

Supplementary Materials

Assessment of Secondary Sulfate Aqueous-Phase Formation Pathways in the Tropical Island City of Haikou: A Chemical Kinetic Perspective

Text S1

H_{SO_2} , K_{s1} and K_{s2} can be estimated by Equations (S1) and (S2) [62],

$$H = H(298K) \exp \left[-\frac{\Delta H_{298K}}{R} \left(\frac{1}{T} - \frac{1}{T_{298K}} \right) \right] \quad (S1)$$

where ΔH_{298K} is the enthalpy change at constant temperature and pressure; the parameters of $\Delta H_{298K}/R$ are shown in Table S1; T indicates the absolute temperature (K); and $H_{SO_2}(298K) = 1.23 \text{ M atm}^{-1}$ (Table S1).

$$K_s = K(298K) \exp \left[-\frac{\Delta H_{298K}}{R} \left(\frac{1}{T} - \frac{1}{T_{298K}} \right) \right] \quad (S2)$$

where ΔH_{298K} is the enthalpy change at constant temperature and pressure; the parameters of $\Delta H_{298K}/R$ are -1960 and -1500 , respectively; T indicates the absolute temperature (K); and $K(298K)$ are $1.3 \times 10^{-2} \text{ M}$ for K_{s1} and $6.6 \times 10^{-8} \text{ M}$ for K_{s2} .

Text S2

The influences of ionic strength on the reaction rate of the S(IV)+NO₂ pathway can be estimated by Equation (S3) [11,63],

$$\log \frac{k_{S(IV)+NO_2}^{I=i}}{k_{S(IV)+NO_2}^{I=0}} = b I_i \quad (S3)$$

where $k_{S(IV)+NO_2}^{I=i}$ is the rate constant at $I=i$ (M); I_i is the ionic strength, which was calculated by the ISORROPIA II model; $k_{S(IV)+NO_2}^{I=0}$ (M⁻¹ s⁻¹) represents the rate constant at $I=0$ M; and b is the kinetic salting coefficient, taken as 0.5 [11].

Text S3

The influences of ionic strength on the reaction rate of the S(IV)+H₂O₂ pathway can be estimated by Equation (S4) [64],

$$\log \frac{k_{S(IV)+H_2O_2}^{I=i}}{k_{S(IV)+H_2O_2}^{I=0}} = -\frac{2 \times 0.509 \times \sqrt{I_i}}{1 + 0.17 \times \sqrt{I_i}} + 2 \times 0.18 I_i \quad (S4)$$

where $k_{S(IV)+H_2O_2}^{I=i}$ (M⁻¹ s⁻¹) is the rate constant at I=i (M); I_i is the ionic strength, which was calculated by the ISORROPIA II model; and $k_{S(IV)+H_2O_2}^{I=0}$ (M⁻¹ s⁻¹) represents the rate constant at I=0 M.

Text S4

The influences of ionic strength on the reaction rate of the S(IV)+O₃ pathway can be estimated by Equation (S5) [65],

$$\frac{k_{S(IV)+O_3}^{I=i}}{k_{S(IV)+O_3}^{I=0}} = 1 + 1.94I_i \quad (S5)$$

where $k_{S(IV)+O_3}^{I=i}$ (M⁻¹ s⁻¹) is the rate constant of the S(IV)+O₃ pathway at I=i (M);

I_i is the ionic strength, which was calculated by the ISORROPIA II model; and

$k_{S(IV)+O_3}^{I=0}$ (M⁻¹ s⁻¹) represents the rate constant at I=0 M.

Text S5

The rate expression of Fe(III)-catalyzed oxidation of S(IV) into secondary SO_4^{2-} varied with aerosol pH [26,42,66,67],

pH 0 to 3:

$$R_{aq(Fe+O_2)} = k_{(Fe+O_2)1} [H^+]^{-1} [Fe(III)] [S(IV)] \quad (S6)$$

pH 3 to 4.5:

$$R_{aq(Fe+O_2)} = k_{(Fe+O_2)2} [Fe(III)]^2 [S(IV)] \quad (S7)$$

pH 4.5 to 6.5:

$$R_{aq(Fe+O_2)} = k_{(Fe+O_2)3} [S(IV)] \quad (S8)$$

pH > 6.5:

$$R_{aq(Fe+O_2)} = k_{(Fe+O_2)4} [S(IV)] \quad (S9)$$

where $k_{(Fe+O_2)1} = 6 \text{ s}^{-1}$, $k_{(Fe+O_2)2} = 1.0 \times 10^9 \text{ M}^{-2} \text{ s}^{-1}$, $k_{(Fe+O_2)3} = 1.0 \times 10^{-3} \text{ s}^{-1}$ and $k_{(Fe+O_2)4} = 1.0 \times 10^{-4} \text{ s}^{-1}$ [26,42] (Table S2); $[H^+]$ is H^+ concentration and calculated by the ISORROPIA II model; and $[Fe(III)]$ is the concentrations of Fe(III) in aerosol water, which was calculated by Wang T et al. [10]:

