

Article

Generalized Finsler Geometry and the Anisotropic Tearing of Skin

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Abstract: A continuum mechanical theory with foundations in generalized Finsler geometry describes the complex anisotropic behavior of skin. A fiber bundle approach, encompassing total spaces with assigned linear and nonlinear connections, geometrically characterizes evolving configurations of a deformable body with the microstructure. An internal state vector is introduced on each configuration, describing subscale physics. A generalized Finsler metric depends on the position and the state vector, where the latter dependence allows for both the direction (i.e., as in Finsler geometry) and magnitude. Equilibrium equations are derived using a variational method, extending concepts of finite-strain hyperelasticity coupled to phase-field mechanics to generalized Finsler space. For application to skin tearing, state vector components represent microscopic damage processes (e.g., fiber rearrangements and ruptures) in different directions with respect to intrinsic orientations (e.g., parallel or perpendicular to Langer's lines). Nonlinear potentials, motivated from soft-tissue mechanics and phase-field fracture theories, are assigned with orthotropic material symmetry pertinent to properties of skin. Governing equations are derived for one- and two-dimensional base manifolds. Analytical solutions capture experimental force-stretch data, toughness, and observations on evolving microstructure, in a more geometrically and physically descriptive way than prior phenomenological models.

Keywords: anisotropy; biological tissue; continuum mechanics; Finsler geometry; nonlinear elasticity; orthotropic symmetry; skin; soft condensed matter

MSC: 53Z05 (primary); 53B40; 74B20



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1. Introduction

Finsler geometry and its generalizations suggest the possibility of enriched descriptions of numerous phenomena in mathematical physics, albeit at the likely expense of greater complexity in the analysis and calculations compared to Riemannian geometry. Fundamentals of Finsler geometry, aptly credited to Finsler [1], are discussed in the classic monograph of Rund and the more recent text of Bao et al. [2,3]. See also the overview article by Eringen [4]. A monograph by Bejancu [5] and research cited therein [6–8] cover more generalized Finsler and pseudo-Finsler geometries, as do several more recent works [9,10].

Generalized Finsler geometry is predominantly used herein since strict classical Finsler geometry falls short in describing all phenomena pertinent to the present class of continuum behaviors. The broad physical sciences witness diverse implementations; a thorough recapitulation is outside the bounds of the current work. Available books discuss applications in optics, thermodynamics, and biology [11], as well as modern physical settings, including spinor-type structures [12]. Finsler geometry and its generalizations have also been used for describing anisotropic space-time, general relativity, quantum fields, gravitation, electromagnetism, and diffusion [13–19]. The current work implements a continuum mechanical framework for the physical response of solid bodies.

1.1. Background

Classical continuum mechanics, encompassing nonlinear elasticity and plasticity theories as example constitutive frameworks, is couched in the context of Riemannian–Cartan manifolds [20–22]. Non-vanishing torsion and/or curvature tensors may emerge, depending on linear connections introduced to describe various incompatibilities and possible sources of residual stresses, including dislocation and disclination in crystals [21,23–25], inhomogeneous temperature distributions [26,27], or biological growth [28–30].

In the classical Riemannian context, a continuous material body is treated as a manifold \mathcal{M} , differentiable and having dimension of n . Coordinate chart(s) $\{X^A\}$ ($A = 1, \dots, n$) provide parameterization. A Riemannian metric is introduced on \mathcal{M} ; the components $G_{AB} = G_{AB}(X)$ comprise the metric tensor field. Dependency on components X^A is implied by notational dependence on X [22]. The covariant derivative operator ∇ , enabled by a linear connection on manifold \mathcal{M} , completes the geometric description. Associated linear connection coefficients generally consist of n^3 independent field components $\Gamma_{BC}^A = \Gamma_{BC}^A(X)$. Although different dimensional spaces are admissible, $n = 3$ is standard for the mechanics of solid continua. Bases of coordinates can be holonomic, or less commonly, anholonomic [31,32]. Anholonomic frames, for which continuous curves over \mathcal{M} need not exist, arise when the deformation gradient is deconstructed in a multiplicative sense [33,34].

In the geometries of Finsler and various extensions, a differentiable \mathcal{M} , covered by chart(s) of coordinates $\{X^A\}$ ($A = 1, \dots, n$), is given. Denoted by $(\mathcal{Z}, \mathcal{M}, \Pi, \mathcal{U})$ is a fiber bundle of the total space \mathcal{Z} , having a dimension of $n + m$. The slit tangent bundle $\mathcal{Z} \rightarrow T\mathcal{M} \setminus 0$ [3] is often associated with the total space with $m = n$, but such an association is not mandatory [5,9,10]. Auxiliary coordinates $\{D^K\}$ ($K = 1, \dots, m$) are assigned for every fiber \mathcal{U} . The total space \mathcal{Z} , therefore, has the parameter set $\{X^A, D^K\}$. Laws of transformation are derived for quantities depending on coordinates (X, D) , including holonomic bases. Coefficients of a nonlinear connection lead to bases that are non-holonomic. These bases advantageously change on $T\mathcal{M}$ in a standard manner for changes in base parameters X^A . To execute all possible forms of covariant differentiation—both horizontal and vertical—at least two and at most four sets of coefficients of linear connections are required, as outlined in [5,35].

The metric of the generalized pseudo-Finsler space has a functional dependency $G_{AB} = G_{AB}(X, D)$, which is always symmetric. In the classical geometry of Finsler, this metric is positive definite. In pseudo-Finsler geometry, positive definiteness is not essential [10]. The G_{AB} are obtained as second partial derivatives of $\frac{1}{2}\mathcal{F}^2$ with respect to D^A in strict Finsler geometry [2,3]. The fundamental Finsler function \mathcal{F} is positively homogeneous of degree one with respect to D . As such, G_{AB} is homogeneous of the zeroth degree with respect to D [2,3]. This implies that, for strict Finsler geometry, G_{AB} shall not have dependence solely on the vector magnitude of an object consisting of the coordinates $\{D^A\}$. The existence of \mathcal{F} and homogeneity of G_{AB} are not required in more general kinds of Finsler spaces [5,6,18,36]. The functional dependence on (X, D) for the metric and linear and nonlinear connection coefficients affects the derived quantities, such as curvature and torsion forms, as well as Stokes' theorem [37].

The motivation for the geometry of Finsler in the mechanics of solid continua is as follows. Auxiliary coordinates $\{D^A\}$ are viewed as vectors at every material particle X . The concept generalizes micropolar, Cosserat, and broad kinds of micromorphic models [38–43] couched in Riemannian geometry to the extended Finsler geometry. In the usual theories, in contrast, the metric tensor is of the classical Riemannian form; coordinates $\{X^A\}$ are sufficient for functional dependencies. The director triads in micromorphic theories affect the governing equations and material response. However, these triads do not manifest in the metrics and connections in the same way as the D of the generalized Finsler space. Formulae for transformations of coordinates and the divergence theorem are simpler in the Riemannian versus the Finsler case.

1.2. Prior Work

The first application of Finsler geometry in the context of continuum mechanics of solids appears to be the treatment of ferromagnetic elastic–plastic crystals of Amari [44]. Conservation laws and field theories, with application to ferromagnetism, were further developed by Ikeda [45–48]. Bejancu [5] provided a generalized Finsler treatment of the kinematics of deformable bodies. More contemporary theories include those of Saczuk and Stumpf [49–51], with underpinnings in a monograph [52]. Different physical phenomena (e.g., different physical meanings of $\{D^K\}$ [51]) are encompassed by their models, which include kinematics, balance laws, and thermodynamics, but their focus is most often on the mechanics of elastic–plastic crystals and dislocations [49,50,52]. See also a recent theory presented in [53], which applies generalized Finsler geometry to topological defects, and the comprehensive review in [54] of prior works on generalized Finsler geometry in continuum physics.

A new theory of Finsler-geometric continuum mechanics was developed for nonlinear elastic solids with evolving microstructure, first published in the article [55] with a preliminary version in a technical report [56]. This variational theory was extended to allow for explicit inelastic deformation and applied to study phase transitions and shear localization in crystalline solids [55,57]. The theory has also been broadened for dynamics and shock waves [58,59], and most recently has been used to describe ferromagnetic solids [54], enriching the governing equations of Maugin and Eringen [60,61] with pertinent aspects arising from Finsler geometry [44,48].

Prior to this theory [54,55], pragmatic solutions to boundary value problems using continuum mechanical models incorporating generalized Finsler geometry appeared intractable due to the complexity of governing equations and unwieldy parameterizations (e.g., uncertain constitutive functions and material constants). Most aforementioned work [5,44–49,51,53] presented purely theoretical constructions without attempt to formulate or solve physical boundary value problems. A material response was calculated by Saczuk and Stumpf [50,52], but motion and internal state coordinates were prescribed a priori, without apparent solution of governing conservation laws for macroscopic and microscopic momentum and energy. In contrast, the present theory [55,56] appears to be the first Finsler geometry-based continuum mechanics theory for which analytical and numerical solutions to the governing equations have been found, as evidenced by solutions to numerous problems for (non)linear elastic materials with evolving microstructure (e.g., fractures, twinning, phase transitions, dislocations), as evidenced in those and subsequent works [54–59,62]. However, as discussed in Section 1.3, discrete models with a basis in Finsler geometry have successfully simulated the complex, nonlinear mechanical response of several real materials, including snakeskin [63].

All prior applications of the present theory [54,55] considered stiff crystalline solids or generic materials. The current research newly applies the theory to soft biological tissues, specifically the skin. Furthermore, prior applications in fracture and cavitation [54,55,59,62] were limited to either locally isotropic damage or to local material separation on a single cleavage plane. The current treatment advances the description of anisotropic fractures or ruptures on multiple material surfaces at a single point X . Most cited prior applications invoked only a single non-trivial state vector component in D (an exception being a multi-component D for twinning and fracture [59]) and most often conformal Weyl-type rescaling of G_{AB} with canonically vanishing nonlinear connection (with a few exceptions studied, [57,62]). The current research incorporates an anisotropic generalized Finsler metric for multi-dimensional problems and non-trivial nonlinear connections to show utility by example.

1.3. Purpose and Scope

The scope of this paper covers two primary purposes:

- The demonstration of the utility of the generalized Finsler geometric theory for describing anisotropic elasticity and anisotropic structural rearrangements in soft biological tissue;
- The consolidation and refinement of the theory for the equilibrium (i.e., quasi-static) case.

The first item furnishes the first known application of Finsler geometry-based continuum theory to analyze finite-strain mechanics of soft biological tissue. Prior work of others [63,64] used ideas from Finsler geometry to model nonlinear stress–strain to failure responses of biological solids, but that work used a discrete, rather than continuum, theory with material points represented as vertices linked by bonds; interaction potentials comprised bonding energies within a Hamiltonian. In that promising and successful approach [65–67], a Finsler metric for bond stretch depends on the orientation of local microstructure entities (e.g., molecular chains or collagen fibers) described by the Finsler director vector field D . From a different modeling perspective, the current continuum theory considers, in a novel way, the effects of the microstructure on anisotropy (elastic and damage-induced) in both a geometric and constitutive sense. The second item includes a renewed examination of Rund’s divergence theorem [37] in the context of an osculating Riemannian metric. It is shown that certain choices of metric and connection coefficients, with the possible addition of a source term to the energy conservation law, can recover governing equations for biologic tissue growth [30] in the quasi-static limit (Appendix B).

1.3.1. Soft Tissue and Skin Mechanics

Most soft tissues have inherent directionality due to their collagen fiber-based and/or aligned cellular microstructures [68,69], toward which tools of analysis from Finsler geometry might be anticipated to aptly apply. The mechanics of skin deformation [68,70,71], degradation [72,73], and tearing [73,74] are investigated herein. Like most biological materials, the microstructure of skin is complex. The respective middle and outer layers of skin are the dermis and epidermis, with elastin, collagen fibers, and cells embedded in a ground matrix. The underlying hypodermis (i.e., adipose) can be labeled as an inner layer of the skin. The microstructure dictates nonlinear, anisotropic, viscoelastic, and tearing behaviors [74–76]. Mechanical behavior at small strains is primarily controlled by the elastin and ground substance, whereby collagen fibers are coiled or slack [75]. Under increasing tensile stretch, the collagen fibers straighten and tighten, supporting most of the load, and compliance decreases. Under more severe stretching, fibers slide, delaminate, and rupture, leading to reduced stiffness, strain softening, and material failure [72–74,77].

Experiments indicate that skin elasticity has orthotropic symmetry [68,70,71,75]. Orthotropy arises from preferred arrangements of the collagen fibers, leading to greater stiffness in the directions where more fibers are aligned. In the plane of the dermis, fibers tend to be dispersed about a primary axis along which stiffness is greatest. In vivo, resting skin tension is greatest along this axis, parallel to Langer’s lines [75]. In typical uniaxial and biaxial tests [68,70,71,74], extracted skin is unstretched initially, but the greater stiffness along the primary direction persists, with differences in stiffness also emerging between orthogonal in-plane and out-of-plane directions [70,75]. As might be expected, damage processes are also anisotropic due to fiber degradation that differs with respect to the direction of loading relative to the microstructure [73,74].

Skin, as is most biological tissue, is simultaneously nonlinear elastic, viscoelastic, and poroelastic [68,76,78,79]; the pertinence of mechanisms depends on the time scale of loading. The present application considers only monotonic loading at a constant rate (e.g., no cycling or rate fluctuations). Loading rates are assumed much slower or faster than viscous relaxation times. Thus, the pseudo-elastic approach is justified to study these experiments [68], whereby hyperelastic models are deemed reasonable [71,80–83], albeit

noting that different elastic constants (e.g., static and dynamic moduli) are needed to fit data at vastly different limiting low and high loading rates [84,85]. In future applications to problems with time dependence, internal state variables can be extended, leading to kinetic laws with explicit viscous dissipation [78,86]. The current study is limited to relatively small samples, tested in vitro, under uniaxial or biaxial extension [68,70,74,87]. The material is modeled as unstressed initially and homogeneous with regard to elastic properties. In the future, the current theory can be extended to study residual stress due to growth or heterogeneous material features, as well as heterogeneous elastic properties. Residual stresses can be addressed, in the context of Riemannian manifolds, using a material metric having a non-vanishing Riemann–Christoffel curvature of its Levi–Civita connection [27,30] or an anholonomic multiplicative term in the deformation gradient [29,88]. These ideas may be extended to generalized Finsler space (e.g., invoking the current fiber bundle approach) in future.

An early nonlinear elastic model described orthotropic symmetry using a phenomenological pseudo-strain energy potential [89]. Another early model delineated the contributions of elastin and collagen fibers [79]. More recently, a class of nonlinear elastic models accounting for anisotropy from fiber arrangements using structure tensors has been successful in representing many soft tissues, including arterial walls [80,90], myocardium [82,91], and skin [71]. Polyconvex energy potentials can be incorporated for stability and to facilitate the existence of (unique) solutions to nonlinear elastic problems [81,90]. Fiber dispersion can be incorporated to modulate the degree of anisotropy [71,92]. To date, most damage models accounting for softening and failure have been phenomenological, whether implemented at the macroscopic scale (either isotropic or along preferred fiber directions) or the scale of individual fibers and their distributions [73,77,90,93]. These damage models, with a basis in continuum damage mechanics [94], are thermodynamically consistent in the sense that damage is dissipative, but their particular kinetic laws and (often numerous) parameters are calibrated to experimental data without much physical meaning. In contrast, the phase-field approach has been recently implemented for soft-tissue fracture or rupture, incorporating relatively few parameters with physical origin (e.g., surface energy) and regularization facilitating unique solutions to problems involving material softening [95,96]. The kinetic law or equilibrium equation for damage is derived from fundamental principles [97] and drives material to a local minimum-energy state, in contrast to ad hoc equations simply selected to match data.

1.3.2. Overview of the Current Work

Implementation of the present generalized Finsler theory consists of four key elements: definition of the internal state D , assignment of the metric tensor, assignment of the linear and nonlinear connections, and the prescription of the local free energy potential. For soft tissue mechanics, the state vector represents the fiber rearrangements. Damage anisotropy is monitored via its direction, with different components of D reflecting fiber reorganization and rupture with respect to orientations of the microstructure features [73,74]; the magnitude of each component of D measures the local intensity of damage in a given material direction. The metric tensor with components $G_{AB}(X, D)$ depends on position X as well as the direction and magnitude of D in the generalized Finsler space; novel D dependence encompasses the rescaling of the material manifold as damaged entities open, close, or rearrange in various directions [54,62]. The preferred linear connection is that of Chern and Rund [3], ensuring compatibility with the divergence theorem used to derive the Euler–Lagrange equations [54,55]. The generalized Finslerian D dependence of both the metric and linear connection explicitly affect the governing equations. Roles of nonlinear connections are newly examined; a non-trivial prescription is shown to influence the fracture energy and stress–strain response.

The free energy density consists of a nonlinear elastic contribution and an internal structure contribution. The nonlinear elastic potential enriches the orthotropic theory of Holzapfel, Ogden, Gasser, and others [71,80,82,83,92] with implicit contributions from

the generalized Finsler metric as well as anisotropic degradation from D . The structural contribution is motivated by phase-field mechanics [95,98]. A previous model for arterial dissection [95] accounted for fiber-scale damage anisotropy using a scalar order parameter. The current theory invokes a more physically descriptive, vector-valued order parameter (i.e., normalized D) of the generalized Finsler type. With regard to skin experiments, solutions obtained for the current model are shown to admirably match extension and failure data, including stress–strain behavior and fracture toughness [73,74,99] with parameters having physical or geometric origins. The general theory is, thus, potentially more physically realistic, and considered more descriptive from a geometric perspective, than past models based on phenomenological damage mechanics [90,94,100,101].

This paper is organized as follows. Mathematical preliminaries (e.g., notation and definitions for objects in referential and spatial configurations) are provided in Section 2. The Finsler-geometric theory of continuum mechanics is presented in Section 3, including kinematics of finite deformation and equilibrium equations derived with a variational approach. The next two sections specialize the theory of modeling soft tissue, specifically skin. In Section 4, a one-dimensional (1D) model for the base manifold \mathcal{M} is formulated. Analytical and semi-numerical solutions are obtained for uniaxial extension and compared to experimental data. In Section 5, a two-dimensional (2D) model for \mathcal{M} is formulated, whereby the skin has orthotropic symmetry; solutions are obtained for biaxial extension with anisotropic damage in orthogonal material directions. The conclusions follow in Section 6.

2. Generalized Finsler Space

The content of Section 2 consolidates a more thorough exposition given in a recent review [54], from which notation is adopted. Other extensive texts include those of Rund, Bejancu, and Bao et al. [2,3,5]. A new contribution in the present Section 2 is an interpretation of the divergence theorem [37,54] using an osculating Riemannian metric, whereby for the further simplifying assumption of the vanishing nonlinear connection, a representation akin to that of classical Riemannian geometry is obtained.

2.1. Reference Configuration

The very general fiber bundle approach of Bejancu [5] encompasses geometric fundamentals of the theory. A reference configuration is linked to a specific time t , where the material body is viewed as undeformed, relative to some intrinsic state. The manifold, denoted by \mathcal{M} , is differentiable and of dimension n . One can classically immerse the true continuous body in the Euclidean N space with restriction $N \geq n$.

Remark 1. *This kind of immersion exclusively holds only for the base space \mathcal{M} . As defined below, the fiber bundle's total space \mathcal{Z} does not usually obey, such an embedding [2,102,103]. Likewise, a Finsler space F_n does not fulfill this type of Euclidean embedding.*

A particle of the material occupies each point $X \in \mathcal{M}$. Notation $\{X^A\} (A = 1, 2, \dots, n)$ defines a chart of material coordinates on \mathcal{M} . Coverage of \mathcal{M} by any individual chart need not be complete. Let D denote a vector field assigned to every particle. Accordingly, the $\{D^K\} (K = 1, 2, \dots, m)$ are viewed as additional coordinates for \mathcal{M} . Parameters $\{D^K\}$ are, by construction, of sufficient smoothness: field D is presumed differentiable over \mathcal{M} , of any necessary class, with respect to material coordinates $\{X^A\}$.

Let \mathcal{Z} be the total space having dimension $n + m$. The fiber bundle is $Z = (\mathcal{Z}, \Pi, \mathcal{M}, \mathcal{U})$. The projection is $\Pi : \mathcal{Z} \rightarrow \mathcal{M}$. A fiber at point X is $\mathcal{U} = \mathcal{Z}_X = \Pi^{-1}(X)$. The dimension of a vector space represented by each fiber is n , where a vector bundle is $(\mathcal{Z}, \Pi, \mathcal{M})$. The set $\{X^A, D^K\}$ serves as a (local) chart for (a portion of) \mathcal{Z} . Denote an open neighborhood about $X \in \mathcal{M}$ by $\mathcal{M}' \subset \mathcal{M}$. Let P_1 be the projection operator to the first factor, and write an isomorphism for vector spaces as Φ . Commutation follows for the diagram below [5]:

$$\begin{array}{ccc}
 \Pi^{-1}(\mathcal{M}') & \xrightarrow{\Phi} & \mathcal{M}' \times \mathbb{R}^m \\
 \downarrow \Pi & \swarrow P_1 & \\
 \mathcal{M}' & &
 \end{array}$$

2.1.1. Coordinate Transformations

Transformations for charts of both sets of coordinates $\{X, D\}$ to $\{\tilde{X}, \tilde{D}\}$ on total space \mathcal{Z} are defined as [5,10]

$$\tilde{X}^A = \tilde{X}^A(X), \quad \tilde{D}^J(X, D) = Q_K^J(X)D^K. \tag{1}$$

The transformation matrix Q_K^J fulfills $\tilde{Q}_K^I Q_J^K = \delta_J^I$, presumably differentiable and non-singular. As usual, $\delta_J^I = 1 \forall I = J, \delta_J^I = 0 \forall I \neq J$. Let $T\mathcal{Z}$ denote the tangent bundle, and $\{\frac{\partial}{\partial X^A}, \frac{\partial}{\partial D^K}\}$ denote the holonomic frame field or holonomic basis. Let $T^*\mathcal{Z}$ be the cotangent bundle and $\{dX^A, dD^K\}$ its holonomic coordinate basis. The transformation law for holonomic frames on $T\mathcal{Z}$, for coordinate changes $(X, D) \rightarrow (\tilde{X}, \tilde{D})$ on \mathcal{Z} per base coordinate changes $X \rightarrow \tilde{X}$ on manifold \mathcal{M} , consistent with (1) is [5,10]

$$\frac{\partial}{\partial \tilde{X}^A} = \frac{\partial X^B}{\partial \tilde{X}^A} \frac{\partial}{\partial X^B} + \frac{\partial D^K}{\partial \tilde{X}^A} \frac{\partial}{\partial D^K} = \frac{\partial X^B}{\partial \tilde{X}^A} \frac{\partial}{\partial X^B} + \frac{\partial \tilde{Q}_J^K}{\partial \tilde{X}^A} \tilde{D}^J \frac{\partial}{\partial D^K}, \tag{2}$$

$$\frac{\partial}{\partial \tilde{D}^J} = \frac{\partial X^B}{\partial \tilde{D}^J} \frac{\partial}{\partial X^B} + \frac{\partial D^K}{\partial \tilde{D}^J} \frac{\partial}{\partial D^K} = \tilde{Q}_J^K \frac{\partial}{\partial D^K}. \tag{3}$$

Likewise, on $T^*\mathcal{Z}$,

$$d\tilde{X}^A = \frac{\partial \tilde{X}^A}{\partial X^B} dX^B + \frac{\partial \tilde{X}^A}{\partial D^K} dD^K = \frac{\partial \tilde{X}^A}{\partial X^B} dX^B, \tag{4}$$

$$d\tilde{D}^J = \frac{\partial \tilde{D}^J}{\partial X^B} dX^B + \frac{\partial \tilde{D}^J}{\partial D^K} dD^K = \frac{\partial Q_K^J}{\partial X^B} D^K dX^B + Q_K^J dD^K. \tag{5}$$

Given (1), $\{\frac{\partial}{\partial X^A}\}$ and $\{dD^K\}$ map differently than standard vectorial objects on \mathcal{Z} . Define [5,9]

$$\frac{\delta}{\delta X^A} = \frac{\partial}{\partial X^A} - N_A^K \frac{\partial}{\partial D^K}, \quad \delta D^K = dD^K + N_B^K dX^B. \tag{6}$$

Non-holonomic basis vectors $\{\frac{\delta}{\delta X^A}\}$ and $\{\delta D^K\}$ obey [10]

$$\frac{\delta}{\delta \tilde{X}^A} = \frac{\partial X^B}{\partial \tilde{X}^A} \frac{\delta}{\delta X^B}, \quad \delta \tilde{D}^J = Q_K^J \delta D^K; \quad \langle \frac{\delta}{\delta X^B}, dX^A \rangle = \delta_B^A, \quad \langle \frac{\partial}{\partial D^K}, \delta D^J \rangle = \delta_K^J. \tag{7}$$

The set $\{\frac{\delta}{\delta X^A}, \frac{\partial}{\partial D^K}\}$ is implemented over $T\mathcal{Z}$ for a local basis; likewise, on $T^*\mathcal{Z}$, a dual basis is taken to be $\{dX^A, \delta D^K\}$ [3,9]. The $N_B^K(X, D)$ are the coefficients of the nonlinear connection, serving as differentiable functions of their arguments. For (7) to hold under coordinate changes $X \rightarrow \tilde{X}$ [3,5],

$$\tilde{N}_A^J = \left(Q_K^J N_B^K - \frac{\partial Q_K^J}{\partial X^B} D^K \right) \frac{\partial X^B}{\partial \tilde{X}^A}, \tag{8}$$

meaning that nonlinear connections do not follow the transformation laws of linear connections. Nonlinear coefficients do not instill covariant differentiation identical to linear coefficients.

Remark 2. The orthogonal decomposition afforded by $T\mathcal{Z}$ with the corresponding nonlinear connection is $T\mathcal{Z} = V\mathcal{Z} \oplus H\mathcal{Z}$. The vertical vector bundle is $V\mathcal{Z}$ with $\{\frac{\partial}{\partial D^A}\}$ being its local frame field, and the horizontal distribution is $H\mathcal{Z}$ with the local field of frames $\{\frac{\delta}{\delta X^A}\}$ [5].

Respective fiber dimensions of $V\mathcal{Z}$ and $H\mathcal{Z}$ are m and n , and are possibly different. For the remainder of this work, let $m = n$, so that the horizontal and vertical spaces have identical dimensionality. Regarding notation, coordinate indices such as J, K, \dots are interchangeable with A, B, \dots for Einstein's sums, now spanning 1 to n . Furthermore, for (1), consider

$$Q_B^A = \frac{\partial \tilde{D}^A}{\partial D^B} = \frac{\partial \tilde{X}^A}{\partial X^B}. \tag{9}$$

Relation (9) is obtained via soldering forms by Minguzzi [10]. Coordinate differentiation operations are expressed as follows, with f being a differentiable function of arguments (X, D) :

$$\partial_A f(X, D) = \frac{\partial f(X, D)}{\partial X^A}, \quad \bar{\partial}_A f(X, D) = \frac{\partial f(X, D)}{\partial D^A}; \quad \delta_A(\cdot) = \frac{\delta(\cdot)}{\delta X^A} = \partial_A(\cdot) - N_A^B \bar{\partial}_B(\cdot). \tag{10}$$

Special cases $f \rightarrow X$ and $f \rightarrow D$ are written [54,55]

$$\partial_B X^A = \frac{\partial X^A}{\partial X^B} = \delta_B^A, \quad \bar{\partial}_B X^A = 0; \quad \partial_B D^A = \frac{\partial D^A}{\partial X^B}, \quad \bar{\partial}_B D^A = \delta_B^A. \tag{11}$$

2.1.2. Length, Area, and Volume

The Sasaki metric tensor [3,35,104] on \mathcal{Z} supplies vectorial scalar products :

$$\mathcal{G}(X, D) = \mathbf{G}(X, D) + \check{\mathbf{G}}(X, D) = G_{AB}(X, D) dX^A \otimes dX^B + \check{G}_{AB}(X, D) \delta D^A \otimes \delta D^B; \tag{12}$$

$$\mathcal{G}_{AB} = G_{AB} = \mathbf{G}\left(\frac{\delta}{\delta X^A}, \frac{\delta}{\delta X^B}\right) = \check{\mathbf{G}}_{AB} = \check{\mathbf{G}}\left(\frac{\partial}{\partial D^A}, \frac{\partial}{\partial D^B}\right) = \check{G}_{BA} = G_{BA} = \mathcal{G}_{BA}. \tag{13}$$

Regarding notation, \mathbf{G} and $\check{\mathbf{G}}$ have equivalent components, hereafter written as G_{AB} , but subspaces spanned by these two tensors are orthogonal. Components in covariant form G_{AB} and their inverse in contravariant form G^{AB} enable respective lowering and raising of indices; G is the determinant of the $n \times n$ non-singular matrices of components of \mathbf{G} or $\check{\mathbf{G}}$:

$$G^{AB} G_{BC} = \delta_C^A; \quad G(X, D) = \det[G_{AB}(X, D)] = \det[\check{G}_{AB}(X, D)]. \tag{14}$$

Remark 3. Let $\mathbf{V} = V^A \frac{\delta}{\delta X^A} \in H\mathcal{Z}$ denote a generic vector field on \mathcal{Z} . Then the magnitude of $\mathbf{V}(X, D)$ is $|\mathbf{V}| = \langle \mathbf{V}, \mathcal{G}\mathbf{V} \rangle^{1/2} = \langle \mathbf{V}, \mathbf{G}\mathbf{V} \rangle^{1/2} = |\mathbf{V} \cdot \mathbf{V}|^{1/2} = |V^A G_{AB} V^B|^{1/2} = |V^A V_A|^{1/2} \geq 0$, where V^A and G_{AB} are evaluated at (X, D) .

