



# Article New Experiment of Diesel Exhaust Treatment by Atmospheric Pressure Plasma–Wood Fiber Combination

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**Abstract:** Herein, a novel process of diesel exhaust purification by non-thermal plasma combined with wood fiber has been investigated to understand the effect of purification efficiency on the emission. The dielectric barrier discharge (DBD) and wood fiber (WF) improved removal efficiency of nitrogen oxide (NO<sub>x</sub>) owing to the positive activity of oxygen-containing functional groups (such as O–H groups or C–O groups) on the wood surface, which promoted the removal of NO<sub>x</sub> by 10%–13%. The mechanism to remove NO<sub>x</sub> in the presence of wood fibers was also deduced through FTIR spectra. When carbon black was loaded on the wood fiber, there was simultaneous removal of carbon soot and NO<sub>x</sub>. Although complete purification was not achieved, a high purification efficiency was obtained under the conditions of room temperature and no catalysts. These advantages highlight the importance of use of wood and non-thermal plasma (NTP), and this research work opens new avenues in the field of emissions treatment.

Keywords: nitrogen oxide (NO<sub>x</sub>); particulate matter (PM); plasma discharge; wood fiber

# 1. Introduction

Diesel engines are increasingly used worldwide due to their compact size, low operating costs, and higher thermal efficiency than gasoline engines. However, their emissions consist of NO<sub>x</sub>, CO, CO<sub>2</sub>, hydrocarbons (HCs), formaldehyde (PAH), and particulate matter (PM). These components are harmful to human health as well as the environment [1]; hence now, there are stricter regulations upon diesel engine emissions. Various related technologies that have been developed in recent years include diesel oxidation catalysts (DOCs) [2–5], diesel particulate filters (DPFs) [6–8], catalytic-diesel particulate filters (CDPFs) [9–13], and selective catalytic reduction (SCR) [14,15], all of which add certain advantages to previous technologies. However, these new technologies still present some limitations. For instance, some studies on DOC system have revealed that the diesel fuel required to add approximately 25%–50% to certain amounts of precious metals (such as Pt, Pd, and cerium) to treat diesel emission more efficiently [16]. Additionally, sulfur oxidation to  $SO_3$  at high temperatures contributes to the increased deposition of metal sulfate [2]. This process of metal nanoparticles formation can seriously affect human health, as these nanoparticles may enter the human bloodstream and inhalation systems [4,5]. The SCR system has several problems such as leakage of reducing agent ammonia gas, catalyst poisoning and high costs [14,15,17]. DPFs have issues of difficulty in regeneration and high back pressure [18,19]. The CDPF is still troublesome with regards to practical applications in diesel engines, namely, the challenge of activating catalysts at low-temperatures as well as high catalyst costs due to the use of noble metals (Pt-Pd, NiAlO, LaCoO<sub>3</sub>, and CoCeO) [11–13].

