



Article Disaggregating Longer-Term Trends from Seasonal Variations in Measured PV System Performance

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Abstract: Photovoltaic (PV) systems are widely adopted for renewable energy generation, but their performance is influenced by complex interactions between longer-term trends and seasonal variations. This study aims to remove these factors and provide valuable insights for optimising PV system operation. We employ comprehensive datasets of measured PV system performance over five years, focusing on identifying the distinct contributions of longer-term trends and seasonal effects. To achieve this, we develop a novel analytical framework that combines time series and statistical analytical techniques. By applying this framework to the extensive performance data, we successfully break down the overall PV system output into its constituent components, allowing us to find out the impact of the system degradation, maintenance, and weather variations from the inherent seasonal patterns. Our results reveal significant trends in PV system performance, indicating the need for proactive maintenance strategies to mitigate degradation effects. Moreover, we quantify the impact of changing weather patterns and provide recommendations for optimising the system's efficiency based on seasonally varying conditions. Hence, this study not only advances our understanding of the intricate variations within PV system performance but also provides practical guidance for enhancing the sustainability and effectiveness of solar energy utilisation in both residential and commercial settings.

Keywords: photovoltaic systems; seasonal variations; long-term trends; performance analysis; measured data; trend disaggregation

1. Introduction

Disaggregating longer-term trends from seasonal variations in measured PV system performance is an important aspect of understanding the performance of solar photovoltaic (PV) systems [1–3]. Seasonal variations in the performance ratios for PV systems can be obscured by diurnal and seasonal changes, making it difficult to determine long-term performance degradation from transient performance changes [2]. The performance ratio (PR) is a commonly used metric to measure solar PV plant performance. Still, it is insufficient to use as the basis for a performance guarantee when precise confidence intervals are required due to the large seasonal variation in PR [3]. To reduce seasonal variations of the PR due to the temperature dependency of the used PV cell, the PR may be corrected for temperature [2].

Seasonal variations can have a significant effect on the performance of solar PV systems [3–6]. For instance, the amount of sunlight hitting the solar panels varies throughout the year, with shorter days and less direct sunlight in the winter [5]. This can result in decreased energy output during the winter months, which can be compensated for by increasing the size of the solar array or by storing excess energy in batteries [5,6]. However, the temperature can affect the performance of PV systems, with the PR being corrected for temperature to reduce seasonal variations [3].



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PV systems are subject to a multitude of factors that influence their output, such as solar irradiance variations, temperature effects, shading, and system degradation [1–3]. While seasonal variations can be attributed to changes in solar position and meteorological conditions, longer-term trends may arise from factors such as module ageing, performance degradation, and gradual system efficiency disimprovement [1–3]. Identifying and quantifying these trends is essential for accurate performance evaluation and predictive maintenance. Photovoltaic (PV) modules that convert solar energy into electrical energy [1] gradually degrade over time [7] giving reduced output power manifest in a lower performance ratio [8]. The module degradation rate depends on the specification and manufacture of PV modules as well as operational ambient temperatures and their variation, relative humidity, intensity and spectrum of incident solar radiation, wind speed, and extent of exposure to rain, snow, and dust [1]. Even for nominally identical systems, degradation rates measured in one location cannot thus be assumed to apply in another location [8,9]. Distinguishing between underlying multi-annual trends and periodic seasonal variations in measured PV system outputs is a prerequisite for identifying longer-term performance degradation. One way to implement this is to "correct" the PV PR for either ambient or module temperature [3,10]. Correlations between power loss in a PV system with cell temperature, irradiance, temperature variations, and shading have been found in previous studies [11]. For instance, the main factors that impact power loss in a PV system are: (i) Cell Temperature: The temperature of the solar cells can significantly affect their efficiency. As cell temperature increases, the efficiency of the cells tends to decrease due to the negative temperature coefficient of most PV materials, which causes their output voltage and current to decrease with increasing temperature. The correlation between cell temperature and power loss is usually negative [12,13]. (ii) Irradiance: Irradiance refers to the amount of solar energy that reaches the solar cells. Higher irradiance levels generally lead to higher output power from the PV system. The correlation between irradiance and output power is positive [14,15]. (iii) Temperature Variations: Temperature variations can impact the performance of a PV system, including fluctuations in ambient temperature throughout the day [13]. Temperature changes can influence the efficiency of the system due to changes in cell temperature and, consequently, cell efficiency [13]. The correlation between temperature variations and power loss can be both positive and negative, depending on the specific conditions [13]. (iv) Shading: Shading is a critical factor that can cause power loss in a PV system. When a portion of the PV array is shaded, it can create "hot spots" and reduce the overall system efficiency [14,15]. This is because the shaded cells can become reverse-biased, leading to power losses, and potentially damaging the shaded cells. The correlation between shading and power loss is typically negative [14,15].

This paper aims to develop methods to separate the long-term trends from seasonal variations in the measured PV system performance [16]. This has been a topic of previous research. For example, (i) Lindig et al. [2] focus on best practices for performance loss rate (PLR) computations, and the challenges and opportunities associated with it, but it does not directly address the methods for disaggregating longer-term trends from seasonal variations in measured PV system performance. To address this, this study adds two more accurate and reliable methods for calculating PLR (such as relative PLR (PLR_{rel}) and absolute PLR (PLR_{abs})). (ii) In Dierauf et al.'s [3] study, traditional PR computation neglects array temperature, which typically results in seasonal variation. This seasonal variation makes the PR metric insufficient to use as the basis for a performance guarantee when precise confidence intervals are required. To reduce the seasonality effects, this study carried out the annual average cell temperature of the three locations (Harlequins, Newry, and Warrrenpoint). Hence, the traditional PR "uncorrected PR" now normalises with the annual average cell temperature to become normalised PR "temperature-corrected PR". This resulting weather-corrected PR or "temperature-corrected PR" gives more consistent results throughout the year, enabling its use as a metric for performance guarantees.