When interpreted as a block diagonal $2n \times 2n$ matrix, the determinant of \mathcal{G} is [49,50,52]

$$\mathcal{G}(X, D) = \det[G_{AB}(X, D)] \det[\check{G}_{AB}(X, D)] = |\det[G_{AB}(X, D)]|^2 = |G(X, D)|^2. \tag{15}$$

Let $d\mathbf{X}$ be a local line element for the base manifold \mathcal{M} , referred to as the basis of $\{\frac{\delta}{\delta X^A}\}$, and let $d\mathbf{D}$ be a corresponding line element for the fiber \mathcal{U} , referred to as $\{\frac{\partial}{\partial D^A}\}$. Their lengths are, squared,

$$|d\mathbf{X}|^2 = \langle d\mathbf{X}, \mathcal{G}d\mathbf{X} \rangle = G_{AB} dX^A dX^B, \quad |d\mathbf{D}|^2 = \langle d\mathbf{D}, \mathcal{G}d\mathbf{D} \rangle = G_{AB} dD^A dD^B. \tag{16}$$

The respective volume element dV of \mathcal{M} , volume form $d\Omega$ of \mathcal{M} , and the area form Ω for its boundary $\partial\mathcal{M}$, are defined as follows [37], where $n = \dim \mathcal{M} = \dim \partial\mathcal{M} + 1$:

$$dV = \sqrt{G} dX^1 dX^2 \dots dX^n, \quad d\Omega = \sqrt{G} dX^1 \wedge dX^2 \wedge \dots \wedge dX^n, \tag{17}$$

$$\Omega = \sqrt{B} dU^1 \wedge \dots \wedge dU^{n-1}. \tag{18}$$

Local coordinates on the hypersurface $\partial\mathcal{M}$, oriented and $(n - 1)$ -dimensional, are given as parametric equations $X^A = X^A(U^\alpha)$ ($\alpha = 1, \dots, n - 1$), $B_\alpha^A = \frac{\partial X^A}{\partial U^\alpha}$, and $B = \det(B_\alpha^A G_{AB} B_\beta^B)$.

2.1.3. Covariant Derivatives

Basis vector gradients in horizontal form are acquired from affine (i.e., linear) connection coefficients, written generically as H_{BC}^A and K_{BC}^A , where $\nabla(\cdot)$ is the covariant derivative:

$$\nabla_{\delta/\delta X^B} \frac{\delta}{\delta X^C} = H_{BC}^A \frac{\delta}{\delta X^A}, \quad \nabla_{\delta/\delta X^B} \frac{\partial}{\partial D^C} = K_{BC}^A \frac{\partial}{\partial D^A}. \tag{19}$$

Analogously, vertical gradients employ generic connection coefficients, V_{BC}^A and Y_{BC}^A :

$$\nabla_{\partial/\partial D^B} \frac{\partial}{\partial D^C} = V_{BC}^A \frac{\partial}{\partial D^A}, \quad \nabla_{\partial/\partial D^B} \frac{\delta}{\delta X^C} = Y_{BC}^A \frac{\delta}{\delta X^A}. \tag{20}$$

For example, let $V = V^A \frac{\delta}{\delta X^A} \in H\mathcal{Z}$ be a vector field. Then the (total) covariant derivative of V is

$$\begin{aligned} \nabla V &= \nabla_{\delta/\delta X^B} V \otimes dX^B + \nabla_{\partial/\partial D^B} V \otimes \delta D^B \\ &= (\delta_B V^A + H_{BC}^A V^C) \frac{\delta}{\delta X^A} \otimes dX^B + (\bar{\delta}_B V^A + Y_{BC}^A V^C) \frac{\partial}{\partial D^A} \otimes \delta D^B \\ &= V_{|B}^A \frac{\delta}{\delta X^A} \otimes dX^B + V^A|_B \frac{\partial}{\partial D^A} \otimes \delta D^B. \end{aligned} \tag{21}$$

Denoted by $(\cdot)_{|A}$ is a horizontal covariant derivative with respect to $\{X^A\}$. Denoted by $(\cdot)|_B$ is a vertical covariant derivative with respect to $\{D^B\}$.

Remark 4. The ordering of lower indices on connections matches some works [4,22,31,98] and is the transpose of others [2,5,34]. For symmetric connections, it is inconsequential.

The horizontal covariant derivative, in components of the horizontal metric tensor $G = G_{AB} dX^A \otimes dX^B$ (i.e., the horizontal part of \mathcal{G}), is

$$\begin{aligned} G_{AB|C} &= \delta_C G_{AB} - H_{CA}^D G_{DB} - H_{CB}^D G_{AD} \\ &= \partial_C G_{AB} - N_C^D \bar{\delta}_D G_{AB} - H_{CA}^D G_{DB} - H_{CB}^D G_{DA}. \end{aligned} \tag{22}$$

For the determinant of the metric $G = \det(G_{AB})$, identified as a scalar density [37],

$$(\sqrt{G})_{|A} = \partial_A(\sqrt{G}) - N_A^B \bar{\delta}_B(\sqrt{G}) - \sqrt{G} H_{AB}^B. \tag{23}$$

The Levi-Civita connection coefficients are written as γ_{BC}^A ; these are also known as Christoffel symbols of the second kind. Cartan’s tensor is C_{BC}^A , and horizontal coefficients of the Chern-Rund and Cartan connections are Γ_{BC}^A . All have null torsion due to symmetry:

$$\gamma_{BC}^A = \frac{1}{2} G^{AD} (\partial_C G_{BD} + \partial_B G_{CD} - \partial_D G_{BC}) = G^{AD} \gamma_{BCD}, \tag{24}$$

$$C_{BC}^A = \frac{1}{2} G^{AD} (\bar{\partial}_C G_{BD} + \bar{\partial}_B G_{CD} - \bar{\partial}_D G_{BC}) = G^{AD} C_{BCD}, \tag{25}$$

$$\Gamma_{BC}^A = \frac{1}{2} G^{AD} (\delta_C G_{BD} + \delta_B G_{CD} - \delta_D G_{BC}) = G^{AD} \Gamma_{BCD}. \tag{26}$$

Remark 5. The coefficients of Cartan, Chern, and Rund are compatible with regard to the covariant differential of $G = G_{AB} dX^A \otimes dX^B$ since $H_{BC}^A = \Gamma_{BC}^A \Rightarrow G_{AB|C} = 0$ for (22). Similarly, the tensor of Cartan is compatible with the vertical covariant differential of the metric G : $Y_{BC}^A = C_{BC}^A \Rightarrow G_{AB|C} = 0$.

From direct calculations with respective (24), (25), and (26), traces of linear connections are related to partial gradients of $G = \det(G)$:

$$\partial_A(\ln \sqrt{G}) = \gamma_{AB}^B, \quad \bar{\partial}_A(\ln \sqrt{G}) = C_{AB}^B, \quad \delta_A(\ln \sqrt{G}) = \frac{1}{2} G^{BC} \delta_A G_{CB} = \Gamma_{AB}^B. \quad (27)$$

Remark 6. Similar to the previous remark, $H_{BC}^A = \Gamma_{BC}^A \Rightarrow G_{|A} = 2G(\ln \sqrt{G})_{|A} = 0$ and $Y_{BC}^A = C_{BC}^A \Rightarrow G|_A = 2G(\ln \sqrt{G})|_A = 0$.

Nonlinear connection coefficients $N_B^A(X, D)$ admissible under (1) and (8) can be obtained in various settings. If $T\mathcal{Z}$ is limited to sections that are locally flat [3,10], $N_B^A = 0$ in a preferred coordinate chart $\{X, D\}$, but \tilde{N}_B^A in (8) does not vanish for heterogeneous transformations under which $\partial_B Q_K^J$ is nonzero. A Lagrangian $L(X, D)$, real and differentiable, can be introduced, from which $N_B^A = G_B^A$, where [5]

$$G_B^A = \bar{\partial}_B G^A = \bar{\partial}_B [G^{AE} (D^C \bar{\partial}_E \partial_C L - \partial_E L)]. \quad (28)$$

Remark 7. Let $G_{AB}(X, D)$ be a positive homogeneous function of degree zero with respect to D . Then G^A below are spray components [3,10], and $N_B^A = G_B^A$ are so-called canonical coefficients of the nonlinear connection that obey (8):

$$G^A = \frac{1}{2} \gamma_{BC}^A D^B D^C, \quad G_B^A = \bar{\partial}_B G^A. \quad (29)$$

For classification, let $K_{BC}^A = H_{BC}^A$ and $Y_{BC}^A = V_{BC}^A$. An extended and complete Finsler connection is written as the triplet $(N_B^A, H_{BC}^A, V_{BC}^A)$. The Chern–Rund connection is $(G_B^A, \Gamma_{BC}^A, 0)$. Cartan’s connection is $(G_B^A, \Gamma_{BC}^A, C_{BC}^A)$. Berwald’s connection is $(G_B^A, G_{BC}^A, 0)$, where $G_{BC}^A = N_{BC}^A = \bar{\partial}_B N_C^A = \bar{\partial}_B \bar{\partial}_C G^A$.

2.1.4. A Divergence Theorem

Let \mathcal{M} denote a differentiable manifold with the dimension of n . Let $\partial\mathcal{M}$ be its $(n - 1)$ -dimensional boundary, a hypersurface positively oriented and of class C^1 . The coordinate-free theorem of Stokes for any C^1 differentiable $(n - 1)$ form α on \mathcal{M} can be written as

$$\int_{\mathcal{M}} d\alpha = \int_{\partial\mathcal{M}} \alpha. \quad (30)$$

Theorem 1. Let \mathcal{M} , $\dim \mathcal{M} = n$, as the base space for a generalized Finsler bundle of the total space \mathcal{Z} . The boundary $\partial\mathcal{M}$ is of positive orientation and class C^1 , having $\dim \partial\mathcal{M} = n - 1$. Let $\alpha(X, D) = V^A(X, D) N_A(X, D) \Omega(X, D)$ denote a differentiable $(n - 1)$ form. Let $V = V^A \frac{\delta}{\delta X^A} \in H\mathcal{Z}$ denote a vector field, and V^A denote its contravariant components. Denote the positive-definite field $G_{AB}(X, D)$ as components of the metric on the horizontal space having $G = \det(G_{AB}) > 0$. Let $H_{BC}^A = H_{CB}^A$ be the symmetric and affine horizontal connection such that $(\sqrt{G})_{|A} = 0$. Lastly, C^1 functional relations $D = D(X)$ are presumed available for vertical coordinates of fibers for all $X \in \mathcal{M}$. Stokes’ theorem (30) can then be expressed explicitly as follows for an assigned chart $\{X^A\}$, appealing to definitions of forms for volumes and areas in the second of (17) and (18):

$$\int_{\mathcal{M}} [V_{|A}^A + (V^A C_{BC}^C + \bar{\partial}_B V^A) D_{;A}^B] d\Omega = \int_{\partial\mathcal{M}} V^A N_A \Omega. \quad (31)$$

The horizontal covariant derivative is $V_{|A}^A = \delta_A V^A + H_{BA}^B V^A$, the definition $D_{;A}^B = \partial_A D^B + N_{BA}^B$ with $\partial_A D^B = \partial D^A / \partial X^B$, and N_A is a unit outward normal component of $N = N_A dX^A$ to $\partial\mathcal{M}$.

Proof. The proof, not repeated here, is given in the review [54], suggested but not derived formally in an earlier work [55]. The proof of (31) [54] extends that of Rund [37], which considered a strict Finsler space F_n with the metric obtained from a fundamental function \mathcal{F} and used Cartan’s connection $(G_B^A, \Gamma_{BC}^A, C_{BC}^A)$. The proof in [54] extends Rund’s proof to general Finsler spaces having arbitrary positive-definite $G_{AB}(X, D)$ and arbitrary $N_B^A(X, D)$. \square

Remark 8. As per the theorem of Stokes, (31) applies if the base space \mathcal{M} and boundary $\partial\mathcal{M}$ is interchanged with a compact region of $\mathcal{M}' \subset \mathcal{M}$ and its boundary of positive orientation.

Remark 9. The affine horizontal coefficients $H_{BC}^A = \Gamma_{BC}^A$ of Cartan, Chern, and Rund uniquely fulfill symmetry and metric-compatibility requirements.

Remark 10. An alternative basis and the dual of that basis on \mathcal{M} could be prescribed for the vector field \mathbf{V} and normal field \mathbf{N} , given certain stipulations [54]. However, geometric interpretation of covariant differentiation on the left side of (31) suggests $\{\frac{\delta}{\delta X^A}\}$ should be used for \mathbf{V} , by which, the dual basis $\{dX^B\}$ should be used for \mathbf{N} to ensure invariance: $\langle \mathbf{V}, \mathbf{N} \rangle \rightarrow V^A N_B \langle \frac{\delta}{\delta X^A}, dX^B \rangle$. If instead \mathbf{V} is referred to the holonomic basis $\{\frac{\partial}{\partial X^A}\}$, then $N_B^A = 0$ should be imposed for invariance with $N_B dX^B$. As noted prior to (28), this choice would restrict (31) to homogeneous transformations of coordinates $\{X, D\}$.

As assumed in Theorem 1 [37,54,55], C^1 functions $D = D(X)$ must exist over all $X \in \mathcal{M}$. Relations of generalized Finsler geometry [5] still apply, but additional relations emerge naturally when metric G_{AB} is interpreted as an osculating Riemannian metric [2,44]. Specifically, an alternative representation of (31) is newly proven in the following.

Corollary 1. Given C^1 functions $D = D(X)$, set $\tilde{G}_{AB}(X) = G_{AB}(X, D(X))$ as components of the osculating Riemannian metric derived from $\mathbf{G} = G_{AB} dX^A \otimes dX^B$. Then (31) is equivalent to

$$\int_{\mathcal{M}} \tilde{V}^A_{;A} d\Omega = \int_{\partial\mathcal{M}} \tilde{V}^A \tilde{N}_A \Omega, \tag{32}$$

where the vector $\tilde{V}^A(X) = V^A(X, D(X))$, unit normal $\tilde{N}_A(X) = N_A(X, D(X))$, and covariant derivative $\tilde{V}^A_{;A} = \partial_A \tilde{V}^A + \tilde{\gamma}^B_{BA} \tilde{V}^A$ with connection $\tilde{\gamma}^B_{BA}(X) = \partial_A (\ln \sqrt{\tilde{G}(X)}) = \tilde{\gamma}^B_{AB}(X)$ and $\tilde{G} = \det(\tilde{G}_{AB})$.

Proof. The right of (32) is identical to the right of (31), given the change of variables. On the left of (32), from chain-rule differentiation, vanishing (23), and (27),

$$\partial_A \tilde{V}^A = \partial_A V^A + \bar{\partial}_B V^A \partial_A D^B, \tag{33}$$

$$\begin{aligned} \tilde{V}^A \tilde{\gamma}^B_{BA} &= \tilde{V}^A \partial_A (\ln \sqrt{\tilde{G}}) = V^A [\partial_A (\ln \sqrt{G}) + \bar{\partial}_B (\ln \sqrt{G}) \partial_A D^B] \\ &= V^A [\delta_A (\ln \sqrt{G}) + N_A^B \bar{\partial}_B (\ln \sqrt{G}) + C_{BC}^C \partial_A D^B] \\ &= V^A [\delta_A (\ln \sqrt{G}) + C_{BC}^C (N_A^B + \partial_A D^B)] \\ &= V^A [H_{AB}^B + C_{BC}^C D^B_{;A}] = V^A [H_{BA}^B + C_{BC}^C D^B_{;A}]. \end{aligned} \tag{34}$$

Adding (33) to (34), and canceling $\pm N_A^B \bar{\partial}_B V^A$ terms, produces

$$\begin{aligned} \tilde{V}^A_{;A} &= \{\partial_A V^A + \bar{\partial}_B V^A \partial_A D^B - N_A^B \bar{\partial}_B V^A\} + \{N_A^B \bar{\partial}_B V^A + V^A [H_{BA}^B + C_{BC}^C D^B_{;A}]\} \\ &= \delta_A V^A + V^A H_{BA}^B + \bar{\partial}_B V^A (\partial_A D^B + N_A^B) + V^A C_{BC}^C D^B_{;A} \\ &= V^A_{|A} + (\bar{\partial}_B V^A + V^A C_{BC}^C) D^B_{;A}. \end{aligned} \tag{35}$$

Integrands on the left sides of (31) and (32) are, thus, verified to match, completing the proof. \square

Remark 11. Coefficients of the Levi–Civita connection of \tilde{G}_{AB} satisfy the symmetry and metric-compatibility requirements used to prove (32):

$$\tilde{\gamma}_{BC}^A = \frac{1}{2}\tilde{G}^{AD}(\partial_C\tilde{G}_{BD} + \partial_B\tilde{G}_{CD} - \partial_D\tilde{G}_{BC}) = \tilde{G}^{AD}\tilde{\gamma}_{BCD}. \tag{36}$$

Remark 12. Given (36), the form of the divergence theorem in (32) appears analogous to that of a Riemannian manifold with boundary. It is not identical, however, since the non-holonomic basis $\{\frac{\delta}{\delta X^A}\}$ is used for \mathbf{V} . As in Remark 2.1.3, the holonomic basis $\{\frac{\partial}{\partial X^A}\}$ could be used in a preferred chart $\{X, D(X)\}$, wherein $N_B^A = 0$; under such special conditions the distinction vanishes.

2.1.5. Finsler and Pseudo-Finsler Spaces

The preceding presentation holds for generalized Finsler geometry, by which a Lagrangian function is not necessary to obtain components of the metric tensor [5,6,36]. Subclasses of generalized spaces of Finsler necessitate the existence of a Lagrangian \mathcal{L} . Denote the tangent bundle for \mathcal{M} excluding the $D = 0$ zero section as $\mathcal{Z} = T\mathcal{M}\setminus 0$. Function $\mathcal{L}(X, D) : \mathcal{Z} \rightarrow \mathbb{R}$ is positively homogeneous of second order with respect to D and differentiable to any required class in $\{X^A\}$ and $\{D^A\}$, C^∞ being the usual assumption [3], C^5 usually acceptable [10]. In this case, $(\mathcal{M}, \mathcal{L})$ fulfills the requirements for a pseudo-Finsler space if $n \times n$ matrix G_{AB} is both non-singular over \mathcal{Z} and obtained from Lagrangian \mathcal{L} :

$$G_{AB}(X, D) = \bar{\partial}_A\bar{\partial}_B\mathcal{L}(X, D), \quad \mathcal{L} = \frac{1}{2}G_{AB}D^AD^B. \tag{37}$$

When $G_{AB}(X, D)$ is strictly positive definite on \mathcal{Z} , a pseudo-Finsler space becomes a Finsler space, written as the set $(\mathcal{M}, \mathcal{F})$ or simply F_n where $n = \dim \mathcal{M}$. The fundamental function $\mathcal{F}(X, D)$ for the F_n is first-order positively homogeneous with respect to D , whereby [2,3]

$$\begin{aligned} \mathcal{F}(X, D) &= \sqrt{2\mathcal{L}(X, D)} = |G_{AB}(X, D)D^AD^B|^{1/2} \\ \leftrightarrow \quad \mathcal{L}(X, D) &= \frac{1}{2}\mathcal{F}^2(X, D); \quad \mathcal{F}(X, D) > 0 \forall D \neq 0. \end{aligned} \tag{38}$$

In Finsler geometry [2,3,5], conditions $L = \mathcal{L}$ and $G^A = G^A$ in (28) and (29), and

$$\begin{aligned} G_{AB} &= \frac{1}{2}\bar{\partial}_A\bar{\partial}_B(\mathcal{F}^2), & G_B^A &= \gamma_{BC}^AD^C - C_{BC}^A\gamma_{DE}^CD^D D^E = \Gamma_{BC}^AD^C; \\ C_{ABC} &= \frac{1}{4}\bar{\partial}_A\bar{\partial}_B\bar{\partial}_C(\mathcal{F}^2). \end{aligned} \tag{39}$$

Reductions and embeddings for Finsler spaces are discussed elsewhere [2,3,10,54,102,103].

2.2. Spatial Configuration

A description of a fiber bundle analogous to that of Section 2.1 is invoked for the spatial or current representation of a continuum. Let \mathfrak{m} and n denote the differentiable, spatial base manifold, and its dimension. Immersion in an external Euclidean N space is possible for the base manifold under stipulation $N \geq n$.

Remark 13. Definitions in Section 2.2 parallel those of Section 2.1. Upper-case symbols and indices for referential quantities are now exchanged with lower-case ones for most spatial variables.

In the current configuration, $x \in \mathfrak{m}$ depicts a point or particle location. A chart of spatial coordinates on \mathfrak{m} is $\{x^a\} (a = 1, 2, \dots, n)$. Every point on the spatial base manifold supports a local vector written as \mathbf{d} , with $\{d^k\} (k = 1, 2, \dots, m)$ auxiliary coordinates for \mathfrak{m} . The total space of dimension $n + m$ is \mathfrak{z} , and $\mathbf{z} = (\mathfrak{z}, \pi, \mathfrak{m}, \mathfrak{u})$ is the fiber bundle. Let $\pi : \mathfrak{z} \rightarrow \mathfrak{m}$ be the projection. A fiber is $\mathfrak{u} = \mathfrak{z}_x = \pi^{-1}(x)$. Composite chart $\{x^a, d^k\}$ is associated with \mathfrak{z} . The vector bundle is $(\mathfrak{z}, \pi, \mathfrak{m})$; every fiber comprises a vector space of dimension n .

Denote the motion function by φ , which globally maps reference material points to spatial points. Denote $\Xi = (\varphi, \theta)$ as the set of functions that correspondingly updates total spaces among configurations. General functional forms are $\varphi(X, D) : \mathcal{M} \rightarrow \mathfrak{m}$ and $\Xi(X, D) : \mathcal{Z} \rightarrow \mathfrak{z}$. As described in Section 3.1, $\varphi(X, D)$ and $\Xi(X, D)$ can have more specific representations [54]. Time (t) dependence is possible in the most general theories [50,58,59]. However, explicit time dependence is excluded from the current theoretical presentation that focuses on equilibrium configurations [55,62]. The following diagram commutes [5]:

$$\begin{array}{ccc} \mathcal{Z} & \xrightarrow{\Xi} & \mathfrak{z} \\ \downarrow \Pi & & \downarrow \pi \\ \mathcal{M} & \xrightarrow{\varphi} & \mathfrak{m} \end{array}$$

2.2.1. Coordinate Transformations

Let $\{x, d\}$ to $\{\tilde{x}, \tilde{d}\}$ be a change of coordinates for \mathfrak{z} ; the Finsler relationships akin to (1) are

$$\tilde{x}^a = \tilde{x}^a(x), \quad \tilde{d}^j(x, d) = q_k^j(x) d^k. \tag{40}$$

Differentiable matrix q_k^j is non-singular with inverse \tilde{q}_k^j , whereby $\tilde{q}_k^j q_j^k = \delta^i_i$. Tangent bundle $T\mathfrak{z}$ has $\{\frac{\partial}{\partial \tilde{x}^a}, \frac{\partial}{\partial \tilde{d}^k}\}$ for its holonomic basis. The cotangent bundle $T^*\mathfrak{z}$ has $\{dx^a, dd^k\}$. Bases of non-holonomic vectors are $\{\frac{\delta}{\delta \tilde{x}^a}\}$ and $\{\delta d^k\}$; these map conventionally as $x \rightarrow \tilde{x}$:

$$\frac{\delta}{\delta x^a} = \frac{\partial}{\partial x^a} - N_a^k \frac{\partial}{\partial d^k}, \quad \delta d^k = dd^k + N_b^k dx^b. \tag{41}$$

The set $\{\frac{\delta}{\delta \tilde{x}^a}, \frac{\partial}{\partial \tilde{d}^k}\}$ is used as a local basis on $T\mathfrak{z}$, and $\{dx^a, \delta d^k\}$ is used for $T^*\mathfrak{z}$. The orthogonal decomposition of the tangent bundle, given its nonlinear connection, is $T\mathfrak{z} = V\mathfrak{z} \oplus H\mathfrak{z}$. Notation is as expected for the former vertical vector bundle and the latter horizontal distribution. Nonlinear connection coefficients transform as

$$\tilde{N}_a^j = \left(q_k^j N_b^k - \frac{\partial q_k^j}{\partial x^b} d^k \right) \frac{\partial x^b}{\partial \tilde{x}^a}. \tag{42}$$

Henceforth, set $m = n$. Thus, $j, k, \dots \rightarrow a, b, \dots$ for the index notation with sums covering 1 to n on repeated indices. Furthermore, per (40), the transformation for d^a is akin to that of vectors of contravariant form on \mathfrak{m} :

$$q_b^a = \frac{\partial \tilde{d}^a}{\partial d^b} = \frac{\partial \tilde{x}^a}{\partial x^b}. \tag{43}$$

Condensed notation is used for derivatives with respect to coordinates on $\mathfrak{m}, \mathfrak{z}$:

$$\partial_a f(x, d) = \frac{\partial f(x, d)}{\partial x^a}, \quad \bar{\partial}_a f(x, d) = \frac{\partial f(x, d)}{\partial d^a}; \quad \delta_a(\cdot) = \frac{\delta(\cdot)}{\delta x^a} = \partial_a(\cdot) - N_a^b \bar{\partial}_b(\cdot); \tag{44}$$

$$\partial_b x^a = \frac{\partial x^a}{\partial x^b} = \delta_b^a, \quad \bar{\partial}_b x^a = 0; \quad \partial_b d^a = \frac{\partial d^a}{\partial x^b}, \quad \bar{\partial}_b d^a = \delta_b^a. \tag{45}$$

2.2.2. Length, Area, and Volume

A scalar product for vectors on \mathfrak{z} is obtained from the metric tensor of Sasaki [104]:

$$\mathfrak{g}(x, d) = \mathfrak{g}(x, d) + \check{\mathfrak{g}}(x, d) = g_{ab}(x, d) dx^a \otimes dx^b + \check{g}_{ab}(x, d) \delta d^a \otimes \delta d^b; \tag{46}$$

$$\mathfrak{g}_{ab} = g_{ab} = \mathfrak{g}\left(\frac{\delta}{\delta x^a}, \frac{\delta}{\delta x^b}\right) = \check{\mathfrak{g}}_{ab} = \check{\mathfrak{g}}\left(\frac{\partial}{\partial d^a}, \frac{\partial}{\partial d^b}\right) = \check{\mathfrak{g}}_{ba} = g_{ba} = \mathfrak{g}_{ba}. \tag{47}$$

Denote by dx and dd , respectively, line elements of m and u . The former has the basis vector $\{\frac{\delta}{\delta x^a}\}$, the latter $\{\frac{\partial}{\partial d^a}\}$. Line lengths squared satisfy

$$|dx|^2 = \langle dx, gdx \rangle = g_{ab} dx^a dx^b, \quad |dd|^2 = \langle dd, gdd \rangle = g_{ab} dd^a dd^b. \tag{48}$$

Let $\dim m = n$ with $\dim \partial m = n - 1$ the dimension of the boundary. The local volume (scalar) element and volume form, followed by the local area form, are respectively

$$dv = \sqrt{g} dx^1 dx^2 \dots dx^n, \quad d\omega = \sqrt{g} dx^1 \wedge dx^2 \wedge \dots \wedge dx^n, \quad \omega = \sqrt{b} du^1 \wedge \dots \wedge du^{n-1}. \tag{49}$$

The surface embedding in manifold m is $x^a = x^a(u^\alpha)$ ($\alpha = 1, \dots, n - 1$), $b_\alpha^a = \frac{\partial x^a}{\partial u^\alpha}$, and $b = \det(b_\alpha^a g_{ab} b_\beta^b)$.

