

Development and Verification of Hybrid Power Controller Using Indoor HIL Test for the Solar UAV

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Article

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Abstract: A hybrid power system (HPS) is developed for the photovoltaic (PV) powered and tethered multirotor unmanned aerial vehicle (UAV) based on the robot operating system (ROS) and verified using an indoor hardware-in-the-loop (HIL) test. All the processes, including a UAV flight mode change (i.e., takeoff, hovering, and landing) and power flow control (consisting of PV modules, a LiPo battery pack, and a UAV) are completely automated using a combination of Pixhawk 2.1 and the Raspberry Pi 3 Model B (RPi 3B). Once the indoor HIL test starts, (1) the UAV takes off and hovers with a preassigned 10 m altitude at a fixed point and keeps hovering until the voltage drops below 13.4 V; (2) the UAV lands when the voltage drops below 13.4 V, and the hybrid power controller (HPC) starts to charge the LiPo battery pack using the energy from PV modules; and (3) the UAV takes off when the voltage of the battery pack becomes more than 16.8 V, and the procedure repeats from (1). A PV-powered and tethered multirotor UAV using the proposed HPS can fly more safely for a longer time, particularly in an urban area, and so it is competitive to the traditional multirotor type UAV in the sense of both the flight time and the surveillance mission performance.

Keywords: hardware-in-the-loop (HIL); hybrid power controller (HPC); hybrid power system (HPS); photovoltaic (PV) module; state of charge (SOC); unmanned aerial vehicle (UAV)

1. Introduction

Increasing the flight time of an unmanned aerial vehicle (UAV) is getting important as the application of UAVs into 4D (dirty, dangerous, dull, and dear) missions is increasing. A fixed-wing type UAV has, in general, a higher flight endurance compared to the multirotor type UAVs, and thus the former type has been widely applied in surveillance missions that require long endurance. However, the application of using a fixed-wing UAV is typically limited to vast and open plains since it requires a runway for hand or pneumatic launch during takeoff and a safe touch down during landing. Therefore, people have recently started to use multirotor type UAVs, which can perform vertical takeoff and landing (VTOL), mitigating geographic limitations in operations. For continuous aerial surveillance around urban areas with high congestion, the tethered multirotor type UAV is the appropriate choice in the sense of stability and maneuverability.

The main contribution of this paper can be categorized into two parts: (1) a photovoltaic (PV) based hybrid power system (HPS) and (2) a hardware-in-the-loop (HIL) based automatic flight test bench (AFTB). To highlight the main contributions of this manuscript, several previous research works are analyzed in two parts, (1) PV-based HPS and (2) HIL-based AFTB, as follows.

1.1. PV-Based HPS

For even higher flight endurance, there have been approaches to develop a hybrid power system using various combinations of energy sources.



Gong and et al. developed a HPS for a fixed-wing vehicle fusing a fuel cell, a battery pack, and a supercapacitor; they tested it using an HIL-based flight simulation and performed a real flight test [1–3]. Lee et al. managed a three-hybrid energy source to power a small long-endurance UAV using an active power management method to ultimately maintain a target state of charge (SOC) of batteries at 45% [4]. Harmon et al. developed the parallel hybrid-electric propulsion system using a rule-based controller and showed that the overall energy consumption could be tremendously reduced [5]. Malaver et al. used the maximum power point (MPPT), a battery charger, and a power path manager using a BQ24030 electronic chip from Texas Instruments Inc. to supply regulated power to a UAV [6–9]. Meyer et al. developed a power management system for a solar-powered UAV, meeting the nominal system voltage of 22.2 V using PV cells, isolation switches, LiPo batteries, and a power management computer [10]. The Naval Research Laboratory (NRL) developed a hydrogen fuel-cell-based propulsion system by introducing autonomous soaring algorithms with which the UAV flight time is tremendously extended [11,12].