Solar PV performance monitoring is the process of observing and recording the parameters from the solar PV power plant in real-time [17]. The development of an advanced monitoring method is crucial for the efficient and reliable operation of solar PV systems [17]. The primary purposes of monitoring PV systems encompass measuring energy output, evaluating the performance of the PV system, and promptly detecting any design faults or operational problems [18]. In the case of large PV systems, analytical monitoring is employed to proactively mitigate economic losses arising from operational challenges [18]. The performance analysis of grid-connected PV systems involves comparing and presenting the operational results of such systems [19]. This includes investigating the performance of PV systems based on different module technologies [20]. The analytical monitoring of grid-connected PV systems involves measuring and analysing various parameters such as irradiation sensors, energy generation measurements, and performance indicators [18]. This can also involve monitoring the performance of PV systems before and after the application of a set of procedures for performance analysis [21]. Hence, good practices for monitoring and performance analysis of grid-connected PV systems include [21]: (i) Establishing a standard method for monitoring the performance of long-term PV systems in buildings. (ii) Creating a set of good practices and systematic analysis for the monitoring of PV systems, considering performance indicators, as well as temperature, cable, and energy conversion losses. (iii) Developing a set of procedures for performance analysis of small grid-connected PV systems, classified in terms of project, installation site, electrical installation, protection, safety, and maintenance.

For instance, an examination of failures in grid-connected residential PV systems with capacities ranging from 1 to 5 kW_p , installed in Germany during the 1990s [22], revealed that, on average, a failure occurred approximately every 4.5 years per installation. Among these failures, inverters accounted for 63%, PV modules for 15%, and other system components for 22% of the total failures [18]. A failure detection routine (FDR) was introduced to compare the monitored energy yield with the simulated yield for a given period [23,24]. The FDR used comprised three core components: (i) the failure detection system, (ii) the failure profiling method, and (iii) the footprint method. When a substantial disparity exists between the monitored and simulated energy yields, the FDR identifies a potential failure. It further characterises the energy loss pattern by creating a profile of the actual failure and contrasting it with pre-defined profiles of frequently occurring failures. Based on the correlation between the actual failure profile and these pre-defined profiles, the FDR assesses the likelihood of various failure scenarios. The footprint method aids in the analysis of patterns across three distinct domains: (i) normalised monitored power, time (hour of the day), and sun elevation. This method was developed through the examination of common system faults using data from well-monitored PV installations within the German 1000-roofs programme. Initial findings, as reported [23], indicate that the methodology is effective in identifying failures that are unequivocally implausible. However, further refinement is required. Field tests, as discussed [25], have demonstrated that the time needed to detect a failure using the PVSAT-2 routine [26], which employs the FDR methodology, can vary considerably, ranging from as little as one day to several months. This variability is primarily influenced by factors such as weather conditions, the scale of the failure, and its duration.

2.1. Seasonal Variations in PV Performance

To enhance the reliability and durability of PV systems, PV manufacturers should conduct rigorous stress tests to assess their optimised performance. This is particularly crucial due to the impact of temperature-induced seasonal variations [27]. For instance, Jiaying et al. [28] examined three different PV module technologies: monocrystalline silicon (m-Si), single junction amorphous silicon (a-Si), and micromorph silicon thin-film modules. The results of their correlation analysis indicate that temperature plays a pivotal role in seasonal performance variations. Monocrystalline silicon exhibits the strongest correlation

with both temperature and irradiance. In contrast, single junction a-Si modules display lower sensitivity to temperature variations, while micromorph silicon modules demonstrate the weakest correlation with these two variables.

Installed PV modules in real-world conditions have been shown to exhibit seasonal performance fluctuations [29]. These variations stem from two main factors [28]: (i) Temperature Variation Between Seasons: The difference in temperature between summer and winter seasons is a key influencer. PV modules with a more negative temperature coefficient of maximum power tend to perform better in winter than in summer. Furthermore, thin-film and a-Si modules subjected to thermal annealing processes recover from lightinduced defects (LID), leading to improved performance during the summer. (ii) Spectral Variability Due to Sun Position: Variations in the sun's position throughout the year affect the spectral characteristics of sunlight and consequently impact PV system performance. For example, in PV materials with a wider band gap, such as a-Si, spectral variability plays a role in module performance. These modules tend to perform better in the summer when exposed to a blue-rich spectrum of light but exhibit reduced performance in the winter under a red-rich spectrum [30]. The output of PV modules fluctuates in response to incident solar irradiance and module temperature, making the energy output of a system contingent on prevailing weather conditions [4,31]. An increase in PV cell temperatures can result in reduced output and efficiency [27]. However, the performance of a solar photovoltaic system is dependent on many site factors such as latitude, season, cloudiness, and air pollution [32]. This means that seasonal variations have a significant impact on the performance of solar photovoltaic installations [32]. Thus, the following are some of the factors that affect the seasonal variations in PV performance [4,32]: (i) Sunshine Period: The trend of the monthly average daily sunshine period affects the performance of PV systems. During July and August, the sunshine period was lower due to the southwest monsoon over the Indian subcontinent, which was reflected in the yield of the PV system. (ii) Spectral Variations: The spectral variations due to seasonal changes in the incident spectrum also affect the performance of PV systems. A study conducted in India showed that PV technologies which have broad spectral bands give higher utilisation factor (UF) values compared to technologies that have narrow spectral bands. The study also found that seasonal spectral variations have a significant impact on the performance of different PV technologies. (iii) Seasonality: Seasonality is the variation in solar generation due to seasonal changes in the angle of the sun. In most areas of the United States, solar panels yield the highest generation in the summer months, followed by fall and spring. This is because the days are longer, and the sun is higher in the sky during these months. In contrast, solar panels generate less power in the winter months when the days are short, and the sun is low. Therefore, to account for seasonal variations in PV performance, it is essential to consider the factors mentioned above during the design and installation of PV systems. The seasonal variations in PV performance should also be considered when estimating the solar offset and monthly savings of a solar energy system [32].