$$[Fe(III)] = \text{Min} \left(C_{Fe} \times F / M_{Fe} / AWC, \frac{K_{sp,Fe(OH)_3}}{[OH^-]^3} \right) \quad (S10)$$

where C_{Fe} (ng m^{-3}) is the concentration of water-soluble Fe; F is the fraction of Fe(III) in water-soluble Fe, which is 10% during the day and 90% at night [68]; M_{Fe} (g mol^{-1}) is the molecular weight of Fe; AWC is the aerosol water content in L m^{-3} and was calculated by the ISORROPIA II model; and $K_{sp,Fe(OH)_3}$ represents the solubility product constant of $Fe(OH)_3$, which was taken as $6 \times 10^{-38} \text{ M}$ [69].

The influences of ionic strength on the reaction rate of the S(IV)+Fe pathway

can be estimated by Equation (S11) [10],

$$\log \frac{k_{(Fe+O_2)}^{I=i}}{k_{(Fe+O_2)}^{I=0}} = -4 \frac{\sqrt{I_i}}{1+\sqrt{I_i}} \quad (S11)$$

where $k_{Fe+O_2}^{I=i}$ is the rate constant of the S(IV)+Fe pathway at I=i (M); I_i is the ionic strength, which was calculated by the ISORROPIA II model; and $k_{Fe+O_2}^{I=0}$ represents the rate constant at I=0 M.

The rate expression for the Mn(II)-catalyzed oxidation reaction is zero-order kinetics, for the S(IV) concentrations above 100 μ M [70],

$$R_{aq(Mn+O_2)} = k_{(Mn+O_2)1} [Mn(II)]^2 \quad (S12)$$

For S(IV) concentration below 1 μ M, the reaction obeys first order in S(IV) [70],

$$R_{aq(Mn+O_2)} = k_{(Mn+O_2)2} [Mn(II)] [S(IV)] \quad (S13)$$

where $k_{(Mn+O_2)1} = 680 \text{ M}^{-1} \text{ s}^{-1}$; $k_{(Mn+O_2)2} = 1000 \text{ M}^{-1} \text{ s}^{-1}$ [26]; and [Mn(II)] is the concentration of Mn(II) in aerosol water, which was calculated by Wang T et al. [10]:

$$[Mn(II)] = \min \left(C_{Mn} / M_{Mn} / AWC, \frac{K_{sp, Mn(OH)_2}}{[OH^-]^2} \right) \quad (S14)$$

where C_{Mn} (ng m^{-3}) is the concentration of water-soluble Mn; M_{Mn} (g mol^{-1}) is the molecular weight of Mn; AWC is the aerosol water content in L m^{-3} , which was calculated by the ISORROPIA II model; and $K_{sp, Mn(OH)_2}$ represents the solubility product constant of Mn(OH)₂, which is $1.6 \times 10^{-13} \text{ M}$ [69].

The influences of ionic strength on the reaction of the S(IV)+Mn pathway can be estimated by Equation (S15) [26],

$$\log \frac{k_{(Mn+O_2)}^{I=i}}{k_{(Mn+O_2)}^{I=0}} = -4.07 \frac{\sqrt{I_i}}{1+\sqrt{I_i}} \quad (S15)$$

where $k_{\text{Mn}+\text{O}_2}^{I=i}$ ($\text{M}^{-1} \text{s}^{-1}$) is the rate constant of the S(IV)+Mn pathway at $I=i$ (M);

I_i is the ionic strength, which was calculated by the ISORROPIA II model; and

$k_{\text{Mn}+\text{O}_2}^{I=0}$ ($\text{M}^{-1} \text{s}^{-1}$) represents the rate constant at $I=0$ M.

Text S6

The influences of ionic strength on the reaction rate of the S(IV)+Fe×Mn pathway can be estimated by Equation (S16) [10],

$$\log \frac{k_{(Fe \times Mn + O_2)}^{I=i}}{k_{(Fe \times Mn + O_2)}^{I=0}} = -4 \frac{\sqrt{I_i}}{1 + \sqrt{I_i}} \quad (S16)$$

where $k_{Fe \times Mn + O_2}^{I=i}$ ($M^{-2} s^{-1}$) is the rate constant of the S(IV)+Fe×Mn pathway when $I=i$ (M); I_i is the ionic strength, which was calculated by the ISORROPIA II model; and $k_{Fe \times Mn + O_2}^{I=0}$ ($M^{-2} s^{-1}$) represents the rate constant at $I=0$ M.