2.2.3. Covariant Derivatives

Let $\nabla(\cdot)$ denote the operator for covariant differentiation. Generic affine coefficients H_{bc}^a and K_{bc}^a are used for horizontal derivatives, V_{bc}^a and Y_{bc}^a for vertical derivatives:

$$\nabla_{\delta/\delta x^b} \frac{\delta}{\delta x^c} = H_{bc}^a \frac{\delta}{\delta x^a}, \quad \nabla_{\delta/\delta x^b} \frac{\partial}{\partial d^c} = K_{bc}^a \frac{\partial}{\partial d^a}; \tag{50}$$

$$\nabla_{\partial/\partial d^b} \frac{\partial}{\partial d^c} = V_{bc}^a \frac{\partial}{\partial d^a}, \quad \nabla_{\partial/\partial d^b} \frac{\delta}{\delta x^c} = Y_{bc}^a \frac{\delta}{\delta x^a}. \tag{51}$$

For example, on \mathfrak{z} the covariant differential is obtained like (21), now for $V = V^a \frac{\delta}{\delta x^a} \in H\mathfrak{z}$:

$$\nabla V = \nabla_{\delta/\delta x^b} V \otimes dx^b + \nabla_{\partial/\partial d^b} V \otimes \delta d^b = V^a|_b \frac{\delta}{\delta x^a} \otimes dx^b + V^a|_b \frac{\partial}{\partial d^a} \otimes \delta d^b. \tag{52}$$

Herein, $(\cdot)|_a$ and $(\cdot)|_b$ denote differentiation horizontally with respect to x^a and vertically with respect to d^b . Let γ_{bc}^a be coefficients of the Levi-Civita connection on \mathfrak{z} , C_{bc}^a be the coefficients of the Cartan tensor on \mathfrak{z} , and Γ_{bc}^a be the coefficients of Cartan, Chern, and Rund (horizontal) on \mathfrak{z} :

$$\gamma_{bc}^a = \frac{1}{2} g^{ad} (\partial_c g_{bd} + \partial_b g_{cd} - \partial_d g_{bc}) = g^{ad} \gamma_{bcd}, \tag{53}$$

$$C_{bc}^a = \frac{1}{2} g^{ad} (\bar{\partial}_c g_{bd} + \bar{\partial}_b g_{cd} - \bar{\partial}_d g_{bc}) = g^{ad} C_{bcd}, \tag{54}$$

$$\Gamma_{bc}^a = \frac{1}{2} g^{ad} (\delta_c g_{bd} + \delta_b g_{cd} - \delta_d g_{bc}) = g^{ad} \Gamma_{bcd}. \tag{55}$$

2.2.4. A Divergence Theorem

The generalized Finsler bundle of the total space \mathfrak{z} is assigned base manifold m noting $\dim m = n$. The boundary denoted by ∂m is of class C^1 and is of positive orientation. A vector field $V = V^a \frac{\delta}{\delta x^a} \in H\mathfrak{z}$ has contravariant components V^a . The $(n - 1)$ form $\alpha(x, d) = V^a(x, d) n_a(x, d) \omega(x, d)$ is differentiable. Metric tensor components $g_{ab}(x, d)$, which are positive definite, apply for the horizontal distribution, and $g = \det(g_{ab}) > 0$. The affine horizontal connection $H_{bc}^a = H_{cb}^a$ is chosen to ensure $(\sqrt{g})|_a = 0$ (e.g., $H_{bc}^a = \Gamma_{bc}^a$). The existence is required for fiber coordinates $d = d(x)$, representing functions of class $C^1 \forall x \in m$. Forms for area and volume are defined in (49). Then (30) is in the coordinate form with respect to $\{x^a\}$,

$$\int_m [V^a|_a + (V^a C_{bc}^c + \bar{\delta}_b V^a) d^b_{;a}] d\omega = \int_{\partial m} V^a n_a \omega. \tag{56}$$

Denoted by n_a is the covector of the unit length normal to ∂m , $V^a|_a = \delta_a V^a + V^a H_{ba}^b$, and $d^b_{;a} = \partial_a d^b + N_a^b$. The proof matches that of Theorem 1 upon changes in variables; a corollary akin to Corollary 1 also holds.

3. Finsler-Geometric Continuum Mechanics

The original theory of Finsler-geometric continuum mechanics [55,56] is formulated for finite strains with conservation of momenta applying at equilibrium states (i.e., quasi-static conditions). Subtle differences exist among certain assumptions for different instantiations, incrementally revised in successive works. Most differences are explained in a review [54].

3.1. Motion and Deformation

Let $\varphi : \mathcal{M} \rightarrow \mathfrak{m}$ denote the motion of a material particle and $\Phi : \mathfrak{m} \rightarrow \mathcal{M}$ the inverse motion. These functions are differentiable of class C^3 and are one-to-one:

$$x^a = \varphi^a(X), \quad X^A = \Phi^A(x), \quad (a, A = 1, 2, \dots, n) \quad (57)$$

with $(\Phi \circ \varphi)(X) = X$. Write $\Xi = (\varphi, \theta)$ to represent the motion in total, whereby $\Xi : \mathcal{Z} \rightarrow \mathfrak{z}$. Refer to Figure 1.

Remark 14. The material field D and spatial field d are alternatively called director vectors or internal state vectors. They need not be unit vectors herein. The physical meanings of these fields depend on the particular application of the theory [54].

The class C^3 motion functions for the internal state fields are

$$d^a = \theta^a(X, D), \quad D^A = \Theta^A(x, d), \quad (a, A = 1, 2, \dots, n). \quad (58)$$

Remark 15. Herein, the dimensions of fibers are $m = n$, so $n = \dim \mathcal{U} = \dim \mathcal{M} = \dim \mathfrak{m} = \dim \mathfrak{u}$. Allowance for $m \neq n$ is conceivable [5,45]. But taking $m = n$ allows for a clearer interpretation of physics on the vertical vector bundle. Furthermore, $m = n$ enables (9) and (43) that simplify notation and calculations. For usual three-dimensional solid bodies, $n = 3$, as implied in parts of prior work [54], but other dimensions are permissible (e.g., two-dimensional membranes ($n = 2$) and one-dimensional rods ($n = 1$)).

From (57) and (58), a differentiable function $h(x, d) : \mathfrak{z} \rightarrow \mathbb{R}$ obeys the following laws of transformation for configurational changes in coordinates of partial differentiation:

$$\frac{\partial(h \circ \Xi)}{\partial X^A} = \frac{\partial h}{\partial x^a} \frac{\partial \varphi^a}{\partial X^A} + \frac{\partial h}{\partial d^a} \frac{\partial \theta^a}{\partial X^A}, \quad \frac{\partial(h \circ \Xi)}{\partial D^A} = \frac{\partial h}{\partial d^a} \frac{\partial \theta^a}{\partial D^A}. \quad (59)$$

Remark 16. Bases, metrics, and connections can be prescribed independently for \mathcal{Z} and \mathfrak{z} . This allowance is in accordance with the field theory of classical continua [20,105]. Unlike Chapter 8 of Bejancu [5], fields of frames are not required to convect from $T\mathcal{Z}$ to $T\mathfrak{z}$ in sync with Ξ . As such, $(\frac{\delta}{\delta x^a}, \frac{\partial}{\partial d^a}, \mathcal{G}_{ab}, H_{bc}^a, K_{bc}^a, V_{bc}^a, Y_{bc}^a, N_b^a)$ need not be obtained via push-forward operations by Ξ from $(\frac{\delta}{\delta X^A}, \frac{\partial}{\partial D^A}, \mathcal{G}_{AB}, H_{BC}^A, K_{BC}^A, V_{BC}^A, Y_{BC}^A, N_B^A)$. But choosing N_b^a as the push-forward of N_B^A [5] is beneficial since

$$N_a^b \frac{\partial \varphi^a}{\partial X^A} = N_A^B \frac{\partial \theta^b}{\partial D^B} - \frac{\partial \theta^b}{\partial X^A} \Rightarrow \frac{\delta(h \circ \Xi)}{\delta X^A} = \frac{\delta h}{\delta x^a} \frac{\partial \varphi^a}{\partial X^A} = \frac{\delta h}{\delta x^a} \frac{\delta \varphi^a}{\delta X^A} = \frac{\delta h}{\delta x^a} F_A^a, \quad (60)$$

by which $\delta_A(\cdot) = F_A^a \delta_a(\cdot)$ is a simple relation among δ derivatives on \mathcal{Z} and \mathfrak{z} .

The two-point tensor $F : H\mathcal{Z} \rightarrow H\mathfrak{z}$ is the deformation gradient, implicit in (60). By definition,

$$F = \frac{\delta \boldsymbol{\varphi}}{\delta \mathbf{X}} = \frac{\delta \varphi^a}{\delta X^A} \frac{\delta}{\delta x^a} \otimes dX^A = \frac{\partial \varphi^a}{\partial X^A} \frac{\delta}{\delta x^a} \otimes dX^A, \quad (61)$$

with (57) used in the rightmost equality. The gradient of inverse motion $f : H\mathfrak{z} \rightarrow H\mathcal{Z}$ follows by definition as

$$f = \frac{\delta\Phi}{\delta x} = \frac{\delta\Phi^A}{\delta x^a} \frac{\delta}{\delta X^A} \otimes dx^a = \frac{\partial\Phi^A}{\partial x^a} \frac{\delta}{\delta X^A} \otimes dx^a. \tag{62}$$

Remark 17. Accordingly, $F_A^a(X)f_b^A(x(X)) = \delta_b^a$ and $F_A^a(X)f_a^B(x(X)) = \delta_A^B$. Usual stipulations that the motion functions in (57) be regular hold. Thus $\det(F_A^a) > 0$ and $\det(f_a^A) > 0$.

Line element differentials introduced in (16) and (48) obey the following formulae:

$$dx = dx^a \frac{\delta}{\delta x^a} = F_A^a dX^A \frac{\delta}{\delta x^a} = FdX, \quad dX = dX^A \frac{\delta}{\delta X^A} = f_a^A dx^a \frac{\delta}{\delta X^A} = fdx. \tag{63}$$

Advancing (63), with the definition of the determinant, recall (17) (reference) and (49) (spatial) for elements and forms of volume. Denoting Jacobian determinants of transformations as $J = \det(F_A^a)\sqrt{g/G}$ and $j = 1/J = J^{-1} > 0$ (e.g., [22,98]), coordinate transformations give

$$dv = JdV = [\det(F_A^a)\sqrt{g/G}]dV, \quad dV = jd v = [\det(f_a^A)\sqrt{G/g}]d v, \tag{64}$$

$$\varphi^*d\omega = Jd\Omega, \quad \Phi^*d\Omega = jd\omega. \tag{65}$$

Strain can be quantified using the Lagrangian deformation tensor $C = C_{AB}dX^A \otimes dX^B$ (symmetric in covariant form via $C_{AB} = C_{BA}$):

$$|dx|^2 = F_A^a g_{ab} F_B^b dX^A dX^B = C_{AB}dX^A dX^B = \langle dX, CdX \rangle, \quad C_{AB} = F_A^a g_{ab} F_B^b = G_{AC}C_B^C. \tag{66}$$

From (64), $\det(C_{AB}) = \det(C_A^C G_{CB}) = J^2 G$. Then from the first of (50) and (60) [56,62],

$$\nabla_{\delta/\delta X^A} \frac{\delta}{\delta x^c} = \frac{\delta x^a}{\delta X^A} \nabla_{\delta/\delta x^a} \frac{\delta}{\delta x^c} = \delta_A \varphi^a H_{ac}^b \frac{\delta}{\delta x^b} = F_A^a H_{ac}^b \frac{\delta}{\delta x^b}. \tag{67}$$

Similarly, the second of (50) gives $\nabla_{\delta/\delta X^A} \frac{\partial}{\partial d^c} = F_A^a K_{ac}^b \frac{\partial}{\partial d^b}$, although this is not needed later.

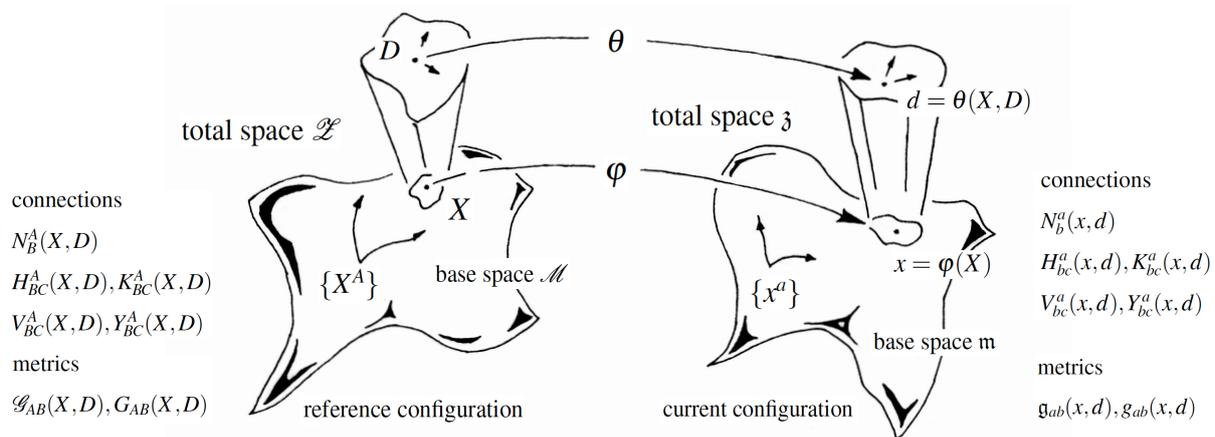


Figure 1. Total deformation $\Xi = (\varphi, \theta) : \mathcal{Z} \rightarrow \mathfrak{z}$ of material manifold \mathcal{M} ($\dim \mathcal{M} = n = m = 2$) with base-space coordinates $\{X^A\}$ to spatial representation \mathfrak{m} with base-space coordinates $\{x^a\}$. Internal structure fields are (D, d) on total spaces $(\mathcal{Z}, \mathfrak{z})$; arrows depict local components of state vectors D and d for neighborhoods centered at X and x .

3.2. Particular Assumptions

3.2.1. Director Fields

The divergence theorem (31) is invoked to obtain conservation laws for macroscopic and microscopic momenta in Section 3.3.3. Its derivation [37,54] requires the existence of functional relations

$$D^A = D^A(X), \quad d^a = d^a(x). \tag{68}$$

The latter relation of (68) arises from the former via the application of (56) and (57) (i.e., switching of independent variables). Then (57), (58), and (68) produce the following various dependencies of director motion functions:

$$d^a = \theta^a(X, D) = \hat{\theta}^a(X, D(X)) = \bar{\theta}^a(X), \quad D^A = \Theta^A(x, d) = \hat{\Theta}^A(x, d(x)) = \bar{\Theta}^A(x). \quad (69)$$

Remark 18. In some prior work [55,56], other functional forms of motion functions with internal state vectors as arguments were implemented. These likely more complex alternatives are admissible but inessential [54]. The current theory, like some others [44,50,52], does not always require θ or Θ to be specified explicitly, although the use of the former is implied later in Section 5.

The canonical and pragmatic rendering for $\theta(X, D)$, upon considering the existence of functions $D^A(X)$, becomes [62]

$$d = D \circ \Phi \Leftrightarrow d(x) = D(\Phi(x)) \Rightarrow \theta^a(D(X)) = D^A(X) \langle \delta d^a, \frac{\partial}{\partial D^A} \rangle = D^A(X) \delta_A^a, \quad (70)$$

where δ_A^a is viewed as a shifter between $V\mathfrak{z}$ and $V\mathcal{Z}$. Accordingly, $\delta_A^a = 1 \forall a = A$, $\delta_A^a = 0 \forall a \neq A$.

Remark 19. Invoking (70), $\partial_A \theta^a(D(X)) = 0$ by definitions of $\theta^a = \theta^a(D(X))$ and $\partial_A(\cdot) = (\partial(\cdot)/\partial X^A)|_{D=\text{const}}$ in (10). Also, $\bar{\partial}_A \theta^a(D(X)) = \delta_A^a$ by (11) and (70). Then (60) reduces to $N_b^a = N_B^A f_b^B \delta_A^a$, and conveniently for the degenerate case: $N_B^A = 0 \Leftrightarrow N_b^a = 0$.

3.2.2. Connections and Metrics

Invocation of (31) with permissible $G_{AB}(X, D)$ necessitates affine connection coefficients with metric compatibility for G_{AB} implying $H_{BC}^A = \Gamma_{BC}^A$, where Γ_{BC}^A is the connection of Cartan, Chern, and Rund in (26). For vertical affine connections, $V_{BC}^A = 0$ is elementary, which is consistent with the coefficients of Chern and Rund [2,3,106]. Setting $N_B^A = G_B^A$ via (29) further invokes the prescriptions of Chern and Rund, but this is inessential for generalized Finsler geometry. Choices $K_{BC}^A = H_{BC}^A$ [55,56] and $Y_{BC}^A = V_{BC}^A$ are logical, given (9), but these are not mandatory. Setting $K_{BC}^A = 0$ leading to metricity with regard to δ_{AB} , the metric of the Cartesian space may also be of utility [54].

Let the metric tensor of Sasaki, \mathcal{G} in (12), be assigned. From G_{AB} of (13), pragmatic connection coefficients over \mathcal{Z} are summarized in (71); complementary connections over \mathfrak{z} given \mathfrak{g} , where $g_{ab}(x, d)$ is found in (47) (i.e., the spatial Sasaki metric), follow thereafter:

$$H_{BC}^A = \Gamma_{BC}^A, \quad V_{BC}^A = Y_{BC}^A = 0; \quad H_{bc}^a = \Gamma_{bc}^a, \quad V_{bc}^a = Y_{bc}^a = 0; \quad N_b^a = N_B^A f_b^B \delta_A^a. \quad (71)$$

Remark 20. Note that K_{BC}^A and K_{bc}^a are left unspecified to admit mathematical descriptions of different physics, in contrast to Y_{BC}^A and Y_{bc}^a set equal to their purely vertical counterparts for simplicity. Since nonlinear connection N_B^A is also not explicitly chosen in (71) but is left general to admit more physics than considered previously [54], (8) need not always hold for any transformation. Thus N_B^A must be checked for correct behaviors under coordinate changes. Once the former N_B^A is chosen, N_b^a in (71) presumes (70) is invoked with (60).

Remark 21. If the fields $G_{AB}(X, D)$ and $g_{ab}(x, d)$ are known, relations in Sections 2.1 and 2.2 can be used to procure affine connections in (71). Zero-degree homogeneity of G_{AB} with regard to D is not required but is admitted. The G_{AB} entries are not required to be consistent with \mathcal{L} or \mathcal{F} (i.e., a Lagrangian function or fundamental scalar of Finsler), though this is admissible per Section 2.1.5. Physical arguments and material symmetries suggest \mathcal{G} dependencies with respect to X and D . Similar statements describe spatial metric \mathfrak{g} and components g_{ab} .

The decomposition of G_{AB} as \bar{G}_{AC} , a Riemannian term, and an internal state term \hat{G}_B^C is useful for describing fundamental physics and solving boundary value problems [55–57,62]:

$$\begin{aligned} \mathbf{G} &= \bar{\mathbf{G}}\hat{\mathbf{G}}; & G_{AB}(X, D) &= \bar{G}_{AC}(X)\hat{G}_B^C(X, D); \\ \bar{\mathbf{G}} &= \bar{G}_{AB} dX^A \otimes dX^B; & \hat{\mathbf{G}} &= \hat{G}_B^A \frac{\delta}{\delta X^A} \otimes dX^B. \end{aligned} \tag{72}$$

More specific functional forms in (72) are advocated here, implied by past applications [54]:

$$\begin{aligned} G_{AB}(X, D) &= \bar{G}_{AC}(X)\hat{G}_B^C(D(X)) = \hat{G}_A^C(D(X))\bar{G}_{CB}(X); \\ \bar{G}_{AB} &= \bar{G}_{BA}, & \hat{G}_A^C G_{BC} &= \hat{G}_B^C G_{CA}. \end{aligned} \tag{73}$$

Remark 22. Components of \bar{G}_{AB} are chosen to best represent the physics under consideration. Typically, rectangular, spherical, polar, or cylindrical systems for \mathcal{M} are witnessed in elasticity. Components of \hat{G}_B^C are chosen, corresponding to the way internal structure D manifests in length, area, and volume, as observed in \mathcal{Z} , meaning the total space of the body with the evolving microstructure [54,55,62].

Ideas apply analogously to the spatial metric $g_{ab}(x, d)$ upon variable changes $X \rightarrow x$ and $D \rightarrow d$. For example, the spatial analog of (73) is

$$g_{ab}(x, d) = \bar{g}_{ac}(x)\hat{g}_b^c(d(x)) = \hat{g}_a^c(d(x))\bar{g}_{cb}(x); \quad \bar{g}_{ab} = \bar{g}_{ba}, \quad \hat{g}_a^c g_{bc} = \hat{g}_b^c g_{ca}. \tag{74}$$

All metrics in (73) and (74) are assumed invertible with positive determinants. A symmetric tensor $\bar{\mathbf{C}}$ [62] and volume ratio $\bar{J} > 0$ are defined to exclude the internal state-dependence of strain:

$$\bar{\mathbf{C}}(X) = \bar{C}_{AB}(X) dX^A \otimes dX^B, \quad \bar{C}_{AB} = F_A^a \bar{g}_{ab} F_B^b, \quad \bar{C}_B^A = \bar{G}^{AC} \bar{C}_{CB}; \tag{75}$$

$$\bar{J}(X) = \sqrt{\det(\bar{C}_B^A(X))}; \quad \bar{J} = J\sqrt{\hat{G}/\hat{g}}, \quad \hat{G} = \det(\hat{G}_B^A), \quad \hat{g} = \det(\hat{g}_b^a). \tag{76}$$

3.3. Energy and Equilibrium

3.3.1. Variational Principle

A variational principle [54–56] is implemented. Let Ψ denote the total energy functional of $\mathcal{M}' \subset \mathcal{M}$ (a compact base space domain) having $\partial\mathcal{M}'$ as its boundary of positive orientation. Free energy density ψ , on a referential volume basis of material, is the integrand in

$$\Psi[\boldsymbol{\varphi}, \mathbf{D}] = \int_{\mathcal{M}'} \psi(F_A^a, D^A, D_{|B}^A, X^A) d\Omega. \tag{77}$$

One surface force is $\mathbf{p} = p_a dx^a$, the traction vector for the mechanical force divided by referential area. A second is $\mathbf{z} = z_A \delta D^A$, serving as the conjugate thermodynamic traction to the vector of the internal state. Denote a generic local, vector-valued volumetric source term conjugate to structure variations by $\mathbf{R} = R_A \delta D^A$, extending prior theory [54–56] to accommodate more physics [30,107] (Appendix B). A variational principle for Finsler-geometric continuum mechanics, holding X fixed but with $x = \varphi(X)$ and D independently variable parameters, is

$$\delta\Psi[\boldsymbol{\varphi}, \mathbf{D}] = \oint_{\partial\mathcal{M}'} (\langle \mathbf{p}, \delta\boldsymbol{\varphi} \rangle + \langle \mathbf{z}, \delta\mathbf{D} \rangle) \Omega + \int_{\mathcal{M}'} \langle \mathbf{R}, \delta\mathbf{D} \rangle d\Omega. \tag{78}$$

In coordinates with variation of \mathbf{D} in parentheses to distinguish from the basis $\{\delta D^A\}$,

$$\delta \int_{\mathcal{M}'} \psi d\Omega = \oint_{\partial\mathcal{M}'} \{p_a \delta\varphi^a\} \Omega + \oint_{\partial\mathcal{M}'} \{z_C \delta(D^C)\} \Omega + \int_{\mathcal{M}'} \{R_C \delta(D^C)\} d\Omega. \tag{79}$$

Several results used in Section 3.3.3 are now noted, with $\alpha = 1$ or $\alpha = 2$ derived in Appendix A via (71):

$$\delta F_A^a = \delta_A(\delta\varphi^a), \quad \delta D_{|B}^A = [\delta(D^A)]_{|B} - (\bar{\partial}_C N_B^A - \bar{\partial}_C K_{BD}^A D^D)\delta(D^C), \quad (80)$$

$$\delta(d\Omega) = \frac{1}{2}\alpha G^{AB}\bar{\partial}_C G_{AB}\delta(D^C)d\Omega = \alpha\bar{\partial}_C(\ln\sqrt{G})\delta(D^C)d\Omega = \alpha C_{CA}^A\delta(D^C)d\Omega. \quad (81)$$

3.3.2. General Energy Density

As evident in (78), the independent variables entering the total free energy density function ψ per unit reference volume, consist of the gradient of deformation, the director vector of the internal state, its horizontal covariant derivative, and the reference position of the material particle:

$$\psi = \psi(\mathbf{F}, \mathbf{D}, \nabla\mathbf{D}, \mathbf{X}) = \psi(F_A^a, D^A, D_{|B}^A, X^A). \quad (82)$$

Deformation gradient dependence via \mathbf{F} measures strain energy of elasticity. The state dependence via \mathbf{D} renders the evolving microstructural contributions. The energy arising from the heterogeneity of the microstructure (e.g., internal material surfaces) is captured by the dependence on the internal state gradient:

$$\nabla\mathbf{D} = D_{|B}^A \frac{\partial}{\partial D^A} \otimes dX^B + D^A|_B \frac{\partial}{\partial D^A} \otimes \delta D^B; \quad (83)$$

$$D_{|B}^A = \delta_B D^A + K_{BC}^A D^C = \partial_B D^A - N_B^A + K_{BC}^A D^C, \quad D^A|_B = \bar{\partial}_B D^A + V_{BC}^A D^C = \delta_B^A. \quad (84)$$

The dependence on \mathbf{X} permits heterogeneous properties. Prior work [54,55] motivates (82).

Remark 23. The vertical gradient $D^A|_B = \delta_B^A$, calculated from $V_{BC}^A = 0$ by (71), provides no information, so it is excluded from the arguments of energy density in (82).

The expansion of the integrand on the left in (79), with $\delta X^A = 0$ by definition, is

$$\begin{aligned} \delta\psi &= \frac{\partial\psi}{\partial F_A^a} \delta F_A^a + \frac{\partial\psi}{\partial D^A} \delta(D^A) + \frac{\partial\psi}{\partial D_{|B}^A} \delta D_{|B}^A = P_a^A \delta F_A^a + Q_A \delta(D^A) + Z_A^B \delta D_{|B}^A; \\ P_a^A &= \frac{\partial\psi}{\partial F_A^a}, \quad Q_A = \frac{\partial\psi}{\partial D^A}, \quad Z_B^A = \frac{\partial\psi}{\partial D_{|B}^A}. \end{aligned} \quad (85)$$

Denoted by \mathbf{P} is the mechanical stress tensor (i.e., the first Piola–Kirchhoff stress, a two-point tensor, and generally non-symmetric). The internal thermodynamic force vector \mathbf{Q} is complementary to \mathbf{D} , and the internal stress tensor \mathbf{Z} is complementary to gradient $\nabla\mathbf{D}$.

3.3.3. Euler–Lagrange Equations

Connection coefficients in (71) are employed along with (57), (67), (68), (80), and (81). Inserting (85) on the left side of (79), then integrating repeatedly by parts with (31) (i.e., application of the theorem of Stokes in coordinate form, Theorem 1), gives

$$\begin{aligned} \delta \int_{\mathcal{M}'} \psi d\Omega &= \int_{\mathcal{M}'} \{P_a^A \delta F_A^a + Q_A \delta(D^A) + Z_A^B \delta D_{|B}^A\} d\Omega + \int_{\mathcal{M}'} \psi \delta(d\Omega) \\ &= - \int_{\mathcal{M}'} \{\partial_A P_a^A + \bar{\partial}_B P_a^A \partial_A D^B + P_a^B \Gamma_{AB}^A - P_c^A \Gamma_{ba}^c F_A^b + P_a^A C_{BC}^C (\partial_A D^B + N_A^B)\} \delta\varphi^a d\Omega \\ &\quad - \int_{\mathcal{M}'} \{\partial_A Z_C^A + \bar{\partial}_B Z_C^A \partial_A D^B + Z_C^B \Gamma_{AB}^A - Z_B^A K_{AC}^B - Q_C \\ &\quad \quad + Z_A^B [\bar{\partial}_C N_B^A - \bar{\partial}_C K_{BD}^A D^D + \delta_C^A C_{ED}^D (\partial_B D^E + N_B^E)] - \alpha\psi C_{CA}^A\} \delta(D^C) d\Omega \\ &\quad + \oint_{\partial\mathcal{M}'} \{P_a^A \delta\varphi^a\} N_A \Omega + \oint_{\partial\mathcal{M}'} \{Z_C^A \delta(D^C)\} N_A \Omega. \end{aligned} \quad (86)$$

Local Euler–Lagrange equations corresponding to $\delta\boldsymbol{\varphi}$ and δD (i.e., admissible variations of parameters) for every $X \in \mathcal{M}'$, and boundary conditions of natural form over $\partial\mathcal{M}'$ are obtained as follows. Steps parallel those outlined in [55,56] with minor departures [54].