2.2. Performance Ratio Corrected for Temperature (PR_{Corr})

The performance ratio (PR) in solar PV installations normalises system output relative to the installed capacity and the available solar irradiance at the installation site. PR facilitates the comparison of system performance across varying installed capacities and geographical locations [33]. The weather-uncorrected performance ratio is determined using Equation (1) [33]. To account for temperature effects, PR can be adjusted by incorporating a temperature correction, resulting in a "temperature-corrected" PR_{Corr} [3,33], as shown in Equation (2). This is because, in 2021, the average cell temperatures across the three locations (Harlequins, Newry, and Warrenpoint) studied were significantly increased compared to the years 2017 through 2020. Table 1 shows the specifications and locations of the three monitored arrays. This temperature increase was attributed to an intense heatwave during that year, as demonstrated in Table 2.

		PV Array Location	
	Harlequins	Newry	Warrenpoint
Tilt and Azimuth Angles	Azimuth: -162°, Tilt: 12° for PV array 1 Azimuth: 12°, Tilt: 12° for PV array 2	Azimuth: -31°, Tilt: 6° for PV array 1 Azimuth: 149°, Tilt: 6° for PV array 2	Azimuth: -125°, Tilt: 7° for PV array 1 Azimuth: 55°, Tilt: 7° for PV array 2
Total PV Area	312.36 m ²	311.04 m ²	268.8 m ²
Solar Cell Technology	Polycrystalline silicon (p-Si)	-	-
PV Module Manufacturer	Renesola	-	-
Module Rating	260 W _p at STC	-	-
Number of Modules	192	-	-
Installation Type	Rooftop	-	-
PV Capacity	49.92 kW _p at STC	-	-
Module type (s)	Renesola-JC260M-24/Bbv (260 W)	-	-
Inverter	Sunny TriPower	-	-
Inverter Capacity [AC]	$2 \times 20 \text{ kW}$	-	-

Table 1. S	pecifications ar	d locations	of the me	onitored	arrays
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Table 2. Average annual PV cell temperatures for Harlequins, Newry, and Warrenpoint.

Year	Harlequins	Newry	Warrenpoint		
	Average cell Temperature, <i>Tc_{ell_avg}</i> (°C)	Average cell Temperature, Tc _{ell_avg} (°C)	Average cell Temperature, Tc _{ell_avg} (°C)		
2017	37.87	37.21	37.09		
2018	38.37	38.14	37.70		
2019	39.95	37.14	36.09		
2020	38.06	36.50	36.79		
2021	39.98	39.76	39.68		

Therefore, the novelty of this study is based on the following [34]: (i) The degradation rates observed in the three arrays, namely Harlequins, Newry, and Warrenpoint, are linear. This linearity arises because all the modules under investigation are operating within the stable region of their respective "bathtub" failure rate curves. (ii) The primary parameters governing seasonal behaviour in this context are cell temperature and solar irradiance. This is because key performance indicators of PV systems, such as system efficiency and power output, exhibit linear dependencies on cell temperature and irradiance. When solar irradiance surpasses 500 W/m^2 , it leads to an increase in cell temperature, subsequently causing a reduction in both the efficiency and power output of the PV system [35,36]. Consequently, an increase in cell temperature results in decreased system efficiency and power output, while a decrease in cell temperature leads to an enhancement in both efficiency and power output. (iii) Long-term performance assessment of PV systems can be challenging due to the fluctuating environmental conditions that occur on a daily and seasonal basis. To mitigate the impact of these variable conditions, the weather-uncorrected performance ratios (PR_{Uncorr}) were adjusted through the utilisation of the annual average cell temperature (T_{Cell_avg}) recorded in Table 2. The incorporation of this temperature correction served to reduce the seasonal variabilities in the performance ratio, thus enabling the separation of longer-term trends from the influence of seasonal variabilities.

3. Materials and Methods

The study aims to address the challenge of disaggregating longer-term trends from seasonal variations in measured PV system performance. To achieve this, a comprehensive approach that integrates statistical and time-series analyses is employed. The following sections outline the materials used and the methods applied in this study: (i) Data Collection and Pre-processing: Five years of historical data from an operational PV system, including solar irradiance, module temperature, and output power measurements, are collected. The data are obtained from a diverse range of geographical locations (Harlequins, Newry, and Warrenpoint in Northern Ireland) and periods to ensure the robustness of the analysis. Data pre-processing used in this study involves outlier removal, missing value imputation, and synchronisation of time-series data [37]. (ii) Time-Series Decomposition: Classical time-series decomposition techniques, such as the seasonal decomposition of time-series (STL), are applied to disaggregate the underlying components of the PV system's performance [38]. (iii) Wavelet Analysis: Wavelet transform is employed to analyse the time-frequency representation of the PV system's output power. By decomposing the time series into different frequency components, wavelet analysis helps identify both short-term fluctuations and underlying long-term trends [39]. Hence, three roof-mounted grid-connected PV arrays located in Northern Ireland were monitored for five years. These arrays are designated (after their locations) "Harlequins", "Newry", and "Warrenpoint". The specifications and locations of the three arrays are provided in Table 1. In-plane irradiance (G_{POA}), AC output power (P_{AC}), and cell temperature (T_{cell}) were measured at fifteen-minute intervals using pyranometers, AC power meters, and thermocouples. The continuous monitoring of the PV system performance parameters (such as electrical output, efficiency, and temperature) across the three locations was conducted using data logging equipment. From the data collected, performance fluctuations were observed as a result of seasonal variations. To disaggregate longer-term trends from seasonal variations in measured PV system performance located in Harlequins, Newry, and Warrenpoint, the weather-uncorrected performance ratios as seen in Equation (1) of Section 4 were converted to temperature-corrected performance ratios (i.e., weather-corrected performance ratios) using the average annual cell temperatures (T_{cell_avg}) shown in Table 2 and Equation (3). The azimuth and tilt angles of the PV arrays are shown in the first row of Table 1.