Text S7

$$J_{aq,lim} = \min\{J_{aq}(SO_2), J_{aq}(O_{xi})\} \quad (S17)$$

where $J_{aq}(O_{xi})$ refers to the limiting mass transfer rate of the oxidants (NO_2 , H_2O_2 , O_3).

$$J_{aq}(X) = K_{MT}(X) \cdot p(X) \cdot H(X) \quad (S18)$$

where X represents the SO_2 or the other oxidants (NO_2 , H_2O_2 , O_3); $p(X)$ is the gas-phase partial pressure (atm); $H(X)$ is the Henry's law constant ($M^{-1} \text{ atm}^{-1}$); and K_{MT} is the mass transfer rate coefficient (s^{-1}), and can be calculated as:

$$K_{MT}(X) = \left[\frac{R_p^2}{3D_g} + \frac{4R_p}{3\alpha v} \right]^{-1} \quad (S19)$$

where $\frac{R_p^2}{3D_g}$ and $\frac{4R_p}{3\alpha v}$ refer to the continuum regime resistance and the kinetic (or free-molecular) regime resistance, respectively. R_p is the radius of aerosol (m), which we assumed as 1.5×10^{-7} m. D_g ($m^2 \text{ s}^{-1}$) is the gas-phase molecular diffusion coefficient, and we adopted the values from the literature as 2×10^{-5} [14]. A is the mass accommodation coefficient of X on the droplet surface: for SO_2 , it is 0.11; for O_3 , 5×10^{-4} ; for H_2O_2 , 0.23; and for NO_2 , 2×10^{-4} [26,71]. v ($m \text{ s}^{-1}$) is the mean molecular speed of X .

Table S1. Rate constants for calculating Henry's law.

Gas species	Equilibrium	Constants (298K) (M atm ⁻¹)	$\Delta H_{298k}/R(K)$	Reference
SO ₂	$SO_2(g) \leftrightarrow SO_2(aq)$	H _{SO2} =1.23	-3145.3	[26]
NO ₂	$NO_2(g) \leftrightarrow NO_2(aq)$	H _{NO2} =1.0×10 ⁻²	-2516.2	
H ₂ O ₂	$H_2O_2(g) \leftrightarrow H_2O_2(aq)$	H _{H2O2} =1.0×10 ⁵	-7297.1	
O ₃	$O_3(g) \leftrightarrow O_3(aq)$	H _{O3} =1.1×10 ⁻²	-2536.4	

Table S2. Rate constants and ionic strength effects of the reactions.

Oxidants	Rate constants	E/R(K)	I impact	References
NO ₂	$k_{S(IV)+NO_2,low} = (0.14\sim 2) \times 10^6 (M^{-1} s^{-1})$ $k_{S(IV)+NO_2,high} = (1.24\sim 1.67) \times 10^7 (M^{-1} s^{-1})$	–	$\log \frac{k}{k^{I=0}} = 0.5I$	[11,27,28]
H ₂ O ₂	$k_{(S(IV)+H_2O_2)1}(298K) = 7.45 \times 10^7 (M^{-1} s^{-1})$ $k_{(S(IV)+O_3)1} = 2.4 \times 10^4 (M^{-1} s^{-1})$	4430 –	$\log \frac{k}{k^{I=0}} = -\frac{2 \times 0.509\sqrt{I}}{1 + 0.17 \times \sqrt{I}} + 2 \times 0.18I$	[26,29,64]
O ₃	$k_{(S(IV)+O_3)2}(298K) = 3.7 \times 10^5 (M^{-1} s^{-1})$ $k_{(S(IV)+O_3)3}(298K) = 1.5 \times 10^9 (M^{-1} s^{-1})$	5530 5280	$\frac{k}{k^{I=0}} = 1 + 1.94I$	[26,65]
Fe	pH<3 $k_{(Fe+O_2)1} = 6(s^{-1})$ 3<pH<4.5 $k_{(Fe+O_2)2} = 1.0 \times 10^9 (M^{-2} s^{-1})$ 4.5<pH<6.5 $k_{(Fe+O_2)3} = 1.0 \times 10^{-3} (s^{-1})$ pH>6.5 $k_{(Fe+O_2)4} = 1.0 \times 10^{-4} (s^{-1})$	–	$\log \frac{k}{k^{I=0}} = -4 \frac{\sqrt{I}}{1 + \sqrt{I}}$	[10,66,67]
Mn	S(IV)>100μM $k_{(Mn+O_2)1} = 680 (M^{-1} s^{-1})$ S(IV)<1μM $k_{(Mn+O_2)2} = 1000 (M^{-1} s^{-1})$	–	$\log \frac{k}{k^{I=0}} = -4.07 \frac{\sqrt{I}}{1 + \sqrt{I}}$	[26,70]
Fe×Mn	pH≤4.2 $k_{(Fe \times Mn + O_2)1}(297K) = 3.72 \times 10^7 (M^{-2} s^{-1})$ pH≥4.2 $k_{(Fe \times Mn + O_2)2}(297K) = 2.51 \times 10^{13} (M^{-2} s^{-1})$	8430	$\log \frac{k}{k^{I=0}} = -4 \frac{\sqrt{I}}{1 + \sqrt{I}}$	[26,31]

Table S3. The mean concentrations and ranges of water-soluble inorganic ions
($\mu\text{g m}^{-3}$) in different seasons.

