



Article Dual Penta-Compound Combination Anti-Synchronization with Analysis and Application to a Novel Fractional Chaotic System

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Abstract: This paper studies a fractional-order chaotic system with sine non-linearities and highlights its dynamics using the Lyapunov spectrum, bifurcation analysis, stagnation points, the solution of the system, the impact of the fractional order on the system, etc. The system considering uncertainties and disturbances was synchronized using dual penta-compound combination anti-synchronization among four master systems and twenty slave systems by non-linear control and the adaptive sliding mode technique. The estimates of the disturbances and uncertainties were also obtained using the sliding mode technique. The application of the achieved synchronization in secure communication is illustrated with the help of an example.

Keywords: synchronization; secure communication; bifurcation analysis; Lyapunov dynamics

1. Introduction

The three-centuries-old theory of fractional calculus, which is the generalization of integer calculus, has found glory quite recently. Fractional calculus is being implemented to model various real-life systems in almost all disciplines. In fact, fractional calculus is seen as the future of mathematical modeling. Fractional calculus with its better hered-itary properties is used to model various biological models such as the prey-predator model [1] and the human liver [2], engineering models such as harmonic oscillators [3] and thermostats [4], geophysical models such as Earth's dynamo [5], and so on. Fractional computations have attracted researchers worldwide in dynamical systems such as the Chua circuit, the Duffing system, and the logistic system. Chaotic systems being highly sensitivity to system values have contributed greatly in the development of information security, computers, communications [6], and encryption [7]. Chaotic systems help mask the information signal to avoid hacking by intruders. Chaos synchronization plays a major role in the decryption of the information signal from the masked signal. Chaotic systems with other



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). chaotic systems. Many standard and non-standard chaotic systems have been constructed recently. The chaotic systems are classified on the basis of the number of stagnation points, the stability of stagnation points—stable, unstable, partially stable—[8], and the shape of the chaotic attractorsone to four wings [9], spherical shape [10], torus shape [11], and double scroll [12]. The study of these chaotic/hyperchaotic systems highlights their unique and mesmerizing dynamics.

Credit is due to Pecora and Carroll [13], who first performed complete synchronization between two chaotic systems in 1990 by designing controllers. Many synchronization techniques such as double compound synchronization [14], difference synchronization [15], lag synchronization, phase synchronization [16], combination synchronization [17], parallel synchronization [18], dislocated synchronization [19], and fractional matrix and inverse fractional matrix synchronizations [20,21] have been developed since then. Various control techniques have been designed to achieve synchronization such as the parameter estimation adaptive technique, the sliding mode technique, the tracking control technique, and the active control technique. Active control is considered the easiest to apply, and sliding mode control is considered as the most robust. Disturbances and uncertainties are also estimated using this technique.

Chaos synchronization, which was introduced in the case of a one master and one slave system, was generalized by increasing the number of master and slave systems such as combination synchronization(two master systems with a slave system or vice versa), combination–combination synchronization [22] (two or more master systems with two or more slave systems), compound synchronization [23] (three master systems—scaling and base master systems with one slave system), compound combination synchronization [24] (comprising both compound and combination synchronization), and so on. In this paper, we generalize these techniques to four master systems and twenty slave systems viz. dual penta-compound combination anti-synchronization.

Motivated by the above, a novel fractional-order chaotic system with two sine nonlinearities is given. Thorough analysis [25] was performed using the Lyapunov spectrum [26], bifurcation analysis, the solution of the system, stagnation points, and the effect of the fractional order on system. The novel system considering uncertainties and disturbances was synchronized by introducing dual penta-compound combination antisynchronization among four master systems and twenty slave systems using different methods. The estimation of unknown disturbances and uncertainties was also performed, and the technique was applied in secure communication with an example.

The present paper is divided as follows: Section 2 gives the preliminaries of fractional derivatives. Section 3 introduces the novel fractional-order chaotic system. Section 4 discusses the dynamics of the novel system. Section 5 introduces the novel synchronization technique viz. dual penta-compound combination anti-synchronization via non-linear control and adaptive sliding mode control and gives its proposed application. Section 6 concludes the paper.

2. Preliminaries

The fractional-order derivative can be defined in various forms such as Riemann–Liouville's derivative, Grünwald–Letnikov's derivative, Caputo's derivative, etc.

Riemann-Liouville's derivative:

$$_{t_0}D_t^{\alpha}f(t) = \frac{d^n}{dt^n} \left[\frac{1}{\Gamma(n-\alpha)} \int_{t_0}^t \frac{f(\tau)}{(t-\tau)^{\alpha-n+1}} d\tau\right], \quad t > t_0.$$

where α is the fractional derivative, $n - 1 < \alpha < n, n \in \mathbb{N}$, and $\Gamma(\alpha) = \int_0^\infty x^{\alpha - 1} e^{-x}$ is the Gamma function.

Caputo's derivative:

$$_{t_0}D_t^{\alpha}f(t) = rac{1}{\Gamma(n-\alpha)}\int_{t_0}^t rac{f^{(n)}(\tau)}{(t-\tau)^{\alpha-n+1}}d\tau, \quad t>t_0.$$

where α is the fractional derivative, $n - 1 < \alpha < n, n \in \mathbb{N}$, and $\Gamma(\alpha) = \int_0^\infty x^{\alpha - 1} e^{-x}$ is the Gamma function.

