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# A Residential Energy Hub Model with a Concentrating Solar Power Plant and Electric Vehicles

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**Abstract:** Renewable energy generation and electric vehicles (EVs) have attracted much attention in the past decade due to increasingly serious environmental problems as well as less and less fossil energy reserves. Moreover, the forms of energy utilization are changing with the development of information technology and energy technology. The term “energy hub” has been introduced to represent an entity with the capability of energy production, conversion and storage. A residential quarter energy-hub-optimization model including a concentrating solar power (CSP) unit is proposed in this work, with solar energy and electricity as its inputs to supply thermal and electrical demands, and the operating objective is to minimize the involved operation costs. The optimization model is a mixed integer linear programming (MILP) problem. Demand side management (DSM) is next implemented by modeling shiftable electrical loads such as EVs and washers, as well as flexible thermal loads such as hot water. Finally, the developed optimization model is solved with the commercial CPLEX solver based on the YALMIP/MATLAB toolbox, and sample examples are provided for demonstrating the features of the proposed method.

**Keywords:** energy hub; concentrating solar power (CSP); demand side management (DSM); thermal storage system (TSS); electric vehicle (EV)

## 1. Introduction

The technical basis and organizational structure of the energy industry are gradually changing due to less and less reserves of fossil fuels and increasingly serious environmental problems [1–3]. More efficient, sustainable and safer utilization modes of energy are gaining much attention. The conception of the “energy internet” was first proposed in [4]. A new energy utilization system, which is a combination of new energy technologies and information technology, was introduced and named “energy internet”. As one of the important parts of the energy internet, the term “energy hub” was first proposed in [5], and defined as a virtual entity consisting of energy production, conversion and storage functions.

An energy hub represents an interface between different energy infrastructures and loads [6]. From a systematic point of view, each hub can own many different energy carriers as inputs and outputs, as described in Figure 1. Over the past few years, the operating and planning problems of energy hubs have been addressed by many researchers. Besides the electricity from a power grid, natural gas is widely used as the other energy input in these studies due to the recently developed power-to-gas (P2G) and combined heat and power (CHP) technologies [7–12]. In [13] a framework is

developed to optimally design and size interconnected energy hubs, and the physical constraints of the natural gas and electricity networks as well as environmental issues are considered. An optimal expansion planning model for energy hubs is proposed in [14], which is used for the optimal selection of transmission lines and CHP units. A bi-level optimization methodology for the optimal operation of energy hubs and energy networks is presented in [15]. There are many advantages of natural gas as the input to energy hubs, but it will still produce carbon emissions and the cost of natural gas is relatively high (0.56 \$/m<sup>3</sup> in Beijing, China). The development of concentrating solar power (CSP) provides a new way of thinking for the operation of energy hubs.

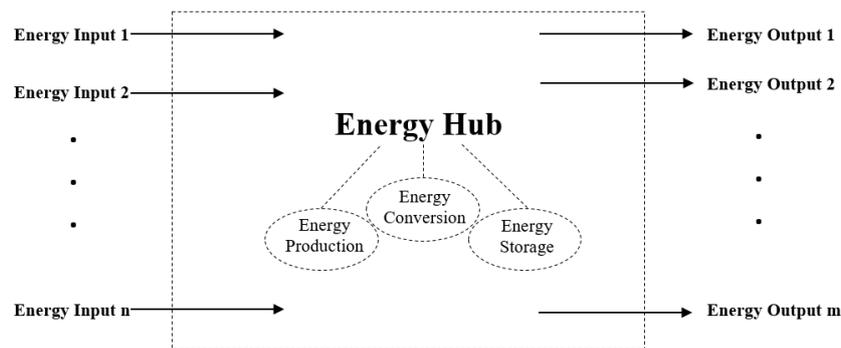


Figure 1. An illustrative energy hub.

Same as photovoltaic (PV) generation, CSP units use solar energy as the primary energy source, and there is almost no carbon emission problem [16]. The difference is that the thermal energy of sunlight is utilized in CSP units to generate electricity, and the output characteristics are similar to those of conventional steam turbines, which are adjustable and have very good performance in the power ramp rate. In addition, an advantage of CSP over many renewables is that it is usually equipped with a thermal storage system (TSS), which allows 15-hour continuous full-load power generation in the absence of sunlight or other extreme cases [17]. The medium materials in a TSS are usually molten salt, with high efficiency and low cost [18].

The structure of a CSP plant is broadly described in Figure 2 [19], and consists of solar fields, a heat transfer fluid/steam generation system, a Rankine steam turbine/generator cycle, and the TSS. In this work, the solar fields are designed in a hybrid solution combining the trough collectors and panels for improving system performance during low solar radiation periods [20–22]. CSP plants use heat transfer fluid (HTF), mostly heat transfer oil in the existing CSP plants, to absorb radiant energy in a solar receiver. The use of molten salts and phase changing material as HTFs can effectively improve the plant energy efficiency [23,24]. In solar fields, the lower temperature oil is heated to almost 400 °C, and the collected solar energy is exchanged to the steam generator, which can produce superheated steam (10.4 MPa, 370 °C). The superheated steam is then fed to a conventional reheat steam turbine/generator to produce electricity. This heat absorbed by HTF can be used immediately to generate power or stored in the TSS for later use for power generation in off-sun hours [25].

In the past few decades there has been a spurt in research reporting interesting results on the choice of working fluids for organic Rankine cycle-based power generation [26–29]. However, the integration of a solar field with supercritical CO<sub>2</sub> Brayton power cycles can achieve a high level of thermal efficiency due to the high solar concentration ratio associated with solar central receiver systems [30]. When CO<sub>2</sub> is operated beyond its critical point (T = 304.1 K, P = 7.37 MPa), it is called supercritical CO<sub>2</sub> [31]. The integration of the solar field with supercritical CO<sub>2</sub> Brayton power cycles in CSP plants was studied in [32,33], and the applicability and efficiency were proved.