Species	Autumn	Winter	Spring	Summer
nss-SO ₄ ²⁻	2.9±1.8	4.1±1.8	3.9±2.1	1.5±0.7
	0.1-8.6	1.1-9.2	1.0-13	0.7-4.1
ss-SO ₄ ²⁻	0.1±0.04	0.1±0.1	0.1±0.04	0.04±0.02
	0.02-0.2	0.02-0.3	0.02-0.2	0.02-0.1
NO ₃ ⁻	0.4±0.7	3.2±3.0	1.0±1.1	0.5±0.3
	0.1-4.3	0.4-13	0.2-6.0	0.1-1.3
NH ₄ ⁺	0.7±0.6	1.8±1.3	1.1±0.7	0.4±0.3
	0.1-2.4	0.3-5.9	0.2-3.4	0.1-1.3
Ca ²⁺	0.3±0.4	0.2±0.1	0.3±0.2	0.3±0.1
	0.1-2.4	0.03-0.5	0.02-0.8	0.1-0.6
Na ⁺	0.3±0.2	0.4±0.2	0.3±0.1	0.2±0.1
	0.1-0.9	0.1-1.0	0.1-0.7	0.1-0.3
Cl ⁻	0.2±0.2	0.7±0.3	0.3±0.2	0.2±0.1
	0.02-1.1	0.2-1.7	0.03-1.0	0.03-0.5
K ⁺	0.1±0.1	0.2±0.2	0.1±0.1	0.1±0.04
	0.03-0.6	0.1-0.8	0.03-0.3	0.02-0.2
Mg ²⁺	0.04±0.02	0.1±0.03	0.1±0.02	0.03±0.01
	0.01-0.1	0.02-0.2	0.01-0.1	0.01-0.1

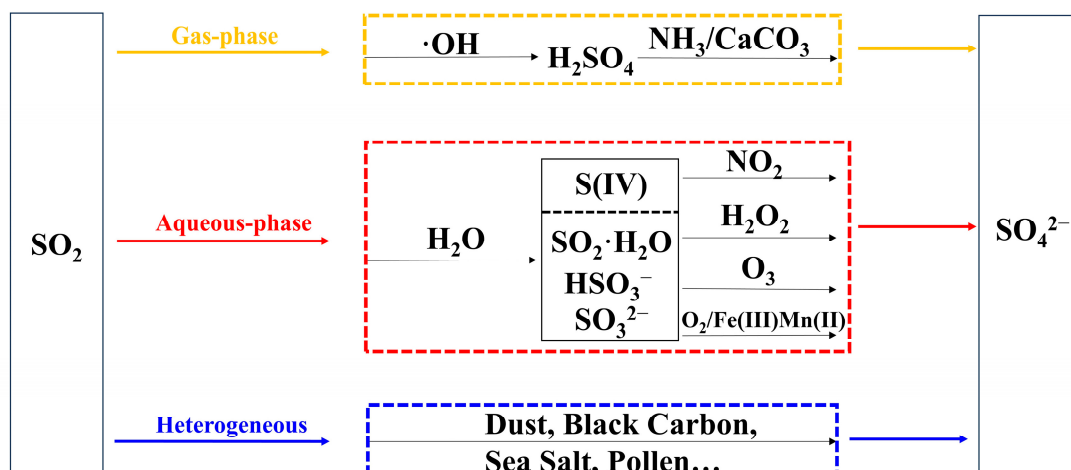


Figure S1. The schematic of sulfate formation pathways.