Grünwald-Letnikov's derivative:

$$_{t_0}D_t^{\alpha}f(t)\mid_t=kh=lim_{h\to 0}\frac{1}{h^{\alpha}}\sum_{j=0}^{\lfloor\frac{t-c}{h}\rfloor}\omega_j^{\alpha}f(kh-jh).$$

where *h* shows the sample time. |.| is the floor function, and the coefficients:

$$\omega_j^{\alpha} = \frac{(-1)^j \Gamma(\alpha + 1)}{\Gamma(j+1) \Gamma(\alpha - j + 1)}, j = 0, 1, 2, \dots, k$$

Among the many fractional derivative [27] definitions, in this paper, Caputo's derivative of fractional order is considered. Caputo's definition uses the integer derivative for computation, whereas Riemann–Liouville's derivative uses the fractional derivative for computation. Therefore, Caputo's derivative has an edge over other derivatives.

3. New Fractional Chaotic System

Introduce the fractional chaotic system as:

$$D^{q}Z_{1} = Z_{2} + Z_{3} - Asin(Z_{2}).$$

$$D^{q}Z_{2} = -Z_{1} + Z_{3}.$$

$$D^{q}Z_{3} = -Z_{1} - Z_{3} + Bsin(Z_{1}).$$
(1)

where $Z \in R^3$ are state variables for $A, B \in R$.

For A = 5, B = 5, and initial conditions (0.000001, 3, 0) for fractional order 0.987, System (1) is chaotic as displayed in Figures 1 and 2 in time series and phase plots, respectively.



Figure 1. State trajectories of (1).



Figure 2. Phase diagrams of (1).

4. Dynamics of the Novel System

4.1. Symmetry, Dissipativity, and Stagnation Points

The novel fractional-order chaotic system (1) does not show rotational symmetry about any axis, as the system does not remain invariant under the transformation $Z_i \rightarrow -Z_i$, $Z_j \rightarrow -Z_j$, $Z_k \rightarrow Z_k$. However, the system shows symmetry about the origin as the system remains invariant under $Z_1 \rightarrow -Z_1$, $Z_2 \rightarrow -Z_2$, $Z_3 \rightarrow -Z_3$.

The matrix form of System (1) is:

$$\begin{bmatrix} D^q Z_1 \\ D^q Z_2 \\ D^q Z_3 \end{bmatrix} = \begin{bmatrix} K_1(Z_1, Z_2, Z_3) \\ K_2(Z_1, Z_2, Z_3) \\ K_3(Z_1, Z_2, Z_3) \end{bmatrix} = \begin{bmatrix} Z_2 + Z_3 - Asin(Z_2) \\ -Z_1 + Z_3 \\ -Z_1 - Z_3 + Bsin(Z_1) \end{bmatrix}$$

The divergence of vector field *K* is:

$$\nabla K = \frac{\partial (Z_2 + Z_3 - Asin(Z_2))}{\partial Z_1} + \frac{\partial (-Z_1 + Z_3)}{\partial Z_2} + \frac{\partial (-Z_1 - Z_3 + Bsin(Z_1))}{\partial Z_3}$$
$$= 0 + 0 - 1.$$

i.e.,

$$\nabla K = -1 < 0.$$

Hence, System (1) is dissipative.

Equating $K_i(V_1, V_2, V_3)$ to zero for i = 1, 2, 3, the stagnation points are:

$$Z_2 + Z_3 - Asin(Z_2) = 0.$$

 $-Z_1 + Z_3 = 0.$
 $-Z_1 - Z_3 + Bsin(Z_1) = 0.$

For A = B = 5, we have stagnation point (0,0,0).

4.2. Solution of the Novel Fractional-Order Chaotic System

The novel fractional-order chaotic system is expressed as:

$$D^q Z(t) = \Psi(Z(t)),$$

where $t \in (0, T]$ and $Z(0) = Z_0$. Here:

$$Z = \begin{bmatrix} Z_1 \\ Z_2 \\ Z_3 \end{bmatrix}, Z_o = \begin{bmatrix} Z_1 o \\ Z_2 o \\ Z_3 o \end{bmatrix},$$

$$\Psi(Z(t)) = \begin{bmatrix} Z_2 + Z_3 - Asin(Z_2) \\ -Z_1 + Z_3 \\ -Z_1 - Z_3 + Bsin(Z_1) \end{bmatrix}.$$

The solution is examined in the region $\omega \times I$, where I = (0, T] and $\omega = (Z_i) : max|Z_i| \le P$ for i = 1, 2, 3, P > 0, where constant *P* designs a boundary in the phase space.

Equivalently, the I.V.P. is:

$$Z(t) = Z_o + \int_0^t \Psi(Z(s)) ds.$$

Let $Z_o + \int_0^t \Psi(Z(s)) ds = S(Z)$ with $Z_1, Z_2 \in \mathbb{R}^3$. Then:

$$S(Z_1) - S(Z_2) = \int_0^t (\Psi(Z_1(s)) - \Psi(Z_2(s))) ds$$

Hence:

$$|S(Z_1) - S(Z_2)| = |\int_0^t (\Psi(Z_1(s)) - \Psi(Z_2(s)))ds|.$$

We define the norm for $g(t) \in C(0,T]$ given by $Sup_{t\in(0,T]}|g(t)|$ and for matrix $G = [g_{ij}(t)]$ with $g_{ij}(t) \in C(0,T]$; define $||G|| = \sum_{i,j} Sup_{t\in(0,T]}|g_{ij}(t)|$.

$$\Rightarrow ||S(Z_1) - S(Z_2)|| \le P_1 ||Z_1 - Z_2||.$$

where $P_1 = Tmax(7, 6, 3)$.

Thus, for S(Z), $0 < P_1 < 1$ is a contraction mapping.