Current challenges of the HPS include (1) increasing energy density; (2) decreasing weight; (3) being operable in the wide system operation voltage, current, and power; (4) possessing a precision state estimation algorithm of all energy sources; and (5) being compatible with the robot operating system (ROS) through the MAVLink on ROS (MAVROS) ROS package.

Here, MAVROS is the "MAVLink extendable communication node for ROS with the proxy for ground control station (GCS)" [13]. MAVLink is a protocol for communicating with UAVs [14]. The MAVROS ROS-package-based MAVLink extendable communication is essential to communicate with ROS-based computers, MAVLink-based autopilots, and MAVLink-based GCSs. With the MAVROS-based hybrid power controller (HPC), which can communicate through MAVLink, we could implement the precision state estimation algorithm of all energy sources for a safe and long mission operation of a UAV.

1.2. HIL-Based AFTB

HIL simulation, also called HILS and HITL, is one of the indoor test methods that is listed as model-in-the-loop (MIL), software-in-the-loop (SIL), processor-in-the-loop (PIL), and HIL. Although all the listed simulation steps are necessary to develop and test real-time embedded systems, we only focus on HIL simulation in this paper.

Akcakoca and et al. presented an SIL- and HIL-based UAV development and verification architecture structured on the ROS, in particular, by using Gazebo, AirSim, and V-REP flight simulators [15]. Lepej and et al. developed a modular-based flexible HIL architecture for the rapid system configuration using ROS [16]. Odelga and et al. developed a ROS and Gazebo-based HIL simulation setup to test algorithms and computational feasibility on a UAV's hardware platform [17]. Ebeid and et al. presented a survey of existing open-source UAV platform elements that could be utilized for an HIL simulation [18].

None of the above-listed studies developed an HIL-based AFTB to develop a PV-based HPS, and eliminating this gap is the main focus of this paper.

This paper presents the system overview of the HPS, UAV, and GCS in Section 2. Section 3 describes the HPS. Section 4 presents the UAV. Section 5 presents the GCS. Sections 6 and 7 show the test methods and results. Section 8 shows improvements and comparisons to the existing research works. Lastly, Section 9 concludes the paper.

2. System Overview

The overall system (Figure 1) is composed of an HPS (Section 3), a UAV (Section 4), and a GCS (Section 5). Throughout the paper, each primary system, the HPS, UAV, and GCS, is deeply investigated.

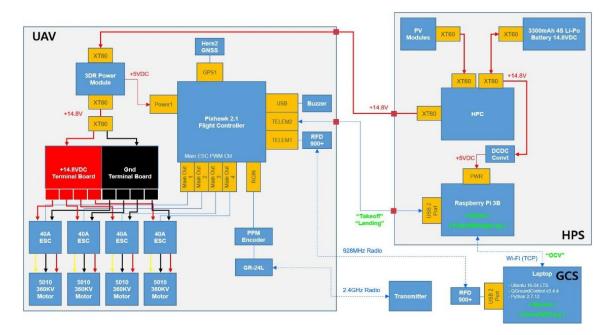


Figure 1. System overview of unmanned aerial vehicle (UAV), hybrid power system (HPS), and ground control system (GCS).

3. HPS

An HPS, which consists of a hybrid power controller (HPC), a PV, and a LiPo battery, is developed to manage the power flow among PV modules, a battery pack, and a UAV.

3.1. HPC

The HPC is the main component of the HPS, and it is necessary to intelligently manage the power flow among PV modules, the battery pack, and the UAV. The HPC is based on a Raspberry Pi 3 Model B (RPi 3B), and so it can communicate with a GCS through Wi-Fi. Detailed specifications and an overview of the HPC are shown in Table 1 and Figure 2. The conceptual electrical interconnection diagram and software are shown in Figures 3 and 4. In particular, we chose the RPi 3B as an onboard computer and Python as the development language since; (1) there is an incomparable number of communities and forums for getting support to solve development issues and (2) the hardware itself is cheap, small, and light enough to be mounted on the small UAV.

Table 1. Specifications of the hybrid power controller (HPC).

