



Figure S1. Results of linear regression analyses examining the relationship of Anderson v. observed rates of spread (A) alongside Anderson v. corrected rates of spread (B). Coloured lines represent the regression and dashes are 95% confidence intervals. The black line is the 1:1 LPA and individual observations of fire behaviour are shown as dots. ESS is estimated steady state and ILL is ignition line length.

Table S1. Fuel structural characteristics for all prescribed burns in Legg et al. [59], including the grouped fuel classes to which they belong.

Fuel Beds	Model Type	Class	1-Hr Fuel Load (t ha ⁻¹)	10-Hr Fuel Load (t ha ⁻¹)	100-Hr Fuel Load (t ha ⁻¹)	Live Herb Fuel Load (t ha ⁻¹)	Live Woody Fuel Load (t ha ⁻¹)	Fuelbed Depth/ <i>Calluna</i> height (m)	1-Hr Moisture Content (%)	10-Hr Moisture Content (%)	100-Hr Moisture Content (%)	Live Herb Moisture Content (%)	Live Woody Moisture Content (%)	Wind Speed (km hr ⁻¹)	Slope (%)	Observed ROS (m min ⁻¹)
High	Static	High	2.5	0	0	8.0	5.6	0.45	17.00	17.00	17.00	75.00	55.00	5.00	0	N/A
Medium	Static	Medium	2.5	0	0	8.6	3.6	0.29	17.00	17.00	17.00	75.00	55.00	5.00	0	N/A
Low	Static	Low	1.4	0	0	6.7	1.9	0.19	17.00	17.00	17.00	75.00	55.00	5.00	0	N/A
BE2P1	Static	High	3.3	0	0	8.0	8.7	0.45	17.21	17.21	17.21	80.71	80.71	11.12	0	4.37
BE2P11	Static	High	3.0	0	0	10.6	4.3	0.45	17.21	17.21	17.21	60.87	60.87	8.28	0	8.91
BE2P15	Static	High	2.8	0	0	5.9	8.7	0.51	15.98	15.98	15.98	75.05	75.05	14.62	0	7.85
BE2P20	Static	High	2.4	0	0	7.6	5.6	0.34	17.21	17.21	17.21	75.43	75.43	5.83	0	1.34
BE2P3	Static	High	2.3	0	0	8.0	7.5	0.47	17.21	17.21	17.21	55.19	55.19	18.22	0	12.64
BE2P6	Static	High	2.4	0	0	8.9	4.5	0.39	17.21	17.21	17.21	69.29	69.29	24.91	0	11.71
BE2P8	Static	High	3.5	0	0	10.6	8.9	0.46	20.68	20.68	20.68	97.18	97.18	15.19	0	1.92
BH4	Static	High	3.9	0	0	8.1	5.3	0.30	16.53	16.53	16.53	61.18	61.18	17.50	0	3.00
BH7	Static	High	2.4	0	0	6.5	3.4	0.23	15.67	15.67	15.67	70.45	70.45	31.21	0	6.35
BE2P13	Static	Medium	2.5	0	0	9.5	4.4	0.29	29.00	29.00	29.00	76.90	76.90	16.31	0	2.14
BE2P14	Static	Medium	1.8	0	0	7.9	4.3	0.28	24.35	24.35	24.35	63.65	63.65	8.24	0	2.98
BE2P21	Static	Medium	2.0	0	0	9.1	3.6	0.29	24.35	24.35	24.35	73.92	73.92	8.50	0	1.93
BE2P4	Static	Medium	2.7	0	0	8.7	3.0	0.28	24.35	24.35	24.35	95.11	95.11	16.67	0	2.51
BE2P5	Static	Medium	2.5	0	0	8.2	2.5	0.30	24.35	24.35	24.35	63.34	63.34	14.22	0	5.48
BE2P7	Static	Medium	1.7	0	0	7.3	2.9	0.27	24.35	24.35	24.35	80.15	80.15	27.00	0	4.37
BE2P9	Static	Medium	3.2	0	0	8.6	5.4	0.30	22.68	22.68	22.68	84.32	84.32	10.37	0	2.37
BH1	Static	Medium	1.9	0	0	8.1	2.6	0.20	18.15	18.15	18.15	63.15	63.15	15.52	0	2.13
BH5	Static	Medium	2.8	0	0	10.0	4.4	0.29	27.55	27.55	27.55	66.80	66.80	32.51	0	6.76
BE2P10	Static	Low	1.6	0	0	4.0	0.2	0.12	19.60	19.60	19.60	87.10	87.10	14.51	0	0.00
BE2P16	Static	Low	1.3	0	0	6.7	1.9	0.19	27.04	27.04	27.04	91.22	91.22	16.02	0	1.78
BE2P19	Static	Low	1.4	0	0	6.7	1.9	0.21	19.60	19.60	19.60	93.48	93.48	7.16	0	0.67
BE2P2	Static	Low	0.9	0	0	5.4	1.8	0.19	19.60	19.60	19.60	87.42	87.42	8.64	0	3.19
BE2P22	Static	Low	3.3	0	0	7.6	4.6	0.25	16.95	16.95	16.95	73.74	73.74	10.44	0	3.05
BE2P23	Static	Low	2.2	0	0	9.6	2.1	0.27	19.60	19.60	19.60	62.97	62.97	10.51	0	0.54
BE2P24	Static	Low	1.0	0	0	6.2	1.4	0.20	19.60	19.60	19.60	71.42	71.42	20.77	0	0.80
BH2	Static	Low	2.9	0	0	7.2	0.6	0.16	19.54	19.54	19.54	66.70	66.70	11.88	0	1.53
BH3	Static	Low	1.1	0	0	6.9	2.1	0.17	14.87	14.87	14.87	72.93	72.93	31.50	0	7.07