4.3. Lyapunov Dynamics and Bifurcation Analysis

With the idea of the rate of separation of closely lying trajectories in the phase space, the Lyapunov spectrum values are found. For A = B = 5 and initial conditions (0.000001, 3, 0), the Lyapunov dynamics for q = 0.987 are:

$$0.6193.$$

 $-0.0724 pprox 0$
 $-1.6056.$

The first component being positive confirms chaos. The dimension (K.Y.) is found by:

$$D_{YK} = p + \frac{\sum_{s=1}^{p} L.E._s}{|L.E._{p+1}|}.$$

where *p* is maximum number satisfying $\sum_{s=1}^{p} L.E_{s} \ge 0$ and $\sum_{s=1}^{p+1} L.E_{s} < 0$. Therefore, the K.Y. dimension is 2.34062.

Parameter values and initial conditions have a very sensitive dependence on the system dynamics. A slight change in these values of the system can lead to drastically

different dynamics. Even in the smallest neighborhood of the parameter values, the dynamics may vary in the number of equilibrium points (none, finite, countably infinite, uncountably infinite), their stability, and from the regular nature to the periodic to the chaotic nature. In bifurcation analysis, only one parameter value is varied in a slight neighborhood, while others are kept constant. In Figure 3a, *A* is varied in (4.75, 5.25) and *B* = 5; in Figure 3b, *B* is varied in (4.75, 5.25) and *A* = 5. The effect of the fractional order is given in Figure 4.



Figure 3. Bifurcation diagram of (1) for (a) $4.75 \le A \le 5.25$ and (b) $4.75 \le B \le 5.25$.



Figure 4. Dynamics of (2) for $0.8 \le q \le 1$.

4.4. Stability of the Trivial Equilibrium Point

Clearly, the origin is the equilibrium point of the system. We check its stability by finding the Jacobian matrix as:

0	-4	1]	
$^{-1}$	0	1	
4	0	-1	

The eigenvalues of the above matrix are:

$$\mu_1 = 1.43459 + 1.02145i.$$

 $\mu_2 = 1.43459 - 1.02145i.$
 $\mu_3 = -3.86919.$

Here, μ_1 , μ_2 are complex eigenvalues with a positive real part and μ_3 is a negative eigenvalue, which together imply that the system is unstable.

Since all eigenvalues have a non-zero real part, the equilibrium point is hyperbolic.

5. Dual Penta-Compound Combination Anti-Synchronization

Consider four master systems and twenty slave systems, the first ten slave systems corresponding to the first two master systems and the next ten slave systems corresponding to the next two master systems for dual penta-compound combination anti-synchronization.

Master System I:

$$D^{q}Z_{11} = Z_{12} + Z_{13} - 5sin(Z_{12}) + \bar{U}_{1}.$$

$$D^{q}Z_{12} = -Z_{11} + Z_{13} + \bar{U}_{2}.$$

$$D^{q}Z_{13} = -Z_{11} - Z_{13} + 5sin(Z_{11}) + \bar{U}_{3}.$$
(2)

For I.C. (0.000001, 3, 0), q = 0.987, (2) is chaotic. Here, $\overline{U}_1, \overline{U}_2, \overline{U}_3$ are controllers to be designed.

Master System II:

$$D^{q}Z_{21} = Z_{22} + Z_{23} - 5sin(Z_{22}) + \triangle H_{1} + D_{1} + \bar{U}_{4}.$$

$$D^{q}Z_{22} = -Z_{21} + Z_{23} + \triangle H_{2} + D_{2} + \bar{U}_{5}.$$
(3)

$$D^{q}Z_{23} = -Z_{21} - Z_{23} + 5sin(Z_{21}) + \triangle H_{3} + D_{3} + \bar{U}_{6}.$$

For I.C. (0.000001, 3, 0), q = 0.987, (3) is chaotic. Here, U_4 , U_5 , U_6 are controllers to be designed.

Master System III:

$$D^{q}Z_{31} = Z_{32} + Z_{33} - 5sin(Z_{32}) + \bar{V}_{1}.$$

$$D^{q}Z_{32} = -Z_{31} + Z_{33} + \bar{V}_{2}.$$

$$D^{q}Z_{33} = -Z_{31} - Z_{33} + 5sin(Z_{31}) + \bar{V}_{3}.$$
(4)

For I.C. (0.000001,3,0), q = 0.95, (4) is chaotic. Here, V_1, V_2, V_3 are controllers to be designed.

Master System IV:

$$D^{q}Z_{41} = Z_{42} + Z_{43} - 5sin(Z_{42}) + \triangle H_4 + D_4 + \bar{V}_4.$$

$$D^{q}Z_{42} = -Z_{41} + Z_{43} + \triangle H_5 + D_5 + \bar{V}_5.$$

$$D^{q}Z_{43} = -Z_{41} - Z_{43} + 5sin(Z_{41}) + \triangle H_6 + D_6 + \bar{V}_6.$$
(5)

For I.C. (0.000001, 3, 0), q = 0.95, (5) is chaotic. Here, V_4 , V_5 , V_6 are controllers to be designed.

Phase portraits of (2)–(5) are given in Figure 5.



Figure 5. Phase portraits of Master Systems (2)-(5).

Slave System I:

$$D^{q}\psi_{11} = 121\psi_{12} - 5\psi_{11}.$$

$$D^{q}\psi_{12} = \psi_{11}\psi_{13} - \psi_{12} + \psi_{11}.$$

$$D^{q}\psi_{13} = -\psi_{11}\psi_{12} - \psi_{13}.$$
(6)

For I.C. (0.1, 1.2, 0.5) and q = 0.987, Figure 6a gives the phase diagram.

