



# **Supplementary Materials**

# Core-shell Fe<sub>3</sub>O<sub>4</sub>@zeolite NaA as an Adsorbent for Cu<sup>2+</sup>

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#### SI Supporting Materials and Methods

**Batch Adsorption Experiments** 

#### S1.Preparation of Cu<sup>2+</sup> Solutions

Prepared a standard  $Cu^{2+}$  stock solution (500 mg/L) by dissolving  $Cu(SO_4)_25H_2O$  in a beaker. The solution was then diluted to the desired concentration using deionized water.

#### S2.Adsorption Study

All adsorption experiments were performed in a batch mode using a shaking table (MPS-1500, Ningbo, zhejiang province, China) at a controlled temperature. The pH of the solution was adjusted to the desired value by adding negligible volume of 0.1 M NaOH and 0.1 M HCl solution. The determination of pH value is measured by SMART PH818 PH meter. After the adsorption test, the sample was immediately filtered through a syringe filter (0.45  $\mu$ m syringe filter, PP filter medida, Yuecheng, China), and the remaining Cu<sup>2+</sup> concentration in the supernatant was measured by inductively coupled plasma spectrometer (ICP- OES) analysis (8300, PerkinElmer, USA). The adsorption experiment was performed in a reciprocating water bath shaker at a shaking speed of 170rpm. The adsorption capacity (Qe, mg/g) and adsorption efficiency of the adsorbents were calculated using the following Equations (S1) and (S2) [1]:

$$Q_e = \frac{C_0 - C_e}{M} \times V$$
(S1)
$$R_{emoval\%} = \frac{C_0 - C_e}{C_0} \times 100$$
(S2)

Where Qe is the adsorption capacity (mg/g); C<sub>0</sub> is the initial Cu<sup>2+</sup> concentration (mg/L); Ce is the final Cu<sup>2+</sup> concentration (mg/L); M (g) is the weight of the adsorbent used and V (L) is the volume of the Cu<sup>2+</sup> solution. Removal% is the removal rate of Cu<sup>2+</sup> by the adsorbent; Each experiment was repeated three times to obtain average results.

(S2)

#### **Adsorption Kinetics Study**

The knowledge of adsorption kinetics is important information for designing batch adsorption systems. To examine the adsorption kinetics of the adsorbent for Cu<sup>2+</sup>, the Lagergren pseudo-first-order and pseudo-second-order kinetic models were examined [2].

(1) Lagergren pseudo-first-order kinetic model:

$$In(Q_e - Q_t) = InQ_e - K_1 t$$
 (S3)

(2) Lagergren pseudo-second-order kinetic model:

$$\frac{t}{Q_t} = \frac{1}{K_2 Q_e^2} + \frac{t}{Q_e}$$
(S4)

where Qe is the amounts of adsorption at equilibrium, mg/g; Qt is the amounts of adsorption at time t, mg/g; k1 is the first order rate constant,  $min^{-1}$ ; k2 is the second order rate constants,  $min^{-1}$ .

## Adsorption Isotherm Study

The liner form of Langmuir adsorption isotherm is one of the most famous well-adopted models used to describe the solid phase adsorption systems [3].

$$\frac{C_{e}}{Q_{e}} = \frac{C_{e}}{Q_{\max}} + \frac{1}{K_{L}Q_{\max}}$$
(S5)  
$$R_{L} = \frac{1}{1 + K_{L}C_{0}}$$
(S6)

Where  $Q_{max}$  is the Langmuir maximum adsorption capacity (mg/g), and K<sub>L</sub> is the Langmuir binding constant. Where C<sub>0</sub> and K<sub>L</sub> are the initial concentration of arsenic and Langmuir isotherm constant. If the value of O < R<sub>L</sub> < 1, it represents favourable adsorption.

The Freundlich model indicates the heterogeneity of the adsorbent surface and considers multilayer adsorption. The linear form of Freundlich adsorption model is as follows [4]:

$$InQ_e = Ink_f + \frac{1}{n}InC_e$$
(S7)

Where  $K_f$  and 1/n are Freundlich constants, related to adsorption capacity and adsorption intensity (heterogeneity factor) respectively. The values of  $K_f$  and 1/n were obtained from the slope and intercept of the linear Freundlich plot of ln  $Q_e$  versus ln  $C_e$ .

The Temkin model is a modification equation of the Langmuir model. The adsorption enthalpy declined linearly with the increase of adsorption amounts. The Temkin model is described by equation S8:

$$Q_{\rm e} = B_1 InK_t + B_1 InC_e (S8)$$

where  $B_1$  and  $K_t$  are constants related to adsorption enthalpy and capacity of the adsorbent.

# Thermodynamic Study

Using the slope and intercept of the plot the lnk<sub>d</sub> versus 1/T is presented in Equation 9, the enthalpy change ( $\Delta H^{\circ}$ ) and entropy change ( $\Delta S^{\circ}$ ) can be calculated. T(K) is the Kelvin temperature. R(8.314J/(mol·K)) is the universal gas constant. The Gibbs free-energy change of the sorption of Cu<sup>2+</sup> ions using adsorbent is given using Equation 9:

$$K_d = \frac{Q_e}{C_e}$$

$$InK_{d} = \frac{\Delta S^{0}}{R} - \frac{\Delta H^{0}}{RT} (S9)$$

The standard enthalpy change ( $\Delta$ H<sup>o</sup>), and standard entropy change ( $\Delta$ S<sup>o</sup>) was calculated using following equation <sup>[5]</sup>:

$$\Delta G^0 = \Delta H^0 - T \Delta S^0 (\mathbf{S10})$$

Where  $(\Delta H^0)$  is standard enthalpy change (KJ/mol) and  $(\Delta S^0)$  is standard entropy change (KJ/mol K).

	Items	Content(w %)
-	Fe <sub>3</sub> O <sub>4</sub>	47.003
	SiO <sub>2</sub>	51.663

Table S1. XRF analyze of Fe<sub>3</sub>O<sub>4</sub>@SiO<sub>2</sub> (w %).



Figure S1. TEM image of magnetic zeolite NaA.



Figure S2. Separation ability test of Fe<sub>3</sub>O<sub>4</sub>@zeolite NaA.

## References

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