

**Function (S1)**

**function Bootstrap**

```
global MER5212 MER678 %i5212 i678 aa bb cc TT obj1 obj2 CL
```

```
global obj1
```

```
i = 0;
MER5212 = [];
for func=4.3:0.2:4.5
    for OHV=obj1:1:obj1
%    for pp=861.1:1:861.1
        for Cp_spec=2.3:1:2.3
            MER5212(i+1,:) = [func,OHV,Cp_spec];
            i=i+1;
        end
    end
end
%i5212 = height(MER5212);
MER5212;

MER678 = [];
interval = 0.25;
max = 1.00;
min = 0.00;
limit = 0.50;
i = 0;
for hs=limit:interval:max
    for p=min:interval:limit
        for s=min:interval:limit
%for p=0.01:interval:0.01
%    for s=0.20:interval:0.20
%        for hs=0.79:interval:0.79
            if hs+p+s == max
                MER678(i+1,:) = [p,s,hs];
                i=i+1;
            end
        end
    end
end
```

```
        end
    end
end
%i678=height(MER678);
```

```
end
```

```
%The selection of the limits and intervals in the above defined variables
%is a task that requires expertise or educated guess from
%literature review, consultation and laboratory experimentation.
%Moreover, the limits and intervals is a great factor in the speed
%of the execution of the overall code
%and the accuracy of its result.
```

```
%Thus, focus on this matter may be very beneficial.
%The coder must look closely on narrowing limits,
%determining acceptable intervals,
%or prioritizing certain values.
```

```
%The convention of using the terms "coder-defined", "coder limited",
%or the like does not necessarily pertain to any claim by the code.
%Rather, it may pertain to variables defined or limited not by user-input
%through a user-interface, say a message box.
```

**Function (S2)**

**function Recipe**

**global** mer NW0 NCO2 Totalm cat T0 Ts H0 NBp0 Nbs0 NBt0 NBet0 BA r0 V W\_MW P\_atm S TT Toluene\_Cp

**global** E A h cp Ug Uf Ant\_const vaphba Area VoverA Nc R RR Toluene Toluene\_MW Toluene\_MolarCp Boltz

**global** MER5212 MER678 i5212 i678

**%efficiency of reactions**

ef=1; %ef/Ef/eff/Eff = 'effective'/'reactive'

**%Matrix of Isocyanate & Polyol Properties (A & B Ingredients)-----**

**%rows are only updated by MER512 & MER678 in Bootstrap**

| %      | 1     | 2    | 3  | 4  | 5  | 6  | 7  | 8  | 9  | 10 |                            |
|--------|-------|------|----|----|----|----|----|----|----|----|----------------------------|
| %      | A     | B1   | B2 | B3 | B4 | B5 | B6 | B7 | B8 | B9 |                            |
| mer= [ | 44.46 | 50   | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %1 Mass (g)             |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %2 OHV of Bi            |
|        | 369.9 | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %3 MW (g/mol)           |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %4 Moles                |
|        | 2.7   | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %5 Functionality        |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %6 Xp of Bi             |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %7 Xs of Bi             |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %8 Xhs of Bi            |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %9 Molar Cp (J/mol-K)   |
|        | 1.23  | 1.08 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %10 Density (g/cm^3)    |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %11 Eq.Wt. (eq/g)       |
|        | 1.799 | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %12 Specific Cp (J/g-K) |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %13 Volume (cm^3)       |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %14 Moles p in Bi       |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0; %15 Moles s in Bi       |
|        | 0     | 0    | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0]; %16 Moles hs in Bi     |

mer(5,2) = MER5212(i5212,1);

**%Func. of B1 = Polyol Mix**

mer(2,2) = MER5212(i5212,2);

**%OHV of B1 = Polyol Mix**

mer(12,2) = MER5212(i5212,3);

**%Sp.Cp of B1 = Polyol Mix**

```

mer(6,2) = MER678(i678,1);      %Xp  of B1 = Polyol Mix
mer(7,2) = MER678(i678,2);      %Xs  of B1 = Polyol Mix
mer(8,2) = MER678(i678,3);      %Xhs of B1 = Polyol Mix

```

```

for i=2:2    %up to 10
mer(3,i)=56100*mer(5,i)/mer(2,i);    %MW of Polyols
end

```

```

for i=1:2    %up to 10
mer(4,i)=mer(1,i)/mer(3,i)*ef;        %Moles of Reactants
mer(9,i)=mer(12,i)*mer(3,i)/mer(5,i); %Molar Cp of Reactants
mer(11,i)=mer(3,i)/mer(5,i);          %Eq. Wt. of Reactants
mer(13,i)=mer(1,i)/mer(10,i);         %Volume of Reactants
end

```

```

for i=2:2    %up to 10
mer(14,i)=mer(4,i)*mer(5,i)*mer(6,i); %Moles p in Bi
mer(15,i)=mer(4,i)*mer(5,i)*mer(7,i); %Moles s in Bi
mer(16,i)=mer(4,i)*mer(5,i)*mer(8,i); %Moles hs in Bi
end

```

```

%-----

```

```

%Initial amount of c(13), c(14), c(15)    %up to 10
NBp0 = mer(14,2); %= sum(mer(14,2:10)) %Total Bp
NBS0 = mer(15,2); %= sum(mer(15,2:10)) %Total Bs
NBt0 = mer(16,2); %= sum(mer(16,2:10)) %Total Bhs

```

```

%Initial amount of c(11)
NBt0 = 0; %mer(4,10)*mer(5,10)*mer(7,10); %Total Epoxy

```

```

%Initial amount of c(19)    %up to 10 (= sum(mer(4,2:10))/100)
NCO2 = (mer(4,2))/100; %Intrinsic CO2 in system

```

```

%CBA: Water
W_m=0;          %Mass (g)
W_M=W_m*ef;     %Eff. Mass (g)
W_MW=18;        %MW (g/mol)
nW0=(W_m/W_MW); %Moles
NW0=nW0*ef;     %Eff. Moles (= W_M/W_MW)