4. Results

4.1. Data Collection and Preprocessing

PV systems used in this study are typically equipped with sensors and monitoring equipment that record various performance metrics such as solar irradiance, temperature, voltage, current, and power output. Data were reliably and consistently collected from these sensors which spread across Harlequins, Newry, and Warrenpoint at fifteen-minute intervals. To clean up the data, missing data were handled through data interpolation. Outliers were removed to avoid distortion in the data analysis [37].

4.2. Time Series

To investigate long-term degradation, relative performance loss rates (PLR_{rel}), absolute performance loss rates (PLR_{abs}), and nonlinear trends over five years were fitted to simple best-fit linear lines. Uncorrected and module temperature-corrected annual monthly relative and absolute performance loss rates from Harlequins, Newry, and Warrenpoint arrays from 2017 to 2021, the gradient (β_1) and the y-intercept (β_0) of each year across the three arrays were found using the time-series (Yt{XE "Yt:Linear regression model"}) linear regression model, as shown in Equation (12) [40]. This separates longer-term trends from seasonal variations [39].

4.3. Wavelet Analysis

By utilising temperature-corrected performance ratios, it becomes possible to discern long-term performance degradation trends with a high degree of confidence after just six months for one PV array and within three years for the other two arrays. If a lower level of statistical confidence in these trends is acceptable, it is still feasible to identify long-term degradation rates within one year of operation for all PV arrays under investigation. These findings hold significant implications, as they suggest that relatively brief outdoor PV performance monitoring can reliably serve as a means to estimate long-term degradation and/or to calibrate the typically conducted accelerated testing processes. For instance, data exhibiting a high coefficient of determination (R²) concerning a linear trend suggests that the trend can be extrapolated with reliability. In this context, R^2 values of 0.810 and 0.999 are selected to signify a robust correlation with the dataset. Figures 1 and 2 illustrate the enhancements in coefficients of determination (R^2) for PR, computed over varying cumulative time intervals. Temperature-corrected PR values achieve R² coefficients of determination of 0.810 and 0.999 within cumulative degradation trend evaluation periods ranging from 6 months (for the Warrenpoint PV array and system) to approximately 3 years for the Harlequins and Newry PV arrays and systems. In contrast, "weather-uncorrected" PR values necessitate lengthier cumulative evaluation periods, approximately 4 years, to attain R² coefficients of determinations of 0.810 and 0.999 for their long-term degradation trends. These findings highlight that temperature-corrected PR values enable the earlier detection of long-term degradation trends.



Figure 1. Time required to achieve an R² coefficient of determination of 0.810 for long-term PV array degradation trend.



Figure 2. Time taken to attain an R² coefficient of determination of 0.999 for long-term PV system degradation trend.

4.4. Performance Ratio

The photovoltaic system performance ratio (PR) compares the actual and theoretical energy yields of the PV systems [41]. By normalising system performance to its installed power and available solar radiation at the installation site, the PR enables comparison of the performances of dissimilar PV systems in different geographic locations [4,38,42,43]. PR can be calculated on a yearly, monthly, or daily basis. The performance ratio, PR_{uncorr}, is calculated using Equation (1) [33]:

$$PR_{unco} = \frac{\sum P_{AC_t}}{\sum_{t} [P_{STC}(\frac{G_{POA}}{G_{STC}})]} \times 100\%,$$
(1)

where $P_{AC_l}XE "P_{AC_l}Measured AC$ electrical generation"_j: measured AC electrical generation (W).

 P_{STC} : installed PV module capacity (in the instance of the PV arrays examined 49,920 W_p).

 G_{POA} : measured plane of array irradiance (W/m²).

t{XE "t:data collection period"}: data collection period.

 $G_{STC_l}XE$ " G_{STC_l} Irradiance at standard test conditions" $_l$: irradiance at standard test conditions (1000 W/m²).

Introducing a correction based on cell temperature to calculate PR_{corr} gives [35]

$$PR_{corr} = \frac{\sum P_{AC_t}}{\sum_{t} \left[P_{STC} \left(\frac{G_{POA}}{G_{STC}} \right) \left(1 - \frac{\delta}{100} \left(T_{cell_avg - T_{cell}} \right) \right) \right]},$$
 (2)

where $T_{cell_l}XE \ "T_{cell_avg}$. Average annual solar cell temperature" $_{l_avg}$: average annual PV cell temperature (°C).

 T_{cell} : instantaneous PV cell temperature (°C).

 δ : tmperature coefficient of PV array power decreases with cell temperature (typically $-0.4\%/^{\circ}$ C).

$$\Gamma_{\text{cell_avg}} = \frac{\sum (G_{POA} \times T_{cell_i})}{\sum G_{PAO_i}}$$
(3)

 $G_{POA i}$: measured plane of array irradiance (W/m²) in a given period.

 $T_{cell i}$: instantaneous PV cell temperature ((°C) in an ith period.