Table S2. Fire behaviour summary table used to generate model performance testing versus observed fire behaviour. ‘Fire name’, ‘Class’, ‘Observed’ fire behaviour and their relative fuel structures were from Legg et al. [59]. RMSE values were calculated using the ‘rmse’ function in the R ‘Metrics’ package [63]. Correction RMSE values are for Anderson versus Correction rates of spread.

Rates of Spread (m min ⁻¹)									
Fire Name	Class	Observed	Davies 1	Davies 2	Anderson	Correction	Roth	BehavePlus	Farsite
BE2P1	High	4.37	5.83	5.12	11.00	23.70	3.16	3.12	2.58
BE2P11	High	8.91	4.41	5.73	8.67	48.28	2.32	2.35	1.94
BE2P15	High	7.85	9.14	8.71	16.85	42.56	6.01	6.01	4.96
BE2P20	High	1.34	2.30	2.37	5.30	7.27	0.79	0.79	0.65
BE2P3	High	12.64	9.78	11.23	19.77	68.51	7.42	7.35	6.07
BE2P6	High	11.71	9.00	9.13	23.94	63.46	11.02	9.99	8.25
BE2P8	High	1.92	8.01	5.52	11.03	10.41	3.91	3.86	3.19
BH4	High	3.00	4.22	5.52	16.54	10.64	7.71	7.75	6.40
BH7	High	6.35	4.42	4.81	27.65	22.51	12.87	7.27	6.00
BE2P13	Medium	2.14	3.78	3.59	5.61	11.58	0.59	0.06	0.05
BE2P14	Medium	2.98	2.26	3.48	4.21	16.13	0.73	0.74	0.65
BE2P21	Medium	1.93	2.38	2.60	4.24	10.44	0.76	0.75	0.66
BE2P4	Medium	2.51	3.62	1.68	7.61	13.59	2.77	2.79	2.44
BE2P5	Medium	5.48	3.56	4.71	7.36	29.71	3.05	3.08	2.69
BE2P7	Medium	4.37	5.06	4.46	12.71	23.66	5.21	1.24	1.08
BE2P9	Medium	2.37	2.88	2.05	5.75	12.82	1.65	1.63	1.43
BH1	Medium	2.13	2.14	3.42	11.09	7.54	2.42	2.44	2.13
BH5	Medium	6.76	6.77	7.33	12.85	23.96	5.21	0.64	0.56
BE2P10	Low	0.00	1.23	0.26	7.07	0.00	2.11	2.16	1.89
BE2P16	Low	1.78	2.01	0.58	5.19	9.65	0.73	0.12	0.11
BE2P19	Low	0.67	1.50	0.11	4.28	3.64	0.49	0.48	0.42
BE2P2	Low	3.19	1.44	0.43	5.01	17.30	0.48	0.46	0.40
BE2P22	Low	3.05	2.26	2.50	8.66	16.52	2.18	2.16	1.89
BE2P23	Low	0.54	2.51	3.78	7.58	2.95	1.8	1.77	1.55
BE2P24	Low	0.80	2.61	3.05	12.94	4.34	2.85	0.70	0.61
BH2	Low	1.53	1.43	2.42	6.91	5.43	2.2	2.26	1.98
BH3	Low	7.07	2.84	3.11	26.41	25.04	4.8	3.81	3.34
Mean ± Standard Deviation	High	6.46 ± 4.14	6.34 ± 2.69	6.46 ± 2.70	15.64 ± 7.34	33.04 ± 23.41	6.31 ± 4.04	5.39 ± 3.01	4.45 ± 2.48