```

```

W_dens=1;           %Density (g/cm^3)
W_v=W_m/W_dens;    %Volume (cm^3)
W_V=W_v*ef;        %Eff. Volume (cm^3) (= W_M/W_dens)

%Matrix of PBA Properties (9 Entities)-----
%           1           2           3           4           5           6           7           8           9
%           MF           n-Pen       iso-Pen       cyc-Pen       n-Hex       cyc-Hex       nButane       solstice       Forane
BA = [           0           0           0           0           0           0           0           0           0; %1
Mass (g)
      60.052       72.151       72.151       70.135       86.178       84.162       58.124       130.5       130.5; %2
MW (g/mol)
           0           0           0           0           0           0           0           0           0; %3
Moles
           0.98       0.626       0.616       0.751       0.6548       0.7781       0.551       1.27       1.27; %4
Density (g/cm^3)
      129.3897     167.19       164.85           128       197.66           156       98.49       300       300; %5
Heat capacity J/mol-K
           304.95     309.25           301       322.41       341.15       353.85           0           0           0; %6
Boiling Point (K)
           0           0           0           0           0           0           0           0           0]; %7
Volume (cm^3)

for i=1:9
BA(3,i)= BA(1,i)/BA(2,i); %moles PBA
BA(7,i)= BA(1,i)/BA(4,i); %volume PBA
end
%-----

%Matrix of Catalyst Mass & Eff. Catalyst Mass (11 Entities)-----
%           1           2           3           4           5           6           7           8           9           10           11
%           cat5      cat8      UL-1      UL-6      UL-22      UL-29      UL-38      33-LV      BL-17      Stan      SUL-4
cati=[ 0.12,         0,         0,         0,         0,         0,         0,         0,         0,         0,         0]; %cat mass (g)

cat = cati*ef; %eff. cat mass (g)
%-----

%Other Ingredients Mass Input (g)
TCPPi=0;           %F.R.

```

```

L6900i=0;          %Surf.
Toluenei=0;        %Solv.

%Other Ingredients Eff. Mass (g)
TCPP=TCPPi*ef;
L6900=L6900i*ef;
Toluene=Toluenei*ef;

%Toluene Properties
Toluene_dens = 0.86694; %g/cm3
Toluene_MW = 92.14; %g/mol
Toluene_MolarCp = 155.96; %J/mol-K
Toluene_Cp=(Toluene/Toluene_MW)*Toluene_MolarCp; %J/K (eff.)
Toluene_v = Toluenei/Toluene_dens; %cm^3 (volume)
Toluene_V = Toluene/Toluene_dens; %cm^3 (eff. volume)

%Total (Initial) Mass of Mixture %up to 10 (use: sum(mer(1,1:10)))
Totalm=sum(mer(1,1:2))+W_m+sum(BA(1,1:9))+sum(cati(1,1:11))+TCPPi+L6900i+Toluenei; %(g)

%Total (Initial) Volume of Mixture %up to 10 (use: sum(mer(13,1:10)))
%dens of cati(1:11), TCPPi, L6900i approx. 1 g/cm^3
V=sum(mer(13,1:2))+W_v+sum(BA(7,1:9))+sum(cati(1,1:11))+TCPPi+L6900i+Toluene_v; %(cm^3)

%Initial Temp. of Reactions (K)
Tr=TT;          %room temp.
T0=Tr+273.15;   %initial temp. of reactants
Ts=Tr+273.15;   %temp. of surr.

%Initial Height of Mixture (cm)
H0=1.5;

%Surfactant & Cell Structure Consideration*****

Csurf = (L6900/Totalm) + 2.1E-5;          %eff. concentration of surfactant (in total mixture) %in w/w >>
why add 2.1E-5?

```

```

st = (21.046-(1.4378*log(Csurf)))/1000; %surface tension (original comment says unit is in N/m) >> formula
in the Publication is in dyn/cm, 1 dyn/cm = 10^-3 N/m
% >> Publication: Modeling the Impact of Surfactants on
Polyurethane Foam Polymerization (2015)

r0 = 3.4E-3; %initial bubble radius (in cm; if in m = 3.4E-5 m or 0.000034 m)

WW = 0.05; %energy introduced by mixing (in J) >> assumed equal to Kanner's
Study: 10 seconds mixing, 1200 rpm >> review, if time permits
% >> Publication: Urethane Foam Formation–Role of the Silicone
Surfactant (1969)

Nc = WW/(4*pi*st*((r0/100)^2)); %no. of nucleation sites or  $N_c = W / (4 \pi \cdot st \cdot (r_0/100)^2)$ 
% [dimensional analysis:  $J / ((N/m) \cdot (m^2)) = J / (N \cdot m) = N \cdot m / (N \cdot m)$  >>
dimensionally correct, dimensionless overall]

R = 82.05736; %gas constant in atm-cm^3/mol-K (with 5 decimal places)

RR = 8.31446; %gas constant in J/mol-K (with 5 decimal places)

```

Function (S3)

function Database

global E A h cp Ug Uf Ant\_const vapHba

Press=1;

% ptot=1;

%Antoine equation constants, Pc, and Tc of BAs-----

| %          | A        | B       | C        | D        | Pc   | Tc     |                                      |
|------------|----------|---------|----------|----------|------|--------|--------------------------------------|
| Ant_const= | -6.99601 | 0.89328 | -2.52294 | -3.16636 | 60   | 487.2; | %BA 1: Methyl Formate                |
|            | -7.28936 | 1.53679 | -3.08367 | -1.02456 | 33.7 | 469.7; | %BA 2: n-Pentane                     |
|            | -7.12727 | 1.38996 | -2.54302 | -2.45657 | 33.9 | 460.4; | %BA 3: iso-Pentane (2-methyl butane) |
|            | -6.51809 | 0.38442 | -1.11706 | -4.50275 | 45.1 | 511.7; | %BA 4: cyclo-Pentane                 |
|            | -7.46765 | 1.44211 | -3.28222 | -2.50941 | 30.1 | 507.5; | %BA 5: n-Hexane                      |
|            | -6.96009 | 1.31328 | -2.75683 | -2.45491 | 40.7 | 553.5; | %BA 6: cyclo-Hexane                  |
|            | -6.88709 | 1.15157 | -1.99873 | -3.13003 | 38   | 425.2; | %BA 7: n-Butane                      |
|            | -3.70105 | -5.6665 | 3.99824  | -0.02625 | 35   | 450 ;  | %BA 8: Sol                           |
|            | -4.77394 | -2.7714 | -0.78228 | -0.02772 | 35   | 450 ]; | %BA 9: Forane                        |