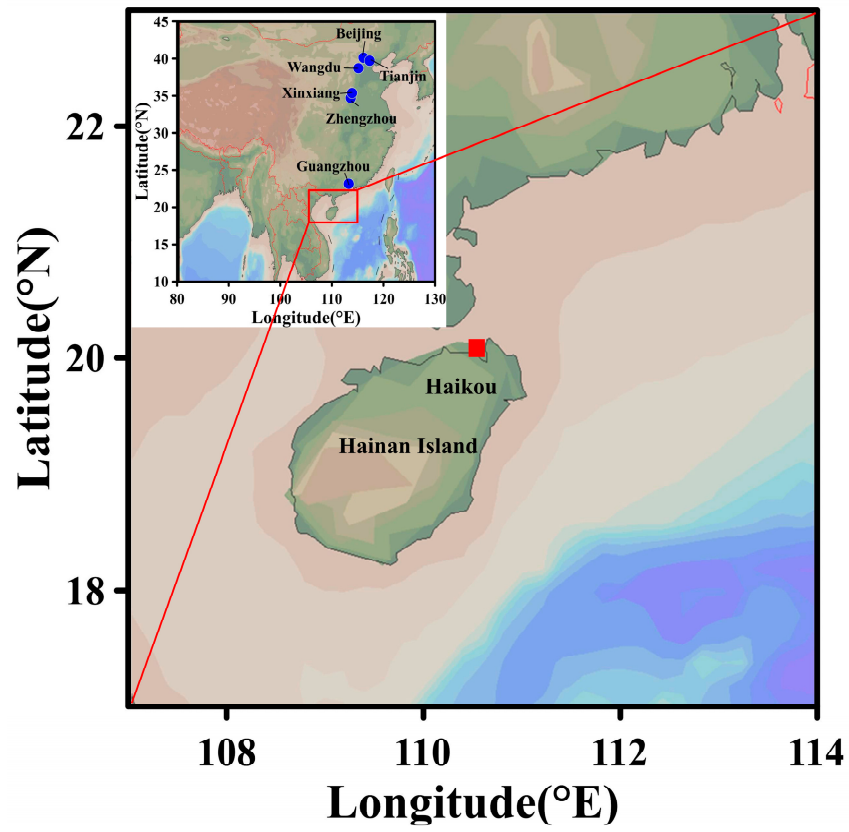


Figure S2. Sampling location.

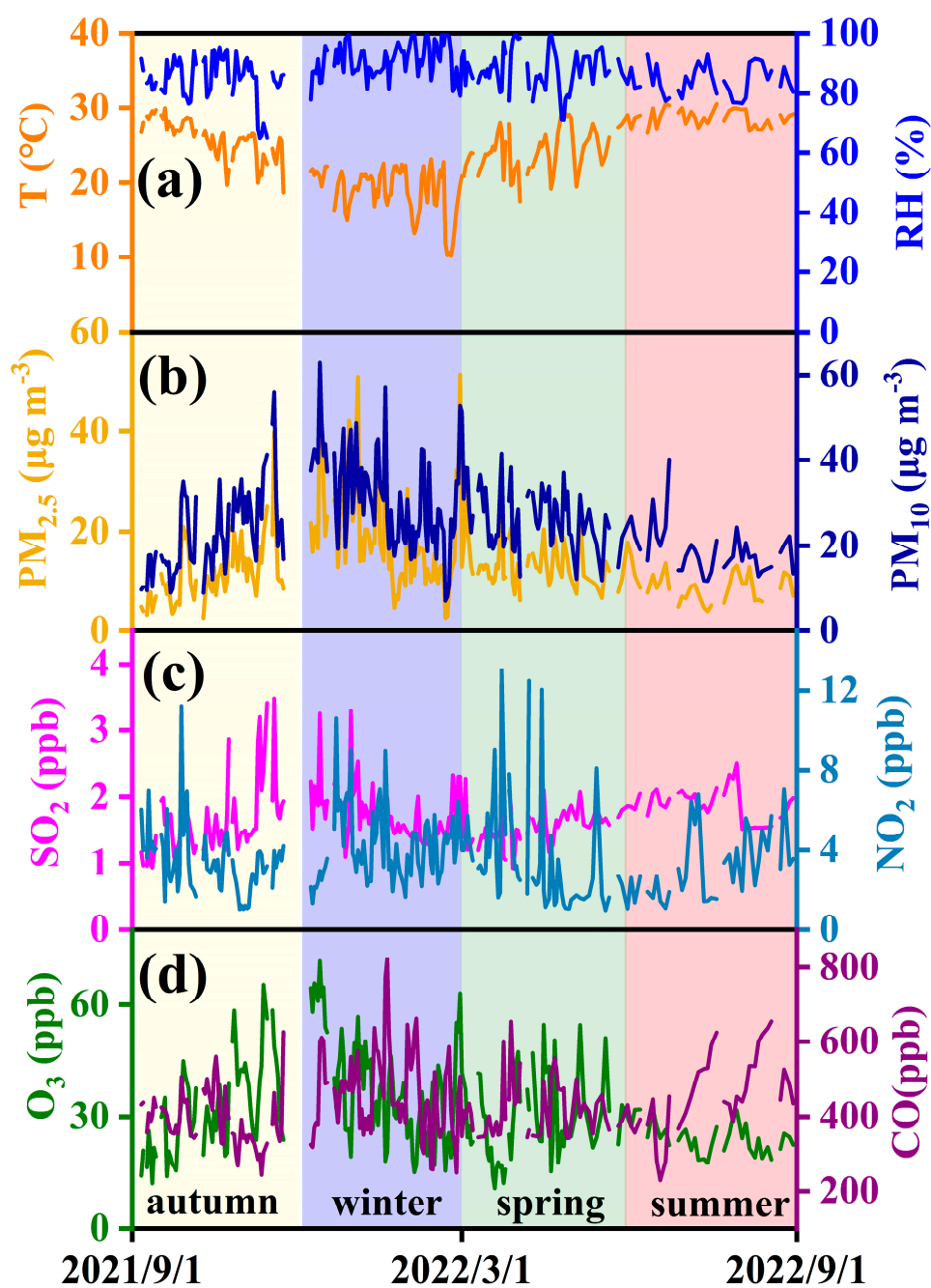


Figure S3. Hourly concentrations of T, RH, PM_{2.5}, PM₁₀, SO₂, NO₂, O₃, and CO from September 2021 to August 2022. (The yellow, blue, green, and red bars represent autumn, winter, spring, and summer, respectively).