According to the estimation of the US Department of Energy, the power generation cost of a CSP plant will be as low to 0.06 \$/kWh in 2020 [34]. Previous research into CSP is mainly from the perspective of its electricity generation performance, but the utilization of its thermal energy has not



(thermal output/electrical input) is in the range of 3.0–4.0 when the ambient temperature is above 0 °C. Thus, the coordination of the heat pump and the heat recovery unit as well as TSS can provide a stable heat supply for users.

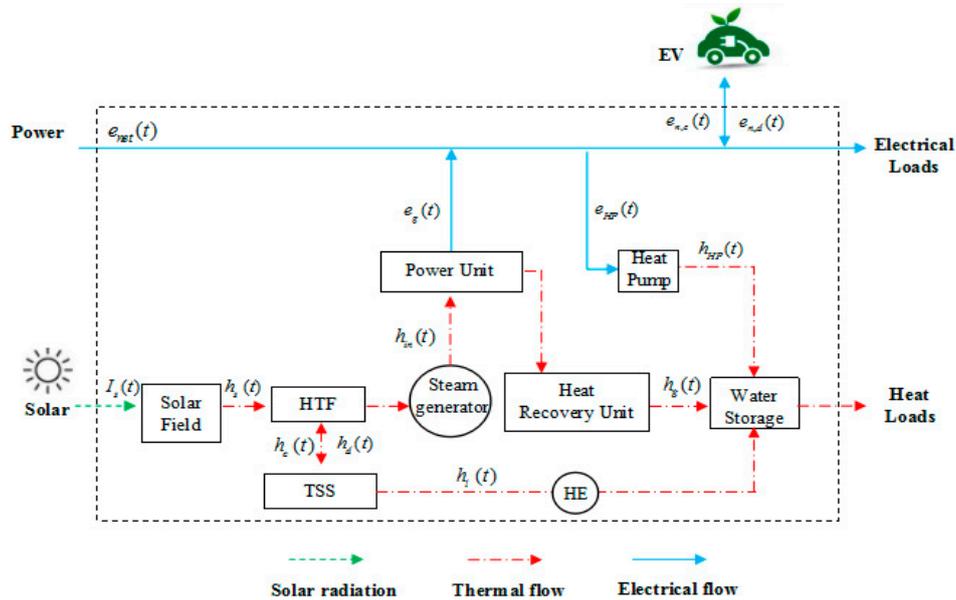


Figure 3. The proposed residential quarter energy hub model.

### 3. Problem Formulation

In this section, the proposed energy hub and detailed electrical and thermal loads are formulated mathematically.

#### 3.1. Objective Function

The optimal operation model is formulated from an economic perspective [37–39], with the objective of minimizing the costs associated with the power generation of the CSP unit and the electricity purchased from the power network during the day. It is worth noting that the electricity can be sold back to the network when the power generated from the energy hub is redundant, and  $e_{net}(t)$  takes a negative value in this case. The objective function is expressed as:

$$\min \sum_{t=1}^T [e_{net}(t)p_{net}(t)\Delta t + e_g(t)p_g(t)\Delta t] \tag{1}$$

where  $e_{net}(t)$  and  $e_g(t)$  represent the power exchanged with the power network concerned and the output of a CSP unit at time  $t$ , respectively; and  $p_{net}(t)$  and  $p_g(t)$  represent the corresponding costs, respectively.

As it can be seen from (1), it is assumed that the price of purchasing/selling electricity from/to the main grid is always the same for each time interval, and the power generation cost of the CSP unit is simplified as a piecewise linear function.

#### 3.2. Load Modeling

Demand side management is implemented by utilizing shiftable electrical loads and flexible thermal loads.

##### 3.2.1. Electrical Load Modeling

(1) EV modeling. The charging load of electric vehicles (EVs) is shiftable. It is interruptible and can be dispatched flexibly in smart grid environment. Moreover, EVs can also be used as distributed

energy storage devices. The energy stored in EVs can be transmitted back to the power network concerned, the so-called vehicle-to-grid (V2G) function. The constraints of EVs can be formulated as follows ( $\forall n \in N_{EV}$ ):

$$e_{n,c}(t) = x_{n,c}(t)E_c \quad (2)$$

$$e_{n,d}(t) = x_{n,d}(t)E_d \quad (3)$$

$$x_{n,c}(t) + x_{n,d}(t) \leq 1 \quad (4)$$

$$S_{n,a} = S_n(t_{n,a}) \quad (5)$$

$$S_{n,tg} \leq S_n(t_{n,l}) \leq 1 \quad (6)$$

$$S_n(t) = S_n(t-1) + \mu_c^{EV} \frac{e_{n,c}(t)}{b_n} \Delta t - \frac{e_{n,d}(t)}{\mu_d^{EV}} \frac{1}{b_n} \Delta t \quad (7)$$

where  $e_{n,c}(t)$  and  $e_{n,d}(t)$  represent the charging and discharging power of an EV  $n$  at time  $t$ , respectively;  $x_{n,c}(t)$  and  $x_{n,d}(t)$  are the binary decision variables respectively used to represent the charging and discharging status of EV  $n$  at time  $t$ ;  $E_c$  and  $E_d$  represent the rated charging and discharging power of an EV, respectively;  $S_n(t)$  represents the state of charge (SOC) of an EV  $n$  at time  $t$ ;  $S_{n,a}$  and  $S_{n,tg}$  represent the SOC of an EV  $n$  at the arrival time  $t_{n,a}$  and the target SOC of an EV  $n$  at the departure time  $t_{n,l}$ , respectively;  $\mu_c^{EV}$  and  $\mu_d^{EV}$  respectively represent the charging and discharging efficiencies of EVs; and  $b_n$  represents the battery capacity of EV  $n$ .

