

1 ***Supporting information***

2 **Mechanisms of adsorption of heavy metal cations from**
3 **waters by an amino bio-based resin derived from rosin**

4
5 Wanting Huang¹, Kaisheng Diao¹, Xuecai Tan¹, Fuhou Lei¹, Jianxin Jiang^{1, 2},
6 Bernard A. Goodman^{1,3}, Yahong Ma¹, Shaogang Liu^{1*}

7 ¹ *Guangxi Key Laboratory of Chemistry and Engineering of Forest Products,*
8 *Guangxi Colleges and Universities Key Laboratory of Food Safety and*
9 *Pharmaceutical Analytical Chemistry, School of Chemistry and Chemical*
10 *Engineering, Guangxi University for Nationalities, Nanning 530008, Guangxi,*
11 *China.*

12 ² *Department of Chemistry and Chemical Engineering, MOE Engineering Research*
13 *Center of Forestry Biomass Materials and Bioenergy, Beijing Forestry University,*
14 *Beijing 100083, China.*

15 ³ *College of Physical Science and Engineering, Guangxi University, Nanning*
16 *530004, Guangxi, China.*

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18 Corresponding author: (S G, Liu) Phone: 86-0771-3267019; e-mail:
19 liushaogang2005@163.com

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21 The supporting information includes 31 pages, 9 texts, 9 figures, and 7 tables.

22

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72 complexation with Pb(II) (in Å°).

73 **Supplementary References**

74 **Text S1. Resin Synthesis.**

75 Polymerization was performed in a mixture of monomer (9.5 g methylacrylic
76 acid), crosslinking agent (1.0 g EGMRA, prepared as described in Scheme S1)),
77 initiator (0.2 g AIBN), and toluene (50 mL) at 85 °C for 3 h, whilst being
78 deoxygenated with nitrogen gas. The rosin-based resin of methylacrylic acid (MAR)
79 was separated by filtration, and washed repeatedly with deionized water (60 °C) and
80 ethanol to remove residual materials; the yield was 73%. The synthetic process is
81 shown in Scheme 1.

82 EDAR was then synthesized by adding ethylenediamine dropwise to refluxing
83 MAR (10 g) in thionyl chloride (50 mL) and the mixture refluxed for 4 h; prior to
84 the reaction, MAR was soaked in benzene (50 mL) at room temperature for 12 h,
85 EDAR was filtered, washed with deionized water, then subsequently extracted with
86 ethanol for 4 h. The final product was dried under vacuum at 50 °C for 8 h before
87 characterization and use in absorption studies. The overall synthetic process is
88 shown in Scheme 1.

89

90 **Text S2. Characterization of Resin.**

91 ¹³C nuclear magnetic resonance (NMR) spectra were obtained at room
92 temperature (~22 °C) in 1% deuterated acetic acid using a Bruker AMX 500
93 spectrometer (100.62 MHz for ¹³C NMR). Elemental analyses were performed with
94 an Elemental Analyzer (EA, Elemental Vario MICRO) and Fourier transform
95 infrared (FT-IR) spectra were obtained with a Nicolet 5700 FTIR spectrometer
96 (Thermo Nicolet Co., USA). Sample morphology was examined by field emission
97 scanning electron microscopy (FE-SEM, SUPRA 55, Carl Zeiss AG), and thermal
98 stability was tested using a TGA Q50 simultaneous thermal analyzer (Waters, USA),
99 in which the sample was heated from 35 to 700 °C at a rate of 10 °C/min under a N₂
100 flow rate of 100 mL/min. Zeta potentials of EDAR and MAR were measured in a
101 Zetasizer 2000 Analyzer (Malvern, Mastersizer 2000 Instruments Co., USA). The
102 BET specific surface areas and pore sizes of adsorbents were determined by N₂
103 adsorption–desorption isotherms using an automatic surface analyzer (ASAP2020,
104 Micromeritics, USA). Chemical analyses of EDAR and its HM-loaded composites
105 were conducted by X-ray photoelectron spectroscopy (XPS, ESCALAB 250), in
106 which the XPSPEAK41 software was used to fit the XPS spectra. Electron
107 paramagnetic resonance (EPR) spectra were acquired as either 1st or 2nd derivatives
108 of the microwave absorption at room temperature from selected samples (~25 °C) on
109 a Bruker A300 X-band spectrometer equipped with a Gunn diode microwave source
110 and a high sensitivity resonance cavity. Spectral acquisition parameters were: 5 mW
111 microwave power, 100 kHz modulation frequency, 5 gauss modulation amplitude,
112 center field 3100 gauss, scan range 1500 gauss, and resolution 2048 points.

113 **Text S3. Calculation of adsorption amount and removal efficiency of**

114 **HMs**

115 The amounts of HMs adsorbed by EDAR and their removal efficiency from
116 water were calculated using the following equations:

117
$$q_t = \frac{(C_0 - C_t)V}{m} \quad (S1)$$

118
$$\text{HM removal efficiency \%} = \frac{(C_0 - C_t)}{C_0} \times 100 \quad (S2)$$

119 where C_0 and C_t (mmol/L) are the concentrations of HMs in aqueous solution initially
120 and at time t , respectively; q_t (mmol/g) is the amount of HMs adsorbed at equilibrium,
121 v is the volume of HMs solution (L), m is the mass of adsorbent (g).

122

123 **Text S4. Quantum chemical calculations.**

124 These models and metal complexes were preliminarily optimized by Molecular
125 Mechanics (MM+) prior to more accurate calculation. The geometries of all species
126 were fully optimized by density functional theory (DFT) without restrictions, using
127 the Becke3 parameter exchange function of the Lee-Yang-Parr correlation function
128 (B3LYP) [1] with the 6-31G ** basis set for the C, H, O, N atoms except that the
129 metal ions were in the pseudopotential basis set of Lanl2dz. Single point frequency
130 calculations of these optimized geometries ensured their minimum energy structures.
131 The interaction energy (ΔE) between adsorbate and adsorbent can evaluate the
132 relative electron donating ability of dimers with different functional groups, and its
133 use is feasible for describing the complexation of a given metallic ion. It is defined by
134 Eq. (2).