Slave System II:

$$D^{q}\psi_{21} = 83.6\psi_{22} - 83.6\psi_{23} - 10\psi_{21}.$$

$$D^{q}\psi_{22} = \psi_{21}\psi_{23} - \psi_{22} + 12\psi_{12}.$$

$$D^{q}\psi_{23} = -\psi_{21}\psi_{22} - 12\psi_{21} - \psi_{23}.$$
(7)

For I.C. (-2, 3, 5) and q = 0.987, Figure 6b gives the phase diagram.

Slave System III:

$$D^{q}\psi_{31} = -2\psi_{31} + \psi_{32}\psi_{33}.$$

$$D^{q}\psi_{32} = -2\psi_{32} + \psi_{33}\psi_{31} - 5\psi_{31}.$$

$$D^{q}\psi_{33} = 1 - \psi_{31}\psi_{32}.$$
(8)

For I.C. (-4, 2.5, 2) with q = 0.987, Figure 6c gives the phase diagram. Slave System IV:

$$D^{q}\psi_{41} = 10\psi_{42} - 10\psi_{41}.$$

$$D^{q}\psi_{42} = 28\psi_{41} - \psi_{42} - \psi_{41}\psi_{43}.$$

$$D^{q}\psi_{43} = \frac{8}{3}\psi_{43} + \psi_{41}\psi_{42}.$$
(9)

For I.C. (2, 3, 5) and q = 0.987, Figure 6d gives the phase diagram. Slave System V:

$$D^{q}\psi_{51} = 35\psi_{51} - 35\psi_{51}.$$

$$D^{q}\psi_{52} = -7\psi_{51} - \psi_{51}\psi_{53} + 28\psi_{52}.$$

$$D^{q}\psi_{53} = \psi_{51}\psi_{52} - 3\psi_{53}.$$
(10)

For I.C. (3, 4, 5) and q = 0.987, Figure 6e gives the phase diagram. Slave System VI:

$$D^{q}\psi_{61} = -\psi_{62} - \psi_{63}.$$

$$D^{q}\psi_{62} = \psi_{61} + 0.4\psi_{62}.$$

$$D^{q}\psi_{63} = 0.2 + \psi_{63}(\psi_{61} - 10).$$
(11)

For I.C. (2, -6, 3) and q = 0.987, Figure 6f gives the phase diagram. Slave System VII:

$$D^{q}\psi_{71} = 0.7\psi_{71} - \psi_{72}\psi_{73}.$$

$$D^{q}\psi_{72} = -0.1\psi_{72} + \psi_{71}\psi_{73}.$$

$$D^{q}\psi_{73} = -0.001 - \psi_{73} + \psi_{71}\psi_{72} + 0.1\psi_{73}\psi_{72}.$$
(12)

For I.C. (0.1, 0.2, 0.3) and q = 0.987, Figure 6g gives the phase diagram. Slave System VIII:

$$D^{q}\psi_{81} = 0.7\psi_{81} - 2\psi_{82}\psi_{83}.$$

$$D^{q}\psi_{82} = -0.1\psi_{82} + 2\psi_{81}\psi_{83}.$$

$$D^{q}\psi_{83} = -0.001 - \psi_{83} + 2\psi_{81}\psi_{82} + 0.2\psi_{83}\psi_{82}.$$
(13)

For I.C. (0.2, 0.4, 0.6) and q = 0.987, Figure 6h gives the phase diagram. Slave System IX:

$$D^{q}\psi_{91} = 0.7\psi_{91} - 3\psi_{92}\psi_{93}.$$

$$D^{q}\psi_{92} = -0.1\psi_{92} + 3\psi_{91}\psi_{93}.$$

$$D^{q}\psi_{93} = -0.001 - \psi_{93} + 3\psi_{91}\psi_{92} + 0.3\psi_{93}W_{92}.$$
(14)

For I.C. (0.3, 0.6, 0.9) and q = 0.987, Figure 6i gives the phase diagram. Slave System X:

$$D^{q}\psi_{101} = 0.7\psi_{101} - 4\psi_{102}\psi_{103}.$$

$$D^{q}\psi_{102} = -0.1\psi_{102} + 4\psi_{101}\psi_{103}.$$

$$D^{q}\psi_{103} = -0.001 - \psi_{103} + 4\psi_{101}\psi_{102} + 0.4\psi_{103}\psi_{102}.$$
(15)

For I.C.
$$(0.4, 0.8, 1.2)$$
 and $q = 0.987$, Figure 6j gives the phase diagram. Slave System XI:

$$D^{q}\psi_{111} = 121\psi_{112} - 5\psi_{111}.$$

$$D^{q}\psi_{112} = \psi_{111}\psi_{113} - \psi_{112} + \psi_{111}.$$

$$D^{q}\psi_{113} = -\psi_{111}\psi_{112} - \psi_{113}.$$
(16)

For I.C. (0.1, 1.2, 0.5) and q = 0.987, Figure 6a gives the phase diagram. Slave System XII:

$$D^{q}\psi_{121} = 83.6\psi_{122} - 83.6\psi_{123} - 10\psi_{121}.$$

$$D^{q}\psi_{122} = \psi_{121}\psi_{123} - \psi_{122} + 12\psi_{112}.$$

$$D^{q}\psi_{123} = -\psi_{121}\psi_{122} - 12\psi_{121} - \psi_{123}.$$
(17)

