ \phi \left( t \right) \right\} \Gamma \left( 1 - \alpha \right).$$
(30)

From Equations (24) and (30), Laplace's transform of Caputo's fractional derivative is

$$LT\left\{{}^{c}D_{t}^{(\alpha)}\left[\phi\left(t\right)\right]\right\} = \frac{M\left(\alpha\right)}{\Gamma\left(1-\alpha\right)}LT\left\{\Phi\left(\nu\right)\right\} = M\left(\alpha\right)s^{\alpha}LT\left\{\phi\left(t\right)\right\}. \tag{31}$$

It can be demonstrated similarly that

$$LT\left\{{}^{c}D_{t}^{(\alpha)}\left\{{}^{c}D_{t}^{(\alpha)}\left[\phi\left(t\right)\right]\right\}\right\} = M^{2}\left(\alpha\right)s^{2\alpha}LT\left\{\phi\left(t\right)\right\}. \tag{32}$$

 $M(\alpha)$  will be placed at 1 subsequently.

## 3. The Fractional Model

By applying the Laplace's transform to both members of (23), one obtains from (31) and (32):

$$\epsilon_0 \left( s^{2\alpha} + A_1 s^{\alpha} + A_0 \right) LT \left\{ E(t) \right\} = \left( s^{2\alpha} + C_1 s^{\alpha} + C_0 \right) LT \left\{ D(t) \right\}. \tag{33}$$

Putting  $s = i\omega$ , we have that (33) becomes:

$$\epsilon_0 \left[ (i\omega)^{2\alpha} + A_1 (i\omega)^{\alpha} + A_0 \right] e(i\omega) = \left[ (i\omega)^{2\alpha} + C_1 (i\omega)^{\alpha} + C_0 \right] d(i\omega), \tag{34}$$

i.e., from (1)

$${}^{c}\epsilon^{(\alpha)}(i\omega) = \epsilon_{0} \left[ \frac{(i\omega)^{2\alpha} + A_{1}(i\omega)^{\alpha} + A_{0}}{(i\omega)^{2\alpha} + C_{1}(i\omega)^{\alpha} + C_{0}} \right]. \tag{35}$$

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Equation (35) can be rewritten as

$${}^{c}\epsilon^{(\alpha)}\left(i\omega\right) = \epsilon_{0}\left[1 + \frac{F_{1}\left(i\omega\right)^{\alpha} + F_{0}}{\left(i\omega\right)^{2\alpha} + C_{1}\left(i\omega\right)^{\alpha} + C_{0}}\right],\tag{36}$$

with

$$F_{0} = A_{0} - C_{0} = \left[\frac{\chi_{EP}^{(0)} + (1 - \epsilon_{0})\chi_{PE}^{(0)}}{\epsilon_{0}\chi^{(2)}}\right] > 0,$$

$$F_{1} = A_{1} - C_{1} = \frac{\chi_{PE}^{(0)}}{\epsilon_{0}\chi^{(2)}} > 0.$$
(37)

Observing that:  $(i)^{\alpha} = e^{i\pi(\frac{\alpha}{2})} = \cos[\pi(\frac{\alpha}{2})] + i\sin[\pi(\frac{\alpha}{2})]$  and place  ${}^ce^{(\alpha)}(i\omega) = {}^ce^{''(\alpha)}(\omega) - i{}^ce^{''(\alpha)}(\omega)$ , Equation (36) can be rewritten in two real components:

$${}^{c}\epsilon'^{(\alpha)}(\omega) = \epsilon_{0} \left[ 1 + \frac{\psi_{3}\omega^{3\alpha} + \psi_{2}\omega^{2\alpha} + \psi_{1}\omega^{\alpha} + \psi_{0}}{\omega^{4\alpha} + \xi_{3}\omega^{3\alpha} + \xi_{2}\omega^{2\alpha} + \xi_{1}\omega^{\alpha} + \xi_{0}} \right], \tag{38}$$

$${}^{c}\epsilon''(\alpha)(\omega) = \epsilon_{0} \left[ \frac{\varphi_{3}\omega^{3\alpha} + \varphi_{2}\omega^{2\alpha} + \varphi_{1}\omega^{\alpha}}{\omega^{4\alpha} + \xi_{3}\omega^{3\alpha} + \xi_{2}\omega^{2\alpha} + \xi_{1}\omega^{\alpha} + \xi_{0}} \right], \tag{39}$$

with

$$\psi_3 = F_1 \cos\left[\pi\left(\frac{\alpha}{2}\right)\right], \ \psi_2 = F_1 C_1 + F_0 \cos\left(\pi\alpha\right), \psi_1 = \left(F_0 C_1 + F_1 C_0\right) \cos\left[\pi\left(\frac{\alpha}{2}\right)\right], \ \psi_0 = F_0 C_0,$$