Equations (2)–(4) represent the constraints of the charging and discharging behaviors of EVs. Equations (5) and (6) represent the SOC constraints of EVs at the arrival and departure time, respectively. The time-varying SOC of EVs is formulated as Equation (7).

(2) Washer. Some household appliances, such as washers, can be scheduled based on the electricity price variations, without causing significant discomfort to users. Suppose that smart meters [40] with a bidirectional communication capacity are installed in each house, so that the washers in each house can be dispatched based on the price signal. Moreover, the schedulable time interval  $T_{op}$  is defined in order to not have a big influence on the comfort level of customers [41]. The operational constraints of washers are expressed as ( $\forall i \in N_w$ ):

$$u_i(t) - v_i(t) = x_i(t) - x_i(t-1), \quad \forall t \in T_{op} \quad (8)$$

$$u_i(t) + v_i(t) \leq 1 \quad (9)$$

$$\sum_{t \in T_{op}} x_i(t) = M_i \quad (10)$$

$$\sum_{k=t-U_i+1}^t u_i(k) \leq x_i(t), \quad \forall t \in T_{op} \quad (11)$$

$$\sum_{t \notin T_{op}} x_i(t) = 0 \quad (12)$$

where  $u_i(t)$ ,  $v_i(t)$  and  $x_i(t)$  are the binary decision variables used to represent the startup, shut down and on/off status of washer  $i$  at time  $t$ , respectively; and  $M_i$  and  $U_i$  represent the minimum operating time and minimum startup time of washer  $i$ .

Equations (8) and (9) represent the constraints of the operation status of washers. The minimum operation time for finishing a task and the minimum startup time are expressed by Equations (10) and (11), respectively.

(3) Total electrical loads. The electrical loads of the system consist of the rigid demands, which are nonshiftable and shiftable loads. Thus the electrical loads at time  $t$  can be formulated as:

$$l_e(t) = l_e^R(t) + \sum_{N_w} x_i(t)E_w + \sum_{N_{EV}} e_{n,c}(t) - \sum_{N_{EV}} e_{n,d}(t) \quad (13)$$

where  $l_e(t)$  represents the total electrical load at time  $t$ ;  $l_e^R(t)$  represents the rigid (nonshiftable) electrical demand at time  $t$ ; and  $E_w$  represents the rated power of a washer.

### 3.2.2. Flexible Thermal Load

The thermal load is modeled within the context of the desired hot water temperature. Suppose that the water storage tank is always full, and this means that the volume of injected cold water is always the same as the consumed hot water at each time interval. According to the temperature-dependent model of thermal loads, presented in [42], the mathematical model of hot water is expressed by Equation (14). Moreover, regarding flexible thermal load modeling, the acceptable temperature range is defined by Equation (15).

$$\theta_w(t+1) = \theta_w(t) - \frac{\theta_w(t) - \theta_{cold}}{V} V_{cold}(t) + \frac{1}{\rho \cdot V \cdot C} h_w(t) \Delta t \quad (14)$$

$$\theta_w^{\min} \leq \theta_w(t) \leq \theta_w^{\max} \quad (15)$$

$$l_h(t) = h_w(t) \quad (16)$$

where  $\theta_w(t)$  represents the water temperature in the water storage tank at time  $t$ ;  $\theta_w^{\max}$  and  $\theta_w^{\min}$  represent the maximum and minimum temperatures of water, respectively;  $\theta_{cold}$  represents the temperature of cold water;  $V$  and  $V_{cold}(t)$  represent the volume of the storage tank and the volume of the injecting cold water at time  $t$ , respectively;  $\rho$  and  $C$  represent the density and the specific heat capacity of water, respectively;  $h_w(t)$  represents the heating power of the water storage tank at time  $t$ ; and  $l_h(t)$  represents the total thermal load at time  $t$ .

## 3.3. Constraints

### 3.3.1. Electrical Constraints

$$e_{net}(t) + e_g(t) = e_{HP}(t) + l_e(t) \quad (17)$$

$$e_g(t) = \mu_e h_{in}(t) \quad (18)$$

$$0 \leq e_g(t) \leq E_g^{\max} \quad (19)$$

$$e_{net}(t) \leq E_{net}^{\max} \quad (20)$$

where  $e_{HP}(t)$  represents the electrical input of the heat pump at time  $t$ ;  $h_{in}(t)$  represents the thermal power input of a CSP unit at time  $t$ ;  $\mu_e$  represents the conversion efficiency from thermal power to electric power in a CSP unit [43];  $E_g^{\max}$  and  $E_{net}^{\max}$  represent the maximum power output of a CSP unit and the maximum transmission power of the line, respectively.

The electrical power balance is expressed by Equation (17). The electrical output of a CSP unit is determined by Equation (18). The output limits of a CSP unit and transmission power constraints from the network are expressed by Equations (19) and (20).