	Medium	3.41 ± 1.73	3.60 ± 1.51	3.70 ± 1.69	7.94 ± 3.45	16.60 ± 7.46	2.49 ± 1.79	1.49 ± 1.07	1.30 ± 0.93
	Low	2.07 ± 2.17	1.98 ± 0.60	1.80 ± 1.44	9.34 ± 6.89	9.43 ± 8.38	1.96 ± 1.36	1.55 ± 1.20	1.36 ± 1.05
	All	3.98 ± 3.34	3.98 ± 2.53	3.99 ± 2.75	10.97 ± 6.82	19.69 ± 17.57	3.53 ± 3.19	2.81 ± 2.65	2.37 ± 2.18
RMSE Versus Observed		High	3.03	2.18	10.86	26.66	10.86	3.44	3.79
		Medium	1.01	0.83	5.24	10.84	5.24	2.68	2.77
		Low	1.86	2.15	8.88	6.52	1.67	2.56	2.56
		All	2.13	1.83	8.64	17.03	2.64	2.92	3.09

Table S3. TukeyHSD post-hoc analyses following the ANOVA for rate of spread versus fire behaviour model and fuel class for observed fire behaviour comparisons. Fuel classes are assigned groupings from Legg et al. [59]. CI 95s are 95 % confidence intervals for a given factor interaction. Adjusted p is a significance value adjusted for each interaction at $\alpha = 0.05$.

Factor Comparison	Difference	Lower CI 95	Upper CI 95	Adjusted p
Fire Behaviour Model				
Davies 1 - Davies 2	0.01	-2.42	2.45	1.0000
Davies 1 - Anderson	-6.99	-9.43	-4.56	< 0.0001
Davies 1 - Roth	-0.45	-2.90	2.00	0.9949
Davies 1 - BehavePlus	1.29	-1.15	3.72	0.6478
Davies 1 - Farsite	-1.71	-4.15	0.72	0.3309
Davies 2 - Anderson	-6.98	-9.42	-4.55	< 0.0001
Davies 2 - Roth	-0.46	-2.91	1.99	0.9943
Davies 2 - BehavePlus	1.30	-1.14	3.73	0.6389
Davies 2 - Farsite	-1.72	-4.16	0.71	0.3233
Anderson - Roth	-7.44	-9.89	-4.99	< 0.0001
Anderson - BehavePlus	-8.28	-10.72	-5.85	< 0.0001
Anderson - Farsite	-8.71	-11.14	-6.27	< 0.0001
Roth - BehavePlus	0.84	-1.62	3.29	0.9218
Roth - Farsite	1.26	-1.19	3.71	0.6743
BehavePlus - Farsite	-0.42	-2.86	2.01	0.9960
Fuel Class				
High - Medium	-3.98	-5.40	-2.56	< 0.0001
High - Low	-4.51	-5.94	-3.09	< 0.0001
Medium - Low	0.53	-0.89	1.95	0.6516

Table S4. TukeyHSD post-hoc analyses following the sensitivity analysis ANOVA. Fuel classes are assigned groupings from Legg et al. [59]. CI 95s are 95 % confidence intervals for a given factor interaction. Adjusted p is a significance value adjusted for each interaction at $\alpha = 0.05$.