Plasma is the fourth state of matter and an ionized type of gas consisting of free electrons and ions [20]. Plasma can be divided into two groups: thermal plasma and non-thermal plasma. In thermal plasma, the electrons, ions, and neutral species have same temperature, which may exceed values of  $10^7$  K [21]. The common application of thermal plasma is to melt hazardous materials. In the meantime, non-thermal plasma, the temperature of ions (Ti) and natural gas (Tg) are a few hundred K (sometimes room temperature), while the electron temperature (Te) approaches to few thousand K. This is also called non-equilibrium plasma. The nonthermal plasma (NTP) has received increasing attention in recent years as a promising technology for diesel emission conversion [22,23] because it can produce excited and radical species that can induce a series of complex chemical reactions, which are difficult to obtain under normal conditions. The highlights of plasma technology include oxidation of PM at low temperature ( $\approx$ 200 °C), rapid response at room temperature, generation of high energized electrons within a very short interval of time to promote the desired chemical reactions to eliminate the exhaust components, no secondary pollution, and moderate capital cost [24,25]. Therefore, at present, several researchers are focused on NTP technology to purify automobile exhaust emissions. Among the most representative studies on removal of nitrogen oxides and particulate matter, there is Song C.L.'s research work [26] on approach to reduce  $NO_x$ , HC, PM and  $NO_x$  by deploying the dielectric barrier discharge (DBD) reactor. Therein, the effects of several parameters, such as peak voltage, frequency, and engine load on the contaminant removals was intensively investigated. The results show that the maxima of PM, HC, and NO<sub>x</sub> removal efficiencies could reach more than 80%, 75%, and 65%, respectively. Mok et al. [27] showed that the combination of dielectric barrier discharge (DBD) and catalysis hybrid processing can be applied to remove NO<sub>x</sub> and PM simultaneously from diesel engine exhaust. For NO<sub>x</sub> removal, the catalysis hybrid process was able to remove about 80% of the initial NO<sub>x</sub> at the energy density of 25 J/L and temperature of  $150^{\circ}$ C. The removal of particulate matter did not primarily depend on the electrode structure, but was a strong function of energy density. With 80% removal efficiency, the energy yield for nitrogen oxide was 40 eV/molecule while that for particulate matter was 83 kJ/mg. Okubo M. [28] studied the simultaneous reduction of PM and  $NO_x$ using a catalysis-combined non-thermal plasma reactor.  $\gamma Al_2O_3$  and  $Ag/\gamma Al_2O_3$  catalysts of 2–4 mm diameter were used as packed pellets with carbon PM loaded among the pellets. The principle of simultaneous removal of PM and NO<sub>x</sub> using catalyst was discussed. N radicals reduced NO<sub>x</sub>, while PM was incinerated by the oxygen radicals induced either by NO<sub>x</sub> or ozone reduction under elevated local temperatures among the pellets. The maximum  $NO_x$  and PM removal energy efficiency were 14.2 g(NO<sub>2</sub>)/kWh for O<sub>2</sub> = 0% and 0.92 g(C) /kWh for O<sub>2</sub> = 2%, respectively. In comparison with the study using  $BaTiO_3$  pellets,  $NO_x$  removal energy efficiency was larger, but the PM removal was lower in the case of catalyst packed-bed reactor. M.Babaie [29] investigated the effects of non-thermal plasma on NO<sub>x</sub> emission and PM structure using real diesel exhaust at different discharge powers (by varying the voltage peak-peak in the range of 7.5–13.5 kV at frequency 50 Hz). The results show that plasma reactor was extremely effective for  $NO_x$  emission and PM removal, especially for soot reduction. A maximum reduction of 73% and 37% at an energy density of 27 J/L was found for NO<sub>x</sub> and SOF mass concentrations, respectively. With regards to PM removal efficiency, energy consumption, and PM size distribution on nucleation mode, running the DBD reactor at 12 kV was demonstrated as the optimum operating condition for the given configuration.

In our previous studies [7,8], wood fiber, a natural porous biomass material containing numerous different diameter pores, was employed, which not only adsorb PM including nano-scale particulates, but also serves a catalyst carrier with low back pressure. Compared with the inorganic materials, such as cordierite and silicon carbide that are widely used as catalyst carriers in the area of exhaust purification, the wood-fiber filter has the advantages of multi-aperture, high porosity, large specific surface, excellent adsorption capacity for PM including ultrafine particles, low cost, and ease to be employed as fuel or fertilizer after use [30]. During our previous research, Danfeng Du et al. [8] reported a new kind of diesel particulate filter using gear-shaped wood fiber filter (WFF), which met filtration efficiency of about 85%, the life span of WFF was more than 90 h. The filter had a low cost and