%-----

%Latent Heat of vaporization of BAs (J/mol) [Using Giacalone Equation]-----

| -       | 1          | 2         | 3         | 4        | 5          | 6          | 7        | 8      |
|---------|------------|-----------|-----------|----------|------------|------------|----------|--------|
| %       |            |           |           |          |            |            |          |        |
| 9       |            |           |           |          |            |            |          |        |
| %       | MF         | n-Pen     | iso-P     | cyc-P    | n-H        | cyc-H      | n-But    | Sol    |
| For     |            |           |           |          |            |            |          |        |
| vapHba= | [27648.6,  | 26363.35, | 25372.42, | 26378.7, | 29543.300, | 30108.864, | 22473.6, | 25317, |
|         | 25225.65]; |           |           |          |            |            |          |        |

%-----

-

%\*\*\*\*\*

%Kinetics Consideration\*\*\*\*\*

%Arrhenious Constant for 13 reaction groups, uncatalyzed + catalyzed (with 11 kinds of catalyst)-----



```
% >> used for calculating the Rate Constant, k, for each Reaction using the Arrhenius Equation: k =
A*(e^(E/(RT)))
% >> in the same units as k: [(mol/V)^(1-a)].s^-1, where a = the overall order of the reaction >>
(cm^3)/mol-s
%Rxn. Group:      1          2          3          4          5          6          7          8          9          10          11          12          13
%              P-A/Ap S-A/Ap HS-A/Ap      A-U      Ap-U      A-W      Ap-W      Ap-Am      A-Amp      Ap-Amp      A-Urp      Ap-Ur      Ap-Urp
A = [              0.38      0.13      0.0125      0.012      0.012      0.25      0.25      2.5      2.5      2.5              0              0              0;
%0 uncatalyzed
      80          100          15              0              0          600          600          6000          6000          6000              0              0              0;
%1  cat5
      500           58          42              0              0          540          540          5400          5400          5400              0              0              0;
%2  cat8
           0         8000         1300              0              0              0              0              0              0              0              0              0;
%3  UL-1
           0          300          65              0              0              0              0              0              0              0              0              0;
%4  UL-6
           0         10000         3000              0              0              0              0              0              0              0              0              0;
%5  UL-22
           0          270          60              0              0              0              0              0              0              0              0              0;
%6  UL-29
           0          600         150              0              0              0              0              0              0              0              0              0;
%7  UL-38
           0          250          70              0              0              0              0              0              0              0              0              0;
%8  33-LV
           0          60          20              0              0          240          240              0              0              0              0              0;
%9  BL-17
           0          500         150              0              0              0              0              0              0              0              0              0;
%10 Stan
           0          1200         550              0              0              0              0              0              0              0              0              0];
%11 SUL-4
%-----

%Activation Energy (Ea in J/mol) for 13 reaction groups, uncatalyzed + catalyzed (with 11 kinds of
catalyst)-----
%Rxn. Group:      1          2          3          4          5          6          7          8          9          10          11          12          13
%              P-A/Ap S-A/Ap HS-A/Ap      A-U      Ap-U      A-W      Ap-W      Ap-Am      A-Amp      Ap-Amp      A-Urp      Ap-Ur      Ap-Urp
E = [              40000         42000         54000              0              0          39000          39000          39000          39000          39000              0              0              0;
%0 uncatalyzed
      60000          3000          300              0              0          10000          10000          10000          10000          10000              0              0              0;
%1  cat5
```

```

37000  40000  42000  0  0  35000 35000 35000  35000 35000  0  0  0;
%2 cat8
0  40000  50000  0  0  0  0  0  0  0  0  0  0;
%3 UL-1
0  40000  82000  0  0  0  0  0  0  0  0  0  0;
%4 UL-6
0  40000  52000  0  0  0  0  0  0  0  0  0  0;
%5 UL-22
0  40000  78000  0  0  0  0  0  0  0  0  0  0;
%6 UL-29
0  40000  65000  0  0  0  0  0  0  0  0  0  0;
%7 UL-38
0  38000  45000  0  0  0  0  0  0  0  0  0  0;
%8 33-LV
0  38000  45000  0  0  35000 35000 32000  0  0  0  0  0;
%9 BL-17
0  55000  60000  0  0  0  0  0  0  0  0  0  0;
%10 Stan
0  32000  38000  0  0  0  0  0  0  0  0  0  0];
%11 SUL-4

```

```

%-----
-----

```

```

%Heats of Reactions (J/mol) (delta H)-----
%      1      2      3      4      5      6      7
%      P-A     S-A     T-A     A-U     A-W     A-Am     A-Ur    %Monomer or on Polymer
h=[72800, 72800, 72800, 0, 60000, 30000, 0];
%-----

```

```

%cp of Reactants (J/mol-K)-----

```

```

%cp of A (J/mol-K)
cp_A = mer(9,1);

```

```

%cp_ave of B (Polyols) (J/mol-K) %up to 10
cp_Bave=mer(9,2);%(mer(4,2)*mer(5,2)*mer(9,2));%+mer(4,3)*mer(5,3)*mer(9,3)+mer(4,4)*mer(5,4)*mer(9,4)+mer(
4,5)*mer(5,5)*mer(9,5))/(mer(4,2)*mer(5,2)+mer(4,3)*mer(5,3)+mer(4,4)*mer(5,4)+mer(4,5)*mer(5,5));

```

```

%cp of Urethane (J/mol-K)
cp_U=cp_A+cp_Bave;

```

```

%cp Vector (J/mol-K)
%      1      2      3      4      5      6      7
%      A      B      U      W      Am     CO2     Ur
cp=[cp_A, cp_Bave, cp_U, 75.42, 128, 39.6, 361];

%-----

%Heat Transfer Considerations*****

%Overall Heat Transfer Coefficient (to surroundings, in W/m^2-K)
Ug=3;      %gel in (plastic) cup
Uf=2.2;    %foam

%Area of Heat Transfer & V2H Conversion Factor

%wood box
%Area=0.0102+0.004*c(24)*c(25)/273;
%VoverA=22400/102;

%plastic cup
%Area=0.006+0.002*c(24)*c(25)/273;
Area=0.0078;
VoverA=22400/35;

%Harith's small box
% Area=0.0072+0.0024*c(17)*c(18)/273;
% VoverA=22400/36;

%*****

end