Factor Comparison	Difference	Lower CI 95	Upper CI 95	Adjusted p
Fire Behaviour Model				
Davies 1 - Davies 2	-0.01	-0.95	0.93	1.0000
Davies 1 - Anderson	-8.15	-9.09	-7.21	< 0.0001
Davies 1 - Roth	-0.56	-1.49	0.38	0.5380
Davies 1 - BehavePlus	0.56	-0.38	1.50	0.5322
Davies 1 - Farsite	-1.08	-2.02	-0.14	0.0140
Davies 2 - Anderson	-8.16	-9.10	-7.22	< 0.0001
Davies 2 - Roth	-0.54	-1.48	0.39	0.5602
Davies 2 - BehavePlus	0.55	-0.39	1.49	0.5544
Davies 2 - Farsite	-1.07	-2.00	-0.13	0.0156
Anderson - Roth	-8.71	-9.65	-7.77	< 0.0001
Anderson - BehavePlus	-8.71	-9.65	-7.77	< 0.0001
Anderson - Farsite	-9.23	-10.17	-8.29	< 0.0001
Roth - BehavePlus	0.00	-0.94	0.94	1.0000
Roth - Farsite	0.52	-0.42	1.46	0.6094
BehavePlus - Farsite	-0.52	-1.46	0.42	0.6152
Fuel Class				
High - Medium	-2.19	-2.74	-1.65	< 0.0001
High - Low	-3.80	-4.35	-3.26	< 0.0001
Medium - Low	1.61	1.06	2.15	< 0.0001

Table S5. Fire behaviour summary table used to generate all sensitivity analyses. Fuel classes are assigned groupings from Legg et al. [59]. LWPMC is live woody fuel moisture content. High fuel structure fire behaviour.