simple manufacturing process and did not require extremely high quality fuel. Our previous patent [1] also indicated that the emission temperature under the condition of installing the air cooling device, the wood fiber filter showed good performances under temperature 220 °C. This exhaust temperature is typical for light-duty vehicles, or diesel vehicles run in urban and suburban [31]. The above results indicate that our research worked well for the studies that used wood fibers as materials to design diesel particulate matter filters. However, the synergistic role of plasma and wood in the processing of NO<sub>x</sub> is still unclear. As discussed above, NTP is claimed to be an appropriate system for handling low-temperature diesel exhaust gases, which is similar to the real exhaust gas temperature. Several papers have highlighted that the NTP-catalyst combination is commonly used to treat diesel exhaust gases. However, in these systems, the targets need to have low-pressure drop, thermal stability, and high mechanical strength during engine operation. Plasma generated in a wood fiber filter structure is a suitable solution for these requirements. The wood surface consists of numerous narrow holes, which avoids pressure drops and is stable with mechanical vibrations. These are some of the drawbacks of the use catalyst pellets. Herein, the aim is to evaluate the effects of wood fiber combined with NTP on the diesel exhaust treatment. The initial results of this work can open avenues for subsequent research on the manufacture of exhaust gas filter with other optimal parameters (wood material, electrode material, electrode diameter, flow rate gas, frequency, and voltage of a pulse, etc.). The target is to prove the usage of discharge dielectric barrier DBD-wood fiber combination in the field of diesel exhaust treatment.

#### 2. Results

#### 2.1. Effect of Wood Fiber in NOx Removal

The experiment was conducted to assess the effect of wood fibers in the exhaust filter of diesel engines by comparing the results of  $NO_x$  decrease between the case of plasma and plasma-wood fiber combination. The experimental conditions are mentioned in Section 3 (Materials and Method), the wood fiber mass was 10 mg. All these values were determined after the trial experiments. The measurement results are shown in Figure 1.



**Figure 1.** Gas concentrations versus elapsed time at plasma w/o wood fiber; applied voltage 7.5 kV and SED 50 J/L (error bars indicate the standard deviation).

The combination of plasma and wood fiber displayed significantly greater  $NO_x$  reduction efficiency than the plasma alone; i.e., there was a difference of 10%–13% in the  $NO_x$  reduction efficiency between the two methods. This phenomenon may be attributed to some changes in the chemical components of wood fibers under the action of plasma, which resulted in the increase of oxygen functional groups or free radicals on the surface of wood fibers. The main chemical components of wood include cellulose, hemicellulose, and lignin, which all contain numerous oxygen-containing functional groups. Under the action of plasma, the content of oxygen-containing functional group in the wood increased, which promoted the transformation of NO. Hongyan Wang et al. [32] found that after the nitrogen cold plasma treatment, N element was introduced onto the wood surface, and they inferred it as the -NH<sub>2</sub> group. Moreover, the bond energy of NO was lower than that of N<sub>2</sub>, which made it easier for N in NO to be introduced onto the surface. These results indicate that the combination of plasma and wood has a specific nitrogen fixation effect to a certain extent.

After experiments were completed, the infrared spectrum analysis was performed for wood fibers. The absorption peak position of some functional groups are shown in Figure 2. The transmittance of wood after plasma treatment was slightly reduced, which indicates that the content of oxygen-containing functional groups changed under the action of plasma. The absorption peak of the amino group could not be clearly observed in the infrared spectrum. The reason for the phenomenon may be that the absorption peak of amino group has same wavenumber as the absorption peak of O-H, and the absorption intensity of O-H can easily cover the absorption peak of amino group. Based on the assumption of Wang H.Y as discussed above, the enhancement of O-H peak may be partly attributed to the appearance of this amino group. As listed in the Figure 2, C–O (at 1016 cm<sup>-1</sup>) and O-H (at 3276 cm<sup>-1</sup>) significantly changed before and after utilizing plasma, whereas the functional groups at 1249, 1690, and 2846 cm<sup>-1</sup> (C=C, C=O, and C–H, respectively) had no significant change. The characteristic absorption peak of O-H at 3276 cm<sup>-1</sup> belongs to O-H in cellulose and lignin, indicating that plasma may have affected those in the wood. The experiments also show that NO<sub>x</sub> removal increased, suggesting that the combination of wood and plasma was beneficial to promote NO<sub>x</sub> removal.



Figure 2. FTIR spectra of wood fiber w/o plasma treatment.