The first of these culminating Euler–Lagrange equations is the macroscopic balance of linear momentum, derived by setting the first integral on the right-hand side of (86) to zero, which is consistent with the right side of (79). Localizing the outcome and presuming the result must hold for any admissible variation $\delta\varphi^a$,

$$\partial_A P_a^A + \bar{\partial}_B P_a^A \partial_A D^B + P_a^B \Gamma_{AB}^A - P_c^A \Gamma_{ba}^c F_A^b = -P_a^A C_{BC}^C (\partial_A D^B + N_A^B). \quad (87)$$

The second Euler–Lagrange equation describes the equilibrium of the internal state. It is alternatively labeled a micro-momentum balance. It is derived by setting the second volume integral of the right in (86), equal to the term on the far right in (79), and then localizing, giving for any admissible variation $\delta(D^C)$:

$$\begin{aligned} \partial_A Z_C^A + \bar{\partial}_B Z_C^A \partial_A D^B + Z_C^B \Gamma_{AB}^A - Z_B^A K_{AC}^B - (Q_C - R_C) \\ = \alpha\psi C_{CA}^A - Z_A^B [\bar{\partial}_C N_B^A - \bar{\partial}_C K_{BD}^A D^D + \delta_C^A C_{ED}^D (\partial_B D^E + N_B^E)]. \end{aligned} \quad (88)$$

Natural boundary conditions on $\partial\mathcal{M}'$ are derived by setting the second-to-last and last boundary integrals in (86), equal to the remaining first and second boundary integrals, respectively, on the right side of (79), and localizing the results, yielding for any admissible variations, $\delta\varphi^a$ and $\delta(D^C)$,

$$p_a = P_a^A N_A, \quad z_A = Z_A^B N_B. \quad (89)$$

Remark 24. With natural boundary conditions (89) or $(\boldsymbol{\varphi}(X), \mathbf{D}(X))$ enforced along $X \in \partial\mathcal{M}'$ (i.e., essential conditions), and with the local force density vector $\mathbf{R}(X)$ for each $X \in \mathcal{M}'$, (87), and (88) collectively form $2n$ coupled PDEs in $2n$ degrees-of-freedom $x^a = \varphi^a(X)$ and $D^A(X)$. These apply at each $X \in \mathcal{M}'$, and extend to all $X \in \mathcal{M}$ where material exists.

Remark 25. Consider simplified cases when Riemannian metrics are used: null D dependence of \mathbf{G} and no dependence of \mathbf{g} on d . Then $\Gamma_{BC}^A = \gamma_{BC}^A$, $\Gamma_{bc}^a = \gamma_{bc}^a$, and $C_{BC}^A = 0$. The right side of (87) vanishes, so (87) is the classic equilibrium equation for continua without body force [22,23,33]. Also, taking N_B^A and K_{BC}^A independent of D , (88) is similar to equilibrium equations for gradient materials [108], including the phase-field theory [97,109].

Remark 26. Some prior work [55] set $G_{AB}(X, D)$ dependency in ψ , extending (82), and additional stress was obtained for the metric dependence on D instead of the implicit dependence via Q_A . The present approach is favored for brevity [54], but the former is admissible.

Proposition 1. Euler–Lagrange equations can be expressed in the following alternative way:

$$\partial_A P_a^A + \bar{\partial}_B P_a^A \partial_A D^B + P_a^B \gamma_{AB}^A - P_c^A \Gamma_{ba}^c F_A^b = -P_a^A C_{BC}^C \partial_A D^B, \quad (90)$$

$$\begin{aligned} \partial_A Z_C^A + \bar{\partial}_B Z_C^A \partial_A D^B + Z_C^B \gamma_{AB}^A - Z_B^A K_{AC}^B - (Q_C - R_C) \\ = \alpha\psi C_{CA}^A - Z_A^B (\bar{\partial}_C N_B^A - \bar{\partial}_C K_{BD}^A D^D + \delta_C^A C_{ED}^D \partial_B D^E). \end{aligned} \quad (91)$$

Proof. From (10) and (27),

$$\Gamma_{AB}^A = \Gamma_{BA}^A = \partial_B (\ln \sqrt{G}) - N_B^A \bar{\partial}_A (\ln \sqrt{G}) = \gamma_{BA}^A - N_B^A C_{AC}^C. \quad (92)$$

Substituting (92) with symmetry $\gamma_{BC}^A = \gamma_{CB}^A$ into (87) and (88) yields (90) and (91). \square

Remark 27. Notably, (90) and (91) show how the nonlinear connection terms N_B^A cancel, simplifying calculations. Nonlinear connection N_B^A still ultimately affects governing equations via influence

on $D_{|B}^A = \partial_B D^A - N_B^A + K_{BC}^A D^C$, thus affecting $Z_A^B = \partial\psi/\partial D_{|B}^A$, and through $\bar{\partial}_C N_B^A$ in (91). Spatial N_b^a can enter Γ_{bc}^a in (90). The linear connection K_{BC}^A and its gradient $\bar{\partial}_D K_{BC}^A$ in (91) are somewhat unique to the Finsler-geometric continuum mechanics. The emergence of C_{BA}^A , the trace of the tensor of Cartan, for all forms of these Euler–Lagrange equations, is also a distinctive feature. This term, of course, vanishes when G_{AB} is independent of D (i.e., a Riemannian rather than the Finslerian metric).

3.3.4. Spatial Invariance and Material Symmetry

First consider rotations of the spatial frame of reference, given by orthonormal transformation q_b^a in (40) whereby $\det(q_b^a) = 1$ and $\bar{q}_b^a = g^{ac} q_c^d g_{bd}$ (i.e., $q^{-1} = q^T$ [22]). Since $F \rightarrow qF$ under such coordinate changes, ψ in (82) should obey more restricted forms to maintain proper observer independence. Two possibilities are

$$\psi = \hat{\psi}[C(F, g), D, \nabla D, X] = \hat{\psi}(C_{AB}, D^A, D_{|B}^A, X^A), \tag{93}$$

$$\psi = \bar{\psi}[\bar{C}(F, \bar{g}), D, \nabla D, X] = \bar{\psi}(\bar{C}_{AB}, D^A, D_{|B}^A, X^A), \tag{94}$$

noting that (82) can be consistently expressed from (57), (58), (73), and (74), as

$$\psi(F, D, \nabla D, X) = \check{\psi}(F, D, \bar{G}(X), \hat{G}(D), \bar{g}(\varphi(X)), \hat{g}(\theta(X, D)), \nabla D, X). \tag{95}$$

From (66), (75), (93), and (94), the first Piola–Kirchhoff stress P_a^A of (85) is calculated using the chain rule:

$$P_a^A = \frac{\partial\psi}{\partial F_a^A} = 2g_{ab} F_B^b \frac{\partial\hat{\psi}}{\partial C_{AB}} = 2\bar{g}_{ab} F_B^b \frac{\partial\bar{\psi}}{\partial \bar{C}_{AB}}. \tag{96}$$

The resulting Cauchy stress tensors with spatial components σ^{ab} and $\bar{\sigma}^{ab}$ are symmetric in contravariant form, matching traditional conservation of angular momentum [20,22,33]:

$$\sigma^{ab} = \frac{1}{J} g^{ac} P_c^A F_A^b = \frac{2}{J} F_A^a F_B^b \frac{\partial\hat{\psi}}{\partial C_{AB}} = \sigma^{ba}, \quad \bar{\sigma}^{ab} = \frac{1}{\bar{J}} \bar{g}^{ac} P_c^A F_A^b = \frac{2}{\bar{J}} F_A^a F_B^b \frac{\partial\bar{\psi}}{\partial \bar{C}_{AB}} = \bar{\sigma}^{ba}. \tag{97}$$

Now consider changes in the material frame of reference, given by the transformation Q_B^A of (1) and (9) with inverse \bar{Q}_B^A . Under affine changes in coordinates $X^A \rightarrow Q_C^A X^A$, it follows that $dX^A \rightarrow Q_C^A dX^A$, $F_A^a \rightarrow \bar{Q}_C^A F_A^a$, $G_{AB} \rightarrow \bar{Q}_C^A \bar{Q}_D^B G_{AB}$, $C_{AB} \rightarrow \bar{Q}_C^A \bar{Q}_D^B C_{AB}$, $\bar{G}_{AB} \rightarrow \bar{Q}_C^A \bar{Q}_D^B \bar{G}_{AB}$, $\bar{C}_{AB} \rightarrow \bar{Q}_C^A \bar{Q}_D^B \bar{C}_{AB}$, $D^A \rightarrow Q_C^A D^A$, $\delta D^A \rightarrow Q_C^A \delta D^A$, and $D_{|B}^A \rightarrow Q_C^A \bar{Q}_D^B D_{|B}^A$. Energy densities ψ , $\hat{\psi}$, and $\bar{\psi}$ should be invariant under all transformations \bar{Q}_B^A (e.g., rotations, reflections, inversions) belonging to the symmetry group \mathbb{Q} of the material [33,61,81,110] (e.g., $\psi \rightarrow \psi$). The present focus is on polynomial invariants [81,110] with basis \mathcal{P} of invariant functions with respect to $\bar{Q} \in \mathbb{Q}$ and energy offsets $\hat{\psi}_0 = \text{constant}$, $\bar{\psi}_0 = \text{constant}$:

$$\hat{\mathcal{P}} = \{I_1, I_2, \dots, I_\nu\}; \quad I_\alpha = I_\alpha(C, D, \nabla D), \quad \hat{\psi} = \hat{\psi}(I_1, I_2, \dots, I_\nu, X) + \hat{\psi}_0; \tag{98}$$

$$\bar{\mathcal{P}} = \{\bar{I}_1, \bar{I}_2, \dots, \bar{I}_\zeta\}; \quad \bar{I}_\alpha = \bar{I}_\alpha(\bar{C}, D, \nabla D), \quad \bar{\psi} = \bar{\psi}(\bar{I}_1, \bar{I}_2, \dots, \bar{I}_\zeta, X) + \bar{\psi}_0. \tag{99}$$

The total number of applicable invariants is ν or ζ for (93) or (94). Stress of (96) becomes

$$P_a^A = 2g_{ab} F_B^b \sum_{\alpha=1}^{\nu} \hat{\psi}_\alpha \frac{\partial I_\alpha}{\partial C_{AB}} = 2\bar{g}_{ab} F_B^b \sum_{\alpha=1}^{\zeta} \bar{\psi}_\alpha \frac{\partial \bar{I}_\alpha}{\partial \bar{C}_{AB}}; \quad \hat{\psi}_\alpha = \frac{\partial\hat{\psi}}{\partial I_\alpha}, \quad \bar{\psi}_\alpha = \frac{\partial\bar{\psi}}{\partial \bar{I}_\alpha}. \tag{100}$$

Remark 28. A thorough and modern geometric treatment of material symmetry, uniformity, and homogeneity in continuous media is included in a recent monograph [111].

4. One-Dimensional Base Manifold

The framework of Sections 2 and 3 is applied for $n = 1$, a 1D base manifold \mathcal{M} . In Section 4.1, geometry and kinematics are presented, including assumptions that enable tractable solutions to several classes of boundary value problems while at the same time maintaining sufficient generality to address broad physical behaviors. The resulting 1D governing equations are derived in Section 4.2. General solutions are obtained for two problem classes in Section 4.3. Constitutive functions for soft biological tissue, namely a 1D strip of skin under axial extension, are given in Section 4.4. Model parameters and analytical solutions for 1D skin stretching and tearing are reported in Section 4.5.

4.1. Geometry and Kinematics

Let $X = X^1$. A reference domain $\{\mathcal{M} : X \in [-L_0, L_0]\}$ is considered, where the total length relative to a Euclidean metric is $2L_0$, and boundary $\partial\mathcal{M}$ is the endpoints $X = \pm L_0$. The referential internal state vector reduces to the single component $D = D^1$, which is assumed to have physical units, like X , of length. The spatial coordinate is $x = x^1$, and the spatial state component is $d = d^1$. A normalization constant (i.e., regularization length) l is introduced, and the physically meaningful domain for the internal state is assumed as $D \in [0, l]$. The associated order parameter is

$$\xi(X) = \frac{D(X)}{l} = \frac{d(\varphi(X))}{l}, \quad l > 0, \quad (101)$$

with a meaningful domain $\xi \in [0, 1]$, and where (68) and (70) are invoked. For generic f and h , differentiable in their arguments, let

$$f'(X) = \frac{df(X)}{dX}, \quad f''(X) = \frac{d^2f(X)}{dX^2}; \quad \dot{h}(\xi) = \frac{dh(\xi)}{d\xi}, \quad \ddot{h}(\xi) = \frac{d^2h(\xi)}{d\xi^2}. \quad (102)$$

For 1D manifolds, the following metrics apply from (73) and (74):

$$\begin{aligned} G_{11}(X, D) &= G(X, D) = \bar{G}(X)\hat{G}(D) = \hat{G}(D), \\ g_{11}(x, d) &= g(x, d) = \bar{g}(x)\hat{g}(d) = \hat{g}(d). \end{aligned} \quad (103)$$

Since $\bar{g} = \bar{G} = 1$ for isometric 1D Riemannian spaces, setting

$$\hat{g}(d(\varphi(X))) = \hat{G}(D(X)) \leftrightarrow g(\xi) = G(\xi) \quad (104)$$

renders \mathfrak{m} and \mathcal{M} isometric when $\phi(X) = X + c_0 \Leftrightarrow F(X) = 1$, regardless of local values of D, d , or ξ at corresponding points $x = \varphi(X)$.

Remark 29. This assumption (104), used in Section 4, may be relaxed in future applications to address residual stress (e.g., from growth [30]; see Appendix B), especially for $n = \dim \mathcal{M} > 1$.

Henceforth, in Section 4, the functional dependence on D or d is replaced with that on ξ . Then

$$D' = \frac{\xi'}{l}, \quad \frac{\partial f(X, D)}{\partial D} = \frac{1}{l} \frac{\partial f(X, \xi(D))}{\partial \xi}. \quad (105)$$

The following functional forms are assumed for the referential nonlinear connection N_B^A and linear connection K_{BC}^A , with $N_0 = \text{constant}$ and $\hat{K}(X)$ both dimensionless:

$$\begin{aligned} N_B^A &\rightarrow N_1^1 = N = -N_0 l \xi', \\ K_{BC}^A &\rightarrow K_{11}^1(X, \xi) = K(X, \xi) = \frac{\hat{K}(X)}{l \xi} \Rightarrow \bar{\partial}_1 K_{11}^1 D = -K_{11}^1. \end{aligned} \quad (106)$$

Spatial coefficients K_{bc}^a do not affect the governing equations and, thus, are left unspecified. Conditions (71) apply in 1D, leading to, with (101)–(106),

$$\Gamma_{BC}^A \rightarrow \Gamma_{11}^1 = \frac{1}{2G} \delta_1 G = \frac{1}{2G} (\partial_1 G - N_1^1 \bar{\partial}_1 G) = -N \bar{\partial}_1 (\ln \sqrt{G}) = -N C_{11}^1 = -N \frac{\chi}{l}, \quad (107)$$

$$\chi(\xi) = \frac{\dot{G}(\xi)}{2G(\xi)} = \frac{\dot{g}(\xi)}{2g(\xi)} = l C_{11}^1(\xi), \quad (108)$$

$$N_b^a \rightarrow \frac{N}{F} = -\frac{N_0 l \xi'}{F} = -N_0 l \frac{d\xi}{dx}, \quad \Gamma_{bc}^a \rightarrow -\frac{N}{F} \frac{\dot{g}}{2g} = -\frac{N}{F} \frac{\chi}{l}. \quad (109)$$

The deformation gradient, deformation tensor, Jacobian determinant, and director gradient are

$$F_A^a \rightarrow F_1^1 = F = \frac{d\varphi}{dX} = \varphi', \quad (110)$$

$$C_B^A \rightarrow C_1^1 = C = G^{11} g_{11} F_1^1 F_1^1 = F^2 = (\varphi')^2, \quad J = F = \sqrt{C};$$

$$D_{|B}^A \rightarrow D_{|1}^1 = \frac{dD}{dX} - N + KD = (1 + N_0) l \xi' + \hat{K}. \quad (111)$$

From (104), $\bar{C} = \bar{C}_1^1 = C_1^1 = C$ and $\bar{J} = J$ in 1D reductions of (75) and (76).

4.2. Governing Equations

A generic energy density is assigned and equilibrium equations are derived for the 1D case, given prescriptions of Section 4.1.

4.2.1. Energy Density

In 1D, C_{AB} consists of a single invariant C , and D^A and $D_{|B}^A$ likewise. Dependencies in (82) are suitably represented by F , ξ , and (ξ', X) with (101) and (111). Since $\bar{C} = C = F^2$, all energy densities ψ of (82) in (93)–(95) are expressed simply as

$$\psi = \psi(C, \xi, \xi', X). \quad (112)$$

Let μ_0 denote a constant, which is later associated with an elastic modulus, with units of energy density.

Remark 30. For comparison with data from experiments in the ambient Euclidean 3-space, μ_0 can be assigned units of energy per unit (3D) volume, such that $\Psi = \int_{\mathcal{M}} \psi d\Omega$ represents the energy per unit cross-sectional area normal to X . For a 1D \mathcal{M} , this cross-sectional area is, by definition, constant.

Denote by Y_0 a constant, related to surface energy, with units of energy per unit (2D fixed cross-sectional) area. Let W be the strain energy density and the Λ energy density associated with the microstructure. Let w denote a dimensionless strain energy function, y denote a dimensionless interaction function (e.g., later representing elastic degradation from microstructure changes), λ denote a dimensionless phase energy function, and ι denote a dimensionless gradient energy function assigned a quadratic form. Free energy density (112) is then prescribed in intermediate functional form, as follows:

$$\psi(C, \xi, \xi', X) = W(C, \xi) + \Lambda(\xi, \xi', X) = \frac{\mu_0}{2} w(C) y(\xi) + \frac{Y_0}{l} [\lambda(\xi) + \iota(\xi', X)], \quad (113)$$

$$\begin{aligned} \iota &= |D_{|1}^1|^2 - \hat{K}^2 = D_{|1}^1 G_{11} G^{11} D_{|1}^1 - \hat{K}^2 \\ &= [(1 + N_0) l \xi' + \hat{K}]^2 - \hat{K}^2, \quad (N_0 = \text{constant}, \hat{K} = \hat{K}(X)). \end{aligned} \quad (114)$$

Note that $\iota(0, X) = 0$. For null ground-state energy and stress, $\psi(1, 0, 0, X) = 0$ and $\frac{\partial \psi}{\partial C}(1, 0, 0, X) = 0$:

$$w(1) = 0, \quad \frac{dw}{dC}(1) = 0, \quad \frac{d^2w}{dC^2} \geq 0; \quad \lambda(0) = 0. \quad (115)$$

The third of (115) ensures the convexity of w . Thermodynamic forces originating in (85) are derived as

$$P = P_1 = \frac{\partial \psi}{\partial F} = 2 \frac{g}{G} F \frac{\partial \psi}{\partial C} = 2 \sqrt{C} \frac{\partial \psi}{\partial C} = \mu_0 y \sqrt{C} \frac{dw}{dC}, \quad (116)$$

$$Q = Q_1 = \frac{\partial \psi}{\partial D} = \frac{1}{l} \frac{\partial \psi}{\partial \zeta} = \frac{\mu_0}{2l} w \frac{dy}{d\zeta} + \frac{Y_0}{l^2} \frac{d\lambda}{d\zeta} = \frac{Y_0}{l^2} (A_0 w y + \lambda), \quad A_0 = \frac{\mu_0 l}{2Y_0}, \quad (117)$$

$$Z = Z_1 = \frac{\partial \psi}{\partial D_{|1}^1} = \frac{Y_0}{l} \frac{\partial \iota}{\partial D_{|1}^1} = 2 \frac{Y_0}{l} D_{|1}^1 = 2 \frac{Y_0}{l} [(1 + N_0) l \zeta' + \hat{K}]. \quad (118)$$

The volumetric source term in (78) is prescribed as manifesting from changes in energy density, proportional to changes in the local referential volume form (e.g., physically representative of local volume changes from damage/tearing, similar to the effects of tissue growth on energy (Appendix B)):

$$R = R_1 = \beta \psi \bar{\delta}_1(\ln \sqrt{G}) = \frac{\beta}{l} \psi \chi, \quad (\beta = \text{constant}). \quad (119)$$

4.2.2. Linear Momentum

The macroscopic momentum balance, (87) or (90) is, upon the use of relations in Sections 4.1 and 4.2.1,

$$\frac{dP}{dX} = P(N_0 - 1) \chi \frac{d\zeta}{dX} = -(1 - N_0) \frac{P}{2G} \frac{dG}{dX}. \quad (120)$$

This separable ordinary differential equation (ODE) of the first order is integrated directly:

$$\int_{P_0}^P d(\ln P) = -(1 - N_0) \int_{G_0}^G d(\ln \sqrt{G}) \Rightarrow P = P_0 \left(\sqrt{G_0/G} \right)^{1-N_0}. \quad (121)$$

The integration limit on $G(\zeta(X))$ is $G_0 = G(0)$, and P_0 is a constant stress linked to $\zeta = 0$.

Remark 31. If G is Riemannian, then $G = G_0$ and $P = P_0 = \text{constant}$. In the Finslerian setting, P can vary with X if ζ varies with X , and N_0 differs from unity. However, if P vanishes on $\partial \mathcal{M}$ (i.e., at $X = \pm L_0$), then $P_0 = 0$ necessarily, so $P(X) = 0 \forall X \in \mathcal{M}$, meaning this 1D domain cannot support residual stress. The same assertion applies when (104) is relaxed and N_0 vanishes.

From (116) and (121), when μ_0 is nonzero,

$$\sqrt{C(X)} \frac{dw(C(X))}{dC} y(\zeta(X)) \left[\frac{G(\zeta(X))}{G_0} \right]^{(1-N_0)/2} = \frac{P_0}{\mu_0} = \text{constant}, \quad (122)$$

where the value of P_0 , constant for a given static problem, depends on the boundary conditions.

4.2.3. Micro-Momentum

Define $\bar{K}(X) = l\hat{K}(X)$. Then upon use of relations in Sections 4.1 and 4.2.1, and dividing by $2Y_0(1 + N_0)$, the microscopic momentum balance, as expressed in (88) or (91), is

$$\begin{aligned} & \frac{d^2\zeta}{dX^2} + \chi(\zeta) \left[1 - \frac{(1 + N_0)(\alpha - \beta)}{2} \right] \left(\frac{d\zeta}{dX} \right)^2 + \frac{\bar{K}(X)}{l^2} \chi(\zeta) \left[\frac{1}{1 + N_0} - (\alpha - \beta) \right] \frac{d\zeta}{dX} \\ & + \frac{d\bar{K}(X)}{dX} \frac{1}{l^2(1 + N_0)} - \frac{1}{2l^2(1 + N_0)} \left[\frac{d\lambda(\zeta)}{d\zeta} + (\alpha - \beta)\chi(\zeta)\lambda(\zeta) \right] \\ & = \frac{A_0w(C(X))}{2l^2(1 + N_0)} \left[\frac{dy(\zeta)}{d\zeta} + (\alpha - \beta)\chi(\zeta)y(\zeta) \right]. \end{aligned} \tag{123}$$

This is a nonlinear and non-homogeneous second-order ODE with variable coefficients. General analytical solutions are not feasible. However, the following assumption is made in Section 4 to reduce the nonlinearity (second term on the left side) and render some special solutions possible:

$$\beta = \alpha - 2/(1 + N_0). \tag{124}$$

Remark 32. Assumption (124) generalizes, yet is consistent with, physically realistic choices for fractures, shear bands, cavitation, and phase transitions [55,56,62]: $\alpha = 2, \beta = 0, N_0 = 0$.

Applying (124) with notations of (102), (123) reduces to the form studied in the remainder of Section 4:

$$l^2(1 + N_0)\zeta'' - \frac{\lambda}{2} - \frac{\chi\lambda}{1 + N_0} - \bar{K}\chi\zeta' + \bar{K}' = \frac{A_0w}{2} \left[\dot{y} + \frac{2\chi y}{1 + N_0} \right]. \tag{125}$$

This is a linear second-order ODE, albeit generally non-homogeneous with variable coefficients. For the special case that $Y_0(1 + N_0) = 0$, terms on the left of (123) all vanish, and equilibrium demands

$$\mu_0w(C(X)) \left[\frac{dy(\zeta)}{d\zeta} + \frac{2\chi(\zeta)y(\zeta)}{1 + N_0} \right] = 0. \tag{126}$$

4.3. General Solutions

4.3.1. Homogeneous Fields

Consider cases wherein $\zeta(X) \rightarrow \zeta_H = \text{constant} \forall X \in [-L_0, L_0]$. Assign the notation $f_H(X) = f(X, \zeta_H)$. Then stress and momentum conservation in (116) and (121) combine to

$$P_H = \mu_0\sqrt{C} \frac{dw}{dC} y_H = P_0 \left(\frac{G_0}{G_H} \right)^{(1-N_0)/2} = \text{constant}. \tag{127}$$

If μ_0, y_H , and dw/dC are nonzero, the convexity of w suggests $C = C_H = F_H^2 = \text{constant}$. Accordingly, $\varphi_H(X) = F_H X + c_0$. If $\mu_0 = 0, y_H = 0$, or $dw/dC = 0$, then $P_H = 0$, and $\varphi_H(X)$ is arbitrary. Assume now that none of the former are zero, such that $F = F_H, C = C_H, w = w_H = w(C_H)$ are constants. Then equilibrium Equation (125), with $\bar{K}'_H = K'_0$, becomes a dimensionless constant:

$$-\frac{\lambda_H}{2} - \frac{\chi_H\lambda_H}{1 + N_0} + K'_0 = \frac{A_0w_H}{2} \left[\dot{y}_H + \frac{2\chi_H y_H}{1 + N_0} \right]. \tag{128}$$

Remark 33. If φ_H is imposed by displacement boundary conditions, then C_H is known, as is w_H . In that case, (128) is an algebraic equation that can be solved implicitly for ζ_H , the value of which is substituted into (127) for stress P_H . If P_H is imposed by traction boundary conditions, then (127) and (128) are to be solved simultaneously for C_H and ζ_H .

4.3.2. Stress-Free States

Now consider cases wherein $P = 0 \forall X \in [-L_0, L_0]$. Relation (120) is trivially satisfied. Assume μ_0 is nonzero. Then (122) requires, since $C > 0$, $G > 0$,

$$\frac{dw(C(X))}{dC} y(\zeta(X)) = 0. \quad (129)$$

This is obeyed for any $y(\zeta)$ at $C = 1$ (i.e., rigid-body motion) via (115). Assume further that $w = 0$, again satisfied at $C = 1$ via (115). Then the right side of (125) vanishes, leaving

$$\zeta'' - \frac{\bar{K}\chi}{l^2(1+N_0)} \zeta' - \frac{\dot{\lambda}}{2l^2(1+N_0)} - \frac{\chi\lambda}{l^2(1+N_0)^2} + \frac{\bar{K}'}{l^2(1+N_0)} = 0, \quad (130)$$

with functional dependencies $\zeta(X)$, $\chi(\zeta)$, $\bar{K}(X)$, and $\lambda(\zeta)$. The ODE is linear or nonlinear depending on forms of λ and χ ; analytical solutions can be derived for special cases.

If $\bar{K} = \text{constant}$, (130) is autonomous. If $\bar{K} = 0$, then (130) is

$$\frac{d^2\zeta}{dX^2} = \zeta \frac{d\zeta}{d\zeta} = \frac{1}{2l^2(1+N_0)} \left[\frac{d\lambda}{d\zeta} + \frac{2\chi(\zeta)\lambda(\zeta)}{1+N_0} \right], \quad (131)$$

where $\zeta = \zeta' \Rightarrow \zeta'' = \zeta d\zeta/d\zeta$. The right equation can be separated and integrated as

$$\begin{aligned} \frac{1}{2}\zeta^2 &= \frac{1}{2l^2(1+N_0)} \int \left[\frac{d\lambda}{d\zeta} + \frac{2\chi(\zeta)\lambda(\zeta)}{1+N_0} \right] d\zeta + c_1 \\ \Rightarrow \frac{d\zeta}{dX} &= \pm \frac{1}{l\sqrt{1+N_0}} \left(\int \left[\frac{d\lambda}{d\zeta} + \frac{2\chi(\zeta)\lambda(\zeta)}{1+N_0} \right] d\zeta + c_1 \right)^{1/2}. \end{aligned} \quad (132)$$

This first-order ODE can be separated and solved for $\zeta = \arg[X(\zeta)]$, where

$$X(\zeta) = \pm l\sqrt{1+N_0} \int \frac{d\zeta}{\left\{ \int \left[\frac{d\lambda}{d\zeta} + \frac{2\chi(\zeta)\lambda(\zeta)}{1+N_0} \right] d\zeta + c_1 \right\}^{1/2}} + c_2. \quad (133)$$

Integration constants are c_1 and c_2 , determined by boundary conditions.