### 3.3.2. Thermal Constraints

$$h_{HP}(t) + h_g(t) + \mu_{HE} h_l(t) = l_h(t) \quad (21)$$

$$h_s(t) + h_d(t) = h_{in}(t) + h_c(t) \quad (22)$$

$$h_s(t) = \mu_s A_s I_s(t) \quad (23)$$

$$h_g(t) = \mu_h h_{in}(t) \quad (24)$$

$$h_{HP}(t) = \mu_{HP} e_{HP}(t) \quad (25)$$

where  $h_{HP}(t)$  and  $h_g(t)$  represent the thermal power outputs of the heat pump and the CSP unit at time  $t$ , respectively;  $h_l(t)$  represents the thermal demand supplied by the TSS at time  $t$ ;  $h_c(t)$  and  $h_d(t)$  respectively represent the injected and drawn heat from the TSS at time  $t$ ;  $h_s(t)$  represents the thermal power from the solar field at time  $t$ ;  $I_s(t)$  represents the solar radiation intensity at time  $t$ ; and  $A_s$  represents the area of the PV array;  $\mu_{HE}$ ,  $\mu_s$ ,  $\mu_h$  and  $\mu_{HP}$  are the heat exchanger efficiency, photo-thermal conversion efficiency, thermal efficiency of a CSP unit and heating efficiency ratio of the heat pump, respectively.

Equation (21) represents the demand–supply balance of thermal power. Equation (22) represents the thermal power conservation of a CSP unit. Solar radiation power is determined by Equation (23), and the thermal output of a CSP unit and heat pump are expressed by Equations (24) and (25).

### 3.3.3. TSS Constraints

The TSS constraints are specially expressed in this section because TSS is relatively complex and plays an important role in the operation of the system.

$$W_h(t) = W_h(t-1) + \mu_c^{TSS} h_c(t) \Delta t - \frac{h_d(t)}{\mu_d^{TSS}} \Delta t - h_l(t) \Delta t - W_h^{loss}(t) \quad (26)$$

$$W_h^{loss}(t) = \gamma W_h(t) \quad (27)$$

$$W_h^{\min} \leq W_h(t) \leq W_h^{\max} \quad (28)$$

$$W_h^{\max} = \rho^{FLH} \frac{E_s^{\max}}{\mu_e} \quad (29)$$

$$0 \leq h_c(t) \leq x_c^h(t) H_c^{\max} \quad (30)$$

$$0 \leq h_d(t) \leq x_d^h(t) H_d^{\max} \quad (31)$$

$$x_c^h(t) + x_d^h(t) \leq 1 \quad (32)$$

$$\sum_{t=1}^T \left[ \mu_c^{TSS} h_c(t) \Delta t - \frac{h_d(t)}{\mu_d^{TSS}} \Delta t - h_l(t) \Delta t - W_h^{loss}(t) \right] = 0 \quad (33)$$

where  $W_h(t)$  represents the thermal energy stored in TSS at time  $t$ ;  $\mu_c^{TSS}$  and  $\mu_d^{TSS}$  respectively represent the thermal charging and discharging efficiencies of TSS at time  $t$ ;  $W_h^{loss}(t)$  represents the energy loss of TSS at time  $t$ ;  $\gamma$  is the heat loss coefficient;  $W_h^{\max}$  and  $W_h^{\min}$  represent the maximum and minimum capacity limits of TSS, respectively;  $\rho^{FLH}$  represents the full-load hours of a CSP unit;  $x_c^h(t)$  and  $x_d^h(t)$  are the binary decision variables respectively used to represent the injecting and drawing status of TSS at time  $t$ ; and  $H_c^{\max}$  and  $H_d^{\max}$  respectively represent the maximum thermal charging and discharging power of TSS.

Equation (26) represents the thermal energy conservation of TSS. Equation (27) represents the heat loss. The capacity limitation is represented by Equation (28). The maximum capacity is determined by the maximum output of a CSP unit and a full-load hour (FLH) in extreme weather conditions, which is expressed by Equation (29). The charging and discharging of thermal power constraints are represented by Equations (30)–(32). Equation (33) represents that the total amount of injected thermal energies are equal to those of the drawn energies in a dispatching cycle, guaranteeing the consistency of the energy in TSS at the beginning of each cycle.

### 3.4. Solving Method

The proposed cost-minimizing model of the energy hub is a mixed integer linear planning (MILP) problem. CPLEX is a mature commercial solver, and the proposed model is solved by a CPLEX solver based on the YALMIP/MATLAB toolbox.

## 4. Case Studies

### 4.1. Parameter Setting

The proposed model was conducted on a residential quarter energy hub with 3000 households. A CSP power plant with a capacity of 5 MW-e was employed. The hot water demands and nonshiftable electrical demands of each household are shown in Figure 4 [44]. Suppose that each family has a washer, and the number of EVs is 1500. The arrival and departure time of the EVs follows the probability density distributions described by Equations (34) and (35) [45].  $S_{n,a}$  represent random numbers distributed evenly between 10–30%. A day is divided into 96 periods in the case studies with 15 min for each time interval. It was assumed that the parameters remain unchanged in each time interval. Thus, the parameter values for this time interval can be described by the parameter values at the beginning of the period. The time-of-use (TOU) electricity prices are shown in Table 1, while other parameter assumptions are shown in Table 2.