For I.C. (-2, 3, 5) and q = 0.987, Figure 6b gives the phase diagram. Slave System XIII:

$$D^{q}\psi_{131} = -2\psi_{131} + \psi_{132}\psi_{133}.$$

$$D^{q}\psi_{132} = -2\psi_{132} + \psi_{133}\psi_{131} - 5\psi_{131}.$$

$$D^{q}\psi_{133} = 1 - \psi_{131}\psi_{132}.$$
(18)

For I.C. (-4, 2.5, 2) and q = 0.987, Figure 6c gives the phase diagram. Slave System XIV:

$$D^{q}\psi_{141} = 10\psi_{142} - 10\psi_{141}.$$

$$D^{q}\psi_{142} = 28\psi_{141} - \psi_{142} - \psi_{141}\psi_{143}.$$

$$D^{q}\psi_{143} = \frac{8}{3}\psi_{143} + \psi_{141}\psi_{142}.$$
(19)

For I.C. (2, 3, 5) and q = 0.987, Figure 6d gives the phase diagram. Slave System XV:

$$D^{q}\psi_{151} = 35\psi_{151} - 35\psi_{151}.$$

$$D^{q}\psi_{152} = -7\psi_{151} - \psi_{151}\psi_{153} + 28\psi_{152}.$$

$$D^{q}\psi_{153} = \psi_{151}\psi_{152} - 3\psi_{153}.$$
(20)

For I.C. (3, 4, 5) and q = 0.987, Figure 6e gives the phase diagram. Slave System XVI:

$$D^{q}\psi_{161} = -\psi_{162} - \psi_{163}.$$

$$D^{q}\psi_{162} = \psi_{161} + 0.4\psi_{162}.$$

$$D^{q}\psi_{163} = 0.2 + \psi_{163}(\psi_{161} - 10).$$
(21)

For I.C. (2, -6, 3) and q = 0.987, Figure 6f gives the phase diagram. Slave System XVII:

$$D^{q}\psi_{171} = 0.7\psi_{171} - \psi_{172}\psi_{173}.$$

$$D^{q}\psi_{172} = -0.1\psi_{172} + \psi_{171}\psi_{173}.$$

$$D^{q}\psi_{173} = -0.001 - \psi_{173} + \psi_{171}\psi_{172} + 0.1\psi_{173}\psi_{172}.$$
(22)

For I.C. (0.1, 0.2, 0.3) and q = 0.987, Figure 6g gives the phase diagram. Slave System XVIII:

$$D^{q}\psi_{181} = 0.7\psi_{181} - 2\psi_{182}\psi_{183}.$$

$$D^{q}\psi_{182} = -0.1\psi_{182} + 2\psi_{181}\psi_{183}.$$

$$D^{q}\psi_{183} = -0.001 - \psi_{183} + 2\psi_{181}\psi_{182} + 0.2\psi_{183}\psi_{82}.$$
(23)

For I.C. (0.2, 0.4, 9.6) and q = 0.987, Figure 6h gives the phase diagram. Slave System XIX:

$$D^{q}\psi_{191} = 0.7\psi_{191} - 3\psi_{192}\psi_{193}.$$

$$D^{q}\psi_{192} = -0.1\psi_{192} + 3\psi_{191}\psi_{193}.$$

$$D^{q}\psi_{193} = -0.001 - \psi_{193} + 3\psi_{191}\psi_{192} + 0.3\psi_{193}W_{92}.$$
(24)

For I.C. (0.3, 0.6, 0.9) and q = 0.987, Figure 6i gives the phase diagram. Slave System XX:

$$D^{q}\psi_{201} = 0.7\psi_{201} - 4\psi_{202}\psi_{203}.$$

$$D^{q}\psi_{202} = -0.1\psi_{202} + 4\psi_{201}\psi_{203}.$$

$$D^{q}\psi_{203} = -0.001 - \psi_{203} + 4\psi_{201}\psi_{202} + 0.4\psi_{203}\psi_{202}.$$
(25)

For I.C. (0.4, 0.8, 1.2) and q = 0.987, Figure 6j gives the phase diagram. Define the dual penta-compound combination anti-synchronization error:

$$\begin{split} E_1 &= (Z_{11} + Z_{21}) + (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(\psi_{51} + \psi_{61})(\psi_{71} + \psi_{81})(\psi_{91} + \psi_{101}).\\ E_2 &= (Z_{12} + Z_{22}) + (\psi_{12} + \psi_{22})(\psi_{32} + \psi_{42})(\psi_{52} + \psi_{62})(\psi_{72} + \psi_{82})(\psi_{92} + \psi_{102}).\\ E_3 &= (Z_{13} + Z_{23}) + (\psi_{13} + \psi_{23})(\psi_{33} + \psi_{43})(\psi_{53} + \psi_{63})(\psi_{73} + \psi_{83})(\psi_{93} + \psi_{103}).\\ E_4 &= (Z_{31} + Z_{41}) + (\psi_{111} + \psi_{121})(\psi_{131} + \psi_{141})(\psi_{151} + \psi_{161})(\psi_{171} + \psi_{181})(\psi_{191} + \psi_{201}).\\ E_5 &= (Z_{32} + Z_{42}) + (\psi_{112} + \psi_{122})(\psi_{132} + \psi_{142})(\psi_{152} + \psi_{162})(\psi_{172} + \psi_{182})(\psi_{192} + \psi_{202}).\\ E_6 &= (Z_{33} + Z_{43}) + (\psi_{113} + \psi_{123})(\psi_{133} + \psi_{143})(\psi_{153} + \psi_{163})(\psi_{173} + \psi_{183})(\psi_{193} + \psi_{203}). \end{split}$$



Figure 6. Phase portraits of Slave Systems (6)–(25).