Now allow arbitrary $\bar{K}(X)$ but restrict $\chi = 0$ (e.g., $G = G_0$). Assume $\lambda(\zeta)$ is quadratic, such that $\dot{\lambda} = 2\omega_0 + 2\omega_1\zeta$. Now (130) is linear:

$$\frac{d^2\zeta}{dX^2} - \frac{\omega_1}{l^2(1+N_0)} \zeta = \frac{1}{l^2(1+N_0)} \left(\omega_0 - \frac{d\bar{K}}{dX} \right). \quad (134)$$

This ODE is non-homogeneous but has constant coefficients. Assume $\omega_1 > 0$ and $N_0 > -1$. Then

$$\zeta(X) = c_1 \exp \left[(X/l) \sqrt{\omega_1/(1+N_0)} \right] + c_2 \exp \left[-(X/l) \sqrt{\omega_1/(1+N_0)} \right] + \zeta_p(X), \quad (135)$$

where c_1 and c_2 are new constants and ζ_p is the particular solution from ω_0 and $\bar{K}(X) = l\dot{K}(X)$.

4.4. Constitutive Model

The framework is applied to a strip of skin loaded in the tension along the X direction.

Remark 34. A 1D theory cannot distinguish between uniaxial strain conditions, uniaxial stress conditions, or anisotropy. Thus, parameters entering the model (e.g., μ_0 , Y_0) are particular to those loading conditions and material orientations from experiments to which they are calibrated (e.g., uniaxial stress along a preferred fiber direction).

The nonlinear elastic potential of Section 4.4.2 is specialized to 1D in the context of a 3D model [71,82,83,92]. The internal structure variable $\xi = D/l$ accounts for local rearrangements that lead to softening and degradation under the tensile load [72–74,77]: fiber sliding, pull-out, and breakage of collagen fibers, as well as the rupture of the elastin fibers and ground matrix.

Remark 35. Specifically, D is a representative microscopic sliding or separation distance among microstructure constituents, and l is the value of this distance at which the material can no longer support the tensile load. In the context of cohesive theories of the fracture [73,112,113], D can be interpreted as a crack-opening displacement.

Remark 36. Some physics represented by the present novel theory, not addressed by nonlinear elastic-continuum damage [73,90] or phase-field [95,114] approaches, are summarized as follows. The Finslerian metrics $G(\xi) = g(\xi)$ account for local rescaling of material and spatial manifolds \mathcal{M} and \mathfrak{m} due to microstructure changes (e.g., expansion due to tearing or cavitation). A nonlinear connection N_0 rescales the quadratic contribution of the gradient of ξ to the surface energy by a constant, and the linear connection \hat{K} rescales the linear contribution of the gradient of ξ to surface energy by a continuous and differentiable function of X , enabling a certain material heterogeneity.

4.4.1. Metrics

From (16), (48), (66), (103), (104), and (110), the difference in squared lengths of line elements dx and dX is

$$(|dx|^2 - |dX|^2)(C, \xi) = G(\xi)(C - 1)dX dX. \quad (136)$$

Herein, the metric is assigned an exponential form that is frequent in generalized Finsler geometry [7,55] and Riemannian geometry [27,30]:

$$G(\xi) = \exp\left(\frac{2k}{r}\xi^r\right) \Rightarrow \chi(\xi) = \frac{\dot{G}}{2G} = \frac{\dot{g}}{2g} = k\xi^{r-1}. \quad (137)$$

For $\xi \in [0, 1]$, two constants are k , which is positive for expansion, and $r > 0$.

Remark 37. Local regions of \mathcal{M} at X and \mathfrak{m} at $x = \varphi(X)$ are rescaled isometrically by $G(\xi(X))$. Physically, this rescaling arises from changes in structure associated with degradation, to which measure $\frac{1}{2} \ln G(\xi)$ is interpreted as a contributor to remnant strain. For Riemannian metrics, $G = \bar{G} = \bar{g} = g = 1$, in which case (136) is independent of ξ and this remnant strain always vanishes.

The ratio of constants is determined by the remnant strain contribution at failure: $\hat{\epsilon} = \frac{k}{r} = \frac{1}{2} \ln G(1)$. Since $\xi \in [0, 1]$, a smaller r at a fixed $\frac{k}{r}$ gives a sharper increase in $\frac{1}{2} \ln G$ versus ξ ; values of k and r are calibrated to data in Section 4.5; choices of N_0 and \bar{K} are explored parametrically therein. Nonlinear connection $N_0 = \text{constant}$ and linear connection $\hat{K}(X) = \bar{K}(X)/l$ affect the contribution of the state gradient ξ' to surface energy ι via (113) and (114). Constraint $N_0 > -1$ is applied to avoid model singularities and encompass the trivial choice $N_0 = 0$. The value of N_0 uniformly scales the contribution of $(\xi')^2$ to ι and ψ . Function \hat{K} scales, in a possibly heterogeneous way, the contribution of ξ' to ι and ψ . Even when ξ' vanishes, N_0 and \bar{K} can affect solutions.

4.4.2. Nonlinear Elasticity

Strain energy density W in (113) is dictated by the normalized (dimensionless) function $w(C)$:

$$w(C) = (\sqrt{C} - 1)^2 + \frac{a_1}{2b_1} \left[\exp\{b_1(C - 1)^2\} - 1 \right], \quad (138)$$

where dimensionless constants are $a_1 \geq 0$ and $b_1 > 0$, and $\mu_0 > 0$ is enforced along with $Y_0 > 0$ in (113). This adapts prior models for collagenous tissues [71,82,83,92] to the 1D case. The first term on the right, linear in C , accounts for the ground matrix and elastin. The second (exponential) term accounts for the collagen fibers, which, in the absence of damage processes, stiffen significantly at large C . Such stiffening is dominated by the parameter b_1 , whereas a_1 controls the fiber stiffness at a small stretch $\sqrt{C} \approx 1$ [71].

The elastic degradation function $y(\xi)$ and independent energy contribution $\lambda(\xi)$ in (113) are standard from phase-field theories [95,114], where $\vartheta \in [0, \infty)$ is a constant with $\vartheta = 2$ typical for brittle fracture and $\vartheta = 0 \mapsto y = 1$ for purely elastic response:

$$y(\xi) = (1 - \xi)^\vartheta, \quad \dot{y}(\xi) = -\vartheta(1 - \xi)^{\vartheta-1}; \quad \lambda(\xi) = \xi^2, \quad \dot{\lambda}(\xi) = 2\xi. \quad (139)$$

When $\vartheta > 0$, $y(1) = 0$, no strain energy W or tensile load P is supported at X when $D(X) = l$. Verification of (115) for prescriptions (138) and (139) is straightforward [81,82]. Stress P , which is conjugate to $F = \sqrt{C}$, and force Q , which is conjugate to $D = l\xi$, are from (116), (117), (138), and (139):

$$P(C, \xi) = \mu_0(1 - \xi)^\vartheta \left[(\sqrt{C} - 1) + a_1\sqrt{C}(C - 1)\exp\{b_1(C - 1)^2\} \right], \quad (140)$$

$$Q(C, \xi) = \frac{2Y_0}{l^2} \left[\xi - \frac{A_0\vartheta}{2}(1 - \xi)^{\vartheta-1} \left((\sqrt{C} - 1)^2 + \frac{a_1}{2b_1} \left[\exp\{b_1(C - 1)^2\} - 1 \right] \right) \right]. \quad (141)$$

Remark 38. Ideal elasticity (i.e., no structure-mediated metric variation or degradation) is obtained when $k = 0 \Rightarrow G = 1 \Rightarrow \chi = 0$, $\vartheta = 0 \Leftrightarrow y = 1 \Rightarrow \dot{y} = 0$, and $\bar{K}' = 0$. In this case, as $\dot{\lambda}(0) = 0$ by (139), trivial solutions to (121) and (123) are $P(X) = P_0 = \text{constant}$, $\xi(X) = 0 \forall X \in \mathcal{M}$.

4.5. Specific Solutions

Inputs to the model are nine constants $l > 0$, $k, r > 0$, $N_0 > -1$, $\mu_0 > 0$, $a_1 \geq 0$, $b_1 > 0$, $\vartheta \geq 0$, $Y_0 > 0$, and the function $\bar{K}(X)$. These are evaluated for stretching and tearing of skin [73,74,113] by applying the constitutive model of Section 4.4 to the general solutions derived in Section 4.3.

4.5.1. Homogeneous Fields

Here, the skin specimen is assumed to degrade homogeneously in a gauge section of initial length $2L_0$ (i.e., diffuse damage), an idealization fairly characteristic of certain experiments [63,68,72,74,87]. As per Section 4.3.1, assume deformation control, with $F = F_H = \sqrt{C_H} \geq 1$ increased incrementally from unity. The analytical solution for $\xi = \xi_H$ is then the implicit solution of (128) upon substituting (137)–(139), here for $\vartheta > 0$:

$$\begin{aligned} \xi_H + [k/(1 + N_0)]\xi_H^{1+r} &= \frac{1}{2}A_0\vartheta(1 - \xi_H)^{\vartheta-1} \{ (\sqrt{C_H} - 1)^2 + [a_1/(2b_1)] \\ &\times [\exp\{b_1(C_H - 1)^2\} - 1] \} \{ 1 - 2k\xi_H^{r-1}(1 - \xi_H)/[(1 + N_0)\vartheta] \} + K'_0. \end{aligned} \quad (142)$$

This dimensionless solution does not depend on μ_0 , Y_0 , or l individually, but only on the dimensionless ratio $A_0 = \frac{\mu_0 l}{2Y_0}$. However, stress $P_H = P(C_H, \xi_H)$ is found from (140), which depends on μ_0 . The value of μ_0 is comparable to the low-stretch tensile modulus in some experiments [71,75], acknowledging significant variability in the literature.

Stress P is shown in Figure 2a, first assuming $N_0 = 0$ and $K'_0 = 0$ for simplicity. The Finsler model, with $A_0 = 8.5 \times 10^{-2}$, corresponding to baseline parameters given in Table 1, successfully matches experimental data [74]. Stretch corresponding to Figure 5e in the referenced experimental work [74] is defined as engineering strain plus 1.2 here in Figure 2a of Section 4.5.1 and similarly later in Section 5.5.1 to account for pre-stress (≈ 0.7 MPa) and pre-strain (≈ 0.2). Thus $\sqrt{C} = 1$ consistently for stress-free reference states among models and experiments. Stress-free states at null strain are consistent with the data in Figure 3a of the same referenced external work [74]. Alternatively, $2\frac{\sigma_0}{\mu_0}(\sqrt{C} - 1)$,

with $\sigma_0 = \text{constant}$, can be added to w of (138) giving a pre-stress of $P_{(C=1, \zeta=0)} = \sigma_0$ to fit data with pre-stress. This, however, would require relaxation of the second of (115).

Remark 39. *The ideal elastic solution ($\zeta = 0$) is shown for comparison. Excluding structure evolution corresponding to collagen fiber rearrangements, sliding, and breakage, the model is too stiff relative to the data for which such microscopic mechanisms have been observed [74]. The ideal elastic model is unable to replicate the linearizing, softening, and failure mechanisms with increasing stretch \sqrt{C} reported in experiments on the skin and other soft tissues [63,64,68,74,87].*

In Figure 2b, the effects of ϑ on P are revealed for $\hat{\epsilon} = 0.1, r = 2, N_0 = 0,$ and $K'_0 = 0,$ noting $\vartheta = 0$ produces the ideal nonlinear elastic solution $\zeta_H = 0$ in (142). Peak stress increases with decreasing ϑ ; the usual choice from phase-field theory $\vartheta = 2$ provides close agreement with data in Figure 2a. In Figure 2c, the effects of Finsler metric scaling factors $\hat{\epsilon} = \frac{k}{r}$ and r on stress P are demonstrated, where, at fixed $r,$ peak stress increases (decreases) with increasing (decreasing) $\hat{\epsilon}$ and $k.$ Baseline choices $\hat{\epsilon} = 0.1$ and $r = 2$ furnish agreement with the experiment in Figure 2a. A remnant strain of 0.1 is of the same order of magnitude observed in cyclic loading experiments [72,78]. Complementary effects on the evolution of the structure versus stretch are shown in Figure 2e: modest changes in ζ produce significant changes in $P.$ In Figure 2d, the effects of connection coefficients N_0 and K'_0 are revealed, holding material parameters at their baseline values in Table 1. For this homogeneous problem, maximum P decreases with increasing N_0 and $K'_0.$ The corresponding evolution of ζ is shown in Figure 2f. When $K'_0 < 0,$ a viable solution $\zeta_H \in [0, 1]$ exists only for $\sqrt{C} > 1.$

The total energy per unit cross-sectional area of the specimen is $\bar{\Psi},$ found upon integration of $\psi(C_H, \zeta_H)$ in (113) on \mathcal{M} with the local element of volume $dV = \sqrt{G(\zeta_H)} dX:$

$$\frac{\bar{\Psi}}{L_0} = \mu_0 \left[(1 - \zeta_H)^\vartheta \{ (\sqrt{C_H} - 1)^2 + \frac{a_1}{2b_1} [\exp\{b_1(C_H - 1)^2\} - 1] \} + \frac{\zeta_H^2}{A_0} \right] \times \exp\left(\frac{k}{r} \zeta_H^r\right). \tag{143}$$

Table 1. Baseline model parameters for rabbit skin tissue: 1D and 2D theories.

| Parameter | Units | Definition | Value (1D) | Value (2D) |
|----------------|--------------------|--|------------|------------|
| l | mm | length scale | 0.04 | 0.04 |
| k | ... | metric scaling factor | 0.2 | 0.2 |
| m | ... | metric scaling factor | ... | 0.3 |
| r | ... | metric scaling exponent | 2 | 2 |
| μ_0 | N/mm ² | shear modulus (axial 1D) | 0.2 | 0.2 |
| κ_0 | N/mm ² | bulk modulus ($\kappa_0 = k_0\mu_0$) | ... | 1.2 |
| a_1 | ... | nonlinear elastic constant | 2.8 | 2.8 |
| a_2 | ... | nonlinear elastic constant | ... | 6 |
| b_1 | ... | nonlinear elastic constant | 0.055 | 0.055 |
| b_2 | ... | nonlinear elastic constant | ... | 0.17 |
| ϑ | ... | degradation exponent | 2 | 2 |
| ζ | ... | degradation exponent | ... | 2 |
| Υ_0 | mJ/mm ² | isotropic surface energy | 0.47 | 0.47 |
| γ_ζ | ... | anisotropic energy factor | ... | 1 |
| γ_η | ... | anisotropic energy factor | ... | 0.84 |

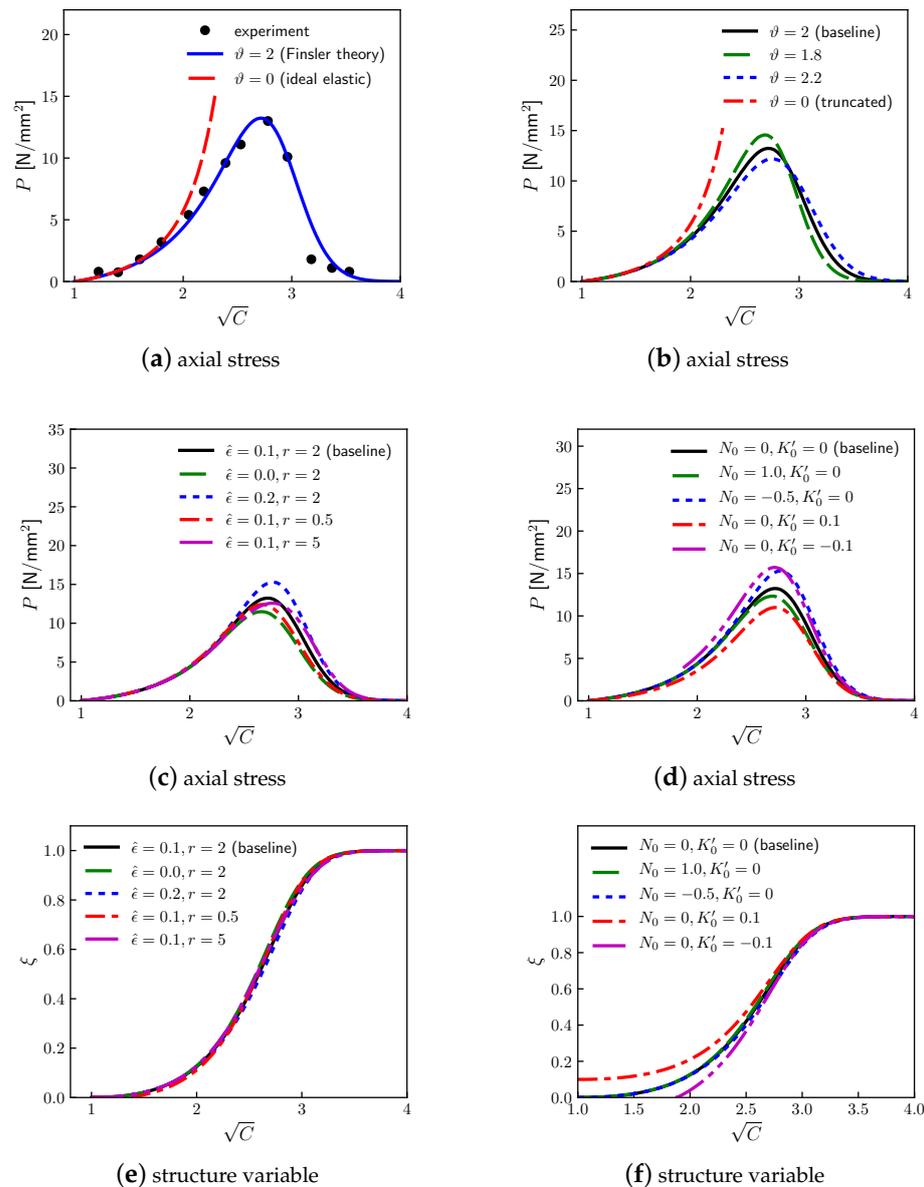


Figure 2. Extension and tearing of skin for the imposed axial stretch ratio \sqrt{C} , 1D model: (a) stress P comparison with data [74] (see text Section 4.5.1 for the definition of experimental stretch ratio) of Finsler model (baseline) and ideal nonlinear elasticity (null structure change) (b) effect on stress P of energy degradation exponent ϑ with $\hat{\epsilon} = 0.1$, $r = 2$, $N_0 = 0$, and $K'_0 = 0$ (c) effect on stress P of Finsler metric scaling $\hat{\epsilon} = \frac{k}{r}$ and r with $\vartheta = 2$, $N_0 = 0$, and $K'_0 = 0$ (d) effect on stress P of nonlinear connection N_0 and linear connection K'_0 with $\vartheta = 2$, $\hat{\epsilon} = 0.1$, and $r = 2$ (e) effect on the internal structure $\zeta = D/l$ of Finsler metric scaling $\hat{\epsilon} = \frac{k}{r}$ and r with $\vartheta = 2$, $N_0 = 0$, and $K'_0 = 0$ (f) effect on the internal structure $\zeta = D/l$ of nonlinear connection N_0 and linear connection K'_0 with $\vartheta = 2$, $\hat{\epsilon} = 0.1$, and $r = 2$.

4.5.2. Stress-Free States

The stress-free solutions of Section 4.3.2 are applied to evaluate the remaining unknown parameters l and Y_0 , given μ_0 and A_0 from Section 4.5.2. Assume the specimen tears completely at its midpoint at $X = 0$, such that $\zeta(0) = 1$. No load is supported anywhere, and only rigid body motion is possible at other locations X where $\zeta(X) > 0$. Assume the specimen is clamped at its ends where it is gripped, such that $\zeta(-L_0) = \zeta(L_0) = 0$. Symmetry conditions $\zeta(-X) = \zeta(X)$ are imposed, with $\zeta'(0)$ discontinuous, such that a solution needs to be calculated only for the half-space $X \in [0, L_0]$.

First, let $\bar{K} = l\hat{K} = 0$, so that (133) holds. Assume $c_1 = 0$ corresponding to $\bar{\zeta}' = 0$ where $\bar{\zeta} = 0$ since the anti-derivative in (132) vanishes at $\bar{\zeta} = 0$ when $\lambda = \bar{\zeta}^2$, $\chi = k\bar{\zeta}^{r-1}$, $r > 0$. It is verified a posteriori [55,59,62] that this closely approximates true boundary conditions $\bar{\zeta}(\pm L_0) = 0$ as well as $\bar{\zeta}'(\pm L_0) = 0$ for $L_0 \gg l$. Then the physically valid (negative) root for the half-domain giving $X \geq 0$ in (133) becomes, with (137) and (139),

$$\frac{X(\bar{\zeta})}{L_0} = -\frac{l}{L_0} \sqrt{1+N_0} \int_{z=1}^{z=\bar{\zeta}} \frac{dz}{z\sqrt{1+2kz^r/[(1+N_0)(2+r)]}}. \quad (144)$$

The lower limit follows from $X(1) = 0$, obviating c_2 in (133). Analytical solution $\bar{\zeta} = \arg X(\bar{\zeta})$ is exact, but it is most easily evaluated by quadrature when k is nonzero, decrementing z from 1 to 0 in small negative steps. The profile of $\bar{\zeta}(X)$ depends on X/L_0 and l/L_0 , but not l or L_0 individually.

Remark 40. This new 1D solution, (144), agrees with more specific solutions derived in past work: $N_0 = 0$ and $r = 1$ [55,56] with slight correction [59] and $N_0 = 0$ and $r = 2$ [59].

Normalized surface energy per two-sided cross-sectional area, $\bar{\gamma}$, is obtained by integration of $\psi = \Lambda$ in (113) over \mathcal{M} :

$$\begin{aligned} \bar{\gamma} &= \frac{1}{2Y_0} \int_{-L_0}^{L_0} \psi \sqrt{G} dX \\ &= \frac{1}{2l} \int_{-L_0}^{L_0} \{\bar{\zeta}^2 + (1+N_0)l\bar{\zeta}'[2\hat{K} + (1+N_0)l\bar{\zeta}']\} \exp[(k/r)\bar{\zeta}^r] dX. \end{aligned} \quad (145)$$

This energy likewise depends on l/L_0 but not l or L_0 individually. Baseline values of k and r are now taken from Table 1. The solution (144) is shown for $N_0 = 0$ and different l/L_0 in Figure 3a. The smaller (larger) the regularization length ratio l/L_0 , the sharper (more diffuse) the zone centered at the midpoint of the domain over which prominent structure changes occur.

The normalized energy density (145) is shown in Figure 3b versus l/L_0 for several N_0 . Increasing N_0 increases this energy, as might be anticipated from (113) with (114) when $\hat{K} = 0$. A stress-free ruptured state is energetically favorable to a stressed homogeneous state (§4.5.1) from applied deformation C_H when $\bar{\Psi} > 2\bar{\gamma}Y_0$, with $\bar{\Psi}$ given by (143). The ratio $\bar{\Psi}/(2\bar{\gamma}Y_0)$ is shown in Figure 3c versus $\sqrt{C} = \sqrt{C_H}$ with $l/L_0 = 10^{-2}$ and several N_0 , recalling $K'_0 = 0$. Increasing N_0 increases $\bar{\gamma}$, reducing $\bar{\Psi}/(2\bar{\gamma}Y_0)$. For cases in Figure 3a–c, $\bar{\zeta}(\pm L_0) < 10^{-8}$ and $|l\bar{\zeta}'(\pm L_0)| < 10^{-8}$ are observed for $l/L_0 \leq 0.03$, verifying $c_1 = 0$ in (133) and (144) under this length constraint.

The remaining parameters l and Y_0 are now quantified. To match the measured energy release rate J_C (i.e., toughness) of skin, $2\bar{\gamma}Y_0 \approx J_C$. Let $L_0 = 4$ mm, the span of specimens [74] whose data are represented in Figure 2a. Then $l/L_0 = 10^{-2} \Rightarrow l = 40 \mu\text{m}$ is more than sufficiently small to adhere to the aforementioned boundary constraints (i.e., $c_1 = 0$) while providing a damage profile of intermediate diffusivity in Figure 3a. This value of l then gives $Y_0 = \frac{\mu_0 l}{2A_0} = 0.47 \text{ kJ/m}^2$ (Table 1).

Remark 41. Along with the choice $N_0 = 0$, the Finsler model with the full set of baseline parameters in Table 1 produces $\bar{\gamma} \approx 1$ in Figure 3b and $2\bar{\gamma}Y_0 = 1.0 \text{ kJ/m}^2$, in concurrence with experimental data: $0.5 \lesssim J_C \lesssim 2.5 \text{ kJ/m}^2$ [73,99,113]. Value $l = 40 \mu\text{m}$ is between $4 \times$ and $40 \times$ the collagen fiber diameter [68,69,74]. Although not shown in Figure 3b, increasing $\hat{\epsilon} = \frac{k}{r}$ from 0.1 to 0.2 at $\vartheta = r = 2$ with $N'_0 = K'_0 = 0$ and $l/L_0 = 10^{-2}$ increases effective toughness to $2\bar{\gamma}Y_0 = 1.02 \text{ kJ/m}^2$. Under the same conditions, reducing $\hat{\epsilon}$ to 0 diminishes the predicted toughness to $2\bar{\gamma}Y_0 = 0.94 \text{ kJ/m}^2$.

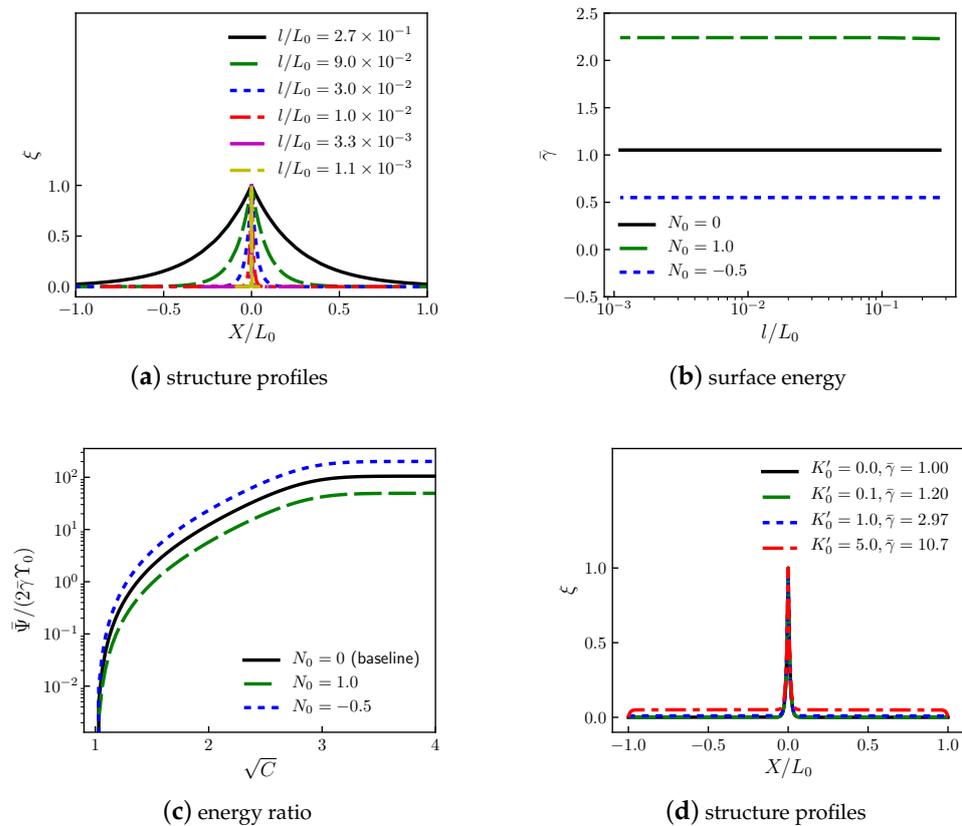


Figure 3. Extension and tearing of skin, 1D model: (a) Stress-free solution for the internal state profile (baseline parameters, $N_0 = 0$); (b) Normalized surface energy for rupture versus regularization length; (c) Ratio of homogeneous energy to energy for stress-free localized rupture; (d) Stress-free solution, $\hat{\epsilon} = 0$, $l/L_0 = 10^{-2}$, heterogeneous connection $\bar{K}(X)$.

Finally, let $k = 0$ but permit nonzero $\bar{K}(X) = l\hat{K}(X)$, such that (135) applies. As an example, let $\bar{K} = -K'_0 l \cdot (1 - X/L_0)$ for $X \in [0, L_0]$ and $\bar{K} = K'_0 l \cdot (1 + X/L_0)$ for $X \in [-L_0, 0]$. Boundary conditions $\bar{\zeta}(0) = 1$ and $\bar{\zeta}(\pm L_0) = 0$ still apply, as does symmetry relation $\bar{\zeta}(X) = \bar{\zeta}(-X)$. From (139), $\omega_1 = 1$ and $\omega_0 = 0$. For the whole domain $X \in [-L_0, L_0]$, $\bar{K}' = K'_0 l/L_0 = \text{constant}$, and simply $\bar{\zeta}_p = K'_0 l/L_0$. Then (135) gives

$$\begin{aligned} \bar{\zeta}(X) &= c_1 \exp[X/\{l\sqrt{1+N_0}\}] + c_2 \exp[-X/\{l\sqrt{1+N_0}\}] + K'_0 l/L_0, \\ c_1 &= 1 - c_2 - K'_0 l/L_0 = \frac{-K'_0 l/L_0 - [1 - K'_0 l/L_0] \exp[-L_0/\{l\sqrt{1+N_0}\}]}{\exp[L_0/\{l\sqrt{1+N_0}\}] - \exp[-L_0/\{l\sqrt{1+N_0}\}]} \end{aligned} \tag{146}$$

Profiles of $\bar{\zeta}(X)$ are shown in Figure 3d for $K'_0 \geq 0$ with baseline $l/L_0 = 10^{-2}$. Normalized surface energy $\bar{\gamma}$ from (145) is reported in Figure 3d for each case, recalling $\hat{\epsilon} = k = 0$ produces Riemannian (Euclidean) metric $G = 1$. Setting $K'_0 > 0$ increases $\bar{\gamma}$ for this problem. Setting $K'_0 < 0$ reduces $\bar{\gamma}$ and produces a physically invalid solution (not shown in Figure 3d) in (146): $\bar{\zeta} < 0$ on part of \mathcal{M} .