```

#### Function (S4)

```
function ReacSim (t,c)
```

```
global mer E A h cat Ts cp Ug dTdt V kk Area VoverA Nc Boltz RR W_MW gm vapHba BA Toluene_Cp
```

```
%-----  
%               Part A: Instantaneous Mixture Cp (J/K)  
%-----
```

```
Cp_solv = Toluene_Cp;  
Cp_A     = cp(1)*c(12);  
Cp_B     = cp(2)*(c(13)+c(14)+c(15));
```

```
Cp_BA = 0;  
for i = 1:9  
    for j = 26:34  
        Cp_BA = Cp_BA + (BA(5,i)*c(j));  
    end  
end
```

```
Cp_U      = cp(3)*c(16);  
Cp_W      = cp(4)*c(17);  
Cp_Am     = cp(5)*c(18);  
Cp_CO2    = cp(6)*c(19);  
Cp_Ur     = cp(7)*c(20);
```

```
Cp_all = Cp_solv + Cp_A + Cp_B + Cp_BA + Cp_W + Cp_U + Cp_CO2 + Cp_Am + Cp_Ur;
```

```
Cp = Cp_all*(1+(c(24)-300)/1000); %Cp_others: FR, surf, cat? Cp_solv = 0; Cp_cat?  
%the (1+(c(24)-300)/1000) maybe some assumptions/heuristics or find literature!
```

```
%-----
```

```
%-----  
%               Part B. Instantaneous Moles of Polymer Resin  
%-----
```

```
moles_AnPoll = sum(c(1:2));    %up to 10  
moles_water = c(17);  
moles_pdpd = c(21);  
moles_BA = 0; %moles_others: FR, surf, cat, solv? moles_solv = 0; moles_surf, moles_cat, + moles_CO2?  
moles_resin = moles_AnPoll + moles_water + moles_pdpd + moles_BA;  
molres = moles_resin;
```

```

%-----

%-----
%                               Part C: Kinetics Consideration
%-----

%Rate Constant Calculation - - - - -

for i = 1:13
    kuncat(i) = V * A(1,i)*exp(E(1,i)/RR*(1/298-1/c(24)));
    kcat5 (i) = cat(1)*A(2,i)*exp(E(2,i)/RR*(1/298-1/c(24)));
    K(i)=kuncat(i)+kcat5(i);
end

ktr(1)=1; ktr(2)=1; ktr(3)=1;

kp(1)=K(1)*ktr(1);
kp(2)=K(2)*ktr(2);
kp(3)=K(3)*ktr(3);

% - - - - -

%Mass Transfer (Coeff) of Water Vapor - - - - -

gm=E1_Viscosity(c(1), c(2), c(21),c(24)); %up to 10

%gm treatment
if gm <= kk
    gm=kk;
else if gm <= 0
    gm=kk;
else if gm > 1.5e13
    gm=1.5E13;
end
end
end

%mass transfer coeff of water from bubbles to resin
wdz= 1.5E-24 * (W_MW^1/3);
kwm=(Boltz*c(24)/(6*pi*gm*wdz));

%updating kk in Main.m -> ReacSim.m for t(i+1)
kk=gm;

% - - - - -