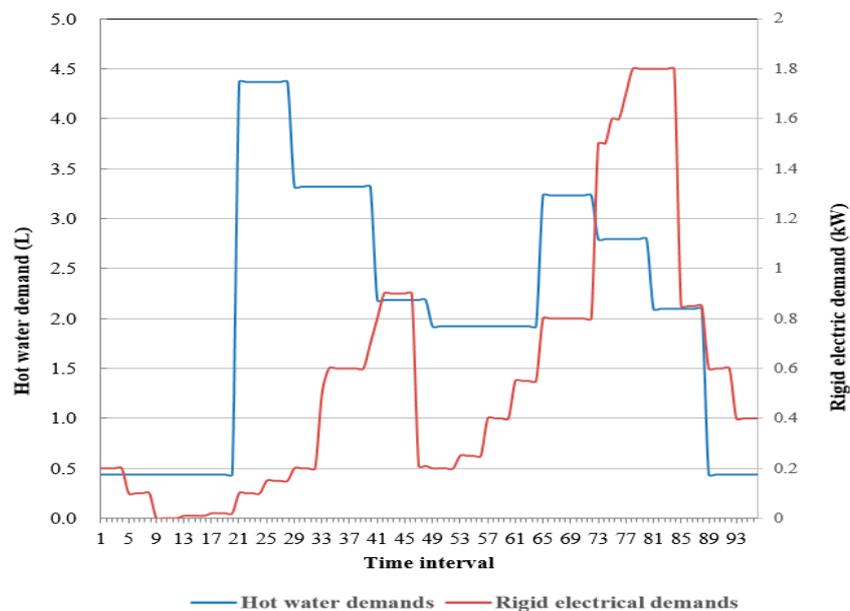


Figure 4. Daily hot water demands and rigid electrical demands for a single residential consumer.

Table 1. Time-of-use (TOU) electricity prices.

Time	TOU	Price (\$/kWh)
7:00 a.m.–8:15 a.m.	Mid-peak	0.102
8:30 a.m.–10:15 a.m.	Sub-peak	0.164
10:30 a.m.–11:30 a.m.	On-peak	0.174
11:45 a.m.–5:45 p.m.	Mid-peak	0.102
6:00 p.m.–6:45 p.m.	Sub-peak	0.164
7:00 p.m.–8:45 p.m.	On-peak	0.174
9:00 p.m.–10:45 p.m.	Sub-peak	0.164
11:00 p.m.–6:45 a.m.	Off-peak	0.041

**Table 2.** Parameter assumption.

Parameter		Value
Rated charging and discharging power of EVs (kW)	$E_c, E_d$	3, 3
Rated power of a washer (kW)	$E_w$	0.5
Target SOC of EV $n$	$S_n, t_g$	0.85
Heat loss coefficient	$\gamma$	0.01
Full-load hour (h)	$\rho^{\text{FLH}}$	15
Battery capacity of EV $n$ (kWh)	$b_n$	20
Minimum operating time of washer $i$ (h)	$M_i,$	1
Minimum startup time of washer $i$ (h)	$U_i$	0.25
Charging and discharging efficiencies of EVs	$\mu_c^{EV}, \mu_d^{EV}$	0.95, 0.95
Maximum and minimum temperature of the water ( $^{\circ}\text{C}$ )	$\theta_w^{\text{max}}, \theta_w^{\text{min}}$	80, 60
Temperature of the cold water ( $^{\circ}\text{C}$ )	$\theta_{\text{cold}}$	10
Maximum power output of a CSP unit (MW)	$E_g^{\text{max}}$	5
Maximum transmission power of the line (MW)	$E_{\text{net}}^{\text{max}}$	2
Conversion efficiency from thermal power to electric power in a CSP unit	$\mu_e$	0.35
Thermal efficiency of a CSP unit	$\mu_h$	0.5
Heat exchanger efficiency	$\mu_{HE}$	0.7
Heating efficiency ratio of the heat pump	$\mu_{HP}$	3
Minimum capacity limit of TSS (MWh)	$W_h^{\text{min}}$	100
Maximum thermal charging and discharging power of TSS (MW)	$H_c^{\text{max}}, H_d^{\text{max}}$	2, 2
Thermal charging and discharging efficiencies of TSS	$\mu_c^{\text{TSS}}, \mu_d^{\text{TSS}}$	0.98, 0.98

The variables to be optimized include the operating status of the flexible loads (e.g., EVs, washers and hot water), power exchanged with the main grid, the output of heat pumps, and the charging/discharging power of the TSS.

$$f_a(x) = \begin{cases} \frac{1}{\sqrt{2\pi}\sigma_a} e^{-\frac{(x+24-\mu_a)^2}{2\sigma_a^2}}, & 0 < x \leq \mu_a - 12 \\ \frac{1}{\sqrt{2\pi}\sigma_a} e^{-\frac{(x-\mu_a)^2}{2\sigma_a^2}}, & \mu_a - 12 < x \leq 24 \end{cases} \quad (34)$$

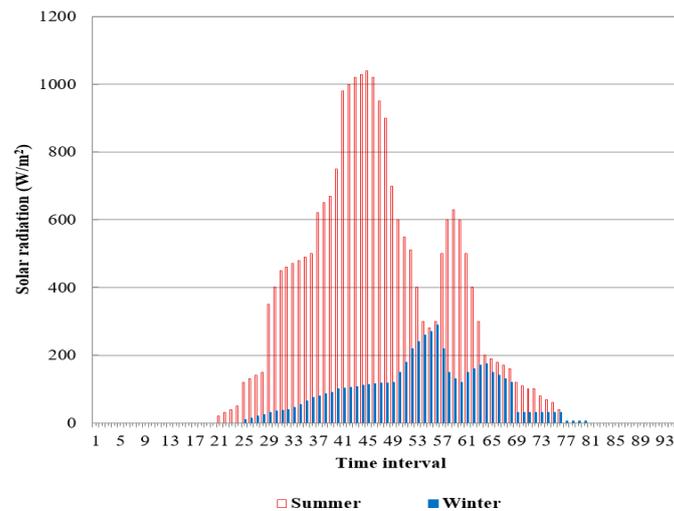
where,  $\mu_a = 17.47$ ,  $\sigma_a = 3.41$ .

$$f_l(x) = \begin{cases} \frac{1}{\sqrt{2\pi}\sigma_l} e^{-\frac{(x-\mu_l)^2}{2\sigma_l^2}}, & 0 < x \leq \mu_l + 12 \\ \frac{1}{\sqrt{2\pi}\sigma_l} e^{-\frac{(x-24-\mu_l)^2}{2\sigma_l^2}}, & \mu_l + 12 < x \leq 24 \end{cases} \quad (35)$$

where,  $\mu_l = 8.92$ ,  $\sigma_l = 3.24$ .