$$(40)$$

$$\varphi_{3} = F_{1} \sin \left[\pi \left(\frac{\alpha}{2}\right)\right], \ \varphi_{2} = -F_{0} \sin \left(\pi \alpha\right),$$
  

$$\varphi_{1} = \left(F_{0}C_{1} - F_{1}C_{0}\right) \sin \left[\pi \left(\frac{\alpha}{2}\right)\right],$$
(41)

$$\xi_3 = 2C_1 \cos\left[\pi\left(\frac{\alpha}{2}\right)\right], \ \xi_2 = C_1^2 + 2C_0 \cos\left(\pi\alpha\right), \xi_1 = 2C_1 C_0 \cos\left[\pi\left(\frac{\alpha}{2}\right)\right], \ \xi_0 = C_0^2.$$

$$(42)$$

For  $\alpha = 1$ , one obtains a Ciancio–Kluitenberg model of the complex permittivity:

$$\lim_{\alpha \to 1} \left[ {}^{c} \varepsilon^{'(\alpha)}(\omega) \right] = \varepsilon^{'}(\omega) = \epsilon_{0} \left[ 1 + \frac{(F_{1}C_{1} - F_{0}) \omega^{2} + F_{0}C_{0}}{\omega^{4} + (C_{1}^{2} - 2C_{0}) \omega^{2} + C_{0}^{2}} \right], \tag{43}$$

$$\lim_{\alpha \to 1} \left[ {}^{c} \epsilon^{"(\alpha)}(\omega) \right] = \epsilon^{"}(\omega) = \epsilon_0 \left[ \frac{F_1 \omega^3 + (F_0 C_1 - F_1 C_0) \omega}{\omega^4 + (C_1^2 - 2C_0) \omega^2 + C_0^2} \right], \tag{44}$$

with  $C_0 = [rad/s]^2$ ,  $F_0 = [rad/s]^2$ ,  $C_1 = [rad/s]$ ,  $F_1 = [rad/s]$ .

## 4. Numerical Results

The fractional model of the complex permittivity (36) is determined uniquely from the possible values of the parameters  $C_0$ ,  $F_0$ ,  $C_1$ ,  $F_1$  that satisfaction (36) with  $C_0 > 0$ ,  $C_1 > 0$ ; this is in accordance with the fact that entropy variation is positive, reference [11], for the 2nd principle of the thermodynamics. The fractional order  $\alpha$  depends on the frequency and parameters by means of undefined function. In [3], the Debye's ordinary model is in accordance with experimental measures at low frequencies. We can formulate the problem in this way:

Let  $\mathbf{x} = (C_0, C_1, F_0, F_1) \in \mathbb{C}^4$ ,  $\omega \in \mathbb{B} = (\omega_{min}, \omega_{max}) \subseteq \mathbb{R}^+$  and let  $\mathbb{S} \subseteq \mathbb{C}^4$  be the solutions set of the system nonlinear equations:

$$\begin{cases}
\epsilon'_{min}(\omega_{min}) = \zeta_{1}(\mathbf{x}; \omega_{min}, \hat{\alpha}), \\
\epsilon''_{min}(\omega_{min}) = \zeta_{2}(\mathbf{x}; \omega_{min}, \hat{\alpha}), \\
\epsilon'_{max}(\omega_{max}) = \zeta_{3}(\mathbf{x}; \omega_{max}, \hat{\alpha}), \\
\epsilon''_{max}(\omega_{max}) = \zeta_{4}(\mathbf{x}; \omega_{max}, \hat{\alpha}),
\end{cases}$$
(45)

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with  $\mathbf{x}$  unknown and  $\epsilon_{min}'$ ,  $\epsilon_{min}''$ ,  $\epsilon_{max}''$ ,  $\epsilon_{max}''$ , known experimental, while  $\hat{\alpha} \in (0,1)$  is value of  $\alpha$  such that solution of system (45) indicated with  $\hat{\mathbf{x}}$  satisfaction (36), and it provides the best predictive model of complex permittivity.

In other words, if  $\alpha = g(\mathbf{x}, \omega)$ , where  $g(\mathbf{x}, \omega)$  is unknown function of  $\alpha$ , denoting with  $\hat{\mathbb{R}} = (\mathbb{R}^+ \times \mathbb{R}^+ \times \mathbb{R}^+ \times \mathbb{R}^+)$ , we have that  $\hat{\alpha}$  is:

$$\hat{\alpha} = \min_{[\mathbf{x} \in \Sigma, \ \omega \in \mathbb{B}]} \{ g(\mathbf{x}, \omega) \}, \tag{46}$$

with  $\Sigma = \mathbb{S} \cap \hat{\mathbb{R}} \neq \emptyset$ .

We propose the following algorithm (Figure 1) to determine the abovementioned parameters of (36).