#### 2.2. Mechanism of NOx Removal in Presence of Wood Fiber

In the pre-reactor step, under strong oxidation conditions of plasma the reactions of oxidation of NO to NO<sub>2</sub> could be summarized as following by reactions (R. 1)–(R. 7):

$$O_2 + e/M \rightarrow e/M + O \bullet + O \bullet$$
 (R. 1)

$$N_2 + e/M \rightarrow N \bullet + N \bullet + e/M$$
 (R. 2)

$$O_2 + O \bullet + e/M \rightarrow O_3 + e/M$$
 (R. 3)

$$NO + N \bullet + e/M \to N_2 + O \bullet + e/M \tag{R.4}$$

$$NO + O \bullet + e/M \rightarrow NO_2 + e/M$$
 (R. 5)

$$NO + O_3 + e/M \rightarrow NO_2 + O_2 + e/M$$
(R. 6)

$$NO_2 + N \bullet + e/M \rightarrow N_2 + O_2 + e/M \tag{R.7}$$

where e/M denotes electron or excited molecules. Then, the active particle, plasma and NO entered the wood fiber reactor. Under the combined action of wood and NTP, the removal of NO was further enhanced. These results indicate that some changes took place on the surface of wood under the action of plasma conditions which changed the activation energy of wood surface and increased the oxygen-containing functional groups on the surface of the wood. As per the hypothetical argument mentioned in the previous section, oxygen-containing functional groups, such as aldehyde (R-HCO) and carboxylic acid/carboxylate (R-COOH) groups, can promote the oxidation of NO to NO<sub>2</sub> as per reactions (R. 8)–(R. 10) [33,34]. Nitrogen may have been introduced as well onto the wood surface in the form of amino, which made the purification of NO<sub>x</sub> more efficient than plasma alone.

$$HCO + O_2 + e/M \rightarrow HO_2 + CO + e/M$$
 (R. 8)

$$COOH + O_2 + e/M \rightarrow HO_2 + CO_2 + e/M$$
(R. 9)

$$HO_2 + NO + e/M \rightarrow OH \bullet + NO_2 + e/M$$
 (R. 10)

#### 2.3. Effect of Wood Fiber Loaded Carbon Soot on NO<sub>x</sub> Removal

The wood fiber loaded carbon black PM mass changed from 10 to 30 mg, while the initial wood mass remained 10 mg. The experimental results of the gas concentrations are shown in Figure 3. As shown in the figure, carbon soot under plasma conditions seems to affect the removal of  $NO_x$ . When plasma treatment with carbon soot was loaded inside the wood fiber, after half an hour of activity the concentration of  $NO_x$  quickly reduced to 125 ppm, while  $NO_x$  concentration in this case without PM decreased to 185 ppm. However, thereafter, the  $NO_x$  concentration did not vary significantly after reaching approximately 115 ppm at 1.5 h of observation. These results prove that presence of carbon soot in the early stage of plasma treatment contributes towards the efficiency of  $NO_x$  removal. Meanwhile, the concentrations of CO and  $CO_2$  increased because of the incineration of PM. The collected carbon PM was effectively incinerated and can be summarized by the following reactions (R. 11)–(R. 17):

$$O_3 + SOF + e/M \rightarrow CO(CO_2) + O_2 + H_2O + e/M$$
 (R. 11)

$$C + O \bullet + e/M \rightarrow CO + e/M$$
 (R. 12)

$$C + 2O \bullet + e/M \rightarrow CO_2 + e/M$$
 (R. 13)

$$C + O_3 + e/M \rightarrow CO + O_2 + e/M$$
(R. 14)

$$2C + 2NO_2 + e/M \rightarrow 2CO_2 + N_2$$
 (R. 15)

$$C + 2NO_2 + e/M \rightarrow CO_2 + 2NO + e/M$$
(R. 16)

$$C + NO_2 + e/M \rightarrow CO + NO + e/M$$
 (R. 17)