Component	Specification	
Micro Controller Unit (MCU)	Raspberry Pi 3 Model B (RPi 3B)	
Storage	16GB Micro SD Card	
Current Sensor	Blkbox 100 A	
Voltage Sensor	In-House Development	
Temperature Sensor	TI LM35	
A/D Converter	MCP3008	
Metal-Oxide-Semiconductor Field-Effect Transistor (MOSFET)	IRF4905	
Weight (kg)	1.373	

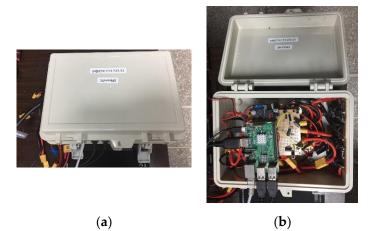


Figure 2. Overview of the HPC: (**a**) outside and (**b**) inside.

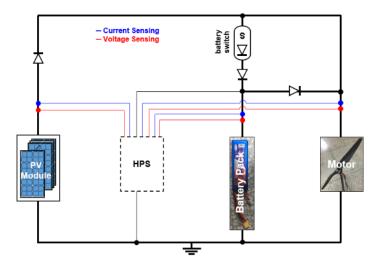


Figure 3. Conceptual electrical interconnection diagram of the HPC.

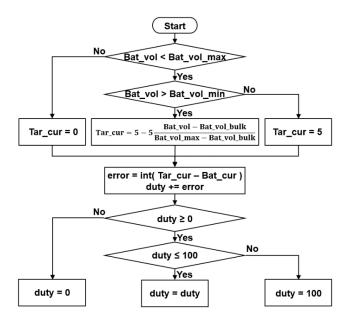


Figure 4. Conceptual software of the HPC.

For the transmission control protocol (TCP) setup between the HPS and GCS through Wi-Fi, an RPi 3B located in the HPS runs the PowerManager.py Python code and acts as a client. The structure of the PowerManager.py Python code is shown in Algorithm 1. Here, OCV represents the open circuit voltage.

Algorithm 1 [CLIENT] PowerManager.py

- 1. [LIBRARY] Import General (time, spidev, keyboard), TCP (socket), Array (numpy), and GPIO (*Adafruit_GPIO*) libraries.
- 2. [DEFINE] Define *PowerManager* class mainly for the duty cycle control and sensor data acquisition. This class contains definitions including __init__, write_duty, spinOnce, tcp, read_sensor_values, update_sensor_values, average_sensor_values, control_battery_charge, led, stdout_logging, and data_logger.
- 3. [MAIN]
 - 3.1 [TCP] Set TCP IP, port, and buffer size. Then, run connect mode.
 - 3.2 While True:
 - Run spinOnce

3.2. PV Module

The PV cells convert light into electricity by the photovoltaic effect as follows: (1) Photons in sunlight are absorbed by semiconducting materials; (2) the absorbed photons excite electrons in the semiconducting materials; (3) excited electrons transmit through a transparent conducting electrode and generate electron–hole pairs; (4) the charge carriers move to cancel out the potential difference; and (5) current flows are captured into either DC or AC.

We used a total of 256 PV cells to form the 32S8P PV-module configuration. One PV module consists of a 32S1P cell configuration, and a total of eight PV modules that are 32S8P are set up to generate about 18 V and 40 A at maximum. Further details of the PV-cell specification (Figure 5) are listed in Table 2.

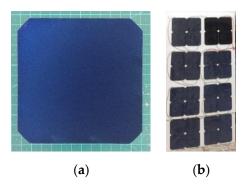


Figure 5. Overview of the PV (a) cell and (b) module.

Table 2. Specifications of the photovoltaic (PV) cell.