135
$$\Delta E = E(\text{DM}) - [E(\text{M}) + E(\text{D})] \quad (\text{S3})$$

136 where $E(\text{DM})$ is the total energy of the complex, $E(\text{M})$ is the acceptor energy of free
137 metal ions, and $E(\text{D})$ the donor energy of free adsorbent dimers.

138

139 **Text S5. Adsorption isotherm models**

140 To quantify the adsorption capacity of EDAR, isotherms for adsorption of
141 Pb(II), Cd(II), and Cu(II) on EDAR at 25 °C were investigated by the Langmuir and
142 Freundlich models using the following equations:

143 Langmuir model [2]: $q_e = \frac{q_m K_L C_e}{1 + K_L C_e}$ (S4)

144 Freundlich model [3]: $q_e = K_F C_e^{\frac{1}{n}}$ (S5)

145 where C_e is the equilibrium concentration of the metal ion (mM), q_e is the
146 equilibrium adsorption capacity (mmol/g), q_m (mmol/g) and K_L (L/mmol) are the
147 maximum adsorption capacity and Langmuir constant, respectively. K_F [(mmol/g)
148 (mmol/L)^{1/n}] and n are the Freundlich constants related to adsorption capacity and
149 adsorption intensity parameter, respectively.

150

151 **Text S6. Adsorption isotherm models for multi-component systems**

152 For binary and ternary systems [4],

153
$$\frac{C_{e,1}}{C_{e,2} q_{e,1}} = \frac{C_{e,1}}{q_{m,1} C_{e,2}} + \frac{K_{L,2}}{K_{L,1} q_{e,1}} \quad (S6)$$

154
$$\frac{C_{e,1}}{q_{e,1} (K_{L,2} C_{e,2} + K_{L,3} C_{e,3})} = \frac{C_{e,1}}{(K_{L,2} C_{e,2} + K_{L,3} C_{e,3}) q_{m,1}} + \frac{1}{q_{m,1} K_{L,1}} \quad (S7)$$

155 where plots of $C_{e,1}/C_{e,2}q_{e,1}$ as a function of $C_{e,1}/C_{e,2}$, and $C_{e,1}/q_{e,1}(K_{L,2} C_{e,2} + K_{L,3} C_{e,3})$
 156 as a function of $C_{e,1}/ (K_{L,2} C_{e,2} + K_{L,3} C_{e,3})$ give intercepts of $K_{L,2}/ K_{L,1}q_{e,1}$ and
 157 $1/q_m K_{L,1}$ for the binary and ternary systems, respectively, with slopes of $1/q_{m,1}$ in each
 158 case.

159 **Text S7. Calculation of thermodynamic parameters**

160 Thermodynamic parameters, such as the standard Gibbs energy change (ΔG°),
161 enthalpy change (ΔH°), and entropy change (ΔS°) for the adsorption of HMs on
162 EDAR, which are calculated by eqns. S8–S10, can provide in-depth information
163 about the energetic changes associated with adsorption. The equations can be written
164 as follows:

165
$$\Delta G^\circ = -RT \ln K_d \quad (\text{S8})$$

166
$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ \quad (\text{S9})$$

167
$$\ln K_d = \frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT} \quad (\text{S10})$$

168 where the distribution coefficient ($K_d = C_{ad}/C_e$) is a dimensionless parameter, and
169 represents the ratio of the concentration of solute adsorbed on the EDAR (C_{ad}) to the
170 residual concentration of the solute in solution at equilibrium (C_e). R is the universal
171 gas constant (8.314 J/mol/K), and T is the absolute temperature. Standard enthalpy
172 change (ΔH°) and entropy change (ΔS°) were obtained by plotting of $\ln K_d$ versus
173 $1/T$ (SI Figure S5). At all temperatures, the values of K_d were in the order $\text{Pb(II)} >$
174 $\text{Cd(II)} > \text{Cu(II)}$, which indicates that the affinity of EDAR resin for Pb(II) (a measure
175 of adsorption ability of EDAR for HMs), is higher than for Cd(II) or Cu(II) .

176 **Text S8. Equations for kinetic models**

177 Understanding the reaction kinetics is important for improving the design of
178 adsorption systems. These can be characterized by pseudo-first-order,
179 pseudo-second-order, and intra-particle diffusion kinetic models, which can be written
180 as follows:

181 First-order kinetic equation [5]: $\lg(q_e - q_t) = \lg q_e - \frac{k_1}{2.303} t$ (S11)

182 Second-order kinetic equation [6]: $\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e}$ (S12)

183 Intra-particle diffusion equation [7]: $q_t = k_p t^{0.5} + C$ (S13)

184 where q_e and q_t are the amounts (mmol) of adsorbate adsorbed per gram of adsorbent
185 at equilibrium and at time t (min) respectively; k_1 (1/min) and k_2 (g/mmol/min) are
186 the adsorption rate constants of the pseudo-first-order and pseudo-second-order
187 kinetics reactions, respectively; k_{id} is the intraparticle diffusion rate constant
188 (mmol/g/min^{0.5}); and c_i is a constant associated with the boundary layer thickness.