Figure 4 showed NO<sub>x</sub> removal with different carbon soot levels loaded inside the wood fiber. The results when carbon load was 15 mg is already presented in Figure 3. As per Figure 4, the NO<sub>x</sub> concentration displayed same trend of decrease and reached equilibrium after about 20–30 min in all cases of different carbon mass loading. These results imply that carbon soot acts as a strong NO<sub>x</sub> reducing agent during the first period time active plasma; however, the removal performance deteriorates with the elapsed time. The decrease in NO<sub>x</sub> amounts were approximately 124.5, 113.5, and 141.5 ppm for the carbon loading of 10, 15 and 30 mg, respectively after 1.5 h of observation. In the current experimental case with wood fiber-loaded carbon soot at 30 mg, the effect of NO<sub>x</sub> removal was

lower than in the other two cases. This may be due to the relatively large amount of carbon filling up the holes on the wood fiber surface that spurred the formation of reactions (R. 16)–(R. 17), which led to a barrier in reducing NO concentration. However, the concentration of CO and CO<sub>2</sub> released was higher than the cases when carbon soot was 10 and 15 mg. In fact, after the end of the observation period, the concentration of  $CO_2$  (30.6 ppm) was approximately double when compared with the case carbon soot load was 10 mg (16.2 ppm). As is well-known, the PM oxidation by active particles in plasma is mainly associated with the oxidation of soluble organic matter (SOF) and carbon (soot). With further increase in PM mass, a large amount of soot (and maybe SOF too) in the reaction may promote further oxidation of PM, increasing the efficiency of purification. As presented in reactions (R. 11)–(R. 17), the carbon C and SOF in PM can be easily oxidized to produce relatively stable chemical CO<sub>2</sub>, at the same time the chemical reactions (R. 4) and (R. 7) are promoted; thereby, the oxidation of PM removal.



**Figure 3.** Effect of NO<sub>x</sub> removal in case of wood fiber loaded CB = 15 mg; applied voltage 7.5 kV and SED 50 J/L (error bars indicate the standard deviation).



**Figure 4.** Effect of NO<sub>x</sub> removal in case: (**a**) wood fiber loaded CB = 10 mg; (**b**) wood fiber loaded CB = 30 mg; applied voltage 7.5 kV and SED 50 J/L (error bars indicate the standard deviation).

Figure 5 shows the amount of PM incineration following the SED at various carbon soot mass levels. In all cases, when SED increased, the PM incineration efficiency also increased. With the increase in SED, the increase in high energy electrons in the plasma reactor led to more frequent collisions with other gas molecules, and the reaction of (R. 1)–(R. 4) intensified, resulting in more active particles and ions. Subsequently, the increase in active particles and ions, such as N, O, and O<sub>3</sub> promoted the

conversion of NO to  $NO_2$  and the reduction carbon by  $NO_2$  was also achieved, resulting in the removal of particulate matter. Nevertheless, NO could not be entirely removed due to the existence of reaction (R. 18).



$$O\bullet + NO_2 + e/M \rightarrow NO + O_2 + e/M$$
(R. 18)

**Figure 5.** PM incineration at wood fiber loaded carbon black 10, 15 and 30 mg (error bars indicate the standard deviation).

# 3. Materials and Methods

The plasma reactor structure is shown in Figure 6; the pre-reactor section is a coaxial reactor with outer material is a quartz glass tube (outer diameter—20 mm, inner diameter—18 mm, length—250 mm). The inner electrode is formed by a metal discharge wire (diameter 2 mm) located at the center of the pre-reactor and main reactor. Inside the main reactor, the length of the wood fiber layer is 100 mm, it was placed inside discharge area. The double-headed perforated Teflon (PTFE) plate provides support while the micro wood fiber was placed inside the discharge zone, as the gas passed through the perforated hole and wood fiber. An aluminum mesh (350 mm length) was wrapped over the outer quartz glass tube, which was the grounded electrode. Notably, no gap should be present between the mesh and dielectric in order to prevent the power loss.



Figure 6. Schematic of experimental setup.