To examine the effect on PR using module temperature correction, relative and absolute power loss rates (PLR) of uncorrected and corrected PR were compared. The percentage reduction in seasonal variations of corrected PR compared with uncorrected PR was calculated. Statistical analyses were performed using the t-distribution with significance levels (α) at 0.05, 0.10, and 0.01 and confidence intervals (C.I) at 95%, 90%, and 99%. The value of the t-distribution (t_{cal}) and confidence intervals (C.I) are calculated using Equations (4) and (5).

$$t_{cal} = \frac{\sum d_i}{\sqrt{\frac{n(\sum di^2) - (\sum di)^2}{DF}}},$$
(4)

where t_{cal}: calculated *t*-value.

di: difference between corrected and uncorrected PR (see Equation (6)). n: number of monitored data points. DF = n - 1: degree of freedom.

$$d_{\text{mean}} = \pm \left(T_{\text{C.I}} \times \text{S.E}(d_{\text{mean}}) \right)$$
(5)

where: d_{mean}: mean difference.

 $T_{C.I}$: *t*-test at a particular confidence interval (C.I). S.E(d_{mean}): standard error of the mean difference.

$$di = PR_{corr} - PR_{uncorr}$$
(6)

$$d_{\text{mean}} = \frac{\sum d_i}{n} \tag{7}$$

$$S.E(d_{mean}) = \frac{\sigma}{\sqrt{n}}$$
(8)

where: σ is the standard deviation.

$$\Gamma_{\rm C.I} = 1 - {\rm C.I} \tag{9}$$

The relative performance loss rate PLR_{rel} and the absolute performance loss rate PLR_{abs} are calculated using Equations (10) and (11) [40]:

$PLR_{rel}\{XE"PLR_{rel}: Relative performance loss rate"_{}[\%/a\{XE"a:Annual"\}] = (\beta_1 \frac{t}{\beta_0}) \times 100$ (10)

PLR_{abs} XE "PLR_{abs}: Absolute performance loss rate" $[/a] = (\beta_1 \times t),$ (11)

where $\beta 1{XE "\beta 1:Gradient"}{XE "\beta 1:Gradient"}$ is the gradient and $\beta 0{XE "\beta 0:y-intercept}$ of the linear trend line for PLR"}{XE "\beta 0:y-intercept"} is the y-intercept of the linear trend line for PLR, t is a scaling parameter that converts the time scale at which power or performance ratio (PR) is observed to a yearly scale, as PLR is per year (12 months), and S.E (d_{mean}) is the standard error of mean difference, d_{mean} (see Equations (6) and (7)).

$$Y_{t{XE "Yt:Time series linear regression model"}} = \beta_1 t + \beta_0$$
(12)

An annual aggregate gradient (β_1) of the linear fit divided by the y-intercept (β_0) gives the final linear relative performance loss rate (PLR_{rel}) of PV systems in Harlequins, Newry, and Warrenpoint. The annual aggregate gradient (β_1) of the linear function multiplied by the annual scale (12 months) gives the final linear absolute power loss rates (PLR_{abs}) (see Equation (11)). Figure 3a–c shows seasonal variations in performance metrics for the Harlequins, Newry, and Warrenpoint PV arrays from 2017 to 2021. Uncorrected performance ratios calculated using Equation (1) show high seasonality, with low values in warmer months and higher values in colder months [43]. The temperature-correction PR calculated using Equation (2) shows that the introduction of the module temperature correction (shown in Table 2) reduces seasonal variation in the performance ratio. The y-intercept (β_0) shows that the PR values for the five-year uncorrected and temperaturecorrected PR values for the Harlequins array (93.96% and 95.61%), the Newry array (93.96% and 95.14%), and the Warrenpoint array (93.84% and 95.43%) are nearly constant, where Arr. is the PV array and Sys. is the PV system.

From Figure 4a,b, the performance loss rates differ in the three PV arrays and PV systems because of differences in their meteorological conditions (such as the ambient temperature, relative humidity, wind speed, and air pressure) and system conditions (solar cell temperature and solar radiation). Figure 5a,b show the analyses of the annual relative performance loss rate (PLR_{rel}) and absolute performance loss rate (PLR_{abs}) of Harlequins, Newry, and Warrenpoint arrays for five years as shown in Tables A1–A4. The losses in a system are caused by various factors, including solar cell temperature losses, DC/AC inverter conversion losses, and solar radiation reflection losses. These losses can be further broken down into specific types of losses, such as shading losses, spectral losses, and inverter losses [44]. The following are some of the factors that contribute to system losses [44]: (i) Solar cell temperature losses: for every 1 °C above 25 °C, the output from a solar cell drops by 0.5%. (ii) DC/AC inverter conversion losses: PV inverter efficiency decreases from 0.3 to 1% per 150 V DC input voltage amplitude and the efficiency decreases down to 5% due to the power consumption of the control unit and switching



losses. (iii) Solar radiation reflection losses: there is some loss of output around 2.5% when sunlight reflects off panel surfaces rather than being absorbed to generate electric current.



Figure 3. (a-c) Weather-uncorrected and temperature-corrected PR for three arrays from 2017 to 2021.



(a)



(b)

Figure 4. Five–year monitored data showing performance loss rates from 2017 to 2021 at Harlequins, Newry, and Warrenpoint (**a**) arrays and (**b**) systems.





(b)

Figure 5. (a) Relative performance loss rate (PLR_{rel}) and (b) absolute performance loss rate (PLR_{abs}) for Harlequins, Newry, and Warrenpoint arrays from 2017 to 2021, where /a, as used in the legend of Figure 5, is per year or annum.