#### 4.2. Simulation and Results

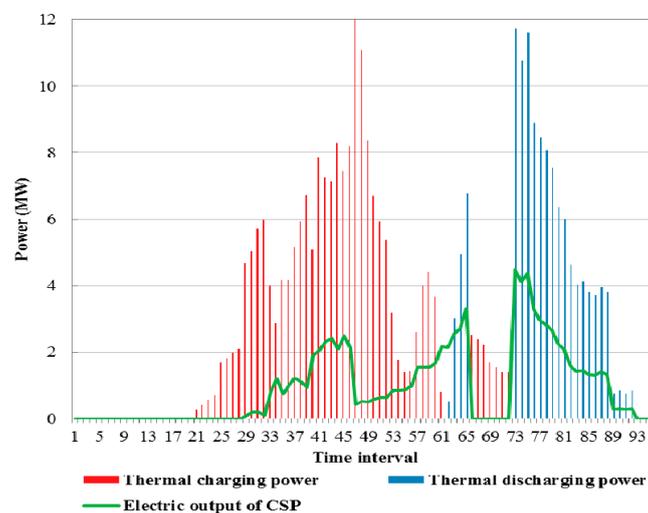
The CPLEX solver based on the YALMIP toolbox in MATLAB was employed to solve the proposed MILP model for typical summer and winter days. The solar irradiance data for a typical day in summer and in winter are shown in Figure 5, which were measured at the Center for Sustainable Energy Systems at the Australian National University [46]. The total operation costs of the energy hub were \$3212.07 and \$5003.48 for a typical summer day and a typical winter day according to the results, respectively. The analysis and comparison of the summer and winter cases will be presented in this section.



**Figure 5.** The solar radiation curves.

#### 4.2.1. Typical Summer Day

The thermal charging and discharging status of the TSS and the power generation of a CSP unit are depicted in Figure 6. The output of the CSP reached the peak in the time interval  $t \in [73, 76]$ , during which the conventional electrical load was also close to the maximum. The optimization module responded to the change of price automatically during the day and acted in a way that mitigated the load level as much as possible during the peak-load hours with on-peak prices. Moreover, the CSP had continuous output in the time interval  $t \in [77, 92]$ , during which the solar radiation intensity was 0 or close to 0, due to the presence of the TSS.



**Figure 6.** Thermal charging/discharging power and the electrical output of a CSP unit on a typical summer day.

Figure 7 illustrates the charging and discharging power of EVs and the operation of washers. EVs discharge on a large scale in  $t \in [34, 46]$  and  $[73, 92]$  periods, which are the peak-price periods for electricity. In these periods, EVs discharge to satisfy the electrical demands, thus reducing the cost of electricity purchased from the power network. The charging power of EVs and working time of washers are concentrated in  $t \in [1, 28]$ ,  $[49, 72]$ , and  $[93, 96]$  periods, during which the electricity prices are lower, i.e., \$0.041 and \$0.102, respectively. Meanwhile, as known from the rigid demand curve,

the centralized discharging time of EVs is also in the peak-load periods. Thus, the introduction of shiftable loads can not only reduce the operation costs, but also plays an important load-shifting role in the system.

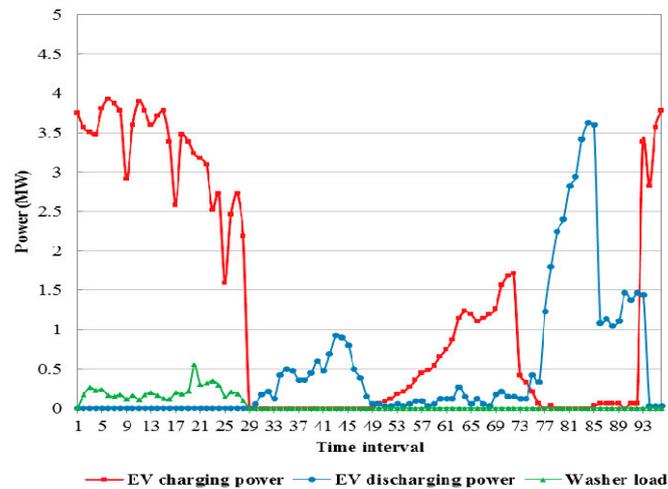


Figure 7. Shiftable electrical loads on a typical summer day.

The heating power of water storage tanks and the hot water temperature curves are shown in Figure 8. As shown in the curves, the thermal output reaches the day's peak in the  $t \in [73, 84]$  period, during which the stored water is constantly heated. The temperature reaches its maximum in the  $t \in [85, 92]$  period. After that, since the cost of CSP generation is greater than the electricity price, the electrical output (as well as the thermal output) of CSP is controlled to be as little as possible. The thermal energy in the TSS is utilized cooperatively to maintain the temperature of the hot water through the heat exchanger.