189

190 **Text S9. Dynamic adsorption performance models.**

191 The Thomas, Yoon-Nelson, and Adams-Bohart models can be used to predict
192 column adsorption performance. The relevant equations are written as follows (Eqs.
193 S14-S16):

194 Thomas model [8]:

$$195 \frac{C_t}{C_0} = \frac{1}{1 + \exp(K_{Th} q_0 m / Q - K_{Th} C_0 t)} \quad (S14)$$

196 Yoon-Nelson model [9]:

$$197 \frac{C_t}{C_0} = \frac{\exp(K_{YN} t - \tau K_{YN})}{1 + \exp(K_{YN} t - \tau K_{YN})} \quad (S15)$$

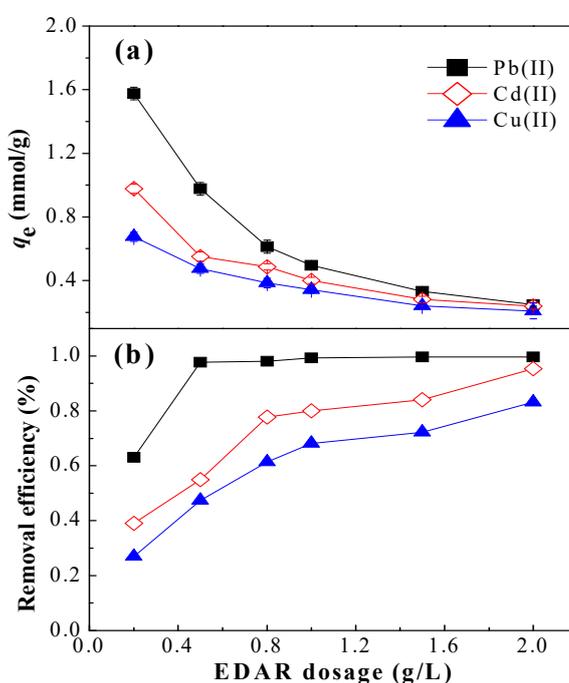
198 Adams-Bohart model [10]:

$$199 \frac{C_t}{C_0} = \exp \left(k_{AB} C_0 t - k_{AB} N_0 \frac{Z}{F} \right) \quad (S16)$$

200 where k_{Th} is the Thomas rate constant (L/min/mmol); q_0 is the uptake of HMs per g
201 of the adsorbent (mmol/g) at equilibrium; m is the amount of adsorbent in the
202 column (g); V_{eff} is the effluent volume (mL); C_0 and C_t are the initial HM
203 concentrations and at time t (mM); v is flow rate (L/min). The value of t is time (min,
204 $t = V_{eff}/V$). k_{AB} is the kinetic constant (ml/mmol/min), F is the linear velocity
205 calculated by dividing the flow rate by the column section area (cm/min), Z is the
206 bed depth of column and N_0 is the saturation concentration (mM). k_{YN} is the rate
207 constant (1/min) and is τ , the time required for 50% adsorbate breakthrough (min).

208 **Fig. S1**

209 The effect of adsorbent dose on the adsorption process was studied by varying
210 the dose of EDAR in the range 0.2–2.0 g/L. As shown in Figure S1, the removal
211 efficiencies for HMs increased with adsorbent dose for low adsorbent concentration,
212 but reached a maximum with Pb for 0.5 g/L, although with both Cd and Cu there
213 was increased adsorption up to 2.0 g/L. Therefore, taking into account the efficiency
214 and economy of operation, 1.0 g/L (solid-to-liquid ratio) was chosen as the optimum
215 adsorbent dosage for all subsequent experiments.

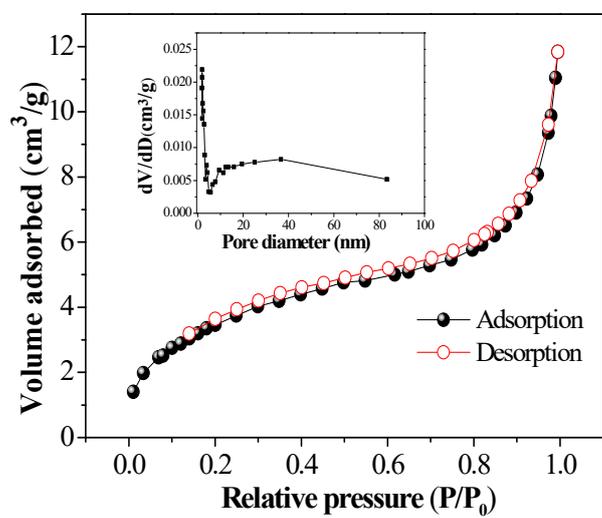


216

217 **Fig. S1.** Effect of adsorbent dose on HMs adsorption on EDAR (a) and removal
218 from solution (b). Experimental conditions: $[HMs]_0 = 0.5$ mM, contact time = 24 h,
219 pH 5.0, 21 ± 1 °C.

220 **Fig. S2**

221



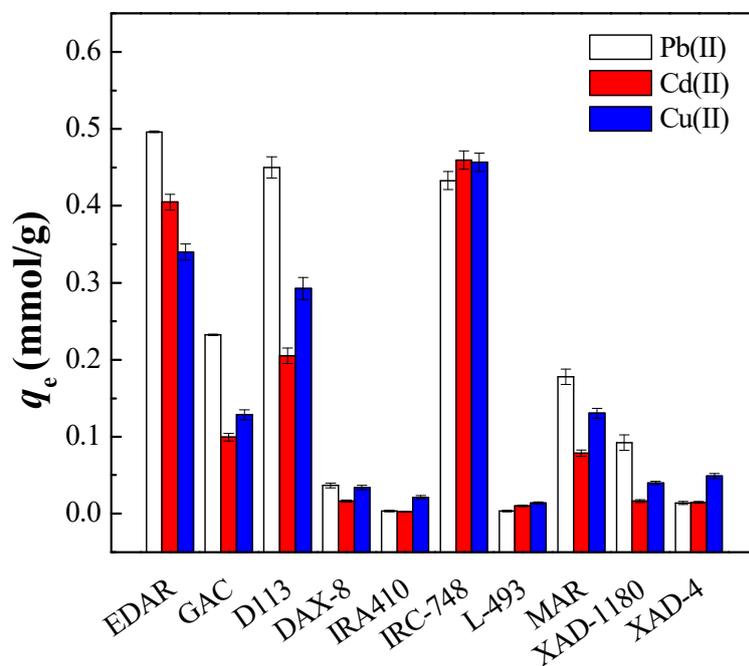
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223 **Fig. S2.** N₂ adsorption-desorption isotherms for EDAR.