5. Two-Dimensional Base Manifold

The framework of Sections 2 and 3 is applied for $n = 2$: a 2D base manifold \mathcal{M} . In Section 5.1, geometry and kinematics are presented. Governing equations are derived in Section 5.2. Solutions are considered for general problem classes in Section 5.3. Constitutive functions for an orthotropic 2D patch of skin under planar deformations are assigned in Section 5.4. Solutions for stretching and tearing are presented in Section 5.5.

5.1. Geometry and Kinematics

Reference coordinates are Cartesian (i.e., orthogonal): $\{X^1, X^2\}$. A reference domain $\{\mathcal{M} : X^1 \in [-L_0, L_0], X^2 \in [-W_0, W_0]\}$ is considered, where the total area relative to a Euclidean metric is $4L_0W_0$, and boundary $\partial\mathcal{M}$ is the edges $(X^1, X^2) = (\pm L_0, \pm W_0)$. The referential internal state vector has coordinates $\{D^1, D^2\}$, both with physical units of length. Spatial coordinates are Cartesian $\{x^1, x^2\}$ and $\{d^1, d^2\}$. A normalization constant (i.e., regularization length) is l , with a physically meaningful domain assumed as $D^A \in [0, l]$ ($A = 1, 2$). With notation $f(X, D) = f(X^A, D^B)$, dimensionless order parameters are, with (68) and (70) invoked,

$$\xi(X) = \frac{D^1(X)}{l} = \frac{d^1(\varphi(X))}{l}, \quad \eta(X) = \frac{D^2(X)}{l} = \frac{d^2(\varphi(X))}{l}, \quad l > 0. \tag{147}$$

Physically meaningful domains are $\xi \in [0, 1]$ and $\eta \in [0, 1]$. For 2D manifolds with Cartesian base coordinates, $\{X^1, X^2\}$ and $\{x^1, x^2\}$, the following metrics apply from (73) and (74):

$$\bar{G}_{AB} = \delta_{AB}, \quad \bar{g}_{ab} = \delta_{ab}; \quad G_{AB}(X, D) = \hat{G}_{AB}(D), \quad g_{ab}(x, d) = \hat{g}_{ab}(d). \tag{148}$$

Herein, the following constraint is imposed:

$$\hat{g}_{ab}(d(\varphi(X))) = \delta_a^A \delta_b^B \hat{G}_{AB}(D(X)) \leftrightarrow g_{ab}(\xi, \eta) = \delta_a^A \delta_b^B G_{AB}(\xi, \eta), \tag{149}$$

making m and \mathcal{M} isometric when $\varphi^a(X) = \delta_a^A X^A + c_0^a \Leftrightarrow F_A^a = \delta_A^a$ regardless of $\{\xi, \eta\}$ at $x = \varphi(X)$.

Remark 42. Equation (149) may be removed in other settings to directly model residual stress (e.g., Appendix B), but all residual stresses are not necessarily eliminated with (149) in place.

Although other non-trivial forms are admissible (e.g., Section 4.1), assume nonlinear N_B^A and linear K_{BC}^A connections vanish:

$$N_B^A = 0 \Rightarrow N_b^a = \delta_a^A N_B^A (F^{-1})_b^B = 0, \quad K_{BC}^A = 0. \tag{150}$$

The K_{bc}^a do not affect the governing equations to be solved later, so they are unspecified.

Applying (71) and (147)–(150),

$$\delta_A G_{BC} = \partial_A G_{BC} - N_A^D \bar{\partial}_D G_{BC} = 0 \Rightarrow \Gamma_{BC}^A = 0, \quad \delta_a g_{bc} = 0 \Rightarrow \Gamma_{bc}^a = 0, \tag{151}$$

$$\chi_A(\xi, \eta) = l C_{AB}^B(\xi, \eta) = l \bar{\partial}_A \{\ln \sqrt{G(\xi, \eta)}\}; \quad l \bar{\partial}_1(\cdot) = \partial(\cdot) / \partial \xi, \quad l \bar{\partial}_2(\cdot) = \partial(\cdot) / \partial \eta. \tag{152}$$

The deformation gradient, deformation tensor, Jacobian determinant, and director gradient are, respectively,

$$F_A^a = \frac{\partial \varphi^a}{\partial X^A}, \quad C_B^A = G^{AC} g_{bc} F_B^b F_C^c = G^{AC} F_C^c \delta_c^F G_{FE} \delta_b^E F_B^b, \quad J = \det(F_A^a) = \sqrt{\det(C_B^A)}, \tag{153}$$

$$D_{|B}^A = \delta_B D^A + K_{BC}^A D^C = \partial_B D^A; \quad D_{|A}^1 = l \partial_A \xi, \quad D_{|A}^2 = l \partial_A \eta. \tag{154}$$

Unless F_A^a and G_{AB} are diagonal, C and \bar{C} can differ. From (75) and (76),

$$\bar{C}_B^A = \delta^{AC} \bar{C}_{CB} = \delta^{AC} \delta_{bc} F_B^b F_C^c, \quad \bar{J} = \sqrt{\det(\bar{C}_B^A)} = J. \tag{155}$$

5.2. Governing Equations

A generic energy density is chosen and equilibrium equations are derived for the 2D case of Section 5.1.

5.2.1. Energy Density

For the present case, dependencies on D^A and $D_{|B}^A$ are suitably represented by (ξ, η) and $(\partial_A \xi, \partial_A \eta)$ of (147) and (154). The functional form of (94) is invoked without explicit X dependency, whereby

$$\psi = \bar{\psi}(\bar{C}_{AB}, \xi, \eta, \partial_A \xi, \partial_A \eta). \quad (156)$$

Henceforth, in Section 5, the over-bar is dropped from ψ to lighten the notation. Let μ_0 denote a constant that will later be associated with a shear modulus, with units of energy density.

Remark 43. For comparison with experiments in ambient 3-space, μ_0 has units of energy per unit 3D volume, so $\Psi = \int_{\mathcal{M}} \psi d\Omega$ is the energy per unit thickness, normal to the X^1 and X^2 .

Let Y_0 denote a constant related to the surface energy with units of energy per unit (e.g., 2D fixed cross-sectional) area, and γ_ξ and γ_η denote two dimensionless constants. Let W be the strain energy density and Λ denote energy density associated with the microstructure. Let w denote a dimensionless strain energy function (embedding possible degradation), λ and ν denote dimensionless phase energy functions, ι denote a dimensionless gradient energy function that is assigned a sum of quadratic forms, and $\nabla_0(\cdot) = \frac{\partial}{\partial X}(\cdot)$ denote the partial material gradient. Free energy (156) is prescribed in intermediate functional form, as

$$\begin{aligned} \psi(\bar{C}, \xi, \eta, \nabla_0 \xi, \nabla_0 \eta) &= W(\bar{C}, \xi, \eta) + \Lambda(\xi, \eta, \nabla_0 \xi, \nabla_0 \eta) \\ &= \frac{\mu_0}{2} w(\bar{C}, \xi, \eta) + \frac{Y_0}{l} [\gamma_\xi \lambda(\xi) + \gamma_\eta \nu(\eta) + \iota(\nabla_0 \xi, \nabla_0 \eta)], \end{aligned} \quad (157)$$

$$\iota = \gamma_\xi l |\nabla_0 \xi|^2 + \gamma_\eta l^2 |\nabla_0 \eta|^2 = l^2 \delta^{AB} (\gamma_\xi \partial_A \xi \partial_B \xi + \gamma_\eta \partial_A \eta \partial_B \eta). \quad (158)$$

Note that $\iota(0, 0) = 0$. Therefore, for null ground-state energy density, ψ , and stress, P_a^A ,

$$w(\delta_{AB}, \xi, \eta) = 0, \quad \frac{\partial w}{\partial \bar{C}_{AB}}(\delta_{AB}, \xi, \eta) = 0; \quad \lambda(0) = \nu(0) = 0. \quad (159)$$

Convexity and material symmetry are addressed in Section 5.4.2.

Applying (96), thermodynamic forces of (85) are

$$P_a^A = \frac{\partial \psi}{\partial F_A^a} = 2\delta_{ab} F_B^b \frac{\partial \psi}{\partial \bar{C}_{AB}} = \mu_0 \delta_{ab} F_B^b \frac{\partial w}{\partial \bar{C}_{AB}}, \quad (160)$$

$$\begin{aligned} Q_1 &= \frac{1}{l} \frac{\partial \psi}{\partial \xi} = \frac{Y_0}{l^2} \left(A_0 \frac{\partial w}{\partial \xi} + \gamma_\xi \frac{d\lambda}{d\xi} \right), \\ Q_2 &= \frac{1}{l} \frac{\partial \psi}{\partial \eta} = \frac{Y_0}{l^2} \left(A_0 \frac{\partial w}{\partial \eta} + \gamma_\eta \frac{d\nu}{d\eta} \right); \quad A_0 = \frac{\mu_0 l}{2Y_0}, \end{aligned} \quad (161)$$

$$\begin{aligned} Z_1^A &= \frac{\partial \psi}{\partial D_{|A}^1} = \frac{Y_0}{l^2} \frac{\partial \iota}{\partial (\partial_A \xi)} = 2Y_0 \gamma_\xi \delta^{AB} \partial_B \xi, \\ Z_2^A &= \frac{\partial \psi}{\partial D_{|A}^2} = \frac{Y_0}{l^2} \frac{\partial \iota}{\partial (\partial_A \eta)} = 2Y_0 \gamma_\eta \delta^{AB} \partial_B \eta. \end{aligned} \quad (162)$$

The source term in (78) manifests from changes in energy proportional to changes in the local referential volume form (e.g., local volume changes from damage, treated analogously to an energy source from tissue growth (Appendix B)):

$$R_A = \beta \psi \bar{\partial}_A (\ln \sqrt{G}) = \frac{\beta}{l} \psi \chi_A, \quad (\beta = \text{constant}; A = 1, 2). \quad (163)$$

5.2.2. Linear Momentum

Linear momentum balance, (87) or (90), invokes relations in Sections 5.1 and 5.2.1,

$$\begin{aligned} \mu_0 \delta_{ab} \left[\frac{\partial^2 \varphi^b}{\partial X^A \partial X^B} \frac{\partial w}{\partial \bar{C}_{AB}} + \frac{\partial \varphi^b}{\partial X^B} \left(\frac{\partial^2 w}{\partial \bar{C}_{AB} \partial X^A} + \frac{\partial^2 w}{\partial \bar{C}_{AB} \partial \xi} \frac{\partial \xi}{\partial X^A} + \frac{\partial^2 w}{\partial \bar{C}_{AB} \partial \eta} \frac{\partial \eta}{\partial X^A} \right) \right] \\ = -\mu_0 \delta_{ab} \frac{\partial \varphi^b}{\partial X^B} \frac{\partial w}{\partial \bar{C}_{AB}} \left[\frac{\partial}{\partial \xi} (\ln \sqrt{G}) \frac{\partial \xi}{\partial X^A} + \frac{\partial}{\partial \eta} (\ln \sqrt{G}) \frac{\partial \eta}{\partial X^A} \right]. \end{aligned} \quad (164)$$

Remark 44. For nonzero μ_0 , (164) is two coupled nonlinear PDEs ($a = 1, 2$) in four field variables: $\varphi^1(X)$, $\varphi^2(X)$, $\xi(X)$, and $\eta(X)$.

5.2.3. Micro-Momentum

The state-space equilibrium conditions (88) or (91), utilizing the relations from Sections 5.1 and 5.2.1, and dividing by $2Y_0$, yield the following two equations:

$$\begin{aligned} \gamma_\xi \delta^{AB} \frac{\partial^2 \xi}{\partial X^A \partial X^B} + \left(1 - \frac{\alpha - \beta}{2} \right) \gamma_\xi \delta^{AB} \frac{\partial}{\partial \xi} (\ln \sqrt{G}) \frac{\partial \xi}{\partial X^A} \frac{\partial \xi}{\partial X^B} - \frac{\gamma_\xi}{2l^2} \frac{d\lambda}{d\xi} \\ + \gamma_\xi \delta^{AB} \frac{\partial}{\partial \eta} (\ln \sqrt{G}) \frac{\partial \xi}{\partial X^A} \frac{\partial \eta}{\partial X^B} - \left(\frac{\alpha - \beta}{2} \right) \gamma_\eta \delta^{AB} \frac{\partial}{\partial \xi} (\ln \sqrt{G}) \frac{\partial \eta}{\partial X^A} \frac{\partial \eta}{\partial X^B} \\ - \left(\frac{\alpha - \beta}{2l^2} \right) \frac{\partial}{\partial \xi} (\ln \sqrt{G}) [\gamma_\xi \lambda + \gamma_\eta \nu] = \frac{A_0}{2l^2} \left[\frac{\partial w}{\partial \xi} + (\alpha - \beta) \frac{\partial}{\partial \xi} (\ln \sqrt{G}) w \right], \end{aligned} \quad (165)$$

$$\begin{aligned} \gamma_\eta \delta^{AB} \frac{\partial^2 \eta}{\partial X^A \partial X^B} + \left(1 - \frac{\alpha - \beta}{2} \right) \gamma_\eta \delta^{AB} \frac{\partial}{\partial \eta} (\ln \sqrt{G}) \frac{\partial \eta}{\partial X^A} \frac{\partial \eta}{\partial X^B} - \frac{\gamma_\eta}{2l^2} \frac{d\nu}{d\eta} \\ + \gamma_\eta \delta^{AB} \frac{\partial}{\partial \xi} (\ln \sqrt{G}) \frac{\partial \eta}{\partial X^A} \frac{\partial \xi}{\partial X^B} - \left(\frac{\alpha - \beta}{2} \right) \gamma_\xi \delta^{AB} \frac{\partial}{\partial \eta} (\ln \sqrt{G}) \frac{\partial \xi}{\partial X^A} \frac{\partial \xi}{\partial X^B} \\ - \left(\frac{\alpha - \beta}{2l^2} \right) \frac{\partial}{\partial \eta} (\ln \sqrt{G}) [\gamma_\xi \lambda + \gamma_\eta \nu] = \frac{A_0}{2l^2} \left[\frac{\partial w}{\partial \eta} + (\alpha - \beta) \frac{\partial}{\partial \eta} (\ln \sqrt{G}) w \right]. \end{aligned} \quad (166)$$

Remark 45. For nonzero Y_0 , (165) and (166) are two coupled nonlinear PDEs in four field variables: $\varphi^1(X)$, $\varphi^2(X)$, $\xi(X)$, and $\eta(X)$, where derivatives of $\varphi^1(X)$ and $\varphi^2(X)$ enter w on the right sides via $\bar{C}_{AB} = \partial_A \varphi^a \delta_{ab} \partial_B \varphi^b$. For the special case $Y_0 = 0$, the left sides of (165) and (166) vanish, whereas for $\mu_0 = 0$, the right sides vanish.

5.3. General Solutions

5.3.1. Homogeneous Fields

Cases for which $\xi(X) \rightarrow \xi_H = \text{constant}$ and $\eta(X) \rightarrow \eta_H = \text{constant}$ at all points $X \in \mathcal{M}$ are examined. The former constants may differ: $\xi_H \neq \eta_H$ in general. The notation $f_H(X) = f(X, \xi_H, \eta_H)$ is applied, and $\mu_0 > 0$ is imposed. Then (160) and (164) reduce to

$$\begin{aligned} \frac{\partial P_a^A}{\partial X^A} = \mu_0 \delta_{ab} \left[\frac{\partial^2 \varphi^b}{\partial X^A \partial X^B} \frac{\partial w}{\partial \bar{C}_{AB}} + \frac{\partial \varphi^b}{\partial X^B} \frac{\partial^2 w}{\partial \bar{C}_{AB} \partial X^A} \right] = 0 \\ \Rightarrow (P_H)_a^A = \frac{\mu_0}{2} \left(\frac{\partial w}{\partial F_A^a} \right)_H = \text{constant}. \end{aligned} \quad (167)$$

This should be satisfied for any homogeneous $F_A^a = (F_H)_A^a$ for which $\partial^2 \varphi^a / \partial X^A \partial X^B = 0$. The micro-momentum conservation laws (165) and (166) become

$$-\gamma_\xi \frac{d\lambda}{d\xi} - (\alpha - \beta) \frac{\partial}{\partial \xi} (\ln \sqrt{G}) [\gamma_\xi \lambda + \gamma_\eta v] = A_0 \left[\frac{\partial w}{\partial \xi} + (\alpha - \beta) \frac{\partial}{\partial \xi} (\ln \sqrt{G}) w \right], \quad (168)$$

$$-\gamma_\eta \frac{dv}{d\eta} - (\alpha - \beta) \frac{\partial}{\partial \eta} (\ln \sqrt{G}) [\gamma_\xi \lambda + \gamma_\eta v] = A_0 \left[\frac{\partial w}{\partial \eta} + (\alpha - \beta) \frac{\partial}{\partial \eta} (\ln \sqrt{G}) w \right], \quad (169)$$

wherein $\lambda = \lambda_H$, $v = v_H$, $(\frac{\partial}{\partial \xi} \ln \sqrt{G})_H$, and $(\frac{\partial}{\partial \eta} \ln \sqrt{G})_H$ are all algebraic functions of (ξ_H, η_H) , while $w = w_H$, $(\frac{\partial}{\partial \xi} w)_H$, and $(\frac{\partial}{\partial \eta} w)_H$ are algebraic functions of $(\xi_H, \eta_H, (F_H)_A^a)$.

Remark 46. The homogeneous equilibrium is satisfied by the six algebraic equations (167) ($a, A = 1, 2$), (168), and (169) in ten unknowns $(P_H)_a^A, (F_H)_A^a, \xi_H, \eta_H$. Given $(P_H)_a^A$ or $(F_H)_A^a$ as the mechanical loading, the remaining six unknowns can be obtained from a simultaneous solution. If $(F_H)_A^a$ is imposed, (168) and (169) are two equations in ξ_H, η_H . Then (167) yields the remaining $(P_H)_a^A$.

Remark 47. Essential boundary conditions for homogeneous states are $\xi = \xi_H$ and $\eta = \eta_H$, both $\forall X \in \partial \mathcal{M}$. Since ξ and η are constants, $Z_A^B = 0$ by (162), so corresponding natural boundary conditions for forces conjugating to internal structure parameters in (89) are $z_A = Z_A^B N_B = 0$.

5.3.2. Stress-Free States

Consider cases whereby $P_a^A = 0 \forall X \in \mathcal{M}$. Linear momentum conservation laws (87), (90), and (164), are trivially satisfied. Restrict $\mu_0 > 0$. Since F_A^a is non-singular, (160) requires $\partial w / \partial \bar{C}_{AB} = 0$. This is obeyed at $\bar{C}_{AB} = \delta_{AB}$ via (159); thus, assume rigid body motion (i.e., $\varphi^a = Q_A^a X^A + c_0^a$, with Q_A^a constant and proper orthogonal and c_0^a constant) whereby $w = 0$ vanishes as well by (159).

Remark 48. General analytical solutions for stress-free states are not apparent without particular forms of functions $w(\bar{C}_{AB}, \xi, \eta)$, $G(\xi, \eta)$, $\lambda(\xi)$, $v(\eta)$, and values of $\gamma_\xi, \gamma_\eta, \alpha, \beta$, and l .

Remark 49. If $\partial w / \partial \xi = \partial w / \partial \eta = 0$ for $\bar{C}_{AB} = \delta_{AB}$, then the right sides of (165) and (166) vanish. Whether or not stress-free deformation states with $\bar{C}_{AB} \neq \delta_{AB}$ (e.g., locally) exist depends on w .

5.4. Constitutive Model

The framework is applied to a rectangular patch of skin loaded in the X^1 - X^2 plane. A 2D theory (i.e., membrane theory) cannot distinguish between plane stress and plane strain conditions [115], nor can it account for out-of-plane anisotropy. Nonetheless, 2D nonlinear elastic models are widely used to represent soft tissues, including skin [68,89]. Thus, parameters entering the model (e.g., μ_0, Y_0) are particular to loading conditions and material orientations from experiments to which they are calibrated (e.g., here, plane stress).

Remark 50. In a purely 2D theory, incompressibility is often used for the 3D modeling of biological tissues [68,71,80,82] cannot be assumed since contraction under biaxial stretch is not quantified in a 2D theory. Incompressibility is also inappropriate if the material dilates due to damage.

The skin is treated as having orthotropic symmetry, with two constant orthogonal directions in the reference configuration denoted by unit vectors n_1 and n_2 :

$$n_1 = n_1^A \frac{\delta}{\delta X^A}, \quad n_2 = n_2^A \frac{\delta}{\delta X^A}; \quad n_i^A \delta_{AB} n_j^B = \delta_{ij} \quad (i, j = 1, 2). \quad (170)$$

Remark 51. The collagen fibers in the plane of the skin need not all align with \mathbf{n}_1 or \mathbf{n}_2 , so long as orthotropic symmetry is respected. For example, each \mathbf{n}_i can bisect the alignments of two equivalent primary families of fibers in the skin whose directions are not necessarily orthogonal [71,92]. In such a case, \mathbf{n}_1 is still a unit vector orthogonal to \mathbf{n}_2 ; planar orthotropy is maintained with respect to reflections about both unit vectors \mathbf{n}_i .

Remark 52. The internal structure variables $\xi = D^1/l$ and $\eta = D^2/l$ account for mechanisms that lead to softening and degradation under tensile load: fiber sliding, pull-out, and breakage of collagen fibers, and rupture of the elastin fibers and ground matrix. Each D^A ($A = 1, 2$) is a representative microscopic sliding or separation distance in the $\mathbf{n}_i\delta_A^i$ direction, with l the distance at which the material can no longer support tensile load along that direction.

Remark 53. In the cohesive zone interpretation, each D^A is viewed as a crack-opening displacement for separation on a material surface (line in 2D) normal to $\mathbf{n}_i\delta_A^i$.

Finslerian metrics $G_{AB}(\xi, \eta) = \delta_A^a \delta_B^b g_{ab}(\xi, \eta)$ of §5.4.1 anisotropically rescale material and spatial manifolds \mathcal{M} and \mathfrak{m} due to microstructure changes in different directions. In the absence of damage, the nonlinear elastic potential of Section 5.4.2 refines a 3D model [71,82,83,92] to 2D.

5.4.1. Metrics

From (16), (48), (148), (149), and (153), the difference in squared lengths of line elements dx and dX is

$$(|dx|^2 - |dX|^2)(F, \xi, \eta) = [\delta_a^E \delta_b^F G_{EF}(\xi, \eta) F_A^a F_B^b - G_{AB}(\xi, \eta)] dX^A dX^B. \quad (171)$$

Remark 54. Local regions of \mathcal{M} at X and \mathfrak{m} at $x = \varphi(X)$ are rescaled isometrically by components $G_{AB}(\xi(X), \eta(X))$. When $F_A^a = \delta_A^a$, $|dx| = |dX|$ regardless of G_{AB} , ξ , or η . For degenerate Riemannian metrics $G_{AB} = \bar{G}_{AB} = \delta_{AB}$ and $g_{ab} = \bar{g}_{ab} = \delta_{ab}$, (171) becomes independent of (ξ, η) .

The Cartesian coordinate chart $\{X^A\}$ is prescribed such that $n_i^A = \delta_i^A$ in (170); thus \mathbf{n}_1 and \mathbf{n}_2 are parallel to respective X^1 and X^2 directions on \mathcal{M} . Rescaling arises from changes in structure associated with degradation and damage in orthogonal directions, to which remnant strain contributions $\frac{1}{2} \ln[G_{11}(\xi)]$ and $\frac{1}{2} \ln[G_{22}(\eta)]$ can be linked. The metric tensor G_{AB} is hereafter assigned specific exponential terms, generalizing the 1D form of Section 4.4.1 to an anisotropic 2D form appropriate for orthotropic symmetry:

$$[G_{AB}(\xi, \eta)] = \begin{bmatrix} \exp\left(\frac{2k}{r}\xi^r\right) & 0 \\ 0 & \exp\left(\frac{2m}{r}\eta^r\right) \end{bmatrix} \quad (172)$$

$$\Rightarrow G(\xi, \eta) = \det[G_{AB}(\xi, \eta)] = \exp\left(\frac{2}{r}[k\xi^r + m\eta^r]\right).$$

For $\xi \in [0, 1]$ and $\eta \in [0, 1]$, two constants in (172) are k and m , and positive for expansion. A third constant $r > 0$ modulates rates of change of $G_{11}(\xi)$ and $G_{22}(\eta)$ with respect to their arguments. Ratios are determined by remnant strain contributions at failure: $\hat{\epsilon}_\xi = \frac{k}{r}$ and $\hat{\epsilon}_\eta = \frac{m}{r}$. Values of k , m , and r are calibrated to data in Section 5.5.1. Isotropy arises in (172) when $\eta = \xi$ and $m = k$.

Remark 55. More general forms of $G_{AB}(\xi, \eta)$, likely with more parameters, are possible; (172) is a simple form sufficient to address experimental observations for extension and tearing of skin.

From (172), non-vanishing components of Cartan's tensor in (25) and (152) are

$$lC_{11}^1 = \chi_1 = \frac{\partial}{\partial \xi} (\ln \sqrt{G}) = k\xi^{r-1}, \quad lC_{22}^2 = \chi_2 = \frac{\partial}{\partial \eta} (\ln \sqrt{G}) = m\eta^{r-1}. \quad (173)$$

5.4.2. Nonlinear Elasticity

The nonlinear elasticity model generalizes that of Section 4.4.2 to a 2D base space \mathcal{M} with the anisotropic Finsler metric depending on two structure variable components, ξ and η in normalized dimensionless form. For the 2D case, the material symmetry of Section 3.3.4 requires careful consideration. Here, the skin is treated as a planar orthotropic solid [68,75,89].

Viewing the D^A as components of a material vector field, orthotropic symmetry suggests invariants ξ^2 and η^2 . For physically admissible ranges $\xi \in [0, 1]$ and $\eta \in [0, 1]$, these can be replaced with ξ and η . Viewing the $D_{|B}^A$, similarly, orthotropic symmetry permits a more general functional dependence than the sum of quadratic forms in ι of (157) and (158). However, the chosen form of ι in (158) allows for partial anisotropy, not inconsistent with orthotropy, when γ_ξ and γ_η differ. Thus, the structure-dependent contribution to ψ , $\Lambda l = Y_0(\gamma_\xi \lambda + \gamma_\eta \nu + \iota)$, more specifically here

$$\lambda(\xi) = \xi^2, \quad \nu(\eta) = \eta^2; \quad \iota(\nabla_0 \xi, \nabla_0 \eta) = l^2 \delta^{AB} (\gamma_\xi \partial_A \xi \partial_B \xi + \gamma_\eta \partial_A \eta \partial_B \eta), \quad (174)$$

is consistent with material symmetry requirements. Strain energy density W in (157) is dictated by dimensionless function $w(\bar{C}_{AB}, \xi, \eta)$. As per the above discussion, ξ and η are treated as scalar invariant arguments. A partial list of remaining invariants [82,91] of (99) for orthotropic symmetry of a 2D material entering w (and, thus, $\psi = \bar{\psi}$) is then deduced, applying $n_i^A = \delta_i^A$ in (170),

$$\begin{aligned} \bar{I}_1 &= \text{tr} \bar{C} = \delta^{AB} \bar{C}_{AB}, & \bar{I}_2 &= J^2 = \det \bar{C}, \\ \bar{I}_3 &= \bar{C}_{AB} n_1^A n_1^B = \bar{C}_{11}, & \bar{I}_4 &= \bar{C}_{AB} n_2^A n_2^B = \bar{C}_{22}. \end{aligned} \quad (175)$$

Remark 56. As n_1 and n_2 are orthonormal, $\bar{I}_1 = \bar{I}_3 + \bar{I}_4$, so one of $\bar{I}_1, \bar{I}_3, \bar{I}_4$ in (175) is redundant. Since $J \geq 1$, dependence on $\bar{I}_2 = \bar{C}_{11} \bar{C}_{22} - (\bar{C}_{12})^2$ can be replaced by J (or by $(\bar{C}_{12})^2$, given \bar{I}_3, \bar{I}_4).