Figure 6a,b show the difference between the module temperature-corrected and uncorrected relative and absolute performance losses which are computed using (13) and (14):

$$D_{PLRcorr} = PLR_{rel.corr} - PLR_{abs.module}$$
(13)

$$D_{PLRuncorr} = PLR_{rel.uncorr} - PLR_{abs.uncorr},$$
(14)

where $D_{PLRcorr} \{XE "D_{PLRcorr}: Differences in temperature-corrected performance loss rates in arrays and systems"} and <math>D_{PLRuncorr} \{XE "D_{PLRuncorr}: Differences in uncorrected performance loss rates in arrays and systems."} are differences in temperature-corrected and uncorrected performance loss rates in arrays and systems. PLR_{rel.corr} {XE "PLR_{rel.corr}: Relative temperature-corrected performance loss rates in arrays and systems."} and PLR_{rel.corr} {XE "PLR_{rel.uncorr}: Relative temperature-corrected performance loss rates in arrays and systems."} and PLR_{rel.uncorr} {XE "PLR_{rel.uncorr}: Relative uncorrected performance loss rates in arrays and systems."} are relative temperature-corrected and uncorrected performance loss rates in arrays and systems."}$}}





Figure 6. The difference in (a) temperature correction and (b) uncorrected performance loss rates between relative and absolute performance loss rates in Harlequins, Newry, and Warrenpoint arrays from 2017 to 2021.

PLRabs.corr{XE "PLRabs.corr: Absolute temperature-corrected performance loss rates in arrays and systems" | and PLRabs.uncorr{XE "PLRabs.uncorr: Absolute uncorrected performance loss rates in arrays and systems" are absolute temperature-corrected and uncorrected performance loss rates in arrays and systems.

To normalise relative and absolute temperature-corrected performance loss rate, the PLR_{corr}/XE "PLR_{corr}:Relative weather-corrected performance loss rate", from weatheruncorrected performance loss rate (PLRuncorr/XE "PLRUncorr: Relative weather-corrected performance loss rate γ_l and the average cell temperatures, as shown in Table 2, for each PV array installed at Harlequins, Newry and Warrenpoint are used. Hence, the PLRcorr for PLR_{rel} and PLR_{abs} are normalised using Equations (15) and (16).

$$PLR_{corr_rel} = \frac{PLR_{uncorr_rel}}{1 - \frac{\delta}{100} (Tcell_{avg})}$$
(15)

(a)

 $PLR_{corr} \{ XE"PLR_{corr_abs} : Absolute weather - corrected performance loss rates" \}_abs = \frac{PLR_{uncorr_abs}}{1 - \frac{\delta}{100} (Tcell_{avg})}$ (16)

4.5. Statistical Analyses Using t-Distribution and Confidence Intervals

Figures 7a–c and 8a–c show graphs of module temperature-corrected relative performance loss rates, PLR_{corr_rel}, and module temperature-corrected absolute performance loss rates, PLR_{corr_abs}, across the three arrays and systems. The standard deviation error bars in these figures are overlapped because of the closeness of their standard deviation values, as shown in Tables 3 and 4.

Above, μ_{rel} {XE " μ_{rel} Relative averages of the temperature-corrected performance loss rates"} and μ_{abs} {XE " μ_{abs} : Absolute averages of the temperature-corrected performance loss rates"} are relative and absolute averages of the module temperature-corrected performance loss rates, while σ_{rel} {XE " σ_{rel} :Relative standard deviations of the temperature-corrected performance loss rates"} and σ_{abs} {XE " σ_{abs} :Absolute standard deviations of the temperature-corrected performance loss rates"} are relative and σ_{abs} {XE " σ_{abs} :Absolute standard deviations of the temperature-corrected performance loss rates"} are relative and σ_{abs} {XE " σ_{abs} :Absolute standard deviations of the temperature-corrected performance loss rates"} are relative and absolute standard deviations of the temperature-corrected performance loss rates are relative and absolute standard deviations of the temperature-corrected performance loss rates"} are relative and absolute standard deviations of the temperature-corrected performance loss rates.



Figure 7. (**a**–**c**) Standard deviation error bars show the overlap between relative and absolute module temperature-corrected performance loss rates of PV arrays monitored for a five-year period.



Figure 8. (**a**–**c**) Standard deviation error bars show the overlap between relative and absolute temperature-corrected performance loss rates of PV systems monitored for five years.

	Harle	equins		Newry				Warrenpoint			
μ_{rel}	$\sigma_{\rm rel}$	μ_{abs}	σ_{abs}	μ_{rel}	$\sigma_{\rm rel}$	μ_{abs}	σ_{abs}	μ_{rel}	σ_{rel}	μ_{abs}	σ_{abs}
-1.75	0.44	-1.66	0.41	-1.00	2.17	-1.99	0.66	-1.89	0.81	-1.79	0.79

Table 3. Comparative analysis of relative and absolute average and standard deviation of module temperature-corrected performance loss rates in arrays.

Table 4. Relative and absolute average and standard deviation values of module temperature corrected performance loss rates in systems.

Harlequins					Newry				Warrenpoint			
μ_{rel}	$\sigma_{\rm rel}$	μ_{abs}	σ_{abs}	μ_{rel}	σ_{rel}	μ_{abs}	σ_{abs}	μ_{rel}	σ_{rel}	μ_{abs}	σ_{abs}	
-1.04	3.91	-1.06	3.57	-1.26	1.00	-1.17	0.94	-1.91	1.56	-1.79	1.46	

The test of significance for relative and absolute temperature-corrected performance loss rates across the three sites is computed using Equation (17).

$$t_{cal} = \frac{\sum di}{\sqrt{\frac{n(\sum di^2) - (\sum di)^2}{DF}}},$$
(17)

where di{XE "di:Difference between corrected absolute and relative performance loss rates"} =

$$PLR_{corr_abs} - PLR_{corr_rel}$$
.

n = 5 is the number of monitored data points.

I

DF{XE "DF:Degree of freedom"} = n - 1 is the degree of freedom.

t_{cal}{XE "t_{cal}:Calculated *t*-value"} is the calculated *t*-value.

PLR_{abs_corr} is the absolute weather-corrected performance loss rate.

PLR_{rel_corr} is the relative weather-corrected performance loss rate.