(26)

(27)

Differentiating (26), from (2)–(25), we have:

$$\begin{split} D^{q}E_{1} &= (Z_{12} + Z_{13} - 5sin(Z_{12}) + U_{1} + Z_{22} + Z_{23} - 5sin(Z_{22}) + \Delta H_{1} + D_{1} + U_{1}) + (121\psi_{12} - 5\psi_{11} + 83.6\psi_{22} - 83.6\psi_{23} - 10\psi_{21})(\psi_{31} + \psi_{41})(\psi_{31} + \psi_{41})(\psi_{31} + \psi_{41})(\psi_{31} + \psi_{10}) + (\psi_{11} + \psi_{21})(-2\psi_{31} + \psi_{32}\psi_{33} + 10\psi_{42} - 10\psi_{41})(\psi_{31} + \psi_{41})(\psi_{31} + \psi_{10}) + (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(35\psi_{51} - 35\psi_{51} + -\psi_{62} - \psi_{63})(\psi_{71} + \psi_{31})(\psi_{91} + \psi_{101}) + (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(\psi_{51} + \psi_{62})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{82})(\psi_{91} + \psi_{101}) + (\psi_{11} + \psi_{21})(\psi_{21} + \psi_{21})(\psi_{21} + \psi_{21})(\psi_{22} + \psi_{62})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{102}) + (\psi_{12} + \psi_{22})(-2\psi_{23} + \psi_{23})(\psi_{22} + \psi_{22})(\psi_{22} + \psi_{22})((-2\psi_{31} + \psi_{32})(\psi_{32} + \psi_{62})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{82})(\psi_{72} + \psi_{102}) + (\psi_{12} + \psi_{22})(\psi_{22} + \psi_{22})(\psi$$

(28)

5.1. Via Non-Linear Control

Design the non-linear control functions:

$$\begin{split} & U_1 = -Z_{12} - Z_{13} + 5sin(Z_{12}) - (121\psi_{12} - 5\psi_{11} + 83.6\psi_{22} - 83.6\psi_{23} - 10\psi_{21})(\psi_{31} + \psi_{41})(\psi_{51} + \psi_{63})(\psi_{71} + \psi_{61})(\psi_{71} + \psi_{61})(\psi_{72} + \psi_{62})(\psi_{72} + \psi_{63})(\psi_{73} + \psi_{63})(\psi_$$

$$\begin{split} \bar{V_6} &= Z_{41} + Z_{43} - 5sin(Z_{41}) - cos(Z_{41}) - (\psi_{113} + \psi_{123})(1 - \psi_{131}\psi_{132} + \frac{8}{3}\psi_{143} + \psi_{141}\psi_{142}) \\ & (\psi_{153} + \psi_{163})(\psi_{173} + \psi_{183})(\psi_{193} + \psi_{203}) - (\psi_{113} + \psi_{123})(\psi_{133} + \psi_{143})(\psi_{153} + \psi_{163})(-0.001 - \psi_{173} + \psi_{171}\psi_{172} + 0.1\psi_{173}\psi_{172} - 0.001 - \psi_{183} + 2\psi_{181}\psi_{182} + 0.2\psi_{183}\psi_{182})(\psi_{193} + \psi_{203}) - 3E_6. \end{split}$$

Substituting (28) into (27):

$$D^Q E_i = -E_i$$

Consider the Lyapunov function as:

$$V(E(t)) = \frac{1}{2}(E_1^2 + E_2^2 + E_3^2 + E_4^2 + E_5^2 + E_6^2).$$

Differentiating:

$$D^{Q}V(E(t)) \le \sum_{i=1}^{6} E_{i}(-E_{i}).$$

= $-\sum_{i=1}^{6} E_{i}^{2}.$

Using the stability theory of Lyapunov, $E_i \rightarrow 0$ for i = 1, 2, 3, 4, 5, 6 as $t \rightarrow \infty$, implying dual penta-compound combination anti-synchronization.

5.2. Via Adaptive Sliding Mode Control

Take $| \triangle H_i | \le A_i$ and $|D_i| \le B_i$. Here, $A_i, B_i > 0$ are constants and \hat{A}_i, \hat{B}_i are estimates A_i, B_i .

Consider the sliding surface:

$$S_i(t) = D^{q-1}E_i(t) + k_i \int_0^t E_i(\xi)d\xi.$$
 (29)

For (27) at (29), the condition is:

$$S_i(t) = 0, \dot{S}_i(t) = 0.$$
 (30)

Differentiating (29):

$$\dot{S}_i(t) = D^q E_i(t) + k_i E_i(t).$$
 (31)

From (30):

$$D^q E_i(t) = -k_i E_i(t). \tag{32}$$

From Matignon's theorem [28], (32) is stable. Designing controllers from (28), (32), and SMC theory:

$$\bar{U}_{1} = -Z_{12} - Z_{13} + 5sin(Z_{12}) - (121\psi_{12} - 5\psi_{11} + 83.6\psi_{22} - 83.6\psi_{23} - 10\psi_{21})(\psi_{31} + \psi_{41})
(\psi_{51} + \psi_{61})(\psi_{71} + \psi_{81})(\psi_{91} + \psi_{101}) - (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(35\psi_{51} - 35\psi_{51} - \psi_{62} - \psi_{63})
(\psi_{71} + \psi_{81})(\psi_{91} + \psi_{101}) - (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(\psi_{51} + \psi_{61})(\psi_{71} + \psi_{81})(0.7\psi_{91} - 3\psi_{92}\psi_{93} + 0.7\psi_{101} - 4\psi_{102}\psi_{103}).$$
(33)