The wood fibers were processed into micro wood fibers to improve the physical and chemical properties of wood fibers. The processing technology is as follows. The wood was treated into cubes of  $60 \times 60 \times 2000$  mm which were cut along the grain by a chipping machine, and the micron-thickness shavings are shown in Figure 7a. Afterwards, the shavings were processed into the micro wood fibers of length 30 to 50 mm, width 1 to 2 mm, and average thickness of about 55 µm via a kneading machine. Finally, micro wood fiber was heat-treated in 160 °C environment using muffle furnace (WD1100, Shanghai, China), and Figure 7b is the result after processing pine wood.



Figure 7. Wood fiber: (a) after being cut along; (b) micro wood fiber following heat treatment.

The purpose of this experiment is closer to the actual diesel exhaust filter, the carbon soot PM sampled from carbon black (CB) was attached to wood fibers via impregnation method (Figure 8). Carbon black was stirred in distilled water solution using digital mixer (JJ-1A, Jiangsu, China) for 1 h. The wood fibers were soaked in carbon black-water solution for 2 h. Thereafter, the wood fibers were placed in a constant temperature drying oven (FT202 2-A, Zhejiang, China) at 80 °C for 1 h. The wood fibers were continued to be baked in the kiln (WD100, Shanghai, China) at 100 °C for one hour. Finally, the amount of carbon PM that was impregnated into the wood fibers was weighed using an electronic scale. The experiment was performed several times to determine the amount of carbon PM loaded into the wood fiber to suit the experimental purposes mentioned in the following section. Depending on the purpose of the experiments, the wood fiber had two functions, including participate in the process convert NO concentration progress and carbon soot absorbed.



Figure 8. Treatment process of wood fibers with carbon black aqueous solution.

The simulated gas had a NO concentration of 300 ppm, O<sub>2</sub> at 2%, and N<sub>2</sub> as remaining gas. The gas flow was controlled at Q = 2 L/min by mass flow controller MFC and was run through mixing chamber. The outlet gas concentrations of NO, CO, and CO<sub>2</sub> were measured using a gas analyzer (NHA–506, GuangDong, China). For each experiment, the data of gas concentration were collected three times,

then use the standard deviation (STDEV) function in Microsoft Excel to perform error bars value calculations. A CTP–2000K intelligent electron impactor (Suman Electronics Co., Nanjing, China) was employed for the DBD reactor which could adjust pulse peak-to-peak voltage 0–30 kV and frequency of 0–20 kHz. The digital oscilloscope was used to determine discharge parameter power discharge P via Lissajous method. The applied voltage was measured using a 60-MHz digital oscilloscope (Rigol DS1062CA, Beijing, China). This system was equipped with a passive high-voltage probe (P6015A, Tektronix, Beaverton, OR, USA) and voltage probe (P6020, Tektronix, Beaverton, OR, USA) to measure high voltage and extend the voltage on micar monitor capacitor C<sub>m</sub> of 0.47  $\mu$ f, respectively. Notably, the monitor capacitor capacitance value C<sub>m</sub> is chosen to be large compared to the capacitance of the actuator without plasma discharge (sometimes called "cold" capacitance). The instantaneous power dissipated by the actuator is:

$$P(W) = V_{a}(t). I_{a}(t) = V_{a}(t). C_{m} \frac{dV_{m}(t)}{dt}$$
(1)

The discharge power over a period T is obtained using Equation (1) and change of variables:

$$P = \frac{1}{T} \int_0^T V_a(t) \cdot C_m \frac{dV_m(t)}{dt} dt = \frac{1}{T} \int V_a \cdot C_m dV_m = \frac{1}{T} \oint_{\substack{\text{one} \\ \text{cycle}}} V_a dQ_m$$
(2)

where  $V_a$  is the voltage across the reactor and  $Q_m$  is the charge on the monitor capacitor. The instantaneous capacitor charge  $Q_m$  and the actuator voltage  $V_a$  plotted against each other generate a Lissajous curve in the  $V_a$ – $Q_m$  curve. Figure 9 show that the area inside closed Lissajous curve divided by the cycle period T is equal to the actuator power.