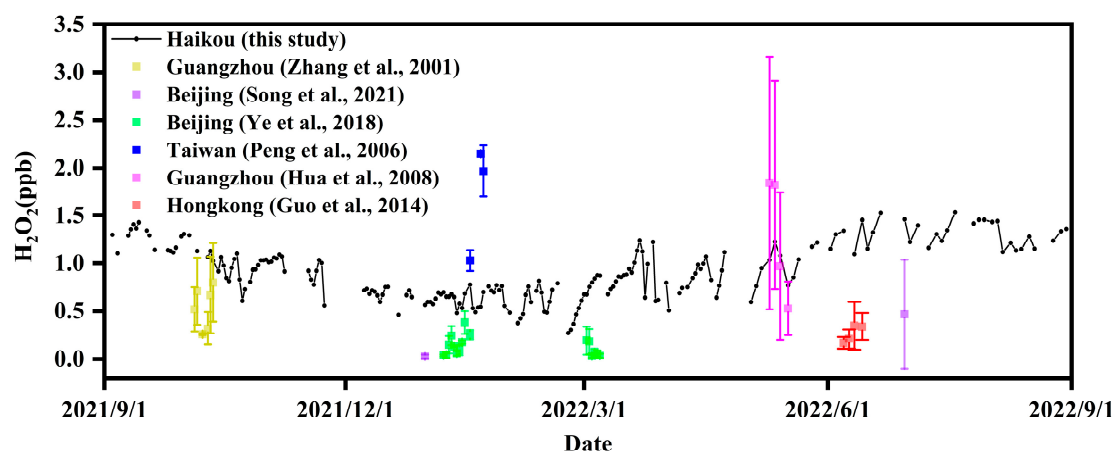


Figure S4. Comparisons of H₂O₂ concentrations at different sites in different seasons.

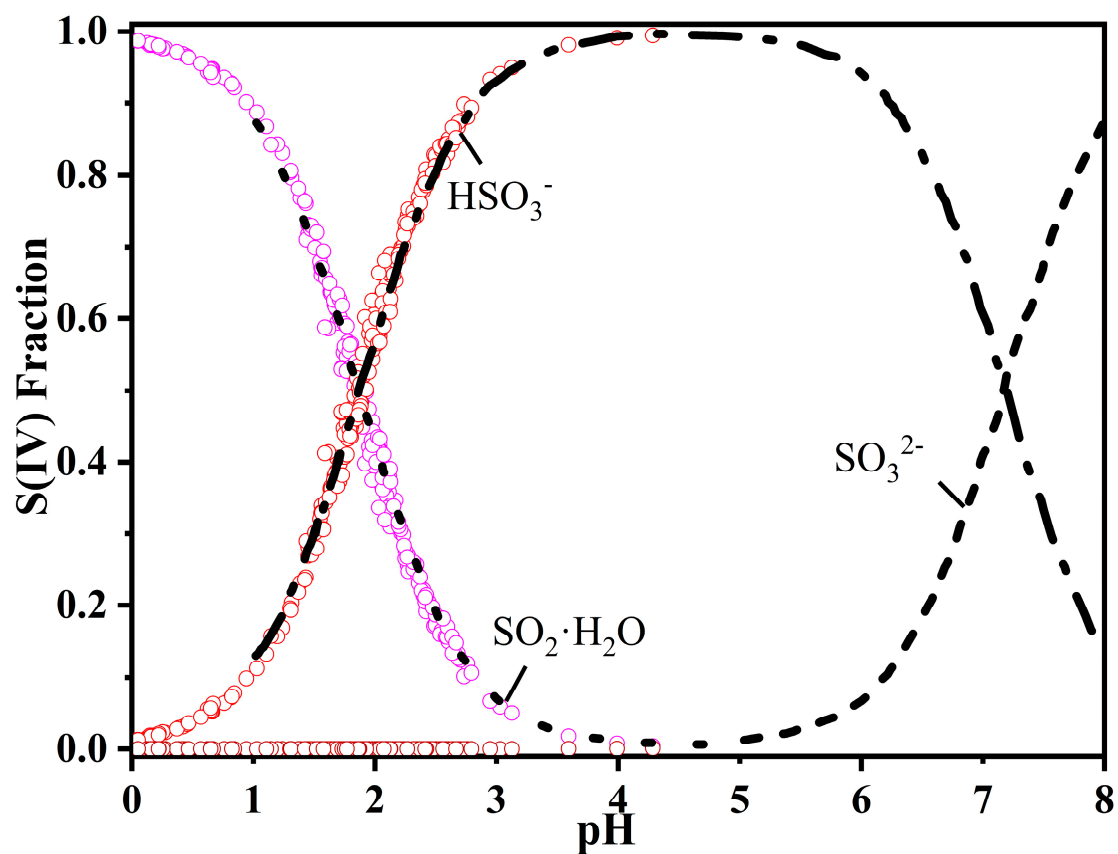


Figure S5. Compositions of S(IV) species with regard to pH. (The different circles indicate the calculated forms of S(IV) using Henry's law. The black dotted lines represent previous results in Seinfeld and Pandis [26].)