Fuel Class	Wind Speed (km hr ⁻¹)	LWPMC (%)	Rates of Spread (m min ⁻¹)					
			Davies 1	Davies 2	Roth	BehavePlus	Farsite	Anderson
High	5	95	2.97	1.10	0.84	0.84	0.62	4.80
High	5	85	2.97	2.07	0.84	0.84	0.62	4.95
High	5	75	2.97	3.04	0.85	0.84	0.63	5.10
High	5	65	2.97	4.01	0.85	0.85	0.63	5.27
High	5	55	2.97	4.98	0.85	0.85	0.63	5.43
High	7	95	3.85	1.90	1.42	1.42	1.12	6.70
High	7	85	3.85	2.87	1.43	1.43	1.12	6.91
High	7	75	3.85	3.84	1.43	1.43	1.13	7.13
High	7	65	3.85	4.81	1.44	1.44	1.13	7.36
High	7	55	3.85	5.78	1.45	1.45	1.14	7.59
High	9	95	4.72	2.71	2.15	2.14	1.70	8.60
High	9	85	4.72	3.68	2.16	2.15	1.71	8.87
High	9	75	4.72	4.65	2.17	2.16	1.72	9.16
High	9	65	4.72	5.62	2.18	2.17	1.73	9.45
High	9	55	4.72	6.59	2.19	2.18	1.74	9.75
High	11	95	5.59	3.51	3.01	3.01	2.39	10.50
High	11	85	5.59	4.48	3.02	3.02	2.39	10.83
High	11	75	5.59	5.45	3.04	3.03	2.41	11.18
High	11	65	5.59	6.42	3.05	3.05	2.41	11.53
High	11	55	5.59	7.39	3.06	3.06	2.42	11.90
High	13	95	6.47	4.31	4.00	4.00	3.19	12.40
High	13	85	6.47	5.28	4.02	4.01	3.20	12.79
High	13	75	6.47	6.25	4.04	4.03	3.21	13.20
High	13	65	6.47	7.22	4.05	4.05	3.22	13.62
High	13	55	6.47	8.19	4.07	4.07	3.24	14.05
High	15	95	7.34	5.12	5.11	5.11	4.08	14.29
High	15	85	7.34	6.09	5.14	5.13	4.10	14.75
High	15	75	7.34	7.06	5.16	5.16	4.12	15.21
High	15	65	7.34	8.03	5.19	5.18	4.15	15.70
High	15	55	7.34	9.00	5.21	5.21	4.18	16.20
High	17	95	8.21	5.92	6.35	6.35	5.22	16.18
High	17	85	8.21	6.89	6.38	6.37	5.24	16.70
High	17	75	8.21	7.86	6.41	6.40	5.27	17.23
High	17	65	8.21	8.83	6.44	6.43	5.30	17.78
High	17	55	8.21	9.80	6.47	6.46	5.33	18.34
High	19	95	9.09	6.72	7.70	7.70	6.45	18.08
High	19	85	9.09	7.69	7.74	7.73	6.47	18.65
High	19	75	9.09	8.66	7.77	7.77	6.50	19.24
High	19	65	9.09	9.63	7.81	7.80	6.53	19.86
High	19	55	9.09	10.60	7.85	7.84	6.56	20.49
High	21	95	9.96	7.53	9.17	9.16	7.71	19.97
High	21	85	9.96	8.50	9.21	9.20	7.75	20.60
High	21	75	9.96	9.47	9.25	9.25	7.80	21.26
High	21	65	9.96	10.44	9.30	9.29	7.85	21.93
High	21	55	9.96	11.41	9.34	9.33	7.90	22.63
High	23	95	10.83	8.33	10.75	10.74	9.15	21.86
High	23	85	10.83	9.30	10.80	10.79	9.20	22.55
High	23	75	10.83	10.27	10.84	10.84	9.25	23.27
High	23	65	10.83	11.24	10.89	10.89	9.30	24.01
High	23	55	10.83	12.21	10.95	10.94	9.35	24.77

Table S5, continued. Medium fuel structure fire behaviour.