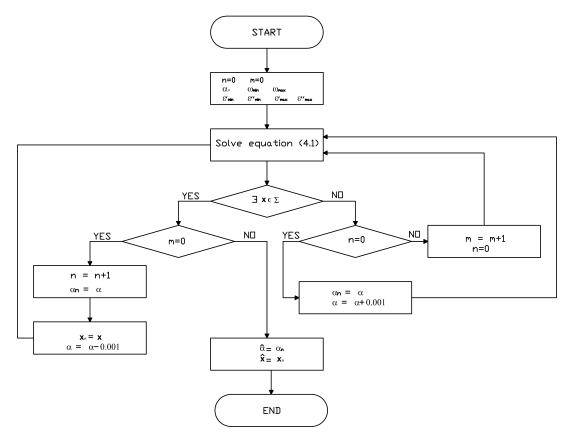
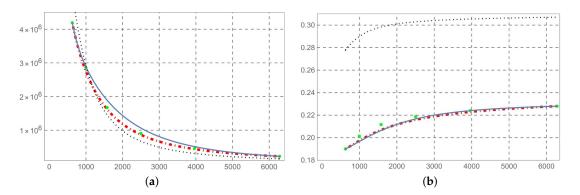


Figure 1. Flow-chart.

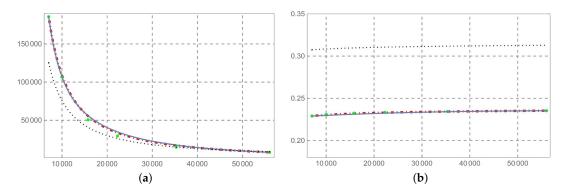
- Step 1 one chooses a frequency range  $(\omega_{min}, \omega_{max})$  and a test value for  $\alpha$ ; one read the correspondent permittivity experimental values:  $\epsilon'^{(\alpha)}(\omega_{min}), \epsilon''^{(\alpha)}(\omega_{min}), \epsilon'^{(\alpha)}(\omega_{max}), \epsilon''^{(\alpha)}(\omega_{max});$  one initializes n=0 and m=0.
- Step 2 one resolves the system at frequencies  $\omega_{min}$  and  $\omega_{max}$ .
- Step 3 If there is a real and positive solution, then if m is not null go to end; otherwise, one puts: n = n + 1; m = 0;  $\alpha_n = \alpha$ ;  $(C_0)_n = C_0$ ;  $(F_0)_n = F_0$ ;  $(C_1)_n = C_1$ ;  $(F_1)_n = F_1$ ; it reduces  $\alpha = \alpha 0.001$  and go back to step 2.
- Step 4 If n is null, one puts  $\alpha_n = \alpha$  and  $\alpha = \alpha + 0.001$  and go back to step 2; otherwise, one puts m = m + 1, n = 0 and goes back to step 2.
  - End The solution so determined is compared with the predictive permittivity model in [10], at a temperature of 37 °C with reference to the human aorta. This method is equally

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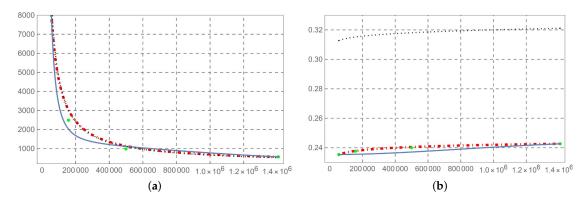
applicable to biological tissues. From Figures 2–8 (horizontal axis rad/s), we observe that a predictive fractional model of the complex permittivity is in accordance with experimental data with good approximation. The experimental data are those relating to measure campaign published in [10]. In particular from Figure 9, we see that percentage error relative permittivity and conductivity to experimental data is, respectively, almost always lower and thorough than that of the Ciancio–Kluitenberg model and Cole–Cole extended model [7–10]. In the frequency range  $2.5 \times 10^3$  @  $9.29 \times 10^{10}$ , the maximum relative error to experimental data of permittivity fractional model is -21% at  $1.58 \times 10^5$  rad/s; of Ciancio–Kluitenberg's model is +25% at  $1.58 \times 10^7$  rad/s and extended of Cole–Cole's model is +35% at  $1.58 \times 10^7$  rad/s; in the same frequency range, the maximum relative error to experimental data of conductivity fractional model is +15% at  $1.95 \times 10^{10}$  rad/s; of Ciancio–Kluitenberg's model is +41% at  $1.95 \times 10^{10}$  rad/s and extended of Cole–Cole's model is -37% at  $2.5 \times 10^3$  rad/s. In Figure 10, we show the trend of fractional order with respect to the frequency.