Figure 9. Waveforms of V-Q Lissajous at applied voltage V = 7.5 kV, 8.0 kV and 8.5 kV.

The specific energy density (SED) value was calculated by dividing the discharge power P (W) obtained from V-Q Lissajous by the gas flow Q (L/min):

$$SED (J/L) = \frac{60P}{Q}$$
(3)

The PM removal efficiency  $\eta$  (%) was obtained from the mass of carbon soot before (C<sub>1</sub> in mg) and after plasma treatment (C<sub>2</sub> in mg).

$$\eta(\%) = \frac{C_1 - C_2}{C_1} \times 100\%$$
(4)

Figure 9 shows an illustration of V-Q Lissajous waveforms for the DBD reactor from the display of a digital oscilloscope at an applied voltage from 7.5 kV (SED 50 J/L) to 8.5 kV (SED 186.5 J/L). These values were maintained constant throughout the experiments. For better understanding the role of wood fiber on NO<sub>x</sub> removal, the wood fibers (blank samples) that did not participate in the experiment and the wood fibers after plasma treatment were scanned at 4 cm<sup>-1</sup> resolution from 4000 cm<sup>-1</sup> to 400 cm<sup>-1</sup> via a Fourier transform infrared spectrometer (FTIR) (Frontier, Perkin Elmer Co., Ltd., Waltham, MA, USA). This method was used to obtain the infrared spectrum of the absorption peaks of different functional groups' positions of the wood fiber.

# 4. Conclusions

The effects of wood fiber combined with non-thermal plasma on decrease in  $NO_x$  and PM were investigated.

1. Compared with NTP, the addition of wood fiber could improve the conversion effect of  $NO_x$  by about 10%–13%, via the change in wood fiber properties. Following NTP treatment of wood fiber, oxygen-containing functional groups (such as O–H groups or C–O groups) on the wood surface provided positive activity and amino groups were introduced on the wood surface, which promoted the removal of  $NO_x$ .

2. The FTIR analysis showed that the chemical components of wood fiber was changed after plasma treatment. Hence, an initial mechanism for the removal of  $NO_x$  in the presence of wood fibers has also been introduced.

3. The carbon soot loaded on wood fiber played the role of a reducing agent, promoting the simultaneous removal of carbon soot and  $NO_X$ . The results show that in the initial stages of turning on the plasma (about 20–30 min), carbon had a stronger effect and led to best  $NO_X$  removal efficiency. Thereafter,  $NO_X$  concentration fell into a saturation state. These results imply that as carbon became older, its role in supporting the removal of  $NO_X$  was no longer evident. When the mass of carbon was increased, the concentration of CO and  $CO_2$  released was higher. Therefore, to treat  $NO_X$  in the presence of PM, PM is required to be continuously regenerated during plasma operation. These results are suitable for future practical applications on real diesel engines because DPM components are constantly refreshed during engine operation. Higher the amount of fresh PM, higher is the  $NO_X$  removal efficiency at this time.

4. The increase in specific energy density had a good effect on the removal of carbon soot in a certain region. With combination of plasma and wood fiber, the complete elimination of  $NO_x$  and PM is not yet achieved. This study provides a new method in the field of emissions treatment and the presented results are a premise to adjust the structure of plasma device with incorporation of wood fibers. The design of the plasma-wood fiber reactor needs to be completed, not only from the electrical engineering standpoint, but also using the multidisciplinary approach in the relevant fields of mechanical, chemical, and physical design parameters with the target to increase residence time for PM decomposition and reduction of  $NO_x$  rate inside the reactor with highest air purification effect.

#### 5. Patents

Guo XR, Liu YX, Du DF, An air cooling device for PM filter made of long wood fiber used in diesel engine exhaust purification, ZL 2014 1 0095027.3, 2014 (In Chinese).

**Author Contributions:** X.G. and K.H.H., data curation; X.G., K.H.H. and D.D., formal analysis; D.D., resources; K.H.H. writing—original draft; X.G. and D.D., writing—review and editing; X.G., funding acquisition and supervision. All authors have read and agreed to the published version of the manuscript.

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