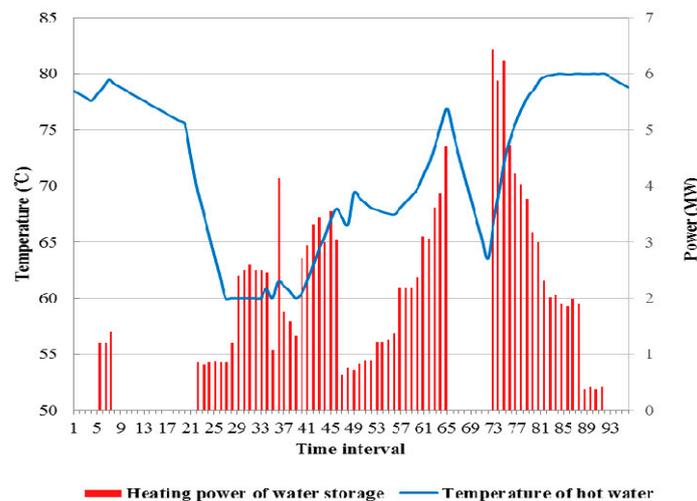
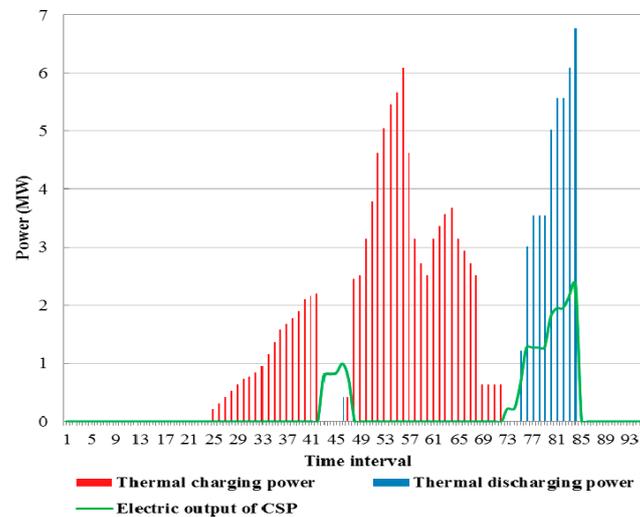


Figure 8. Heating power of the water storage tank and the temperature of hot water on a typical summer day.

#### 4.2.2. Typical Winter Day

The thermal charging and discharging status of the TSS and the power generation of the CSP unit on a typical winter day are shown in Figure 9. The output of the CSP unit only rose in  $t \in [41, 47]$  and  $[73, 84]$  periods. The output of the CSP unit was significantly reduced due to the decrease of

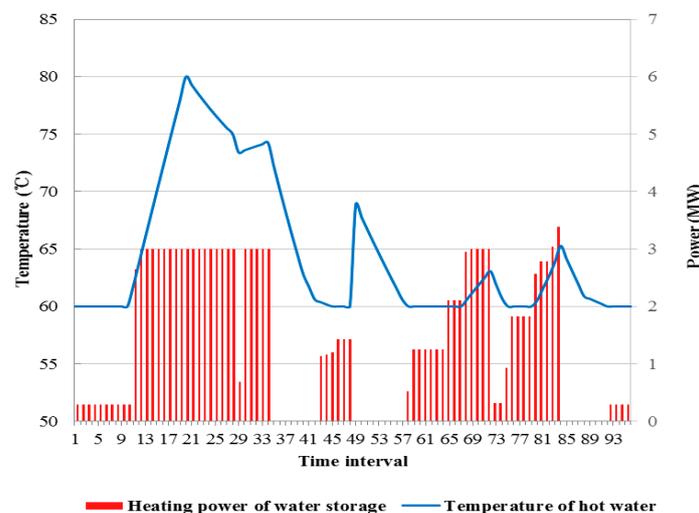
solar radiation intensity compared with a summer day, but still concentrated in the peak load periods. Meanwhile, the cost of the energy hub was increased obviously on winter days due to the reduced CSP output.



**Figure 9.** Thermal charging/discharging power and the electrical output of a CSP unit on a typical winter day.

There is no significant difference in the behaviors of the shiftable electrical loads compared to the summer case, so they are no longer described in detail in this section. Their excellent performance, however, cannot be ignored.

The heating power of the water storage tank and the hot water temperature curves for a typical winter day are shown in Figure 10. The thermal output was reduced due to the decrease of corresponding electrical output, so the temperature of hot water was only maintained at the pre-set minimum level most of the time. It is worth mentioning that the energy purchased from the grid were 36.16 MWh and 62.29 MWh in the summer and winter cases, respectively. Besides the reduction of CSP output, the increase of power consumption of HP, which was used to satisfy the heat demands, caused the larger amount of purchased electricity in winter. That is also an important factor in the increase of costs on a typical winter day.



**Figure 10.** Heating power of the water storage tank and the temperature of hot water on a typical winter day.

Table 3 shows the changes in the operation costs of the system with the variation of EV numbers. It can be seen that the costs decrease with an increase in the numbers of EVs. The excellent cost-reduction performance of EVs for the proposed system is further demonstrated.

**Table 3.** Changes of operation costs with various numbers of EVs.

Number of EVs	Cost (\$)
750	5201.89
1500	5003.48
2250	4927.72

## 5. Conclusions

In this paper, a residential quarter energy hub model with a CSP unit was presented. Solar energy and electricity from the main power grid served as the inputs into the system to provide electrical and thermal loads for residential users. The demand side management was implemented by utilizing shiftable electrical loads and flexible thermal loads. Based on the proposed architecture, an MILP optimization model with the objective of minimizing the operation cost was developed, and then solved by a YALMIP/CPLEX solver. Case studies were carried out, and it was shown by simulations that the proposed model exhibits good performance in cost saving and load shifting.

The following issues will be investigated in future research efforts:

- Integration strategies for biomass boilers with a CSP for backing up CSP production on winter days;
- Integration strategies of CSP with wind power for enhancing the capability of accommodating wind power in the context of the emerging energy internet;
- In-depth ambient temperature sensing analysis in power units for improving the overall working performance of CSP.