Parameter	Specification	
Max voltage (V)	0.55	
Max current (A)	5.8	
Max power (W)	3.19	
Efficiency (%)	20.8	
Size (mm \times mm)	125×125	
Weight (kg)	0.006	

3.3. Battery Pack

We use a LiPo battery pack to give power to the UAV and take power from the PV modules. A LiPo type battery pack is chosen since it has high charging and discharging C-rates compared to the 18,650 prismatic type battery pack. Because of the high charging C-rate, the LiPo battery pack can be quickly charged from the PV module. In addition, due to the high discharging C-rate, the LiPo battery pack can deal with the high current during the takeoff flight mode. Detailed specifications of the LiPo battery pack are shown in Table 3, and the overview is shown in Figure 6.

Parameter	Specification	
Manufacturer	Enrichpower	
Capacity (Ah)	3.3	
Max discharge rate (C)	35	
Max charging rate (C)	5	
Voltage (V)	14.8	
Configuration	4S 1P	
Weight (kg)	0.346	

Table 3. Specifications of the LiPo battery pack.



Figure 6. Overview of the LiPo battery pack.

4. UAV

A UAV, which consists of a flight controller (FC), frame, motors, electronic speed controllers (ESC), blades, a GPS, and telemetries, is developed for a continuous surveillance mission. Detailed specifications of the UAV are shown in Table 4, and the overview is shown in Figure 7.

Component	Specification	
FC	Pixhawk 2.1 (PX4)	
Frame	Tarot Ironman 1000	
Motor	RCtimer 5010-360 KV	
ESC	Simonk 40 A	
Blade	17 × 55 Carbon	
GPS	Here2 GNSS	
Telemetry1	RFD 900+	
Telemetry2	GR-24L Receiver	
Weight (kg)	2.35 (w/o battery pack)	
GPS Telemetry1 Telemetry2	Here2 GNSS RFD 900+ GR-24L Receiver	

Table 4. Specifications of the UAV.



Figure 7. Overview of the UAV.

5. GCS

A GCS is used mainly to send flight mode commands to the client, which is a HPS, and to monitor the UAV status using QGroundControl (QGC). The GCS is also used for the software-in-the-loop (SIL) and HIL tests. Detailed specifications of the GCS are shown in Table 5, and the overview is shown in Figure 8.

Component	Specification
Processor	Intel [®] Core TM i7-7500U
Memory	15 GB
OS	Ubuntu 16.04 LTS
SW	QGroundControl v3.4.4, Python 2.7.12

Table 5. Specifications of the GCS.



Figure 8. Overview of the GCS.

For the TCP setup between the GCS and the HPS through Wi-Fi, the GCS runs the *HoverSOC.py* Python code and acts as a server. The structure of the *HoverSOC.py* Python code is shown in Algorithm 2.

Algorithm 2 [SERVER] HoverSOC.py

- 1. [LIBRARY] Import General (sys, time, struct, keyboard), TCP (socket), and ROS (rospy, geometry_msgs, mavros_msgs) libraries.
- 2. [DEFINE] Define OCV2SOC function for the SOC calculation.
- 3. [DEFINE] Define *fcuModes* class for the flight mode activation using ROS services.
- 4. [DEFINE] Define Controller class for the UAV movement control.
- 5. [MAIN]
 - 5.1 [SOC] Import OCV-SOC curve data.
 - 5.2 [ROS] Initiate ROS node, flight mode object, controller object, ROS loop rate, subscription to UAV state, subscription to UAV's local position, and setpoint publisher.
 - 5.3 [TCP] Set TCP IP, port, and buffer size. Then, run bind, listen, and accept modes.
 - 5.4 While not rospy.is_shutdown():

Receive OCV value from CLIENT, calculate SOC using OCV2SOC function, and save it as SOC variable.
If OCV > 16.8:
Let the UAV arm.
Send a setpoint message to UAV and activate OFFBOARD mode.
If SOC < 13.4:
Let the UAV land and disarm. [SOC] Import OCV-SOC curve data.