$$\begin{split} & U_2 = Z_{11} - Z_{13} - (\psi_{11}\psi_{13} - \psi_{12} + \psi_{11} + \psi_{21}\psi_{23} - \psi_{22} + 12\psi_{12})(\psi_{22} + \psi_{42})(\psi_{22} + \psi_{42})(\psi_{23} + \psi_{43})(\psi_{53} + \psi_{53})(\psi_{53} + \psi_{53})(\psi_{51} + \psi_{52} - 3\psi_{53} + 10\psi_{22} - 10\psi_{41})(\psi_{51} + \psi_{51})(\psi_{71} + \psi_{51})(\psi_{91} + \psi_{10}) - (\psi_{11} + \psi_{21})(\psi_{31} + \psi_{41})(\psi_{51} + \psi_{61})(0.7\psi_{71} - \psi_{72}\psi_{73} + 0.7\psi_{73} - 10\psi_{52} + \psi_{52})(\psi_{22} + \psi_{22})(\psi_{22} + \psi_{22})(\psi_{22} + \psi_{52})(\psi_{52} + \psi_{52})(\psi_$$

Update the parameters as:

$$\dot{A}_i = a_i \mid S_i \mid .$$

$$\dot{B}_i = b_i \mid S_i \mid .$$
(34)

for positive a_i , b_i .

Theorem 1. Fractional Disturbed Master Systems (2)–(5) and Slave Systems (6)–(25) will achieve stability and synchronization using controllers and parameter updates as in (33)–(34).

Proof. Stability using Lyapunov's direct method [29] is proven considering positive definite function *V* and the negative derivative proving error convergence to zero.

Let:

 $V = \sum_{i=1}^{6} V_i.$ (35)

where:

$$V_{1} = \frac{1}{2}S_{1}^{2} + \frac{1}{2a_{1}}(\hat{A}_{1} - A_{1})^{2} + \frac{1}{2b_{1}}(\hat{B}_{1} - B_{1})^{2}.$$

$$V_{2} = \frac{1}{2}S_{2}^{2} + \frac{1}{2a_{2}}(\hat{A}_{2} - A_{2})^{2} + \frac{1}{2b_{2}}(\hat{B}_{2} - B_{2})^{2}.$$

$$V_{3} = \frac{1}{2}S_{3}^{2} + \frac{1}{2a_{3}}(\hat{A}_{3} - A_{3})^{2} + \frac{1}{2b_{3}}(\hat{B}_{3} - B_{3})^{2}.$$

$$V_{4} = \frac{1}{2}S_{4}^{2} + \frac{1}{2a_{4}}(\hat{A}_{4} - A_{4})^{2} + \frac{1}{2b_{4}}(\hat{B}_{4} - B_{4})^{2}.$$

$$V_{5} = \frac{1}{2}S_{5}^{2} + \frac{1}{2a_{5}}(\hat{A}_{5} - A_{5})^{2} + \frac{1}{2b_{5}}(\hat{B}_{5} - B_{5})^{2}.$$

$$V_{6} = \frac{1}{2}S_{6}^{2} + \frac{1}{2a_{6}}(\hat{A}_{6} - A_{6})^{2} + \frac{1}{2b_{6}}(\hat{B}_{6} - B_{6})^{2}.$$
(36)

Differentiating:

$$\begin{split} \dot{V}_{1} &= S_{1}\dot{S}_{1} + \frac{1}{a_{1}}(\hat{A}_{1} - A_{1})\dot{A}_{1} + \frac{1}{b_{1}}(\hat{B}_{1} - B_{1})\dot{B}_{1}.\\ \dot{V}_{2} &= S_{2}\dot{S}_{2} + \frac{1}{a_{2}}(\hat{A}_{2} - A_{2})\dot{A}_{2} + \frac{1}{b_{2}}(\hat{B}_{2} - B_{2})\dot{B}_{2}.\\ \dot{V}_{3} &= S_{3}\dot{S}_{3} + \frac{1}{a_{3}}(\hat{A}_{3} - A_{3})\dot{A}_{3} + \frac{1}{b_{3}}(\hat{B}_{3} - B_{3})\dot{B}_{3}.\\ \dot{V}_{4} &= S_{4}\dot{S}_{4} + \frac{1}{a_{4}}(\hat{A}_{4} - A_{4})\dot{A}_{4} + \frac{1}{b_{4}}(\hat{B}_{4} - B_{4})\dot{B}_{4}.\\ \dot{V}_{5} &= S_{5}\dot{S}_{5} + \frac{1}{a_{5}}(\hat{A}_{5} - A_{5})\dot{A}_{5} + \frac{1}{b_{5}}(\hat{B}_{5} - B_{5})\dot{B}_{5}.\\ \dot{V}_{6} &= S_{6}\dot{S}_{6} + \frac{1}{a_{6}}(\hat{A}_{6} - A_{6})\dot{A}_{6} + \frac{1}{b_{6}}(\hat{B}_{6} - B_{6})\dot{B}_{6}. \end{split}$$
(37)