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**Conflicts of Interest:** The authors declare no conflict of interest.

## Nomenclature

EV	Electric vehicle
CSP	Concentrating solar power
MILP	Mixed integer linear programming
DSM	Demand side management
TSS	Thermal storage system
P2G	Power to gas
V2G	Vehicle to grid
CHP	Combined heat and power
HTF	Heat-transfer fluid
SOC	State of charge
$e_{n,c}(t)$	Charging power of EV $n$ at time $t$ (kW)
$e_{n,d}(t)$	Discharging power of EV $n$ at time $t$ (kW)
$S_n(t)$	SOC of EV $n$ at time $t$
$b_n$	Battery capacity of EV $n$ (kWh)

$l_e(t)$	Electrical loads at time $t$ (MW)
$\theta_w(t)$	Temperature of water in the water storage tank at time $t$ ( $^{\circ}\text{C}$ )
$l_h(t)$	Thermal loads at time $t$ (MW)
$e_{net}(t)$	Power exchanged with power network at time $t$ (MW)
$e_g(t)$	Power output of a CSP unit at time $t$ (MW)
$p_{net}(t)$	The time-of-use electricity price at time $t$ ( $\$/\text{MWh}$ )
$p_g(t)$	The per unit power generation cost of a CSP unit at time $t$ ( $\$/\text{MWh}$ )
$e_{HP}(t)$	Electrical power input of a heat pump at time $t$ (MW)
$h_{in}(t)$	Thermal power input of a CSP unit at time $t$ (MW)
$h_c(t), h_d(t)$	Injected/drawn thermal power from TSS at time $t$ (MW)
$h_{HP}(t)$	Thermal power output of a heat pump at time $t$ (MW)
$h_g(t)$	Thermal power output of a CSP unit at time $t$ (MW)
$h_l(t)$	Thermal demand supplied by TSS at time $t$ (MW)
$W_h(t)$	Thermal energy stored in TSS at time $t$ (MWh)
$W_h^{loss}(t)$	Energy loss of TSS at time $t$ (MWh)
$x_{n,c}(t)$	Binary decision variable used to represent charging status of EV $n$ at time $t$
$x_{n,d}(t)$	Binary decision variable used to represent discharging status of EV $n$ at time $t$
$u_i(t)$	Binary decision variable used to represent start up status of washer $i$ at time $t$
$v_i(t)$	Binary decision variable used to represent shut down status of washer $i$ at time $t$
$x_i(t)$	Binary decision variable used to represent on/off status of washer $i$ at time $t$
$x_c^t(t)$	Binary decision variable used to represent injecting status of TSS at time $t$
$x_d^t(t)$	Binary decision variable used to represent drawing status of TSS at time $t$
$E_d$	Rated discharging power of EVs (kW)
$E_c$	Rated charging power of EVs (kW)
$t_{n,a}$	Arrival time of EV $n$
$t_{n,l}$	Departure time of EV $n$
$S_{n,a}$	SOC of EV $n$ at arrival time
$S_{n,tg}$	Target SOC of EV $n$
$\mu_c^{EV}$	Charging efficiency of EVs
$\mu_d^{EV}$	Discharging efficiency of EVs
$l_h(t)$	Total thermal load at time $t$ (MW)
$T_{op}$	Schedulable time of washers
$b_n$	Battery capacity of EV $n$ (kWh)
$M_i$	Minimum operating time of washer $i$ (h)
$U_i$	Minimum start up time of washer $i$ (h)
$l_e(t)$	Total electrical loads at time $t$ (MW)
$l_e^R(t)$	Rigid electrical loads at time $t$ (MW)
$E_w$	Rated power of washers (kW)
$\theta_{cold}$	Temperature of the cold water ( $^{\circ}\text{C}$ )
$\theta_w^{\max}$	Maximum temperature of water ( $^{\circ}\text{C}$ )
$\theta_w^{\min}$	Minimum temperature of water ( $^{\circ}\text{C}$ )
$V$	Volume of the water storage tank ( $\text{m}^3$ )
$V_{cold}$	Volume of injecting cold water at time $t$ ( $\text{m}^3$ )
$\rho$	Density of water ( $\text{kg}/\text{m}^3$ )
$C$	Specific heat capacity of water ( $\text{J}/(\text{kg}\cdot^{\circ}\text{C})$ )
$h_w(t)$	Heating power of the water storage tank at time $t$ (MW)
$\mu_e$	Conversion efficiency from thermal power to electric power in a CSP unit
$E_g^{\max}$	Maximum power output of a CSP unit (MW)
$E_{net}^{\max}$	Maximum transmission power of line (MW)
$h_s(t)$	Thermal power from solar field at time $t$ (MW)
$A_s$	PV array area ( $\text{m}^2$ )
$\mu_s$	Photo-thermal conversion efficiency
$\mu_h$	Thermal efficiency of a CSP unit
$\mu_{HP}$	Heating efficiency ratio of a heat pump

$I_s(t)$	Solar radiation intensity at time $t$ (MW/m <sup>2</sup> )
$\mu_c^{TSS}$	Thermal charging efficiency of TSS at time $t$
$\mu_d^{TSS}$	Thermal discharging efficiency of TSS at time $t$
$\gamma$	Heat loss coefficient
$W_h^{\min}$	Minimum capacity limit of TSS (MWh)
$W_h^{\max}$	Maximum capacity limit of TSS (MWh)
$\rho^{\text{FLH}}$	Full-load hour (h)
$H_c^{\max}$	Maximum thermal charging power of TSS (MW)
$H_d^{\max}$	Maximum thermal discharging power of TSS (MW)

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