```

```

%Rate Constant (column) vector - - - - -
k = [ K(1) ;    K(2) ;    K(3) ; % 1  2  3      %for A  & B1 reactions: B1p, B1s, B1t
      K(1) ;    K(2) ;    K(3) ; % 4  5  6      %for A  & B2 reactions: B2p, B2s, B2t
      K(1) ;    K(2) ;    K(3) ; % 7  8  9      %for A  & B3 reactions: B3p, B3s, B3t
      kp(1) ;   kp(2) ;   kp(3) ; %10 11 12     %for A  & BP reactions: BpP, BsP, BtP
      kp(1) ;   kp(2) ;   kp(3) ; %13 14 15     %for Ap & B1 reactions: B1p, B1s, B1t
      kp(1) ;   kp(2) ;   kp(3) ; %16 17 18     %for Ap & B2 reactions: B2p, B2s, B2t
      kp(1) ;   kp(2) ;   kp(3) ; %19 20 21     %for Ap & B3 reactions: B3p, B3s, B3t
      kp(1) ;   kp(2) ;   kp(3) ; %22 23 24     %for Ap & BP reactions: BpP, BsP, BtP

      K(4) ;    %25      (4) for A-U(rethane) reaction
      K(5) ;    %26      (5) for Ap-U(rethane) reaction
      K(6) ;    %27      (6) for A-W(ater) reaction
      K(7) ;    %28      (7) for Ap-W(ater) reaction
      K(8) ;    %29      (8) for Ap-Am(ine) reaction
      K(9) ;    %30      (9) for A-Amp(Amine on Polymer) reaction
      K(10);    %31      (10)for Ap-Amp(Amine on Polymer) reaction
      K(11);    %32      (11)for A-Urp(Urea on Polymer)
      K(12);    %33      (12)for Ap-Ur(Urea) reaction
      K(13);    %34      (13)for Ap-Urp(Urea on Polymer) reaction

      %35 36 37 38 39 40 41 42 43 44   45      (k(45): mass transf. from bubbles to resin)
      0; 0; 0; 0; 0; 0; 0; 0; 0; 0; 0; 0; kwm];

% - - - - -

%Concentration of Moieties - - - - -

%mer(j,i), c(i) where i = up to 10
AA=mer(5,1)*c(1);          %of iso moieties
Ap=c(12)-mer(5,1)*c(1);    %of iso moieties on polymer
B1p=mer(5,2)*mer(6,2)*c(2); %of primary hydroxyl moieties in Polyol 1
B1s=mer(5,2)*mer(7,2)*c(2); %of secondary hydroxyl moieties in Polyol 1
B1t=mer(5,2)*mer(8,2)*c(2); %of tertiary hydroxyl moieties in Polyol 1
B2p=mer(5,3)*mer(6,3)*c(3); %of primary hydroxyl moieties in Polyol 2
B2s=mer(5,3)*mer(7,3)*c(3); %of secondary hydroxyl moieties in Polyol 2
B2t=mer(5,3)*mer(8,3)*c(3); %of tertiary hydroxyl moieties in Polyol 2
B3p=mer(5,4)*mer(6,4)*c(4); %of primary hydroxyl moieties in Polyol 3
B3s=mer(5,4)*mer(7,4)*c(4); %of secondary hydroxyl moieties in Polyol 3
B3t=mer(5,4)*mer(8,4)*c(4); %of tertiary hydroxyl moieties in Polyol 3
%Bip=mer(5,i)*mer(6,i)*c(i); %of primary hydroxyl moieties in Polyol i
%Bis=mer(5,i)*mer(7,i)*c(i); %of secondary hydroxyl moieties in Polyol i
%Bit=mer(5,i)*mer(8,i)*c(i); %of tertiary hydroxyl moieties in Polyol i
BpP=c(13)-(B1p+B2p+B3p);   %of primary hydroxyl moieties on polymer -(+Bip)
BsP=c(14)-(B1s+B2s+B3s);   %of secondary hydroxyl moieties on polymer -(+Bis)

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BtP=c(15)-(B1t+B2t+B3t);      %of tertiary hydroxyl moieties on polymer  -(+Bit)
Amine=2*c(18);                 %of amine moieties
AmineP=c(22)-Amine;            %of amine moieties on polymer
Urea=2*c(20);                  %of urea moieties
UreaP=c(23)-Urea;              %of urea moieties on polymer

% - - - - -

%Reaction Rate (column) vector (45 x 1) - - - - -

      %PRIMARY      SECONDARY      H-SECONDARY
r=[k(1)*AA*B1p/V^2;  k(2)*AA*B1s/V^2;  k(3)*AA*B1t/V^2; %A and B1 reaction rate
   k(4)*AA*B2p/V^2;  k(5)*AA*B2s/V^2;  k(6)*AA*B2t/V^2; %A and B2 reaction rate
   k(7)*AA*B3p/V^2;  k(8)*AA*B3s/V^2;  k(9)*AA*B3t/V^2; %A and B3 reaction rate
   % 0; 0; 0; %A and Bi reaction rate]
   k(10)*AA*BpP/V^2; k(11)*AA*BsP/V^2; k(12)*AA*BtP/V^2; %A and BP reaction rate
   k(13)*Ap*B1p/V^2; k(14)*Ap*B1s/V^2; k(15)*Ap*B1t/V^2; %Ap and B1 reaction rate
   k(16)*Ap*B2p/V^2; k(17)*Ap*B2s/V^2; k(18)*Ap*B2t/V^2; %Ap and B2 reaction rate
   k(19)*Ap*B3p/V^2; k(20)*Ap*B3s/V^2; k(21)*Ap*B3t/V^2; %Ap and B3 reaction rate
   % 0; 0; 0; %Ap and Bi reaction rate]
   k(22)*Ap*BpP/V^2; k(23)*Ap*BsP/V^2; k(24)*Ap*BtP/V^2; %Ap and BP reaction rate

   k(25)*AA*c(16)/V^2; %A and Urethane reaction rate
   k(26)*Ap*c(16)/V^2; %Ap and Urethane reaction rate
   k(27)*AA*c(17)/V^2; %A and W reaction rate
   k(28)*Ap*c(17)/V^2; %Ap and W reaction rate
   k(29)*Ap*c(18)/V^2; %Ap and Amine reaction rate
   k(30)*AA*AmineP/V^2; %A and AmineP reaction rate
   k(31)*Ap*AmineP/V^2; %Ap and AmineP reaction rate
   k(32)*AA*UreaP/V^2; %A and UreaP reaction rate
   k(33)*Ap*Urea/V^2; %Ap and Urea reaction rate
   k(34)*Ap*UreaP/V^2; %Ap and UreaP reaction rate

   %35 36 37 38 39 40 41 42 43 44      45      %r(45) = water vap from bubbles to resin,
   0; 0; 0; 0; 0; 0; 0; 0; 0; 0; 0; k(45)*c(35)]; % but input in c(35) is -r(45) = water vap from resin to bubbles

% - - - - -

%Degree of Polymerization Calculation - - - - -

DPx1=(mer(4,1)+mer(4,2))/(c(1)+c(2)+c(21)); %up to 10
%DP(1)=DP(1);
%DPx2=(DPx1^(-2/3));
%DPx2=0.36;
%DPx2=15*((c(2)+c(3)+c(4)));
%DP(2)=1/log(DP(1));
pow=2/3;

```

```

%DPx2a=DPx1^pow;
%DPx2=1/(DPx2a);
%Y=2/DPx2;
Y=2*(DPx1^pow);

% - - - - -

%Stoichiometric Coefficient Matrix (23 x 45) - - - - -

      %1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45  >> add more columns for every additional Bi reaction
sc = [ -1 -1 -1  0  0  0  0  0  0  0 -1 -1 -1  0  0  0  0  0  0  0  0  0  0  0  0 -1  0 -1  0  0 -1  0 -1  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%1 for the reactions of Monomer A (Isocyanate) (with B, BP, U, W, Am/P, CO2, Ur/P)
      -1 -1 -1  0  0  0  0  0  0  0  0  0  0 -1 -1 -1  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%2 for the reactions of Monomer B1 (G76-635) (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%3 for the reactions of Monomer B2 (V360) (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%4 for the reactions of Monomer B3 (R315x) (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%5 for the reactions of Monomer B4 (M5020) (with A and with Ap)

      %1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%6 for the reactions of Monomer B5 ----- (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%7 for the reactions of Monomer B6 ----- (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%8 for the reactions of Monomer B7 ----- (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%9 for the reactions of Monomer B8 ----- (with A and with Ap)

      %1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%10 for the reactions of Monomer B9/ESBO (with A and with Ap)
      0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%11 for the reactions of Total Epoxy (with A and with Ap)

      %1  2  3  4  5  6  7  8  9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45
      -1 -1 -1  0  0  0  0  0  0  0 -1 -1 -1 -1 -1 -1  0  0  0  0  0  0 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1  0  0  0
0  0  0  0  0  0  0  0  0  0  ;%12 for the reactions of Total A (Monomer A + A on Polymer) (with B, BP, U, W, Am/P, CO2,
Ur/P)