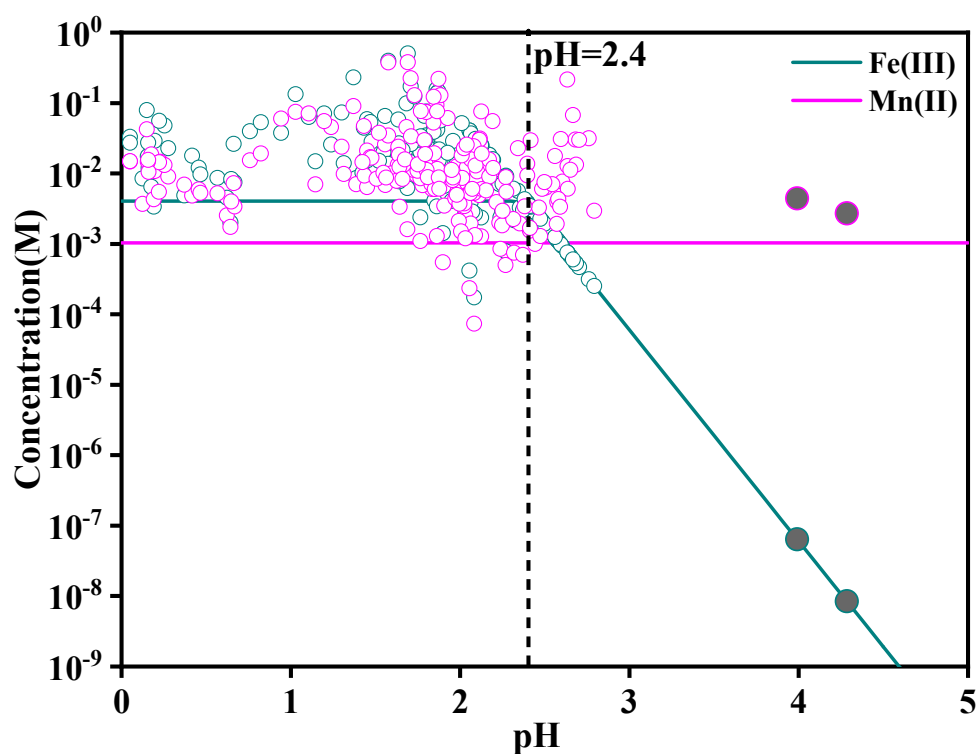


Figure S6. Water-soluble Fe(III) and Mn(II) concentrations as a function of pH. (The solid cyan and purple lines indicate the concentrations of Fe (III) and Mn (II) calculated using the mean values, respectively. The different circles indicate the actual calculated concentrations of Fe(III) and Mn(II). The vertical dashed line indicates pH = 2.4).