224 **Fig. S3**

225

226

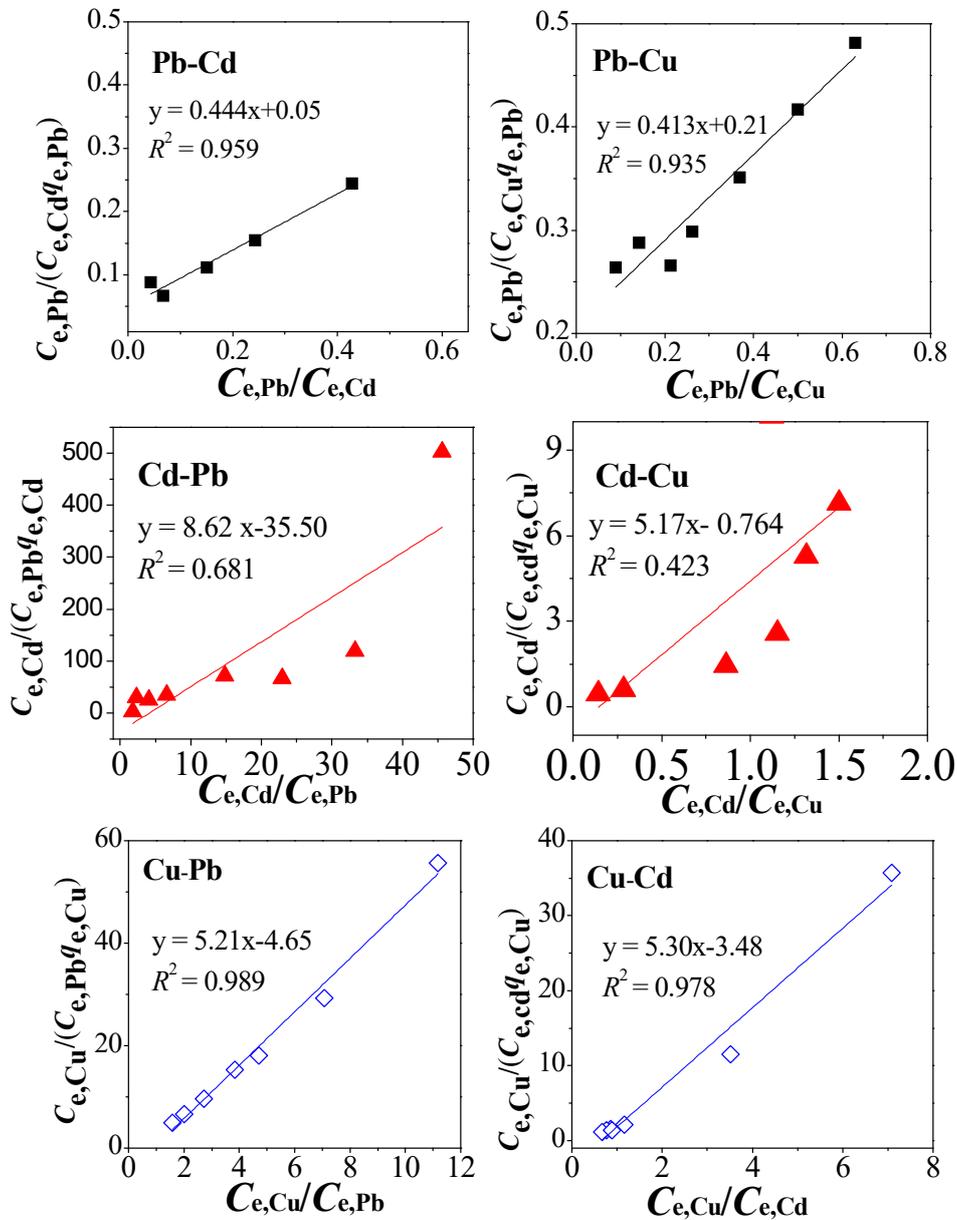


227

228 **Fig. S3.** Adsorption of 0.5 mM Pb(II), Cd(II) and Cu(II) on various adsorbents at pH

229 5.0 and 25 °C using 1.0 g/L adsorbent.