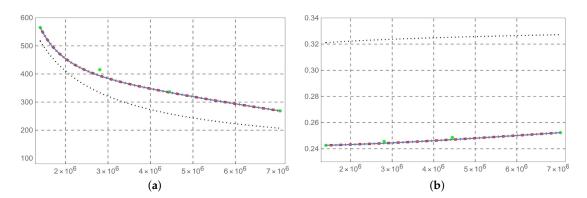
**Figure 2.** (a) Permittivity and (b) conductivity at frequencies 100 Hz @ 1 KHz. Line dot-dashed fractional model  $\alpha = 0.983$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



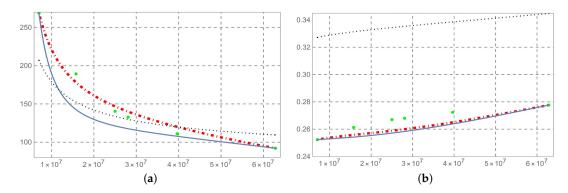
**Figure 3.** (a) Permittivity and (b) conductivity at frequencies 1 KHz @ 9 KHz. Line dot-dashed fractional model  $\alpha = 0.985$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



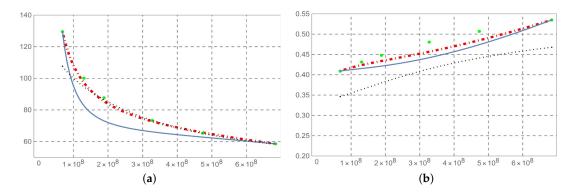
**Figure 4.** (a) Permittivity and (b) conductivity at frequencies 9 KHz @ 224 KHz. Line dot-dashed fractional model  $\alpha = 0.990$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



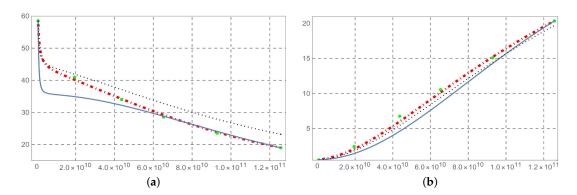
**Figure 5.** (a) Permittivity and (b) conductivity at frequencies 224 KHz @ 1 MHz. Line dot-dashed fractional model  $\alpha=1$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



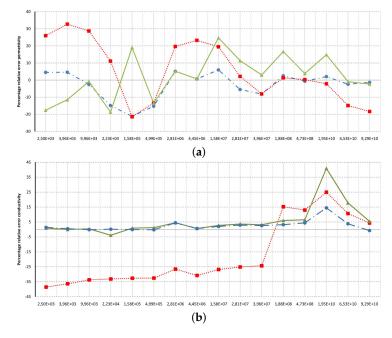
**Figure 6.** (a) Permittivity and (b) conductivity at frequencies 1 MHz @ 10 MHz. Line dot-dashed fractional model  $\alpha=0.975$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



**Figure 7.** (a) Permittivity and (b) conductivity at frequencies 10 MHz @ 100 MHz. Line dot-dashed fractional model  $\alpha=0.936$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



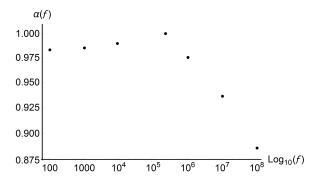
**Figure 8.** (a) Permittivity and (b) conductivity 100 MHz @ 20 GHz. Line dot-dashed fractional model  $\alpha=0.983$ , line continue ordinary model, line dotted extensive Cole–Cole's model, points experimental data.



**Figure 9.** Relative percentage error (a) permittivity and (b) conductivity. Line dot-dashed fractional model, line continue Ciancio–Kluitenberg model, line dotted extensive Cole–Cole's model, points experimental data.

#### 5. Conclusions

It is emphasized that this fractional model derives from a physical theory that justifies the phenomenon of polarization on biological tissues. In particular, the Ciancio–Kluitenberg model has shown how the two time constants are related to strain and rotation of the cells that constitute the polarized biological tissue. Models like that of extended Cole–Cole are characterized by parameters whose values are empirically obtained i.e., without a justification of a physical nature. The transition to the fractional calculation was possible by replacing the ordinary derivative with Caputo's fractional derivative to write the corresponding phenomenological equation of media with dielectric relaxation. From the complex permittivity model obtained, it has been seen (Figure 10) how the topology of the memory operator has fractional dimension frequency dependency and also that this tends to a minimum value in accordance with the 2nd Principle of Thermodynamics. The fractional model of the complex permittivity is in accordance with experimental data with good approximation. The reason why permittivity and conductivity deviates from experimental data at a given frequency ranges is not known, but this probably depends on the type of fractional derivative considered. A possible development of the proposed method is to determine the fixed fractional operator, the optimal fractional order functional with respect to frequency that minimizes the relative percentage error.



**Figure 10.** Trend fractional order respect to frequency.

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**Author Contributions:** These two authors contribute equally to this paper.

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