The Euclidean metric $\bar{G}^{AB} = \delta^{AB}$, rather than the Finsler metric G^{AB} , is used for scalar products in (174) and (175), consistent with (155). In 2-space, \bar{I}_1 and \bar{I}_2 are the complete set of isotropic invariants of \bar{C} . Two orthotropic invariants are \bar{I}_3 and \bar{I}_4 ; several higher-order invariants are admissible [82,91] but excluded here since (175) is sufficient for the present application. The dimensionless strain energy function entering (157) is prescribed specifically as

$$\begin{aligned} w(\bar{C}_{AB}, \xi, \eta) &= \left[\frac{1}{J} (\bar{C}_{11} + \bar{C}_{22}) + k_0 (J - 1)^2 - 2 \right] y_\mu(\xi, \eta) \\ &+ \left[\frac{a_1}{2b_1} \left(\exp\{b_1 (\bar{C}_{11} - 1)^2\} - 1 \right) \right] H(\bar{C}_{11} - 1) y_\xi(\xi) \\ &+ \left[\frac{a_2}{2b_2} \left(\exp\{b_2 (\bar{C}_{22} - 1)^2\} - 1 \right) \right] H(\bar{C}_{22} - 1) y_\eta(\eta). \end{aligned} \quad (176)$$

Dimensionless constants are $k_0 > 0$, $a_1 \geq 0$, $b_1 > 0$, $a_2 \geq 0$, and $b_2 > 0$. Right-continuous Heaviside functions $H(f) = 1 \forall f \geq 0, H(f) = 0 \forall f < 0$. Also, $\mu_0 > 0$ and $Y_0 > 0$ are enforced in (157).

Remark 57. Potential w in (176) extends prior models for collagenous tissues [71,82,83,92] to include anisotropic structure changes. The first term on the right, linear in \bar{I}_1/J , and independent of volume change, accounts for isotropic shearing resistance of ground matrix and elastin. The resistance to volume (area) change is measured by the right-side second bracketed entry with k_0 being a dimensionless bulk (area) modulus finite for a 2D model; the dimensional bulk modulus $\kappa_0 = k_0 \mu_0$. Exponential terms account for stiffening from collagen fibers in orthogonal directions n_i . Heaviside functions prevent fibers from supporting compressive loads [82,116] since they would likely buckle.

Degradation functions are $y_\mu(\xi, \eta)$, $y_\xi(\xi)$, and $y_\eta(\eta)$, where for the anisotropic theory,

$$y_\mu = (1 - \xi)^\vartheta(1 - \eta)^\varsigma = y_\xi y_\eta, \quad y_\xi = (1 - \xi)^\vartheta, \quad y_\eta = (1 - \eta)^\varsigma. \tag{177}$$

Corresponding material constants are $\vartheta \in [0, \infty)$ and $\varsigma \in [0, \infty)$. Notice that matrix strain energy degrades equivalently with the increasing ξ and η via y_μ , maintaining isotropy of the first term in (176). As collagen fibers debond, the ground matrix and elastic simultaneously weaken.

Remark 58. Choices $\vartheta = \varsigma = 2$ are typical for phase-field fracture [98], although other values are possible for soft biologic tissues [95]. Setting $\vartheta = \varsigma = 0$ implies null degradation (i.e., ideal elastic stress–stretch response).

Remark 59. When $\xi = \eta = 0$, w of (176) is polyconvex [81,90], facilitating existence and uniqueness of solutions. Also, ψ with (174), (176), and (177) obeys (159).

Stress components P_a^A conjugating to $F_A^a = \partial_A \varphi^a$ are found from (100), (160), (176), and (177), while forces $Q_{1,2}$ conjugating to ξ, η are found from (161), (174), (176), and (177):

$$\begin{aligned} P_a^A / \mu_0 &= J^{-1}[\delta_{ab}\delta^{AB}F_B^b - \frac{1}{2}\bar{C}_{BC}\delta^{BC}(F^{-1})_a^A + k_0J^2(J - 1)(F^{-1})_a^A](1 - \xi)^\vartheta(1 - \eta)^\varsigma \\ &\quad + [a_1(\bar{C}_{11} - 1)\exp\{b_1(\bar{C}_{11} - 1)^2\}\delta_{ab}\delta_1^A F_1^b](1 - \xi)^\vartheta H(\bar{C}_{11} - 1) \\ &\quad + [a_2(\bar{C}_{22} - 1)\exp\{b_2(\bar{C}_{22} - 1)^2\}\delta_{ab}\delta_2^A F_2^b](1 - \eta)^\varsigma H(\bar{C}_{22} - 1), \end{aligned} \tag{178}$$

$$\begin{aligned} Q_1 l^2 / (2Y_0) &= \gamma_\xi \xi - A_0 \vartheta \left[(1 - \xi)^{\vartheta-1} (1 - \eta)^\varsigma \{ J^{-1} (\bar{C}_{11} + \bar{C}_{22}) + k_0 (J - 1)^2 - 2 \} \right. \\ &\quad \left. - A_0 \vartheta (1 - \xi)^{\vartheta-1} \left[\frac{1}{2} (a_1 / b_1) \left(\exp\{b_1 (\bar{C}_{11} - 1)^2\} - 1 \right) \right] H(\bar{C}_{11} - 1), \right] \end{aligned} \tag{179}$$

$$\begin{aligned} Q_2 l^2 / (2Y_0) &= \gamma_\eta \eta - A_0 \varsigma \left[(1 - \eta)^{\varsigma-1} (1 - \xi)^\vartheta \{ J^{-1} (\bar{C}_{11} + \bar{C}_{22}) + k_0 (J - 1)^2 - 2 \} \right. \\ &\quad \left. - A_0 \varsigma (1 - \eta)^{\varsigma-1} \left[\frac{1}{2} (a_2 / b_2) \left(\exp\{b_2 (\bar{C}_{22} - 1)^2\} - 1 \right) \right] H(\bar{C}_{22} - 1). \right] \end{aligned} \tag{180}$$

Remark 60. An ideal elastic response is obtained when $k = m = 0 \Rightarrow G_{AB} = \delta_{AB} \Rightarrow \chi_A = 0$, and $\vartheta = \varsigma = 0 \Rightarrow \frac{\partial w}{\partial \xi} = \frac{\partial w}{\partial \eta} = 0$. Then since $\frac{d\lambda}{d\xi}(0) = 0$ and $\frac{d\nu}{d\eta}(0) = 0$ by (174), the right side of (164) vanishes identically, and the (trivial) solutions to (165) and (166) are $\xi(X) = \eta(X) = 0 \forall X \in \mathcal{M}$.

Remark 61. An isotropic version of the theory can be obtained, if along with $m = k$ in (172), the following choices are made instead of (177):

$$y_\mu = \frac{1}{2}[(1 - \xi)^\vartheta + (1 - \eta)^\vartheta], \quad \varsigma = \vartheta, \quad y_\xi = y_\eta = 0; \quad \gamma_\xi = \gamma_\eta = \frac{1}{2}\gamma_\mu \geq 0. \tag{181}$$

Collagen fiber contributions to strain energy are removed such that w now only depends on isotropic invariants of \bar{C} . Equilibrium equations (164)–(166) are identical under the change of variables $\xi \leftrightarrow \eta$, implying $\eta(X) = \xi(X)$ if identical boundary conditions on D^A or z_A are applied for each field on $\partial\mathcal{M}$. In this case, one of (165), and (166) is redundant and replaced with $\eta = \xi$.

5.5. Specific Solutions

Possible inputs to the 2D model are seventeen constants $l > 0, k, m, r > 0, \mu_0 > 0, k_0 > 0, a_1 \geq 0, b_1 > 0, a_2 \geq 0, b_2 > 0, \vartheta \geq 0, \varsigma \geq 0, Y_0 > 0, \gamma_\xi, \gamma_\eta, \alpha$, and β . Values of l and Y_0 are taken from the analysis in Section 4.5.2 of the complete tearing of a 1D specimen of skin to a stress-free state. This is appropriate given that 1D and 2D theories are applied to describe surface energy and material length scale pertinent to the same experiments [73,74,99,113], and since stress-free solutions in Section 5.5.3 are perfectly parallel to those of Section 4.5.2. The remaining parameters are evaluated in Section 5.5.1, by applying the constitutive model of Section 5.4 to the general solutions for homogeneous

fields derived in Section 5.3.1 to the uniaxial stress extension of 2D skin specimens along the material’s X^1 and X^2 directions, respectively, aligned perpendicular and parallel to Langer’s lines.

Remark 62. Collagen fibers of the microstructure in the dermis are aligned predominantly along Langer’s lines and are more often pre-stretched in vivo along these directions [75]. In vivo or in vitro, elastic stiffness at finite stretch tends to be larger in directions along Langer’s lines (i.e., parallel to X^2 and n_2) than in orthogonal directions (e.g., parallel to n_1). Degradation and failure behaviors are also anisotropic: rupture stress tends to be larger, and failure elongation is lower when stretching in the stiffer n_2 direction [74,75,87].

In Section 5.5.2, model outcomes are reported for planar biaxial extension [68,70,115] of 2D specimens, highlighting simultaneous microstructure degradation perpendicular and parallel to Langer’s lines. Lastly, in Section 5.5.3, stress-free states analogous to those modeled in a 1D context in Section 4.5.2 are evaluated for the 2D theory.

In Sections 5.5.1 and 5.5.2, equilibrium solutions of Section 5.3.1 hold. Invoking (173), (174), (176)–(178), and dropping $(\cdot)_H$ notation for brevity, (167)–(169) comprise the algebraic system

$$\begin{aligned}
 P_a^A &= \mu_0 J^{-1} [\delta_{ab} \delta^{AB} F_B^b - \frac{1}{2} \bar{C}_{BC} \delta^{BC} (F^{-1})_a^A + k_0 J^2 (J - 1) (F^{-1})_a^A] (1 - \zeta)^\theta (1 - \eta)^\zeta \\
 &\quad + [a_1 (\bar{C}_{11} - 1) \exp\{b_1 (\bar{C}_{11} - 1)^2\} \delta_{ab} \delta_1^A F_1^b] (1 - \zeta)^\theta H(\bar{C}_{11} - 1) \\
 &\quad + [a_2 (\bar{C}_{22} - 1) \exp\{b_2 (\bar{C}_{22} - 1)^2\} \delta_{ab} \delta_2^A F_2^b] (1 - \eta)^\zeta H(\bar{C}_{22} - 1) \\
 &= \text{constant},
 \end{aligned}
 \tag{182}$$

$$\gamma_\zeta \zeta + k \zeta^{r-1} [\gamma_\zeta \zeta^2 + \gamma_\eta \eta^2] = -\frac{A_0}{2} \left[\frac{\partial w(\bar{C}_{AB}, \zeta, \eta)}{\partial \zeta} + 2k \zeta^{r-1} w(\bar{C}_{AB}, \zeta, \eta) \right],
 \tag{183}$$

$$\gamma_\eta \eta + m \eta^{r-1} [\gamma_\zeta \zeta^2 + \gamma_\eta \eta^2] = -\frac{A_0}{2} \left[\frac{\partial w(\bar{C}_{AB}, \zeta, \eta)}{\partial \eta} + 2m \eta^{r-1} w(\bar{C}_{AB}, \zeta, \eta) \right].
 \tag{184}$$

Consistent with (124) for $N_0 = 0$ [55,56,62], $\beta = \alpha - 2$ is assumed in (183) and (184), reducing the number of requisite parameters to fifteen; α and β enter the governing equations only through their difference. Boundary conditions on the internal state, are, for homogeneous conditions,

$$\zeta(X^1 = \pm L_0, X^2 = \pm W_0) = \zeta_H, \quad \eta(X^1 = \pm L_0, X^2 = \pm W_0) = \eta_H.
 \tag{185}$$

Alternative conditions to (182)–(185) are considered for heterogeneous stress-free states in Section 5.5.3.

5.5.1. Uniaxial Extension

First, consider homogeneous uniaxial-stress extension in either the X^1 or X^2 direction. From the symmetry of the loading mode and material model, shear stresses vanish identically: $P_2^1 = 0, P_1^2 = 0$. Similarly, $F_2^1 = 0, F_1^2 = 0$, and $\bar{C}_{12} = \bar{C}_{21} = 0$. The homogeneous deformation fields are

$$\begin{aligned}
 \varphi^1 &= \lambda_1 X^1, \quad \varphi^2 = \lambda_2 X^2; & F_1^1 &= \lambda_1, \quad F_2^2 = \lambda_2; \\
 \bar{C}_{11} &= (\lambda_1)^2, \quad \bar{C}_{22} = (\lambda_2)^2; & J &= \lambda_1 \lambda_2.
 \end{aligned}
 \tag{186}$$

At any single given load increment, stretch ratios are the constants $\lambda_1 > 0$, and $\lambda_2 > 0$.

Mechanical boundary conditions, for extension along X^1 with $\lambda_1 \geq 1$, are

$$\varphi^1(X^1 = \pm L_0) = \pm \lambda_1 L_0, \quad p_2(X^2 = \pm W_0) = P_2^2(X^2 = \pm W_0) = 0.
 \tag{187}$$

In this case, $P_2^2 = 0 \forall X \in \mathcal{M}$, and the sole non-vanishing stress component in (182) is P_1^1 . Note that λ_2 is unknown a priori. Given λ_1 from the first of (187), values consistent with (185) are obtained by solving (182) for $a = A = 2$ with $P_2^2 = 0$, (183), and (184) simultaneously for λ_2 , ξ , and η as functions of λ_1 . Axial stress P_1^1 is then found afterwards using (182) with $a = A = 1$.

For axial loading along X^2 with $\lambda_2 \geq 1$,

$$\varphi^2(X^2 = \pm W_0) = \pm \lambda_2 W_0, \quad p_1(X^1 = \pm L_0) = P_1^1(X^1 = \pm L_0) = 0. \quad (188)$$

Now $P_1^1 = 0 \forall X \in \mathcal{M}$, and the sole non-vanishing stress component in (182) is P_2^2 . Given λ_2 from the first of (188), values consistent with (185) are obtained by solving (182) for $a = A = 1$ with $P_1^1 = 0$, (183), and (184) simultaneously for λ_1 , ξ , and η as functions of λ_2 . Axial stress P_2^2 is found afterwards using (182) with $a = A = 2$.

Values of all baseline parameters are listed in Table 1. Identical values of those constants shared among 1D and 2D theories are found to aptly describe the experimental data for stretching along \mathbf{n}_1 , in conjunction with natural choice $\gamma_\xi = 1$. The 2D theory features additional parameters to account for orthotropic anisotropy (e.g., stiffer response along \mathbf{n}_2 , with peak stress occurring at a lower stretch) as well as an areal bulk modulus κ_0 absent in the 1D theory.

Remark 63. Adherence to physical observations dictates $a_2 > a_1$, $b_2 > b_1$, and $\kappa_0 > \mu_0$. Since degradation is more severe, and toughness lower for stretching along \mathbf{n}_2 , $m > k$ and $\gamma_\eta < \gamma_\xi$. The standard choice [95,98] $\zeta = \vartheta = 2$ in (177) was found sufficient to describe test data.

Model outcomes for non-vanishing stress components and internal state vector components are presented in Figure 4a,b. Experimental P_1^1 versus λ_1 data for loading along \mathbf{n}_1 , with $\lambda_1 \geq 0$ prescribed in the corresponding model calculations, are identical to P versus \sqrt{C} data depicted using the 1D theory in Section 4.5.1. These data [74] are for relatively high-rate extensions of rabbit skin along a longitudinal direction, parallel to the backbone of the torso and perpendicular to Langer's lines. Nonlinear elastic parameters should be viewed as instantaneous dynamic moduli in a pseudo-elastic representation [68,84,85] since loading times are brief relative to stress relaxation times [74]. Single-experiment data of similar fidelities for transverse extensions—parallel to Langer's lines to complete load drops—were not reported, but a maximum stress and strain range was given for the extension along \mathbf{n}_2 [74]. The representative peak stress P_2^2 and corresponding stretch λ_2 based on such data [74] are included in Figure 4a. According to such data [74], the material is stiffer, and ruptures at a higher stress ($\approx \frac{4}{3} \times$) but lower strain ($\approx \frac{2}{3} \times$) in the transverse \mathbf{n}_2 direction.

Remark 64. For loading along \mathbf{n}_1 , $\xi \rightarrow 1$ and $\eta \rightarrow 0$ for $\lambda_1 \gtrsim 3.5$, meaning most internal structure evolution correlates with degradation in this direction, with small transverse effects of η . Analogously, loading along \mathbf{n}_2 gives $\eta \rightarrow 1$ and $\xi \rightarrow 0$ for $\lambda_2 \gtrsim 3$. The rate of increase of η with $\lambda_2 > 1$ is more rapid than the rate of increase of ξ with $\lambda_1 > 1$, since the skin degrades sooner and fails at a lower strain for stretching parallel to Langer's lines. The present diffuse model is an idealization characteristic of experiments when there is no sharp pre-crack [63,68,72,74,87].

Figure 4c,d shows predictions at modest stretch along \mathbf{n}_1 or \mathbf{n}_2 under uniaxial stress conditions identical to those of Figure 4a, as well as uniaxial strain, whereby $\lambda_2 = 1$ or $\lambda_1 = 1$ is enforced using the scheme in Section 5.5.2, rather than respective of $P_2^2 = 0$ or $P_1^1 = 0$. Predictions for the ideal elastic case ($\vartheta = \zeta = 0 \Rightarrow \xi = \eta = 0$) are shown for comparison. The results are stiffer for the ideal elastic case since degradation commensurate with structure change is omitted. In agreement with other data [70], skin is elastically stiffer in uniaxial strain relative to uniaxial stress. Choosing a higher value of $k_0 = \kappa_0/\mu_0 > 1$ in (176) would further increase this difference if merited.

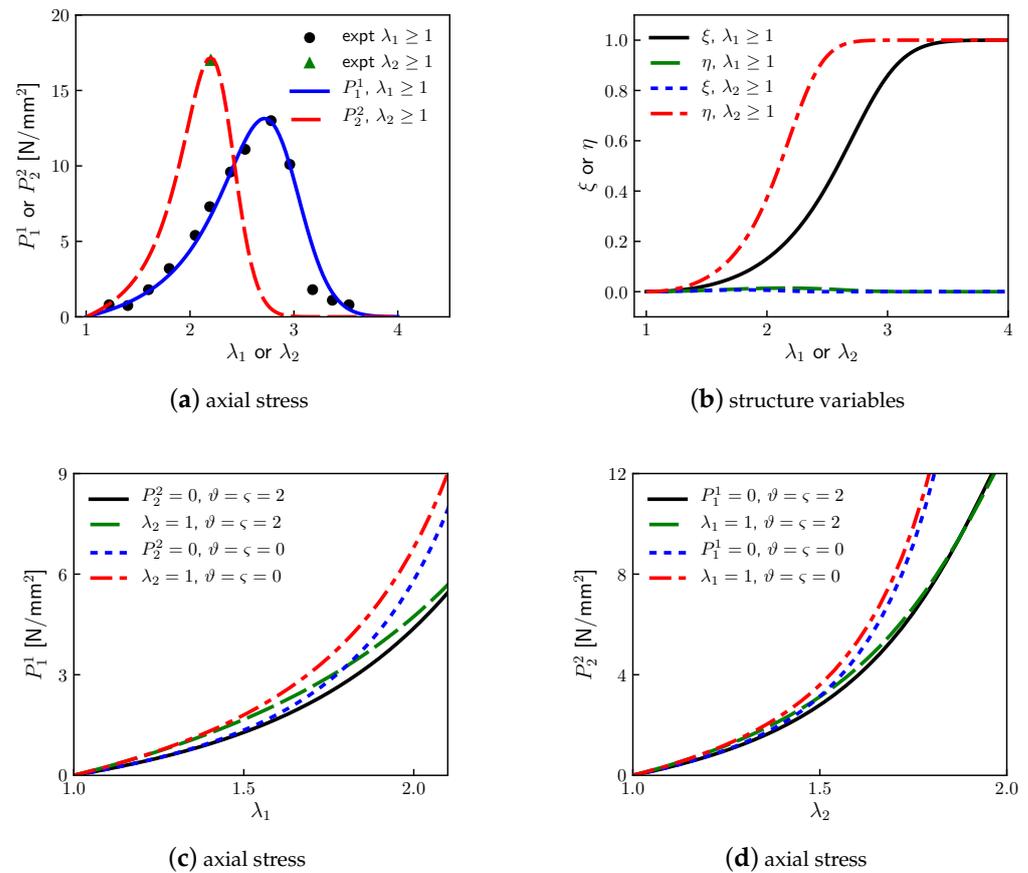


Figure 4. Uniaxial extension and tearing of skin for the imposed axial stretch $\lambda_1 \geq 1$ or $\lambda_2 \geq 1$, 2D model: (a) Stress P_1^1 or P_2^2 (baseline parameters, Table 1) with representative experimental data [74] (see text Section 4.5.1 for the consistent definition of experimental stretch, accounting for pre-stress) for straining perpendicular or parallel to Langer’s lines; (b) normalized internal structure components ξ and η (baseline parameters); (c) stress P_1^1 for moderate extension $\lambda_1 \leq 2.1$ under uniaxial stress ($P_2^2 = 0$) or uniaxial strain ($\lambda_2 = 1$) conditions for the Finsler model (baseline parameters) and the ideal elastic model ($\vartheta = \varsigma = 0$); (d) stress P_2^2 for moderate extension $\lambda_2 \leq 2.0$ under uniaxial stress ($P_1^1 = 0$) or uniaxial strain ($\lambda_1 = 1$) conditions for the Finsler model (baseline) and the ideal elastic model ($\vartheta = \varsigma = 0$).

5.5.2. Biaxial Extension

Now, consider the homogeneous biaxial stress extension in the X^1 and X^2 directions. From symmetry, $P_2^1 = 0, P_1^2 = 0, F_2^1 = 0, F_1^2 = 0$, and $\bar{C}_{12} = \bar{C}_{21} = 0$. The homogeneous deformation fields are

$$\begin{aligned} \varphi^1 &= \lambda_1 X^1, & \varphi^2 &= \lambda_2 X^2; & F_1^1 &= \lambda_1, & F_2^2 &= \lambda_2; \\ \bar{C}_{11} &= (\lambda_1)^2, & \bar{C}_{22} &= (\lambda_2)^2; & J &= \lambda_1 \lambda_2. \end{aligned} \tag{189}$$

Stretch ratios are $\lambda_1 > 0$ and $\lambda_2 > 0$; both are constants over \mathcal{M} . The mechanical boundary conditions are

$$\varphi^1(X^1 = \pm L_0) = \pm \lambda_1 L_0, \quad \varphi^2(X^2 = \pm W_0) = \pm \lambda_2 W_0. \tag{190}$$

With λ_1 and λ_2 prescribed by (190), equilibrium equations (183) and (184) are solved simultaneously for ξ and η as functions of λ_1, λ_2 , giving homogeneous values of fields consistent with (185). Then P_1^1 and P_2^2 are obtained with (182) for $a = A = 1$ and $a = A = 2$.

Model predictions for equi-biaxial stretching, $\lambda_1 = \lambda_2$, are produced using the baseline material parameters of Table 1, obtained for the 2D theory in Section 5.5.1. In

Figure 5a, stresses also include those for the ideal elastic case ($\vartheta = \varsigma = 0 \Rightarrow \zeta = \eta = 0$) that are noticeably higher for $\lambda_1 > 1.5$ and increase monotonically with stretch. For the Finsler theory, under this loading protocol ($\lambda_1 = \lambda_2$), P_2^2 increases more rapidly than P_1^1 , with increasing λ_1 , reaching a slightly lower peak value at a significantly lower stretch. Elastic stiffness during the lower-stretch loading is higher in the n_2 direction due to the preponderance of aligned collagen fibers, but degradation linked to the internal structure evolution is more rapid due to the lower toughness of skin when torn in this direction. The latter phenomena are evident in Figure 5b: $\eta(\lambda_1) > \zeta(\lambda_1)$ for $\lambda_1 \in [1.1, 3.9]$.

Remark 65. Data on failure of skin focus on its uniaxial extension [74,75]. Biaxial data (e.g., [68,70]) do not report stretch magnitudes that are capable of causing tearing, so direct validation does not appear possible. If the skin proves to be stiffer and more damage-tolerant under equi-biaxial stretch, the w of (176) can be modified, so the tangent bulk modulus proportional to k_0 increases more strongly with J , and does not degrade so severely with structure evolution.

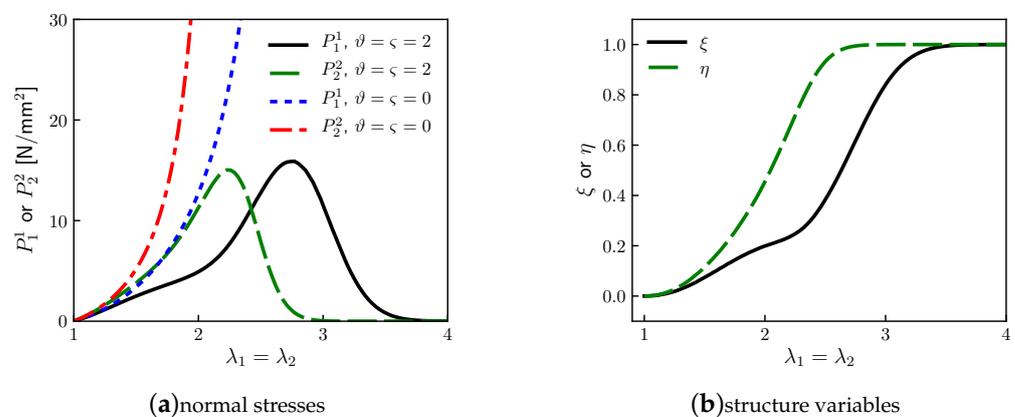


Figure 5. Equi-biaxial extension and tearing of skin, 2D model: (a) stress components from the Finsler model (baseline parameters, $\vartheta = \varsigma = 2$) and the ideal elastic model ($\vartheta = \varsigma = 0$); (b) normalized internal structure components ζ and η .

5.5.3. Stress-Free States

Protocols of Section 5.3.2 now apply. Two boundary value problems are addressed that parallel the 1D analysis of Section 4.5.2. External boundary conditions are set as $\zeta = 0$ and $\eta = 0$, everywhere along $\partial\mathcal{M}$. Stress $P_a^A = 0$ prevails everywhere in \mathcal{M} , ensuring that the mechanical traction $p_a = P_a^A N_A = 0$ over $\partial\mathcal{M}$. For the generalized Finsler metric in (172), it is essential to restrict $r > 1 \Rightarrow \chi_1(\zeta = 0) = \chi_2(\eta = 0) = 0$ in (173).

In the first problem, assume that the specimen undergoes a uniaxial stretch along the n_1 direction (i.e., along X^1 , perpendicular to Langer’s lines) until localized failure occurs. The skin ruptures completely across the midspan at $X^1 = 0$, such that $\zeta(0, X^2) = 1$. In this ruptured state, $\bar{C}_{AB} = \delta_{AB}$ is everywhere on \mathcal{M} for all components, except \bar{C}_{11} , which can differ from δ_{AB} along the line $X^1 = 0$. The solution for $\eta(X^1, X^2)$ is $\eta(X^1, X^2) = 0$, for which (166) is trivially satisfied. From symmetry, the remaining unknown field ζ depends only on $X = X^1$, and $\zeta(-X) = \zeta(X)$. With this partial solution, Equation (165) has a vanishing right side, reducing it to a generally nonlinear, autonomous second-order ODE

$$\gamma_\zeta \frac{d^2 \zeta}{dX^2} = \frac{\gamma_\zeta \zeta}{l^2} (1 + k\zeta^r). \tag{191}$$

Dividing by $\gamma_\zeta > 0$, (191) is identical to (131) with $N_0 = 0$, $\lambda = \zeta^2$, and $\chi = \chi_1 = k\zeta^{r-1}$. Solutions (133) and (144) hold verbatim.

The normalized energy per unit area normal to the X^1 direction is

$$\bar{\gamma}_1 = \frac{1}{2Y_0} \int_{-L_0}^{L_0} \psi \sqrt{G} dX = \frac{\gamma_\xi}{2l} \int_{-L_0}^{L_0} \{\bar{\zeta}^2 + l^2(d\bar{\zeta}/dX)^2\} \exp[(k/r)\bar{\zeta}^r] dX, \quad (192)$$

which is identical to (145) when $\gamma_\xi = 1$ and $N_0 = 0$. Given $\gamma_\xi = 1$, $k = 0.2$, $r = 2$, and $Y_0 = 0.47 \text{ kJ/m}^2$ (Table 1), the outcomes of the 2D theory here match those of the 1D theory in Figure 3a,b with $N_0 = 0$ and $\bar{\gamma}_1 = \bar{\gamma}$. Toughness $2\bar{\gamma}_1 Y_0 = 1.0 \text{ kJ/m}^2$ is consistent with the experiment [73,99,113].