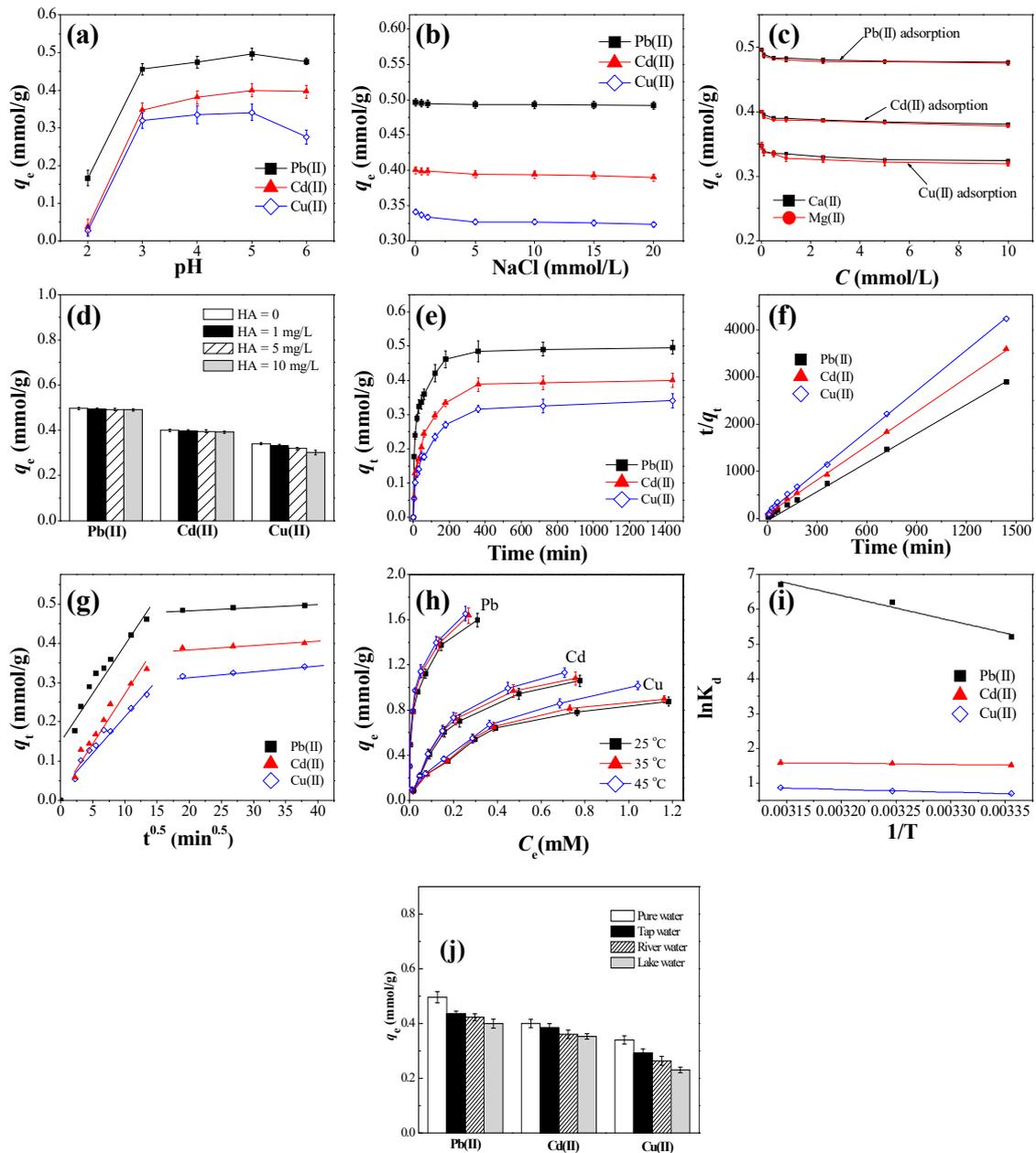
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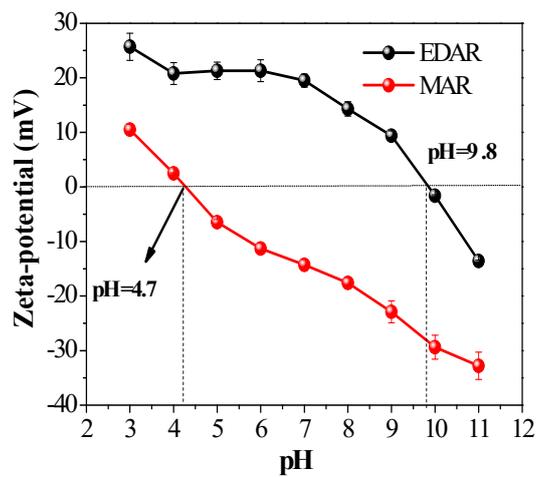
233 **Fig. S4.** Experimental results for the competitive adsorption of Pb, Cd, and Cu in
 234 binary systems presented in the linear form of the Langmuir competitive model.

235



239 **Fig. S5.** Effect of different parameters on the adsorption of HMs by EDAR. (a)
 240 solution pH; (b) ionic strength; (c) Ca(II) and Mg(II); (d) HA. (e) contact time; (f)
 241 pseudo-second-order model; (g) intra-particle diffusion model; (h) temperature; (i)
 242 plots of $\ln k_d$ versus $1/T$ for the adsorption of HMs by EDAR; (j) effects of different
 243 water matrixes. [HMs] = 0.5 mM (except for adsorption isotherm test), [EDAR
 244 dosage] = 1.0 g/L, pH 5.0(except for pH test), 25 °C (except for temperature test).