Medium	5	95	1.71	0.00	0.58	0.58	0.47	4.08
Medium	5	85	1.71	0.90	0.58	0.58	0.47	4.21
Medium	5	75	1.71	1.87	0.58	0.58	0.48	4.34
Medium	5	65	1.71	2.84	0.58	0.58	0.47	4.48
Medium	5	55	1.71	3.81	0.59	0.59	0.48	4.62
Medium	7	95	2.07	0.27	0.98	0.98	0.83	5.70
Medium	7	85	2.07	1.24	0.98	0.98	0.83	5.88
Medium	7	75	2.07	2.21	0.99	0.99	0.84	6.07
Medium	7	65	2.07	3.18	0.99	0.99	0.84	6.26
Medium	7	55	2.07	4.15	0.99	0.99	0.84	6.46
Medium	9	95	2.44	0.61	1.49	1.49	1.27	7.32
Medium	9	85	2.44	1.58	1.49	1.49	1.27	7.55
Medium	9	75	2.44	2.55	1.49	1.49	1.27	7.79
Medium	9	65	2.44	3.52	1.50	1.50	1.28	8.04
Medium	9	55	2.44	4.49	1.50	1.50	1.28	8.29
Medium	11	95	2.80	0.94	2.09	2.08	1.77	8.93
Medium	11	85	2.80	1.91	2.09	2.09	1.78	9.22
Medium	11	75	2.80	2.88	2.10	2.10	1.79	9.51
Medium	11	65	2.80	3.85	2.10	2.10	1.78	9.81
Medium	11	55	2.80	4.82	2.11	2.11	1.79	10.12
Medium	13	95	3.17	1.28	2.78	2.78	2.38	10.55
Medium	13	85	3.17	2.25	2.79	2.78	2.38	10.88
Medium	13	75	3.17	3.22	2.79	2.79	2.38	11.23
Medium	13	65	3.17	4.19	2.80	2.80	2.39	11.58
Medium	13	55	3.17	5.16	2.81	2.81	2.40	11.95
Medium	15	95	3.54	1.62	3.56	3.56	3.05	12.16
Medium	15	85	3.54	2.59	3.57	3.57	3.06	12.54
Medium	15	75	3.54	3.56	3.58	3.58	3.06	12.94
Medium	15	65	3.54	4.53	3.59	3.59	3.08	13.35
Medium	15	55	3.54	5.50	3.60	3.60	3.09	13.78
Medium	17	95	3.90	1.95	4.43	4.42	3.86	13.77
Medium	17	85	3.90	2.92	4.44	4.44	3.88	14.21
Medium	17	75	3.90	3.89	4.45	4.45	3.89	14.66
Medium	17	65	3.90	4.86	4.46	4.46	3.90	15.12
Medium	17	55	3.90	5.83	4.48	4.47	3.91	15.60
Medium	19	95	4.27	2.29	5.38	5.38	4.76	15.38
Medium	19	85	4.27	3.26	5.39	5.39	4.76	15.87
Medium	19	75	4.27	4.23	5.41	5.41	4.78	16.37
Medium	19	65	4.27	5.20	5.42	5.42	4.79	16.89
Medium	19	55	4.27	6.17	5.44	5.44	4.80	17.43
Medium	21	95	4.63	2.63	6.41	6.41	5.69	16.99
Medium	21	85	4.63	3.60	6.43	6.43	5.71	17.53
Medium	21	75	4.63	4.57	6.45	6.44	5.72	18.08
Medium	21	65	4.63	5.54	6.47	6.46	5.74	18.66
Medium	21	55	4.63	6.51	6.49	6.48	5.77	19.25
Medium	23	95	5.00	2.96	7.53	7.52	6.73	18.59
Medium	23	85	5.00	3.93	7.55	7.54	6.75	19.18
Medium	23	75	5.00	4.90	7.57	7.56	6.77	19.79
Medium	23	65	5.00	5.87	7.59	7.59	6.80	20.42
Medium	23	55	5.00	6.84	7.61	7.61	6.82	21.07

Table S5, continued. Low fuel structure fire behaviour and summary statistics. RMSE values were calculated using the 'rmse' function in the R 'Metrics' package [63].