```



```

-1 0 0 0 0 0 0 0 0 -1 0 0 -1 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%13 for the reactions of Total Bp (from Monomers B1, B2, B3... + Bp on Polymer (with A and
with Ap))
0 -1 0 0 0 0 0 0 0 -1 0 0 -1 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%14 for the reactions of Total Bs (from Monomers B1, B2, B3... + Bs on Polymer (with A and
with Ap))
0 0 -1 0 0 0 0 0 0 -1 0 0 -1 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%15 for the reactions of Total Bt (from Monomers B1, B2, B3... + Bt on Polymer (with A and
with Ap))

%1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45
1 1 1 0 0 0 0 0 0 0 1 1 1 1 1 1 0 0 0 0 0 0 1 1 1 -1 -1 0 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%16 for the reactions of Urethane (from A/Ap + B/BP reactions, with A/Ap reactions to
Allophanate)
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 -1 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 1 ;%17 for the reactions of Water (with A/Ap reactions to Amine + CO2 + mass transfer)
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 -1 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%18 for the reactions of Amine (from A/Ap + W reactions, considering Ap-Am reaction only (to
Urea); excludes A & Ap reactions with AmP) BUT Urea formation accounts A & Ap reactions with AmP: sc(20,30-31) is = 1,
though sc(18,30-31) = 0 >> hmmm
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%19 for the reactions of CO2 (from A/Ap + W reactions)
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 0 -1 0 0 0 0
0 0 0 0 0 0 0 0 ;%20 for the reactions of Urea (sc(20,30-31) is = 1, though sc(18,30-31) = 0 >> hmmm; Ap-Ur
reaction only (to Biuret); excludes A & Ap reactions with UrP)

%1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37
38 39 40 41 42 43 44 45
1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -Y -Y -Y 0 -Y 0 0 0 0 -Y 0 0 -Y 0 0 0
0 0 0 0 0 0 0 0 ;%21 for the reactions of P [= product/polymer/resin]
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 -1 -1 -1 0 0 0 0 0 0
0 0 0 0 0 0 0 0 ;%22 for the reactions of Total Amine (from A/Ap + W, includes A & Ap reactions with AmP)
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 -1 -1 -1 0 0 0
0 0 0 0 0 0 0 0 ];%23 for the reactions of Total Urea (from A/Ap + Am/AmP, includes A & Ap reactions with UrP)

% - - - - -

%Temperature Profile Calculation - - - - -

%-----
%
% BA Consideration
%-----

%dbaldt(i) = rate of mass transfer of BA(i) from bubbles to resin
%drdt = rate of change of bubble radius
%dcondt(i) = rate of condensation of BA(i) in bubbles

```

```

[dbaldt,drdt,dcondt]=E2_BA(c(19), c(21), c(24), c(26), c(27), c(28), c(29), c(30), c(31), c(32), c(33), c(34), molres,
c(36), c(37), c(38));

Tdbaldt = sum(dbaldt); %total mass transfer rate of [BAs] (amt/s) >> from bubbles to resin
Tdcondt = sum(dcondt); %total rate of [BAs] that condense in bubbles (amt/s)

for i=1:9
    Hvap(i) = dbaldt(i)*vapHba(i); %heat released by the system in the mass transfer BA(i) (J/s) %from bubbles to
resin, row vector
    Hcond(i) =-dcondt(i)*vapHba(i); %heat released by the system in the condensation a BA(i) in bubbles (J/s) %from
bubbles to resin, row vector
end

THvap = sum(Hvap); %total heat released by the system in the mass transfer of BAs (J/s) >> review
THcond = sum(Hcond); %total heat released by the system in the condensation of BAs in bubbles (J/s)
>> review

%-----

%-----
%
% dTdt Expression
%-----

dTdt_n_h1 = h(1)*(r(1)+r(10)+r(13)+r(22)); %from (P-A) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h2 = h(2)*(r(2)+r(11)+r(14)+r(23)); %from (S-A) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h3 = h(3)*(r(3)+r(12)+r(15)+r(24)); %from (T-A) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h4 = h(4)*(r(25)+r(26)); %from (A-U) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h5 = h(5)*(r(27)+r(28)); %from (A-W) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h6 = h(6)*(r(29)+r(30)+r(31)); %from (A-Am) reactions (J/s) (Monomer + on Polymer)
dTdt_n_h7 = h(7)*(r(32)+r(33)+r(34)); %from (A-Ur) reactions (J/s) (Monomer + on Polymer)
dTdtn_OAHT = Ug*Area*(Ts-c(24)); %Overall Heat Transfer (J/s) %Ug, Area = const.
%THvap = sum(Hvap(1:9)); %Total heat absorbed during vaporization of BAs
(J/s)
%THcond = sum(Hcond(1:9)); %Total heat released during condensation of BAs (in
bubbles) (J/s)
dTdt_n = dTdt_n_h1 + dTdt_n_h2 + dTdt_n_h3 + dTdt_n_h4 + dTdt_n_h5 + dTdt_n_h6 + dTdt_n_h7 + dTdtn_OAHT + THvap + THcond;
(J/s)
dTdt_d = Cp; % (J/K)
dTdt = dTdt_n/dTdt_d; % (K/s)

%-----

% - - - - -

%-----