245 **Fig. S6**

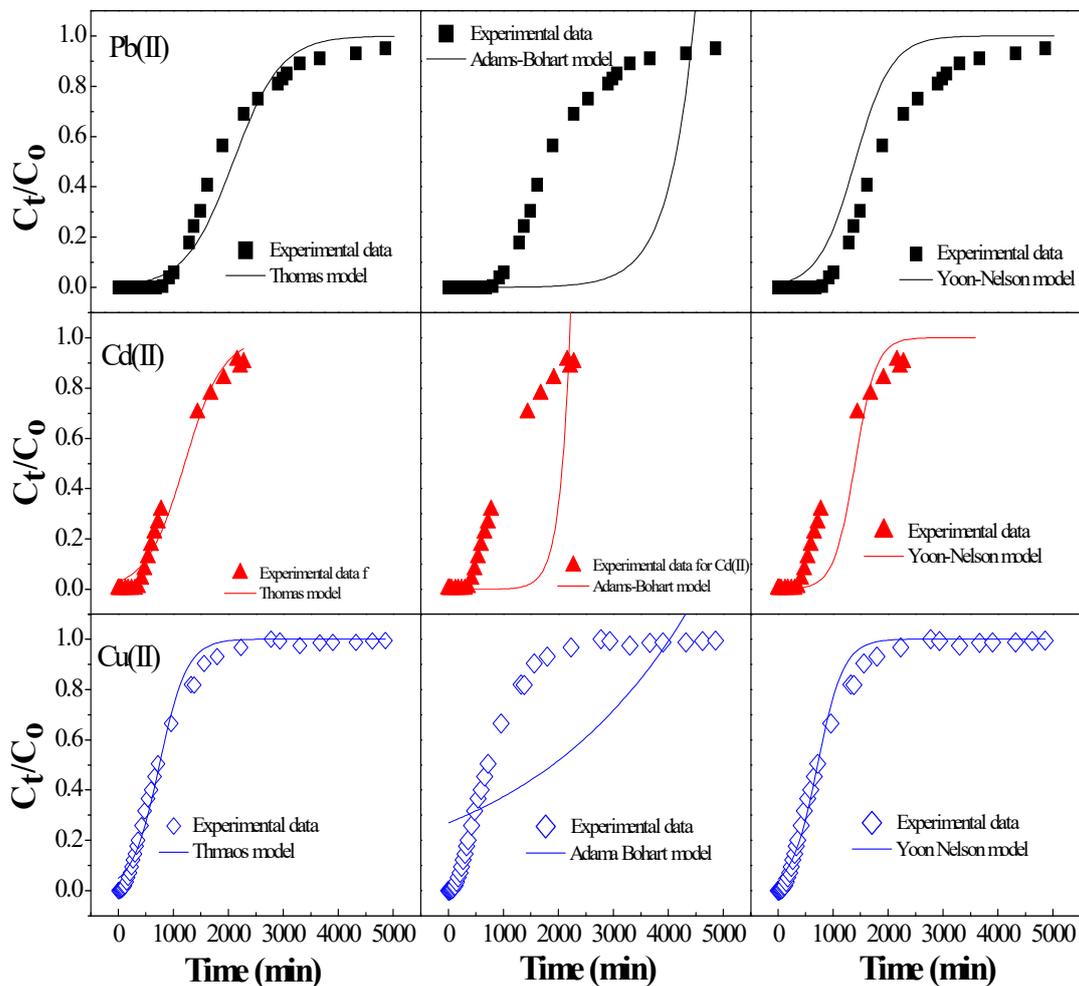


246

247 **Fig. S6** Variation in zeta potential of EDAR and MAR as a function of pH

248

249 **Fig. S7**

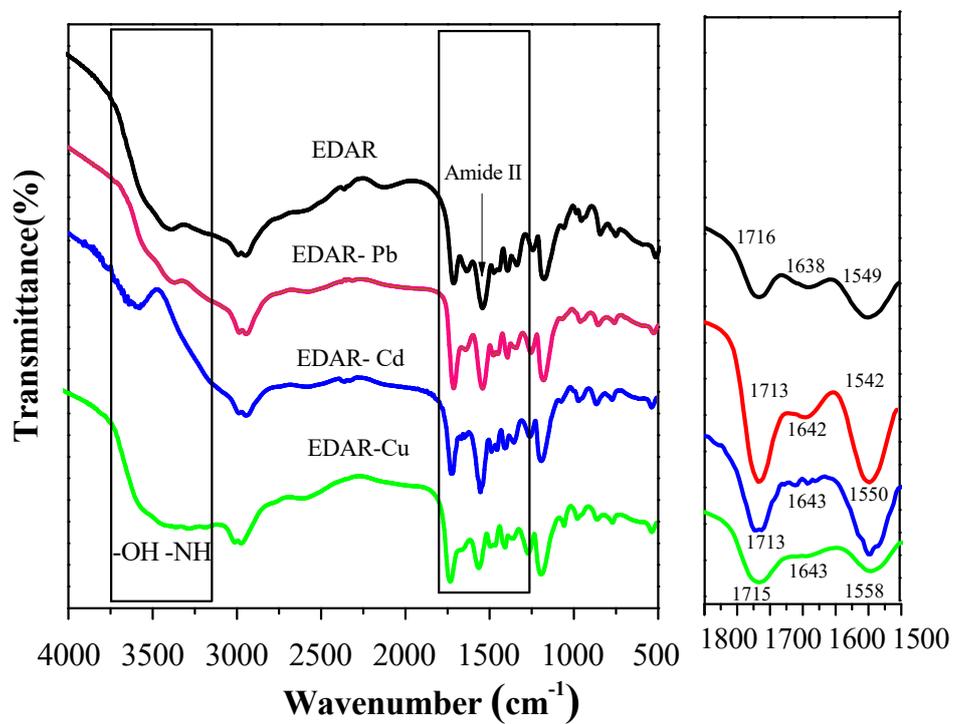


250

251 **Fig. S7.** Comparison of experimental curves for adsorption of Pb(II), Cd(II), and
 252 Cu(II) on EDAR with predicted breakthrough curves obtained from the Thomas,
 253 Adams Bohart, and Yoon–Nelson models.

254

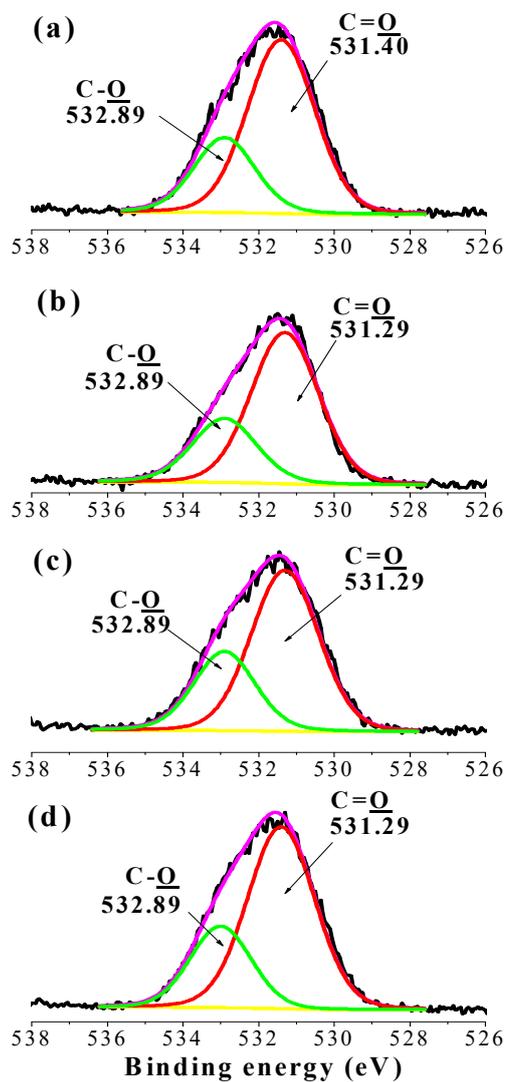
255 **Fig. S8**



256

257 **Fig. S8.** FTIR spectra of EDAR before and after adsorption of Pb(II), Cd(II), and