From (31), we have:

$$\begin{split} \dot{V}_{1} &= S_{1}(D^{q}E_{1} + k_{1}E_{1}) + \frac{1}{a_{1}}(\hat{A}_{1} - A_{1})\dot{A}_{1} + \frac{1}{b_{1}}(\hat{B}_{1} - B_{1})\dot{B}_{1}.\\ \dot{V}_{2} &= S_{2}(D^{q}E_{2} + k_{2}E_{2}) + \frac{1}{a_{2}}(\hat{A}_{2} - A_{2})\dot{A}_{2} + \frac{1}{b_{2}}(\hat{B}_{2} - B_{2})\dot{B}_{2}.\\ \dot{V}_{3} &= S_{3}(D^{q}E_{3} + k_{3}E_{3}) + \frac{1}{a_{3}}(\hat{A}_{3} - A_{3})\dot{A}_{3} + \frac{1}{b_{3}}(\hat{B}_{3} - B_{3})\dot{B}_{3}.\\ \dot{V}_{4} &= S_{4}(D^{q}E_{4} + k_{4}E_{4}) + \frac{1}{a_{4}}(\hat{A}_{4} - A_{4})\dot{A}_{4} + \frac{1}{b_{4}}(\hat{B}_{4} - B_{4})\dot{B}_{4}.\\ \dot{V}_{5} &= S_{5}(D^{q}E_{5} + k_{5}E_{5}) + \frac{1}{a_{5}}(\hat{A}_{5} - A_{5})\dot{A}_{5} + \frac{1}{b_{5}}(\hat{B}_{5} - B_{5})\dot{B}_{5}.\\ \dot{V}_{6} &= S_{6}(D^{q}E_{6} + k_{6}E_{6}) + \frac{1}{a_{6}}(\hat{A}_{6} - A_{6})\dot{A}_{6} + \frac{1}{b_{6}}(\hat{B}_{6} - B_{6})\dot{B}_{6}. \end{split}$$
(38)

Substituting the values in Equation (38):

$$\begin{split} \dot{V}_i &= S_1 [-\bigtriangleup H_i - D_i (\hat{A}_i + \hat{B}_i + r_i) signS_i] + (\hat{A}_i - A_i) |S_i| + (\hat{B}_i - B_i) |S_i|.\\ &\leq (|\bigtriangleup H_i| + |D_i|) |S_i| + (\hat{A}_i - A_i) |S_i| + (\hat{B}_i - B_i) |S_i|.\\ &< (A_i + B_i) |S_i| - (\hat{A}_i + \hat{B}_i + r_i) |signS_i| + (\hat{A}_i - A_i) |S_i| + (\hat{B}_i - B_i) |S_i|.\\ &= -t_i |S_i|. \end{split}$$

Therefore:

$$\dot{V} = \sum_{i=1}^{6} \dot{V}_{i}.$$

$$< -\sum_{i=1}^{6} (t_{i}|S_{i}|).$$
(39)

Now \exists at $\geq 0 \in R$ such that:

$$\sum_{i=1}^{6} t_i |S_i| > t$$

then:

$$\dot{V} < -t\sqrt{S_1^2 + S_2^2 + S_3^2 + S_4^2 + S_5^2 + S_6^2}.$$

$$< 0.$$
(40)

From the Lyapunov stability theory, errors converge to $S_i = 0$.

5.3. Simulations and Proposed Application

The dual penta-compound combination anti-synchronized trajectories and error using the non-linear control method are displayed in Figure 7. The synchronized trajectories using the adaptive SMC technique are displayed in Figures 8a–c and 9a–c. Figures 8d and 9d show the anti-synchronization error using the SMC technique. The sliding surfaces tending to zero are shown in Figures 8e and 9e. The disturbances and uncertainties $\Delta H_1 = 0$, $D_1 = 7sin(t)$, $\Delta H_2 = 0$, $D_2 = sin(7t)$, $\Delta H_3 = cos(Z_{21})$, $D_3 = 0$, $\Delta H_4 = 0$, $D_4 = 7sin(t)$, $\Delta H_5 =$ 0, $D_5 = sin(7t)$, $\Delta H_6 = cos(Z_{21})$, $D_6 = 0$ are estimated and shown in Figures 8f,g and 9f,g by estimating the parameters using I.C. as $\hat{A}_i = \hat{B}_i = 0.1$ and $c_1 = 1$, $c_2 = 2$, $c_3 = 3$, $c_4 = 1$, $c_5 = 2$, $c_6 = 3$, respectively.



Figure 7. Synchronized trajectories and error via the non-linear control method.



Figure 8. (**a**–**c**) Synchronized trajectories via adaptive sliding mode control. (**d**) Error. (**e**) Surface converging to zero. (**f**,**g**) Disturbance estimates.



Figure 9. (**a**–**c**) Synchronized trajectories via adaptive sliding mode control. (**d**) Error. (**e**) Surface converging to zero. (**f**,**g**) Disturbance estimates.

The achieved anti-synchronization is illustrated with an example for application in secure communication. In this synchronization, we have two pairs of penta-compound combinations from which to choose. This adds to the diversity in the options for encrypting the original message. The sum of the chaotic signals from the master systems is added to the original signal; the encrypted signal is formed and transmitted. At the receiving end, upon performing synchronization, the controllers are applied and decrypted.

Suppose S(t) = sin(5t) + cos(6t) as the original signal. Mix S(t) with chaotic signals $Z_{11} + Z_{21}$ to obtain $S_1(t)$. Apply controllers to recover $S_2(t)$ at the receiver, as illustrated in Figure 10.



Figure 10. Proposed application.

6. Conclusions

In this paper, dual penta-compound combination anti-synchronization was performed on a chaotic system with two sine non-linearities. A thorough analysis of the newly introduced fractional-order system was performed. The achieved synchronization was performed between four master systems and twenty slave systems using two techniques. Uncertainties and disturbances were estimated. An application in secure communication was illustrated with the help of an example.

Studying the hidden attractors of the system and its electronic circuit implementation are the future scope.

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