In the second problem, assume that the specimen is stretched along \mathbf{n}_2 (i.e., along X^2 , parallel to Langer's lines). The skin ruptures completely across the midspan at $X^2 = 0$, with $\eta(X^1, 0) = 1$. Now, $\bar{C}_{AB} = \delta_{AB}$ is everywhere for all components, except \bar{C}_{22} , which can differ from δ_{AB} only along $X^2 = 0$. The solution for $\zeta(X^1, X^2)$ is $\zeta = 0$, for which (165) is trivially obeyed. From symmetry, η depends only on $X = X^2$, and $\eta(-X) = \eta(X)$. The balance law (166) reduces to

$$\gamma_\eta \frac{d^2\eta}{dX^2} = \frac{\gamma_\eta \eta}{l^2} (1 + m\eta^r). \quad (193)$$

Dividing by $\gamma_\eta > 0$, (193) matches (131) with $N_0 = 0$, $\nu = \eta^2$, $\chi = \chi_2 = m\eta^{r-1}$, and changes in variables. Solutions (133) and (144) hold. The normalized energy per unit area is

$$\bar{\gamma}_2 = \frac{1}{2Y_0} \int_{-L_0}^{L_0} \psi \sqrt{G} dX = \frac{\gamma_\eta}{2l} \int_{-L_0}^{L_0} \{\eta^2 + l^2(d\eta/dX)^2\} \exp[(m/r)\eta^r] dX \quad (194)$$

for free surfaces normal to the X^2 direction, matching (145) if $\gamma_\eta = 1$ and $N_0 = 0$. Given $\gamma_\eta = 0.84$, $m = 0.3$, $r = 2$, and $Y_0 = 0.47 \text{ kJ/m}^2$ (Table 1), profiles of $\eta(X)$ for this problem are very similar to those of $\zeta(X)$ from the 1D theory in Figure 3a. Energy for $N_0 = 0$ in Figure 3b transforms as $\bar{\gamma}_2 \approx \gamma_\eta \bar{\gamma}$, and $2\bar{\gamma}_2 Y_0 = 0.85 \text{ kJ/m}^2$ is within experimental ranges of 0.5 to 2.5 kJ/m^2 [73,99,113].

Remark 66. Since $2\bar{\gamma}_2 Y_0 < 2\bar{\gamma}_1 Y_0$, the model predicts that skin is more brittle in directions parallel to Langer's lines than in directions perpendicular to Langer's lines, in concurrence with experiment [74,87]. Collagen fibers are less coiled initially in directions parallel to Langer's lines [75], giving the skin's lower compliance and less potential strain accommodation at rupture in those directions.

Remark 67. All parameters in Table 1 have clear physical or geometric origins; none are ad hoc. Constant l is the critical fiber-sliding distance or crack-opening displacement for rupture. Ratios $\frac{k}{r}$ and $\frac{m}{r}$ are associated with the remnant strain contributions in orthogonal \mathbf{n}_1 and \mathbf{n}_2 directions along the primary initial fiber directions (e.g., perpendicular and parallel to Langer's lines). The isotropic shear modulus and bulk modulus for the matrix, consisting of ground substance and elastin, are μ_0 and κ_0 . Nonlinear elastic constants a_1 and b_1 control stiffening due to collagen fiber elongation in the \mathbf{n}_1 direction, while a_2 and b_2 control stiffening due to fiber elongation in the \mathbf{n}_2 direction. The loss of elastic stiffness due to fiber rearrangements and damage processes in matrix, fibers, and their interfaces, in the respective \mathbf{n}_1 and \mathbf{n}_2 directions, is modulated by ϑ and ζ . Isotropic surface energy is Y_0 , with factors γ_ξ and γ_η scaling the fracture toughness in the respective \mathbf{n}_1 and \mathbf{n}_2 directions.

6. Conclusions

A theory of finite-deformation continuum mechanics, rooted in the generalized geometry of Finsler, has been developed and refined. Elements of an internal state vector represent evolving microstructure features and can be interpreted as order parameters. The dependence of the material metric on this internal state affects how distances are measured in the material manifold and how gradients (i.e., covariant derivatives) are resolved. A new application of the theory to anisotropic soft-tissue mechanics has been presented, whereby the internal state is primarily associated with collagen fiber rearrangements and breakages. The material metric contains explicit contributions

from sliding or opening modes in different material directions. Solutions to boundary value problems for tensile extension with tearing in different directions agree with experimental data and microscopic observations on skin tissue, providing physical and geometric insight into the effects of the microstructure.

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Appendix A. Variational Derivatives

The variational derivative $\delta(\cdot)$ of Section 3.3.1 invokes (φ^a, D^A) with $a, A = 1, 2, \dots, n$ as the total set of $2n$ varied independent parameters or degrees of freedom.

Appendix A.1. Deformation Gradient and Director Gradient

The first of (80) follows from (57), (61), and commutation of $\delta(\cdot)$ and $\partial_A(\cdot)$ operators since the variation is performed at fixed X^A :

$$\delta F_A^a(\varphi(X), X) = \delta(\partial_A \varphi^a(X)) = \partial_A(\delta \varphi^a(X)) = \delta_A(\delta \varphi^a(X)) = (\delta \varphi^a(X))|_A, \quad (\text{A1})$$

with F treated as a two-point tensor.

Remark A1. The third equality in (A1) follows from $N_A^B(X, D)\bar{\partial}_B \varphi^a(X) = 0$. The leftmost and rightmost equalities interpret $\varphi^a(X)$ and $\delta \varphi^a(X)$, respectively, as point functions rather than vector fields [20,22].

Let $f(X, D)$ denote a generic differentiable function of arguments $\{X^A, D^A\}$ in a coordinate chart on \mathcal{Z} . The variation of $f(X, D)$ is defined by the first of the following:

$$\delta f(X, D) = f(X, D)|_A \delta(D^A) = \bar{\partial}_A f(X, D) \delta(D^A), \quad (\text{A2})$$

where $(\cdot)|_A$ is the vertical covariant derivative (e.g., as in (21)). For the choices $V_{BC}^A = 0$ and $Y_{BC}^A = 0$ of (71), $f(X, D)|_A = \bar{\partial}_A f(X, D)$ and the rightmost form is obtained, consistent with prior definitions [54,55]. This is used with (84) to obtain the second of (80):

$$\begin{aligned} \delta D_B^A &= \delta(\partial_B D^A) - \delta N_B^A + \delta(K_{BC}^A)D^C + K_{BC}^A \delta(D^C) \\ &= [\partial_B \delta(D^A) - N_B^C \bar{\partial}_C \delta(D^A) + K_{BC}^A \delta(D^C)] - \bar{\partial}_C N_B^A \delta(D^C) + \bar{\partial}_D K_{BC}^A D^C \delta(D^D) \\ &= [\delta(D^A)]|_B - (\bar{\partial}_C N_B^A - \bar{\partial}_C K_{BD}^A D^D) \delta(D^C), \end{aligned} \quad (\text{A3})$$

where it is assumed per (68) that $\bar{\partial}_C \delta[D^A(X)] = \bar{\partial}_C [\delta(D^A)(X)] = 0$ on \mathcal{M} and \mathcal{Z} .

Appendix A.2. Volume Form

Two definitions have been set forth in prior work for the variation of the volume form $d\Omega(X, D)$. The first quoted here sets [54]

$$\begin{aligned} \delta(d\Omega) &= [\delta\sqrt{G}/\sqrt{G}]d\Omega = (\ln \sqrt{G})|_A \delta(D^A)d\Omega = \frac{1}{2}G^{BC}G_{CB}|_A \delta(D^A)d\Omega \\ &= (C_{AB}^B - Y_{AB}^B)\delta(D^A)d\Omega = C_{AB}^B \delta(D^A)d\Omega, \end{aligned} \quad (\text{A4})$$

where the first equality is a definition and (27) and (A2) is used subsequently.

Remark A2. According to (A4), the magnitude of the volume form is varied locally over the n -dimensional base space in (81) with the $\alpha = 1$ prior application of the divergence theorem (31) used to procure (87) and (88) from (86) of Section 3.3.3. The choice (A4) was used in the most recent theory [54] and implied in a prior numerical implementation [59].

The second definition quoted here was used in the original theoretical works [55,56]:

$$\begin{aligned}\delta(d\Omega) &= [\delta\sqrt{\mathcal{G}}/\sqrt{\mathcal{G}}]d\Omega = (\ln\sqrt{\mathcal{G}})|_A\delta(D^A)d\Omega = (\ln\sqrt{G^2})|_A\delta(D^A)d\Omega \\ &= G^{BC}G_{CB}|_A\delta(D^A)d\Omega = 2(C_{AB}^B - Y_{AB}^B)\delta(D^A)d\Omega = 2C_{AB}^B\delta(D^A)d\Omega.\end{aligned}\quad (\text{A5})$$

In the derivation of (A5), the determinant of the Sasaki metric, as defined in (15), has been used along with (27) and (A2).

Remark A3. The definition given by the first equality in (A5) is notionally consistent with another earlier theory [49,50,52]. In the present viewpoint with (A5), the magnitude of the volume form is varied locally in a $2n$ -dimensional total space \mathcal{Z} via (81) with $\alpha = 2$ before integrating over the base n -dimensional space \mathcal{M} in (86) of Section 3.3.3.

Remark A4. Definition (A4) corresponds to $\alpha = 1$ and definition (A5) to $\alpha = 2$ in (81). The only ramification in the governing Euler–Lagrange equations involves the scaling of local free energy density by a factor of one or two through $\alpha\psi C_{CA}^A$ in the micro-momentum balance, in either form (88) or (91). Macroscopic momentum is unaffected by the definition of $\delta(d\Omega)$.

Appendix B. Toward Residual Stress and Growth

Appendix B.1. Macroscopic Momentum

Consideration of residual stress begins with the examination of the balance of linear momentum in the form (90), repeated and reorganized for convenience:

$$\partial_A P_a^A + P_a^B \gamma_{AB}^A - P_c^A \gamma_{ba}^c F_A^b = -\{[\bar{\partial}_B P_a^A + P_a^A \bar{\partial}_B(\ln\sqrt{\mathcal{G}})]\partial_A D^B + P_c^A(\gamma_{ba}^c - \Gamma_{ba}^c)F_A^b\}. \quad (\text{A6})$$

Remark A5. Terms on the left side of (A6) are standard for nonlinear elasticity theory [22]. If the free energy ψ does not depend on D^A or $D_{|B}^A$, then the stress $P_a^A = \partial\psi/\partial F_A^a$ is also conventional, presuming ψ is in the undeformed state $C_{AB} = G_{AB} \Rightarrow P_a^A = 0$. In that case, when the right side of (A6) vanishes, the body manifold \mathcal{M} should not contain residual stresses when $F_A^a = \partial_A \varphi^a$ for regular motions $\varphi^a(X)$ (e.g., in the absence of topological changes).

Remark A6. Departures from classical nonlinear elasticity arise when (i) ψ has dependencies on D^A or $D_{|B}^A$, (ii) when P_a^A or G depends on D^A along with the heterogeneous state field $\partial_A D^B \neq 0$, or (iii) when a different connection than the Levi–Civita connection is used for Γ_{ba}^c (i.e., $\Gamma_{ba}^c \neq \gamma_{ba}^c$ due to the d dependence of the spatial metric g_{ab}). Each of these departures could potentially induce stresses $P_a^A \neq 0$ in a simply connected body externally unloaded via $p_a = P_a^A N_A = 0$ all along its oriented boundary $\partial\mathcal{M}$ (i.e., residual stresses).

Analysis of a particular version of the general theory offers more insight. First, assume in (74) that $\hat{g}_b^a \rightarrow \delta_b^a$, such that $g_{ab}(x, d) \rightarrow g_{ab}(x) = \bar{g}_{ab}(x)$; the spatial metric tensor \mathbf{g} is Riemannian rather than Finslerian. Then, $\gamma_{bc}^a = \Gamma_{bc}^a$. Now, use the osculating Riemannian interpretation of the Finslerian material metric \mathbf{G} offered by Corollary 1 via (68):

$$\tilde{G}_{AB}(X) = G_{AB}(X, D(X)), \quad \tilde{G}(X) = \det(\tilde{G}_{AB}(X)), \quad (\text{A7})$$

$$\tilde{\gamma}_{BA}^A = \partial_B(\ln\sqrt{\tilde{G}}) = \partial_B(\ln\sqrt{G}) + \bar{\partial}_A(\ln\sqrt{G})\partial_B D^A = \gamma_{BA}^A + \bar{\partial}_A(\ln\sqrt{G})\partial_B D^A, \quad (\text{A8})$$

$$\tilde{P}_a^A(X) = P_a^A(X, D(X)), \quad \partial_B \tilde{P}_a^A = \partial_B P_a^A + \bar{\partial}_C P_a^A \partial_B D^C. \quad (\text{A9})$$

Substituting (A8) and (A9) into (A6) gives, with $\gamma_{ba}^c = \Gamma_{ba}^c$,

$$\partial_A \tilde{P}_a^A + \tilde{P}_a^B \tilde{\gamma}_{AB}^A - \tilde{P}_c^A \gamma_{ba}^c F_A^b = 0. \quad (\text{A10})$$

Remark A7. Expression (A10) conforms to the standard form for static equilibrium in classical continuum mechanics, but stress, denoted as \tilde{P}_a^A , and the connection, represented by $\tilde{\gamma}_{BC}^A$, both implicitly depend on the internal state D^A , and the former might also depend on its gradient $D_{|B}^A$, especially if it appears in appearing in ψ . Coefficients $\tilde{\gamma}_{BC}^A$ are those of the Levi–Civita connection of \tilde{G}_{AB} via (36).

Now neglecting the dependence on the internal state gradient in the energy density, requiring D dependence to arise only through G_{AB} , and assuming the body is homogeneous (with a mild abuse of notation):

$$\begin{aligned}\psi &= \psi(F_A^a, D^A) = \psi(F_A^a, G_{AB}(X, D)) \\ &= \tilde{\psi}(F_A^a, \tilde{G}_{AB}(X)) = \tilde{\psi}(C_{AB}(F_A^a, g_{ab}), \tilde{G}_{AB}(X)).\end{aligned}\quad (\text{A11})$$

Recall from (66) that $C_{AB} = F_A^a g_{ab} F_B^b$. As a simple example, consider the case where $n = \dim \mathcal{M}$,

$$\begin{aligned}\tilde{\psi} &= \frac{\mu_0}{2}(C_{AB}\tilde{G}^{AB} - n) \\ \Rightarrow \tilde{P}_a^A &= \frac{\partial \tilde{\psi}}{\partial F_a^A} = \mu_0 g_{ab} \tilde{G}^{AB} F_{A'}^b, \quad \frac{\partial \tilde{\psi}}{\partial \tilde{G}_{AB}^E} = -\frac{\mu_0}{2} \tilde{G}^{AC} \tilde{G}^{BD} C_{CD},\end{aligned}\quad (\text{A12})$$

and where $\mu_0 > 0$ is a constant (e.g., an elastic shear modulus). Now, assume that the spatial manifold \mathfrak{m} is Euclidean [27,30], such that the Riemann–Christoffel curvature tensor from γ_{bc}^a (and, thus, derived from g_{ab}) vanishes identically.

Remark A8. In this case, (A10), the last of (A11), and the example (A12) are consistent with the geometric theory of the growth mechanics of Yavari [30] in the quasi-static setting. Incompressibility can be addressed by appending linear momentum to include contributions from an indeterminate pressure to be determined by boundary conditions under the isochoric constraint $J = 1$ [22]. Otherwise, $\tilde{\psi}$ can be augmented with term(s) to ensure $C_B^A \rightarrow \delta_B^A \Rightarrow \tilde{P}_a^A = 0$ (e.g., (138) for $n = 1$).

The Riemann–Christoffel curvature tensor from $\tilde{\gamma}_{BC}^A$ (and, thus, \tilde{G}_{AB}) need not vanish in general:

$$\tilde{\mathcal{R}}_{BCD}^A = \partial_B \tilde{\gamma}_{CD}^A - \partial_C \tilde{\gamma}_{BD}^A + \tilde{\gamma}_{BE}^A \tilde{\gamma}_{CD}^E - \tilde{\gamma}_{CE}^A \tilde{\gamma}_{BD}^E. \quad (\text{A13})$$

Remark A9. In Riemannian geometry, $\tilde{\gamma}_{BC}^A$ are symmetric, differentiable, and obey (36); (A13) has $\frac{1}{12}n^2(n^2 - 1)$ independent components [31]. For $n = 3$, $\tilde{\mathcal{R}}_{BCD}^A$ contains six independent components, determined completely by the metric and the Ricci curvature $\tilde{\mathcal{R}}_{ABC}^A$ [30,98]. For $n = 2$, $\tilde{\mathcal{R}}_{BCD}^A$ contains only one independent component, determined completely by the scalar curvature $\tilde{\kappa} = \frac{1}{2}\mathcal{R}_{AB}\tilde{G}^{AB}$. For $n = 1$, $\tilde{\mathcal{R}}_{BCD}^A$ always vanishes (i.e., a 1D manifold is always flat in this sense).

When $\tilde{\mathcal{R}}_{BCD}^A$ is nonzero over a region of \mathcal{M} , then no compatible deformation $\tilde{F}_a^A(X)$ exists that can push forward \tilde{G}_{AB} to match the Euclidean metric $g_{ab}(\phi(X))$, which would render the corresponding regions of \mathcal{M} and \mathfrak{m} isometric. In other words, the push-forward $g_{ab} = \tilde{F}_a^A \tilde{G}_{AB} \tilde{F}_b^B$ where $\tilde{F}_a^A = \partial_a \zeta^A$ does not exist, ζ^A being (nonexistent) Euclidean coordinates on \mathcal{M} . In such cases, \mathcal{M} would always have to be deformed (e.g., strained) to achieve its spatial representation \mathfrak{m} since no isometry exists between the two configurations.

Remark A10. If an intrinsically curved body manifold in the reference state \mathcal{M} is stress-free, per the constitutive prescription (e.g., (A12) or any other standard elasticity model), then the intrinsically flat body in the current state \mathfrak{m} would be necessarily strained and stressed, even if external traction p_a vanishes along its boundary. Thus, this particular rendition of the generalized Finsler theory supplies residual stress from a non-Euclidean material metric tensor \tilde{G}_{AB} in a manner matching other works that use Riemannian geometry [27,30].

In the full version of the generalized Finsler theory [54,55], as discussed following (A6), residual stresses could emerge from additional sources to those discussed under the foregoing assumptions of a Euclidean spatial metric, a conventional hyperelastic energy potential, and an osculating Riemannian material metric with non-vanishing curvature. Several different curvature forms can be constructed from the various connections and derivatives of Finsler geometry and its generalizations [3,5]. Further analysis, beyond the present scope, is needed to relate these geometric objects to physics in the continuum mechanical setting, including residual stresses.

Remark A11. The deformation gradient F_A^a could be decomposed into a product of two mappings [62]: $F_A^a(X) = \partial_A \varphi^a(X) = (F^E)_{\alpha}^a(X)(F^D)_{\alpha}^a(D(X))$. In this case, the strain energy potential is written to emphasize the elastic deformation F^E , with the state-dependent deformation F^D explicitly accounting for inelastic deformation mechanisms, including growth [29,107]. In this setting, residual stresses can arise if $(F^E)^{-1}$ and, thus, F^D do not fulfill certain integrability conditions; neither the two-point tensor $(F^E)^{-1}$ nor F^D is always integrable to a vector field [98].

Appendix B.2. Micro-Momentum and Growth

Now, consider the internal state-space equilibrium equation, (91) first, under the aforementioned assumptions used to derive (A10). Furthermore, let $N_B^A = N_B^A(X) K_{BC}^A = \gamma_{BC}^A(X)$, and $\alpha = 1$. Then, with these assumptions, in the osculating Riemannian interpretation of Corollary 1, (91) is

$$\partial_A \tilde{Z}_C^A + \tilde{Z}_C^B \tilde{\gamma}_{AB}^A - \tilde{Z}_B^A \gamma_{AC}^B - Q_C = \psi \bar{\partial}_C (\ln \sqrt{G}) - R_C, \quad (\text{A14})$$

$$\tilde{Z}_B^A(X) = Z_B^A(X, D(X)) = \frac{\partial \psi}{\partial D_B^A}(X, D(X)), \quad Q_A(X, D(X)) = \frac{\partial \psi}{\partial D^A}(X, D(X)), \quad (\text{A15})$$

where (A15) follows from (85). Use the energy density ψ of (A11), so $\tilde{Z}_B^A = 0$ identically. Choose the volumetric source term $R_C = \psi \bar{\partial}_C (\ln \sqrt{G})$, which here represents the local change in referential volumetric energy density due to growth effects on the local volume form $d\Omega(X, D)$, since now, per (A4) of Appendix A, $\psi \delta(d\Omega) = \psi [\bar{\partial}_C (\ln \sqrt{G}) \delta(D^C)] d\Omega = R_C \delta(D^C) d\Omega$.

Remark A12. Physical justification exists in the context of growth mechanics for biological systems: R_C can account for the effect on energy density from changes in mass due to tissue growth [30,107]. Thus, (A14) further reduces to, with (A11), to a form very similar to the equilibrium case of Yavari [30] (e.g., matching Equation (2.73) of ref. [30] with the vanishing time derivative, if, here, $\bar{\partial}_A G_{BC}$ is arbitrary):

$$Q_A = \frac{\partial \psi}{\partial D^A} = \frac{\partial \psi}{\partial G_{BC}} \frac{\partial G_{BC}}{\partial D^A} = \frac{\partial \tilde{\psi}}{\partial \tilde{G}_{BC}} \frac{\partial G_{BC}}{\partial D^A} = 0. \quad (\text{A16})$$

To see how internal state components $\{D^A\}$ can represent growth, consider $n = 2$ (i.e., 2D \mathcal{M} , such as a biological membrane), by which, $\{D^A\} \rightarrow (D^1, D^2) = (l_1 \tilde{\xi}^1, l_2 \tilde{\xi}^2)$, where $l_{1,2} > 0$ are normalization constants that render the $\tilde{\xi}^A$ dimensionless. Choose a polar (i.e., cylindrical $\{X^A\} \rightarrow (R, \Theta)$) coordinate system on a region of \mathcal{M} with (73) applying, such that $\tilde{G} = \text{diag}(1, R^2)$. Assume a generalized Finslerian contribution $\tilde{G} = \text{diag}(\exp(h_1(\tilde{\xi}^1)), \exp(h_2(\tilde{\xi}^2)))$, where $h_1(D(X)) = h_1(D^1(R, \Theta)/l_1)$ and $h_2(D(X)) = h_2(D^2(R, \Theta)/l_2)$ are differentiable functions of their arguments. In matrix form, in this example of anisotropic growth, the second of (73) becomes

$$[G_{AB}] = \begin{bmatrix} G_{RR} & 0 \\ 0 & G_{\Theta\Theta} \end{bmatrix} = [\hat{G}_A^C][\tilde{G}_{CB}] = \begin{bmatrix} \exp(h_1(\tilde{\xi}^1)) & 0 \\ 0 & R^2 \exp(h_2(\tilde{\xi}^2)) \end{bmatrix}. \quad (\text{A17})$$

A more specific case is now studied. Let $\chi(R)$ denote a scalar radial growth function. Then set

$$\zeta = \zeta^1 = \frac{D^1}{l_1} = \frac{D^2}{l_2} = \zeta^2, \quad \xi = \xi(R); \quad h = h_1 = -h_2 = 2\chi, \quad h = h(\xi(R)) = 2\chi(R). \quad (A18)$$

This yields the metric $\tilde{G}_{AB}(X)$ as per Yavari (ref. [30], Equation (2.101)), which corresponds to anisotropic annular growth:

$$\begin{aligned} [G_{AB}(R, \zeta)] &= \begin{bmatrix} \exp(h(\xi(R))) & 0 \\ 0 & R^2 \exp(-h(\xi(R))) \end{bmatrix} \\ \Rightarrow [\tilde{G}_{AB}(R)] &= \begin{bmatrix} \exp(2\chi(R)) & 0 \\ 0 & R^2 \exp(-2\chi(R)) \end{bmatrix}. \end{aligned} \quad (A19)$$

Remark A13. In the special case given by (A19), internal state changes preserve volume via $\det(G_{AB}(X, D)) = R^2$ being independent of χ, ζ , and D , so $C_{AB}^B = 0$.

Now, the energy potential (A12) is applied, so that, for equilibrium of the internal state, (A16) transitions to the following, defining $\dot{h}(\zeta) = dh(\zeta)/d\zeta$,

$$\begin{aligned} Q_A &= -\frac{\mu_0}{2} \tilde{G}^{BD} \tilde{G}^{CE} C_{DE} \bar{\partial}_A G_{BC} = 0 \\ \Rightarrow \begin{cases} 2l_1 Q_1(\zeta, R) = -\mu_0 \exp(-h(\zeta)) C_{RR} \dot{h}(\zeta) = 0, \\ 2l_2 Q_2(\zeta, R) = \mu_0 R^{-2} \exp(h(\zeta)) C_{\Theta\Theta} \dot{h}(\zeta) = 0. \end{cases} \end{aligned} \quad (A20)$$

Thus, the equilibrium of the internal state is only ensured for this particular strain energy function and material metric when $\dot{h} = 0$. A sample function with three equilibrium states at $\zeta = 0, \frac{1}{2}, 1$ is the double-well:

$$h = \zeta^2(1 - \zeta)^2, \quad \dot{h} = 2\zeta(1 - \zeta)(1 - 2\zeta). \quad (A21)$$

Now, the Levi-Civita connection and curvature for the metric \tilde{G} in (A19) are revisited. Denote $h'(\xi(R)) = [dh(\xi(R))/d\xi][d\xi(R)/dR] = \dot{h}(\zeta)\zeta'(R)$. From (36), $\tilde{\gamma}_{BC}^A$ has non-vanishing components

$$\tilde{\gamma}_{RR}^R = \frac{h'}{2}, \quad \tilde{\gamma}_{\Theta\Theta}^R = \exp(-2h) \left(\frac{R^2 h'}{2} - R \right), \quad \tilde{\gamma}_{R\Theta}^\Theta = \tilde{\gamma}_{\Theta R}^\Theta = \frac{1}{R} - \frac{h'}{2}. \quad (A22)$$

Recalling that $\tilde{\kappa}$ is the scalar curvature, the non-vanishing covariant components of $\tilde{\mathcal{R}}_{BCDE} = \tilde{\mathcal{R}}_{BCD}^A \tilde{G}_{AE}$ are from (A13),

$$\begin{aligned} \tilde{\mathcal{R}}_{R\Theta R\Theta} &= \tilde{\mathcal{R}}_{\Theta R \Theta R} = -\tilde{\mathcal{R}}_{R\Theta \Theta R} = -\tilde{\mathcal{R}}_{\Theta R R \Theta} = -R^2 \tilde{\kappa} \\ &= -[\partial_R \tilde{\gamma}_{\Theta\Theta}^R + \tilde{\gamma}_{\Theta\Theta}^R (\tilde{\gamma}_{RR}^R - \tilde{\gamma}_{R\Theta}^\Theta)] \tilde{G}_{RR} \\ &= -\frac{d}{dR} \left[\exp(-2h) \left(\frac{R^2 h'}{2} - R \right) \right] \exp(h) + \left(\frac{R^2 h'}{2} - R \right) \left(\frac{1}{R} - h' \right) \exp(-h) \\ &= -\frac{R}{2} \exp(-h) [R\{h'' - (h')^2\} + 4h'] \\ &= -\frac{R}{2} \exp(-h) \left[R \left(\frac{d^2 \zeta}{dR^2} + \frac{d\zeta}{dR} \frac{d}{dR} \right) \frac{dh}{d\zeta} - R \left(\frac{dh}{d\zeta} \frac{d\zeta}{dR} \right)^2 + 4 \frac{dh}{d\zeta} \frac{d\zeta}{dR} \right]. \end{aligned} \quad (A23)$$

The annular material manifold $\{\mathcal{M} : R \in [R_0, R_1], \Theta \in [0, \Theta_1]\}$, $R_1 > R_0 > 0$, $\Theta_1 < 2\pi$ is considered. Since $R > 0$ and for bounded h , the local flatness condition from (A23) is

$$R\{h'' - (h')^2\} + 4h' = 0 \Leftrightarrow R \left(\frac{d^2 \zeta}{dR^2} + \frac{d\zeta}{dR} \frac{d}{dR} \right) \frac{dh}{d\zeta} - R \left(\frac{dh}{d\zeta} \frac{d\zeta}{dR} \right)^2 + 4 \frac{dh}{d\zeta} \frac{d\zeta}{dR} = 0. \quad (A24)$$

Remark A14. The first of (A24) is a second-order nonlinear ODE detailing the radial distribution of the generic function $h = h(R)$. The second is a second-order nonlinear ODE for $\xi = \xi(R)$, which could be solved if the intermediate functional form $h(\xi)$ is known a priori (e.g., (A21)). Trivial solutions are $h(R) = \text{constant}$ and $\xi(R) = \text{constant}$. General non-trivial analytical solutions are not obvious. Given the boundary conditions, determining the particular non-trivial solutions for flatness, should they exist, appears to require numerical methods.

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