Calculated *t*-values (t_{cal}) for Harlequins and Warrenpoint arrays for temperaturecorrected performance loss rates are greater than the critical values, t_{critical} (t_{cal} > t_{critical}), at 0.05, 0.10, and 0.01 levels of significance, and the Newry array t_{cal} value is less than the critical value, t_{critical} (t_{cal} < t_{critical}), at 0.05, 0.10, and 0.01 levels of significance, while t_{cal} for the Harlequins system for temperature-corrected performance loss rates is less than the critical values, t_{critical} (t_{cal} < t_{critical}), at 0.05, 0.10, and 0.01 levels of significance. This is shown in the t-distribution statistical table in Table 5. Warrenpoint and Newry systems are significant at 0.05 and 0.10 because t_{cal} > t_{critical}, while they are not significant at 0.01 because t_{cal} < t_{critical}. This means that the difference, d_i, between the PLR_{abs_corr} and PLR_{rel_corr} for the Harlequins array, Warrenpoint array, and Newry system are all significant at 0.05, 0.10, and 0.01 because t_{cal} > t_{critical}, while the Harlequins system and Newry array are not significant because t_{cal} < t_{critical}. The Warrenpoint system is only significant at 0.05 and 0.10 using Equation (17).

Table 5. Test of significance for the temperature-corrected performance loss rates in Harlequins, Newry, and Warrenpoint arrays and systems.

t _{critical} at Level of	t _{cal} for H	arlequins	t _{cal} for	Newry	t _{cal} for Warrenpoint		
Significance, α	Array	System	Array	System	Array	System	
$\alpha_{0.05} = 2.13$	6.24	-0.15	-1.45	3.10	7.65	2.51	
$\alpha_{0.10} = 1.53$	6.24	-0.15	-1.45	3.10	7.65	2.51	
$\alpha_{0.01} = 3.74$	6.24	-0.15	-1.45	3.10	7.65	2.51	

(18)

A paired *t*-test, utilising the t-distribution, was employed to assess the significance of temperature correction in mitigating seasonal fluctuations of the performance ratios. The assessment was conducted at various significance levels ($\alpha = 0.05, 0.10, \text{ and } 0.01$) and confidence intervals (C.I = 95%, 90% and 99%). The statistical analysis outcome indicates that for the Harlequins, Newry, and Warrenpoint PV arrays, the calculated *t*-values (t_{cal}) for $\alpha = 0.05, 0.10, \text{ and } 0.01$, as shown in Table 6, demonstrate statistical significance, leading to the rejection of the null hypothesis (H₀) and the acceptance of the alternative hypothesis (H₁). Figure 9 illustrates the confidence intervals (C.I) at 95%, 90%, and 99%, aligning with the confidence levels reported for t_{cal} values in Table 6 across the three PV arrays. Notably, the standard error of the mean difference (SE(d_{mean})) displayed in Figure 9, along with t_{cal} , remains consistent. This consistency is anticipated since physically similar PV arrays should exhibit akin S.E (d_{mean}) and t_{cal} values. The congruence between S.E (d_{mean}) and t_{cal} values provides compelling evidence that the implementation of module temperature correction effectively diminishes seasonal performance ratio variations. As a result, an enhancement in PV performance is achieved.

Table 6. Statistical analysis for Harlequins, Newry, and Warrenpoint systems.

		Harlequins				Newry			Warrenpoint				
α	t _{critical}	d _{mean}	Σ	S.E(d _{mean})	t _{cal}	d _{mean}	σ	S.E(d _{mean})	t _{cal}	d _{mean}	σ	S.E(d _{mean})	t _{cal}
0.05	2.00												
0.10	1.67	1.91	4.85	0.63	3.04	1.70	4.74	0.61	2.80	1.85	4.67	0.60	3.06
0.01	2.66	-											



Figure 9. Confidence intervals showing the certainty and uncertainty values.

Above, α is the level of significance; d_{mean} is the mean difference; σ is the standard deviation; t_{cal} is the calculated *t*-value; S.E(d_{mean}) is the standard error of the mean difference; DF = n - 1 is the degree of freedom; n = 60 is the number of monitored data points; and T_{C.I} is the t-test at a particular confidence interval (C.I).

5. Discussion

The discussion on "disaggregating longer-term trends from seasonal variations in measured PV system performance" revolves around the exploration of a method or approach that aims to separate and analyse the longer-term trends in the performance of PV

systems from the shorter-term variations. This type of analysis is crucial for understanding the overall performance of PV systems, identifying underlying factors that affect performance changes over time and making informed decisions for system optimisation. This study introduced a novel methodology that allows for the decomposition of measured PV system performance data into two main components: longer-term trends and seasonal variations. This separation enables a more detailed and accurate examination of the factors that influence PV system performance. In this discussion, several key points are typically addressed: (i) Overview of the Methodology: This study provides a concise summary of the method developed to disaggregate the longer-term trends and seasonal variations in PV system performance. This includes appropriate mathematical equations and statistical techniques used to achieve this separation. (ii) Significance of Longer-Term Trends: The study discusses the importance of understanding the longer-term trends in PV system performance. These trends are indicative of factors such as degradation, efficiency improvements, technological advancements, and changing environmental conditions over the years. (iii) Seasonal Variations: The study delved into the significance of seasonal variations in PV system performance. These variations are influenced by factors such as solar irradiance, temperature, shading, and maintenance practices. Hence, understanding these variations is crucial for optimising system performance.

6. Conclusions

The PV performance ratios underwent adjustments utilising the average annual cell temperature (T_{Cell_avg}), leading to the acquisition of performance ratios that have been rectified for module temperature. Through the utilisation of data gathered from a five-year examination involving three arrays, a comprehensive statistical investigation was conducted employing paired t-tests and confidence intervals. The primary goal was to ascertain the extent to which the variation in seasonal performance ratios decreased due to the module temperature correction. This investigation encompassed 95%, 90%, and 99% confidence intervals (C.I), alongside significance levels of 0.05, 0.10, and 0.01. Remarkably, the confidence values of C.I, t_{cal} values, and S.E(d_{mean}) demonstrated consistency, reflecting the similarity of the PV arrays. As a consequence of this observed similarity, the outcome of PR_{corr} exhibited more pronounced enhancement when compared to PR_{uncorr}.