```

```

%-----
%                               Part D: Final Output of ReacSim
%-----

dCO2dt=(r(27)+r(28));

dydt=[sc*r;                                %c(1) to c(23) = Amt. of 23 entities (comments on sc)
      dTdt;                                %c(24) = Temperature
      VoverA*(dCO2dt+(-Tdbaldt));          %c(25) = Height
      dbaldt(1);                           %c(26) = Amt.of BA 1 (in liq. resin)
      dbaldt(2);                           %c(27) = Amt.of BA 2 (in liq. resin)
      dbaldt(3);                           %c(28) = Amt.of BA 3 (in liq. resin)
      dbaldt(4);                           %c(29) = Amt.of BA 4 (in liq. resin)
      dbaldt(5);                           %c(30) = Amt.of BA 5 (in liq. resin)
      dbaldt(6);                           %c(31) = Amt.of BA 6 (in liq. resin)
      dbaldt(7);                           %c(32) = Amt.of BA 7 (in liq. resin)
      dbaldt(8);                           %c(33) = Amt.of BA 8 (in liq. resin)
      dbaldt(9);                           %c(34) = Amt.of BA 9 (in liq. resin)
      (-r(45));                            %c(35) = Amt.of Water that vaporized %resin to bubbles
      dCO2dt/Nc;                           %c(36) = Amt.of CO2 that evolved into each bubble
      (-Tdbaldt)/Nc;                       %c(37) = Amt.of Total BA that vaporized into each bubble %resin to bubbles
      drdt;                                %c(38) = Bubble Diameter >> f(c(36), c(37), c(24), c(38), c(21)] in bafn
      Tdcondt];                            %c(39) = Amt.of Total BAs that condensed in bubbles

%-----

%-----
%                               Part E: Safety Nets from Complex Number Calculations
%-----

if t > 20
    if c(21) < 0
        %       if t > 20
            dydt(21)=0; %c(21) = pdp
        %       end
    end
end

%-----

End

```

## Function (S5)

```
function Main

%profile on;
%diary on;
clear;
clc;
close all;
clear title;

global aa bb cc MER5212 MER678 combon zz i5212 i678 NBet0 NBp0 NBs0 NBt0 NCO2 T0 H0 BA NW0 r0

global Matrix_Matches Matrix_MaxPoints Matrix_TempProfile Matrix_ViscoProfile Matrix_HeightProfile trange_min t_int
trange_max mer

global xx y1 y2 y3 y4 y5 y6 matrices_height imax kk CL imax2

%note that B1 = BM or Bmix
%update Ac & Bc of B1, verify for A

B_UserInput
clear title;
lowerCL = (100-CL)/100;
upperCL = (100+CL)/100;

format bank

Bootstrap
rr1 = height(MER5212);
rr2 = height(MER678);
run_size = rr1*rr2;
fprintf('\nMER5212 (Functionality, OH#, Cp) Combinations = %d\n', rr1);
fprintf('\nMER678 (xp, xs, xhs) Combinations = %d\n', rr2);
fprintf('\nExpected runs = %d x %d = %d\n\n', rr1,rr2,run_size);
fprintf('Conditions for Match Finding: %.4f*Input Tmax <= Simulated Tmax <= %.4f*Input Tmax\n\n', lowerCL, upperCL)

combon = 1;
zz = 2;

for i5212 = 1:height(MER5212)
```

```

%combon = 1;

for i678 = 1:1:height(MER678)

    %Solving ReacSim -----
    -----

    D_Database

    kk=1;

    trange_min = 0; t_int = 5; trange_max = cc*60;
    matrices_height = ((trange_max - trange_min)/t_int) + 1;

    6          7          8          9          10          11          %1          2          3          4          5
    B5          B6          B7          B8          B9    T.Epoxy          %A          B1          B2          B3          B4
    [t,c] = ode45( @E_ReacSim, trange_min:t_int:trange_max, [ mer(4,1); mer(4,2); mer(4,3); mer(4,4);
    mer(4,5); mer(4,6); mer(4,7); mer(4,8); mer(4,9); mer(4,10); NBEt0;

    17          18          19          20          21          22          23          %12          13          14          15          16
    W          A          CO2          Ur          T.P          T.Am    T.Ur          %T.A          T.Bp          T.Bs          T.Bt          U
    0;          0;          NCO2;          0;          0;          0;          0; mer(4,1)*mer(5,1); NBp0;          NBS0;          NBT0;          0;

    29          30          31          32          33          34          %24          25          26          27          28
    BA 4          BA 5          BA 6          BA 7          BA 8          BA 9          %Temp          Ht.          BA 1          BA 2          BA 3
    BA(3,3); BA(3,4); BA(3,5); BA(3,6); BA(3,7); BA(3,8); BA(3,9); T0;          H0;          BA(3,1); BA(3,2);

    Cond.BA          %35          36          37          38          39
    %Vap. W          CO2 in Bubb.          T.BA          Bubb.r
    NW0;          6.95E-12;          0;          r0;

    0]);

    %-----
    -----

    %Unnested Viscosity Calculation-----
    -----