Low	5	95	1.17	0.00	0.30	0.30	0.25	3.46
Low	5	85	1.17	0.41	0.30	0.30	0.25	3.57
Low	5	75	1.17	1.38	0.30	0.30	0.25	3.69
Low	5	65	1.17	2.35	0.30	0.30	0.25	3.80
Low	5	55	1.17	3.32	0.30	0.30	0.25	3.93
Low	7	95	1.32	0.00	0.50	0.50	0.43	4.84
Low	7	85	1.32	0.55	0.50	0.50	0.42	4.99
Low	7	75	1.32	1.52	0.50	0.50	0.43	5.15
Low	7	65	1.32	2.49	0.50	0.50	0.42	5.32
Low	7	55	1.32	3.46	0.50	0.50	0.42	5.49
Low	9	95	1.48	0.00	0.76	0.76	0.65	6.21
Low	9	85	1.48	0.69	0.76	0.76	0.65	6.41
Low	9	75	1.48	1.66	0.76	0.76	0.65	6.61
Low	9	65	1.48	2.63	0.76	0.76	0.65	6.82
Low	9	55	1.48	3.60	0.76	0.76	0.65	7.04
Low	11	95	1.63	0.00	1.06	1.06	0.91	7.58
Low	11	85	1.63	0.83	1.07	1.07	0.91	7.83
Low	11	75	1.63	1.80	1.07	1.07	0.92	8.07
Low	11	65	1.63	2.77	1.07	1.07	0.91	8.33
Low	11	55	1.63	3.74	1.07	1.07	0.91	8.60
Low	13	95	1.78	0.00	1.42	1.42	1.22	8.95
Low	13	85	1.78	0.97	1.42	1.42	1.22	9.24
Low	13	75	1.78	1.94	1.42	1.42	1.22	9.53
Low	13	65	1.78	2.91	1.43	1.42	1.21	9.84
Low	13	55	1.78	3.88	1.43	1.43	1.22	10.15
Low	15	95	1.93	0.14	1.82	1.82	1.56	10.32
Low	15	85	1.93	1.11	1.82	1.82	1.56	10.65
Low	15	75	1.93	2.08	1.83	1.82	1.56	10.99
Low	15	65	1.93	3.05	1.83	1.83	1.57	11.34
Low	15	55	1.93	4.02	1.83	1.83	1.57	11.70
Low	17	95	2.08	0.28	2.26	2.26	1.98	11.69
Low	17	85	2.08	1.25	2.27	2.26	1.98	12.06
Low	17	75	2.08	2.22	2.27	2.27	1.99	12.45
Low	17	65	2.08	3.19	2.28	2.28	2.00	12.84
Low	17	55	2.08	4.16	2.28	2.28	2.00	13.25
Low	19	95	2.24	0.42	2.75	2.75	2.44	13.06
Low	19	85	2.24	1.39	2.76	2.75	2.44	13.47
Low	19	75	2.24	2.36	2.76	2.75	2.43	13.90
Low	19	65	2.24	3.33	2.77	2.77	2.45	14.34
Low	19	55	2.24	4.30	2.77	2.77	2.45	14.80
Low	21	95	2.39	0.56	3.28	3.28	2.92	14.42
Low	21	85	2.39	1.53	3.29	3.28	2.92	14.88
Low	21	75	2.39	2.50	3.29	3.29	2.93	15.36
Low	21	65	2.39	3.47	3.30	3.29	2.93	15.84
Low	21	55	2.39	4.44	3.31	3.31	2.95	16.35
Low	23	95	2.54	0.70	3.85	3.85	3.45	15.79
Low	23	85	2.54	1.67	3.86	3.86	3.46	16.29
Low	23	75	2.54	2.64	3.87	3.86	3.46	16.81
Low	23	65	2.54	3.61	3.87	3.87	3.47	17.34
Low	23	55	2.54	4.58	3.88	3.88	3.48	17.89
Mean ± Standard Deviation	High	6.90 ± 2.53	6.66 ± 2.71	5.10 ± 3.27	5.09 ± 3.27	4.20 ± 2.81	14.21 ± 5.90	
	Medium	3.35 ± 1.06	3.39 ± 1.69	3.54 ± 2.28	3.54 ± 2.28	3.10 ± 2.06	12.09 ± 5.02	
	Low	1.86 ± 0.44	2.06 ± 1.36	1.81 ± 1.17	1.81 ± 1.17	1.58 ± 1.05	10.27 ± 4.26	
	All	4.04 ± 2.66	4.03 ± 2.79	3.48 ± 2.74	3.48 ± 2.74	2.96 ± 2.35	12.19 ± 5.32	
RMSE	Versus Davies 1	High		1.99	1.99	2.75	8.04	
		Medium		1.24	1.24	1.04	9.58	
		Low		0.81	0.81	0.71	9.41	
		All		1.42	1.42	1.74	8.97	
	Versus Davies 2	High		2.29	2.29	2.86	8.36	
		Medium		1.89	1.89	1.77	9.60	
		Low		1.55	1.55	1.55	9.24	
		All		1.94	1.94	2.14	9.04	

References (from main text)

59. Legg, C.J.; Davies, G.M.; Kitchen, K.; Marno, P. *Developing a Fire Danger Rating System for Vegetation Fires in the UK: FireBeaters Phase I final report*; Scottish Wildfire Forum, 2007. <https://era.ed.ac.uk/handle/1842/3011> (accessed 2019-09-23).
68. Hamner, B.; Frasco, M.; LeDell, E. *Package 'Metrics': Evaluation Metrics for Machine Learning*; R Foundation for Statistical Computing: Vienna, Austria, 2018. <https://cran.r-project.org/web/packages/Metrics> (accessed 2020-11-01).