6. Test Method

The HPS was tested and verified through an indoor HIL test (Figures 9 and 10). A charger (Model: KIKUSUI PWR800L) and a discharger (Model: KIKUSUI PLZ1004W) were used to mimic PV modules and a UAV, respectively. In particular, the Gazebo flight simulator was used to perform autonomous flight simulation. Here, the discharger and the Gazebo flight simulator are synchronized so that the discharger starts discharging when the UAV in Gazebo takes off and vice versa.



Figure 9. Indoor experiment.

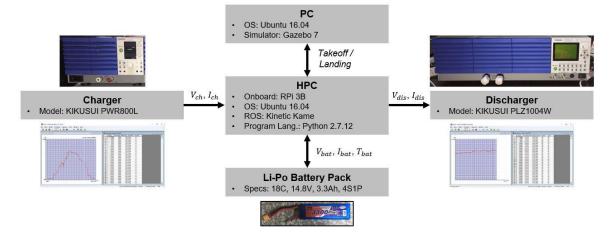


Figure 10. Indoor hardware-in-the-loop (HIL) test setup.

7. Test Result

We obtained the current and voltage profiles of the PV modules for 10 h from 08:00 to 18:00 at a schoolyard on 11 November 2019. The stored current and voltage profiles of the PV modules were then used to obtain the battery pack SOC and the UAV altitude data as shown in Figure 11.

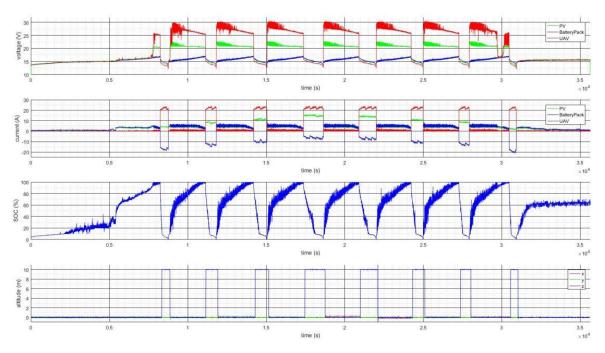


Figure 11. Indoor HIL test result.

Here, the PV profile is shown as green, the battery pack profile is shown as blue, and the UAV profile is shown as red. The coulomb counting method is used to calculate the SOC. If we carefully look into the battery pack profile, the operating voltage range is between 16.8 and 13.4 V; the charging current is managed to be under 5 A, and the SOC range is between 0% and 100% as we designed it. The UAV altitude operates well between 0 and 10 m.

8. Improvements and Comparisons

The presented HPC developed by Chosun University is unique in the sense that it uses low nominal battery voltage, can be applied to a multirotor type UAV, can deal with the highest power, and lastly uses ROS as shown in Table 6.

	Presented Work	Reference [19]	Reference [4]	Reference [20]	Reference [3]
Research Institute	Chosun Univ.	KARI and KAIST	KAIST and KARI	NRL	University of Sydney
Nominal Battery Voltage (V)	14.8 (4S)	25.9 (7S)	25.9 (7S)	25.9 (7S)	14.8 (4S)
Power (W)	770	500	200	Undefined	170
Max. Flight	0.3	1.5	3.8	4.5	0.3
Time (h)	(Multirotor)	(Fixed-Wing)	(Fixed-Wing)	(Fixed-Wing)	(Fixed-Wing)
Appearance		No. for Chemical Control Contr			
ROS Capability	О	Х	Х	О	Х

Table 6. Comparison of the HPC boards managing PV, a fuel cell, and a battery pack.

9. Conclusions

We developed a HPC for a tethered solar multirotor UAV (carrying Pixhawk 2.1 and ROS-based RPi 3B) and verified it using indoor HIL tests. Both the automated flight mode change (including takeoff, hovering, and landing) and the power flow control (including PV modules, a LiPo battery pack, and a UAV) were tested and verified.

In the future, a custom HPC printed circuit board (PCB) having a low weight will be manufactured, installed, and tested on a VTOL-type UAV to demonstrate its effectiveness in the aspect of flight duration.

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Conflicts of Interest: The author declares no conflict of interest.

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