```

```

pdpnk=(mer(4,1)+mer(4,2))-(c(:,1)+c(:,2)); %up to 10 %arithmetic ops = element-wise %row vector
pdpdk=c(:,21); %row vector

TS = (mer(4,1)+mer(4,2))-(c(1,1)+c(1,2)); %up to 10 %threshold

%pdpk calculation, where pdpk = column vector
for i=1:matrices_height
    if pdpnk(i)<=TS %threshold
        pdpk(i,1)=2;
    else
        pdpk(i,1)=pdpnk(i)/pdpdk(i);
    end
end

MWpro=318.*pdpk+700; %column vector
Denpro=1.116;

%values of group contributions to Parameters A & B of some groups
      %1      2      3      4      5      6      7      8      9      10      11      12
% carbon    -CH<    >C<    AR    Ortho    Meta    Para    -OH    -O-    -N=C=O    C-O-C    SugarRing
AGC=[-0.21    -0.15    -1.20    0      -0.12    0.05    -0.01    -2.14    -0.38    -4.83    -0.73    0.42];
BGC=[88      35      400     20      100     -34     -5      1218    140     2176    210     -1408];

%Parameter A
      %A
Ac=[(-6.53+AGC(1)*1)+AGC(4)*2+AGC(5)*2+AGC(10)*2+AGC(11)*2,      (-6.53+AGC(1)*6)+AGC(8)*3+AGC(11)*3];%      %up to 10
6.53+AGC(1)*12)+AGC(8)*5+AGC(11)*9+AGC(12)*1,      (-6.53+AGC(1)*13)+AGC(8)*3+AGC(11)*7];
Acpro=-0.9.*pdpk-21.43; %product %column vector

%Parameter B
      %A
Bc=[(263+BGC(1)*1)+BGC(4)*2+BGC(5)*2+BGC(10)*2+BGC(11)*2,      (263+BGC(1)*6)+BGC(8)*3+BGC(11)*3];%      %up to 10
(263+BGC(1)*12)+BGC(8)*5+BGC(11)*9+BGC(12)*1,      (263+BGC(1)*13)+BGC(8)*3+BGC(11)*7];
Bcpro=500.*pdpk+7085; %product %column vector

%Pure Component Vicosity      %up to 10 + 1
      %A
%Product
      %B1
g3=[mer(10,1)*mer(3,1)*exp(Ac(1)+(Bc(1)./c(:,24))),      mer(10,2)*mer(3,2)*exp(Ac(2)+(Bc(2)./c(:,24))),
Denpro.*MWpro(:,1).*exp(Acpro(:,1)+(Bcpro(:,1)./c(:,24)))]]; %arithmetic ops = element-wise
%mer(10,3)*mer(3,3)*exp(Ac(3)+(Bc(3)./c(:,24))),      mer(10,4)*mer(3,4)*exp(Ac(4)+(Bc(4)./c(:,24)))

%Mass Fractions      %up to 10 + 1
x1=((c(:,1)*mer(3,1))./(c(:,1)*mer(3,1)+(c(:,2)*mer(3,2)+(c(:,21).*MWpro))); %arithmetic ops = element-wise
x2=((c(:,2)*mer(3,2))./(c(:,1)*mer(3,1)+(c(:,2)*mer(3,2)+(c(:,21).*MWpro))); %arithmetic ops = element-wise
x5=(c(:,21).*MWpro)./(c(:,1)*mer(3,1)+(c(:,2)*mer(3,2)+(c(:,21).*MWpro))); %arithmetic ops = element-wise

```

```

%Mixture Viscosity %up to 10 + 1
gm3=exp((x1.*log(g3(:,1)))+(x2.*log(g3(:,2)))+(x5.*log(g3(:,3)))));
%+(x3.*log(g3(:,3)))+(x4.*log(g3(:,4)))

%-----

%Variable Assignment-----

xx = t; %x values for the Profiles
y1 = c(:,24)- 273.15; %y1 = y values for the Temperature Profile (in deg. C)
y2 = gm3(:,1); %y2 = y values for the Viscosity Profile
y3 = c(:,25); %y3 = y values for the Height Profile
%y4 = c(:,13); %y4 = y values for the Bp Profile
%y5 = c(:,16); %y5 = y values for the Urethane Profile
%y6 = c(:,21); %y6 = y values for the pdp Profile

%-----

%For Finding Properties at Maximum-----

imax = find(max(y1) == y1); %the ith row of y1 for which y1 is max
imax2 = find(max(y2) == y2); %the ith row of y2 for which y1 is max

%-----

%Validation-----

fprintf('Combo %d [i5212: %d, i678: %d | ', combon, i5212, i678);

%validity criteria for match-finding
if lowerCL*aa <= y1(imax) && y1(imax) <= upperCL*aa && lowerCL*bb <= xx(imax) && xx(imax) <= upperCL*bb

    fprintf('%.2f %.2f %.2f , %.2f %.2f %.2f | %.2f %.2f, %.2f %.2f] MATCH!\n',
mer(5,2),mer(2,2),mer(12,2),mer(6,2),mer(7,2),mer(8,2),aa,y1(imax),bb,xx(imax));

    beep on; beep;

    %populating match matrices if match is found
    F_Simulate_MatchMatrices

```

```

        %simulating plots if match is found
        G_Simulate_Plot1
        %G_Simulate_Plot2

        %updating zz if match is found
        zz = zz + 1;

    else

        fprintf('%.2f %.2f %.2f , %.2f %.2f %.2f | %.2f %.2f, %.2f %.2f]
Mismatch\n',mer(5,2),mer(2,2),mer(12,2),mer(6,2),mer(7,2),mer(8,2),aa,y1(imax),bb,xx(imax));

    end

    %-----
    -----

    combon = combon + 1;

end

%combon = combon + 1;

end

```



## Function (S6)

```
function FoamSim

global combon xx y1 imax2 trange_max Matrix_Matches

%ensure legend is shown
legend show

%legend for curve
zeys = combon;
text = ['Combo ', num2str(zeys)];

%plot T vs. t curve
%figure
%plot_1 = plot(xx,y1,'DisplayName',text);
plot(xx,y1,'DisplayName',text);
title('Temperature Profile of Matching Runs')
xlabel('Time (s)')
ylabel('Temperature (deg. C)')
axis([0, trange_max, 0, 500-273.15])

%hold plot to superimpose gel point on curve
hold on

%legend for gel point
max_text = ['T_m_a_x of C', num2str(zeys)];

%plot for gel point >> inaccurate imax, use imax of max(y2) instead
plot(xx(imax2),y1(imax2),'^r','DisplayName',max_text);

%hold plot to superimpose plot for next combon
hold on

end

prompt = {'Enter desired max. temp. (in deg. C):','Enter corresponing time for max. temp. (in s):', 'Enter time range  
for profile (in min):', 'Enter Confidence (in %):'};
title = 'Inputs';
dims = [1 48];
definput = {'145','470', '10', '5'};
answer = inputdlg(prompt,title,dims,definput);
aa = str2double(answer{1}); %round(str2double(answer{1}),2);
```

```

bb = str2double(answer{2}); %round(str2double(answer{2}),2);
cc = str2double(answer{3}); %round(str2double(answer{3}),2);
CL = str2double(answer{4}); %round(str2double(answer{4}),2);

prompt = {'Enter room temp. (in deg. C):'};
title = 'Inputs';
dims = [1 48];
definput = {'33'};
answer = inputdlg(prompt,title,dims,definput);
TT = str2double(answer{1}); %round(str2double(answer{1}),2);

nmatches = height(Matrix_Matches);
if nmatches == 0
    fprintf('\nNo match has been found throughout whole run.\n\n');
else if nmatches == 1
    fprintf('\nThere is %d match.\n\n',nmatches);
else
    fprintf('\nThere are %d matches.\n\n',nmatches);
end
end

end

```