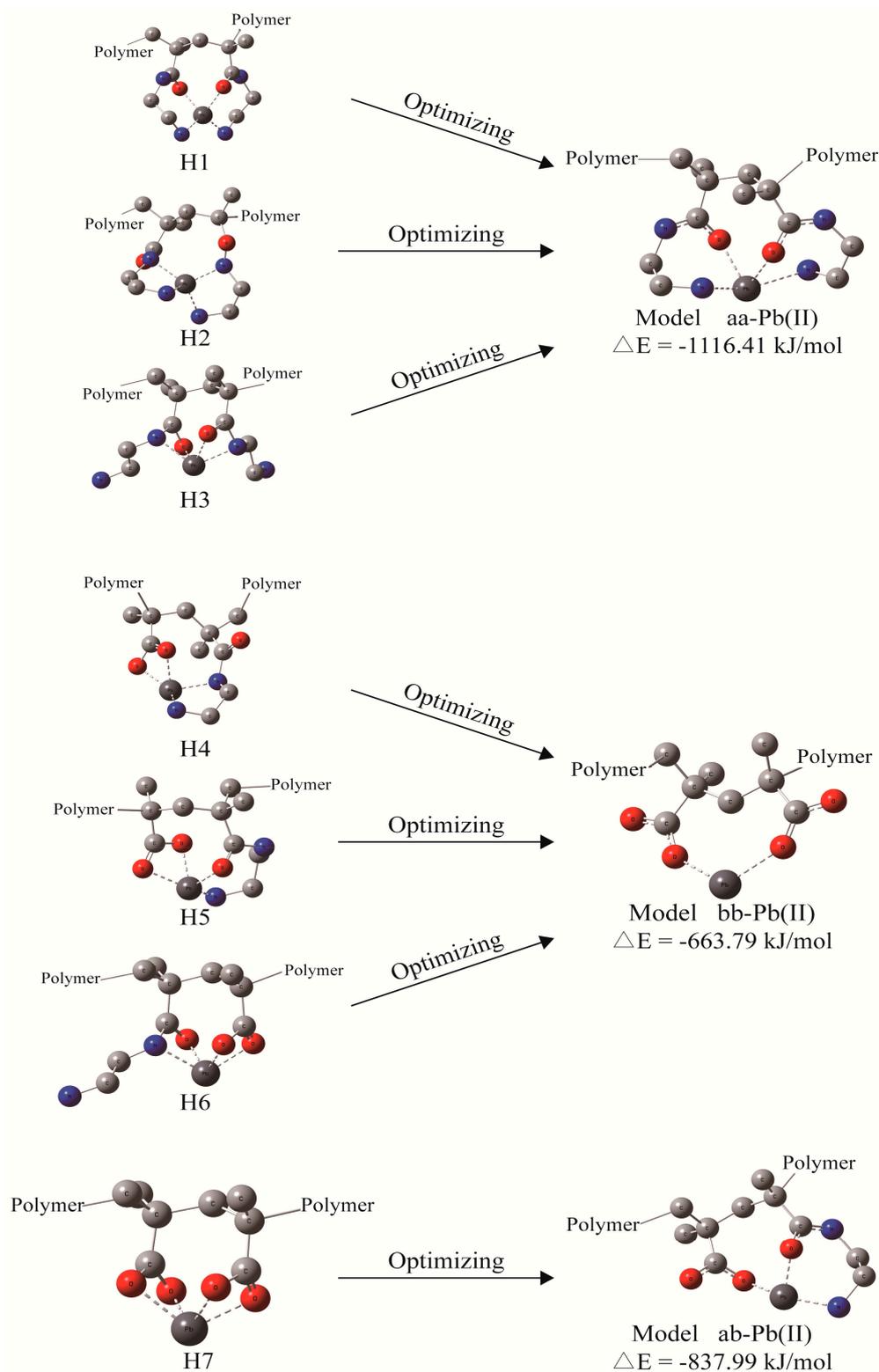
258 Cu(II).



260

261 **Fig. S9.** XPS O1s spectra of EDAR before (a) and after adsorption of Pb(II) (b),

262 Cd(II) (c), and Cu(II) (d).



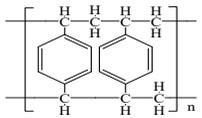
264

265 **Fig. S10.** Initial geometries (H1-H7) used for calculations of Pb(II) coordination to

266 EDAR, and the corresponding optimized coordination geometries (O1-O3).

267 **Table S1**

268 Table S1. Physicochemical properties of commercial adsorbents used in the study.

Adsorbent	Particle size (mm)	BET surface area (m ² /g)	Average pore diameter (nm)	Pore volume (cm ³ /g)	Matrix structure	Functional group
Activated carbon		680		0.78		-COOH, -OH
DAX-8	0.24-0.32	75.8	144.2		Polymethylmethacrylate	-COOCH ₃
D301	0.4-0.7	46.98	274.72	0.18	Polystyrene copolymer	[-N ⁺ (CH ₃) ₂]
D113	0.4-0.7	4.47	37.86	0.52	Polystyrene copolymer	(-COOH)
IRA-410	20-60 mesh				Styrene-divinylbenzene copolymer	-SO ₃ H
IRC 748	0.4-0.7	19.68	16.21	0.079	Styrene-divinylbenzene copolymer	Iminodiacetic acid
L-493		> 1100 ^a	4.6	1.16	Styrene-divinylbenzene copolymer	
XAD-4	0.40-0.70	>750	12.5	0.50	Styrene-divinylbenzene copolymer	

269 As available and reported by supplier.

270 **Table S2**

271 Table S2. Main characteristics of the natural water samples used in this study

Water	DOC (mg/L)	SUVA ₂₅₄ (L/mg·m)	Alkalinity [mM HCO ₃ ⁻]	pH	NH ₄ ⁺ (mg/L)
Tap water	1.5	1.47	1.0	7.2	0.1
River water	3.4	0.69	1.2	8.0	0.4
Lake water	5.2	0.9	2.0	7.8	0.3

272 Note: SUVA₂₅₄ (specific ultraviolet absorbance) was calculated from the ultraviolet absorbance
273 at 254 nm (UV₂₅₄) divided by the DOC.