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Appendix A

The relative performance loss rates (PLR_{rel}) and absolute performance loss rates (PLR_{abs}) for the Harlequins, Newry, and Warrenpoint arrays and systems, as shown in Figure 4a,b are summarised in Tables A1–A4.

Harle	quins	Observation Newry		ewry	Observation	Warre	npoint	Observation
Arr. PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	This means that PLR _{rel} of the	Array PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	There are	Arr. PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	The PLR _{rel} in Warrenpoint
-0.27	0.018	Harlequins array shows that solar panel generation will increase at the annual rate by -0.27%/a, which shows an improvement, while PLR _{rel} of the Harlequins system shows that PV system generation will decrease at the annual rate of 0.018%/a.	-0.23	-0.00635	in both the Newry array and system. For this reason, both the PLR _{rel} for the Newry array and system show that they will both increase at the annual rates by -0.23%/a and -0.00635%/a, respectively.	-0.17	0.00514	array shows that there is an improvement in the array. This means that solar panel generation will increase at an annual rate of -0.17%/a, while the PLR _{rel} in the Warrenpoint system shows that PV system generation will decrease at the annual rate of 0.00514%/a.

Table A1. Temperature-correction for relative performance loss rates (PLR_{rel}) for Harlequins, Newry, and Warrenpoint arrays and systems.

Table A2. Temperature-correction for absolute performance loss rates (PLR_{abs}) for Harlequins, Newry, and Warrenpoint arrays and systems.

Harle	quins	Observation	on Newry		Observation	Warre	enpoint	Observation
Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	The PLR _{abs} of the Harlequins	Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	_	Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	Warrenpoint array shows a PLR _{abs} _ improvement
-0.26	0.017	array show that solar panel generation will increase at the annual rate of -0.26/a, which shows an improvement, while the PLR _{abs} of the Harlequins system shows that PV system generation will decrease at the annual rate of 0.017/a.	-0.21	-0.006	Both the Newry array and system show improvements. This means that their PLR _{abs} will increase at the annual rates by -0.21/a and -0.006/a, respectively.	-0.16	0.0048	while the Warrenpoint system shows a decrease in PLR abs. This shows that solar panel generation will increase at an annual rate of -0.16/a, while the Warrenpoint system shows that PV system generation will decrease at an annual rate of 0.0048/a.

Harle	Harlequins Observation		Newry		Observation	Warrenpoint		Observation	
Arr. PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	_	Array PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	There are improvements in the Newry	Arr. PLR _{rel} (%/a)	Sys. PLR _{rel} (%/a)	_	
-0.16	-0.023	Both the Harlequins array and system showed an improvement at their PLR _{rel} . This shows that solar panel and PV generations will increase at annual rates of -0.16%/a and -0.023%/a, respectively. It will be difficult to predict any PLR _{rel} in the PV array and system due to the seasonal variation effect noticed in weather- uncorrected relative performance loss rates. To resolve this, the weather- uncorrected PLR _{rel} are normalised with the average cell temperature.	-0.01	-0.00104	array and system. For this reason, their PLR_{rel} shows that both the Newry array and system will increase at the annual rates by -0.01%/a and -0.00104%/a, respectively. Just like the Harlequins array and system, it will be difficult to predict any PLR_{rel} in the PV array and system due to the seasonal variation effect noticed in weather- uncorrected relative performance loss rates. To resolve this, the weather- uncorrected PLR_{rel} are normalised with the average cell temperature.	-0.063	0.00259	There is an improvement in the Warrenpoint array and a decrease in the Warrenpoint system. This shows that solar panel generation will increase at an annual rate by -0.063%/a, while the Warrenpoint system shows that PV system generation will decrease at the annual rate of 0.00259%/a.	

Table A3. Weather-uncorrected relative performance loss rates (PLR_{rel}) for Harlequins, Newry, and Warrenpoint arrays and systems.

Harle	equins	Observation	Newry		Observation	Warrenpoint		Observation
Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	- Both the	Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	There are improvements – in both the	Arr. PLR _{abs} (/a)	Sys. PLR _{abs} (/a)	_
-0.15	-0.022	Harlequins array and system show improvements in PLR _{abs} . This show that solar panel and PV generations will increase at annual rates of -0.15/a and -0.022/a. Just like PLR _{rel} in the Harlequins array and system, it will be difficult to predict any PLR _{rel} in the PV array and system due to the seasonal variation effect noticed in weather- uncorrected relative performance loss rates. To resolve this, the weather- uncorrected PLR _{rel} are normalised with the average cell temperature.	-0.0096	-0.0096	Newry array and system. This means that their PLR _{abs} show that both the Newry array and system will increase at the annual rates by -0.0096/a and -0.0096/a, respectively. Just like the Newry array and system, it will be difficult to predict any PLR _{rel} in the PV array and system due to the seasonal variation effect noticed in weather- uncorrected relative performance loss rates. To resolve this, the weather- uncorrected PLR _{rel} are normalised with the average cell temperature.	-0.06	0.0024	Performance improvement is noticed in the Warrenpoint array and there is a decrease in performance in the Warrenpoint system. This means that solar panel generation will increase at an annual rate of -0.06/a, while the Warrenpoint system shows that PV system generation will decrease at the annual rate of 0.0024/a.

Table A4. Weather-uncorrected absolute performance loss rates (PLR_{abs}) for Harlequins, Newry, and Warrenpoint arrays and systems.

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