274 **Table S3**

275 Table S3. Adsorption isotherm model constants for single systems at 25 °C

HMs	Langmuir isotherm			Freundlich isotherm		
	q_{\max} (mmol/g)	K_L (L/mmol)	R^2	n	K_F ((mmol/g) (mmol/L) ^{1/n})	R^2
Single system						
Pb(II)	1.46	87.61	0.893	0.27	2.25	0.970
Cd(II)	1.34	4.78	0.998	0.47	1.26	0.951
Cu(II)	1.12	3.09	0.991	0.86	0.46	0.959

276

Adsorbent	Adsorbate	Adsorbent capacity (mmol/g)	Isotherm model	pH	T (°C)	Ref.
Polyamine-type starch/GMA copolymer	Pb	1.25	Langmuir	5	25	[11]
	Cd	0.83	Langmuir	5	25	
	Cu	2.33	Langmuir	5	25	
Nanocomposite hydrogels based on wheat bran-g-poly(methacrylic acid) and nano-sized clinoptilolite	Pb	0.81	Langmuir	6.8	25	[12]
	Cd	1.57	Langmuir	6.8	25	
	Cu	3.81	Langmuir	6.8	25	
Thiol-functionalized cellulose nanofiber membranes	Pb	0.15	Langmuir	6	27	[13]
	Cd	0.31	Langmuir	6	27	
	Cu	0.31	Langmuir	6	27	
Lignin-based resin	Pb	0.94	Langmuir	6	25	[14]
	Cd	0.44	Langmuir	6	25	
	Cu	0.94	Langmuir	6	25	
Waste mexerica mandarin "Citrus nobilis" peel	Pb	1.92	Langmuir	5	25	[15]
	Cd	2.88	Langmuir	5	25	
	Cu	2.05	Langmuir	5	25	
Chitosan-iso-vanillin	Cd	0.34	Langmuir	5	30	[16]
Torrefied poplar-biomass	Pb	0.14	Sips	4	20	[17]
Carboxymethylated cellulose fiber EDAR	Cu	0.36	Langmuir	6	25	[18]
	Pb	1.8	Freundlich	5	25	This study
	Cd	1.34	Langmuir	5	25	This study
	Cu	1.12	Langmuir	5	25	This study

279 **Table S5**

280

Table S5. Kinetic parameters for the adsorption of Pb(II), Cd(II), and Cu(II) on EDAR

Model	Parameter	Pb(II)	Cd(II)	Cu(II)
Pseudo-first-order model	$q_{e, cal}$ (mmol/g)	0.21	0.20	0.19
	k_1 (1/min)	1.4×10^{-2}	1.3×10^{-2}	9.9×10^{-3}
	R^2	0.873	0.899	0.891
Pseudo-second-order model	$q_{e, cal}$ (mmol/g)	0.50	0.40	0.348
	k_2 (g/mmol/min)	0.12	6.8×10^{-2}	6.7×10^{-2}
	R^2	0.999	0.999	0.999
Intraparticle diffusion model	$k_{id,1}$ (mmol/g/min ^{0.5})	0.030	0.025	0.020
	$c_{i,1}$	0.11	2.5×10^{-2}	2.4×10^{-2}
	R^2	0.863	0.965	0.962
	$k_{id,2}$ (mmol/g/min ^{0.5})	6.1×10^{-3}	6×10^{-3}	1.3×10^{-3}
	$c_{i,2}$	0.474	0.375	0.292
	R^2	0.981	0.999	0.996

281 **Table S6**

282 Table S6. Thermodynamic parameters for the adsorption of HMs on EDAR (0.5 mM

283 HMs)

HM	ΔG° (kJ/mol)			ΔH° (kJ/mol)	ΔS° (kJ/mol/K)	R^2
	25°C	35°C	45°C			
	Pb(II)	-12.89	-15.90	-17.77	59.9	0.245
Cd(II)	-3.75	-3.99	-4.19	12.98	0.081	0.987
Cu(II)	-1.73	-1.97	-2.28	6.59	0.028	0.985

284

285 **Table S7**

286 Table S7. Parameters for the Thomas, Adams–Bohart, and Yoon–Nelson dynamic adsorption models fitted for Pb(II), Cd(II), and Cu(II)

HM	Thomas model			Adams–Bohart model			Yoon–Nelson model	
	q_0	K_T	R^2	N_0	K_{AB}	R^2	K_{YN}	R^2
	(mmol/g)	(L/min/mmol)		(mmol/L)	(ml/mmol/min)		(1/min)	
Pb(II)	1.63	4.2×10^{-3}	0.982	655.3	1.37×10^{-2}	0.852	2.9×10^{-3}	0.853
Cd(II)	1.20	5.7×10^{-3}	0.979	1245.7	8.17×10^{-3}	0.311	2.0×10^{-3}	0.961
Cu(II)	0.75	2.2×10^{-3}	0.987	1921.5	6.46×10^{-3}	0.602	1.6×10^{-3}	0.856

287

288 **Table S8**

289

290 Table S8. Changes in lengths of selected bonds in aa model of EDAR and a result of
291 complexation with Pb(II) (in Å°)

Chemical Bonds	aa model (Å°)	aa-Pb complex model (Å°)	Difference (Å°)
C8=O19	1.26	1.30	0.042
C11-N12	1.46	1.50	0.045
C8-N9	1.37	1.34	-0.033
C14=O28	1.26	1.29	0.030
C17-N18	1.47	1.50	0.029
C14-N15	1.36	1.34	-0.02

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