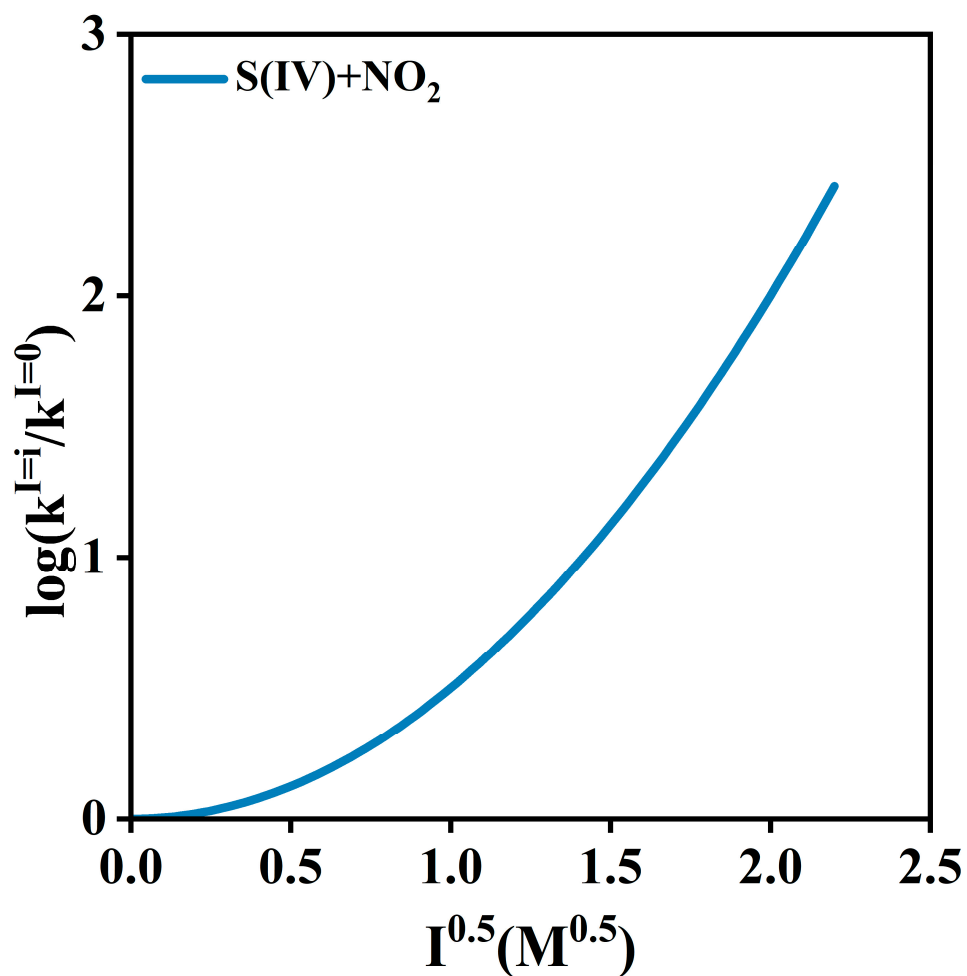


Figure S7. Influence of ionic strength (I) on chemical rate constant $k_{S(IV)+NO_2}$. ($k^{I=i}$ is the rate constant at $I=i$ (M), and $k^{I=0}$ is the rate constant at $I=0$ M. Detailed expressions for the $\log(k^{I=i}/k^{I=0})$ versus I relationship are shown in Table S2.)

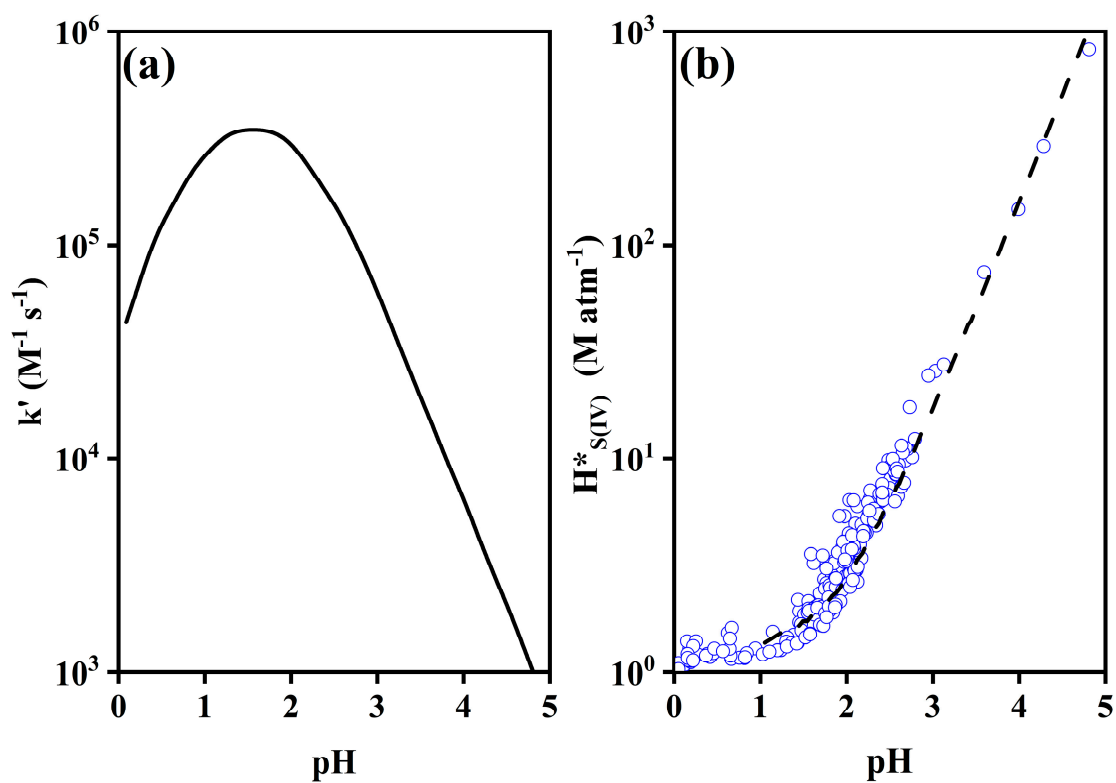


Figure S8. (a) Second-order rate constant for oxidation of S(IV) by H_2O_2 as a function of pH. The line is quoted from Seinfeld and Pandis [26]. (b) Effective Henry's law constant ($H^*_{\text{S(IV)}}$) for SO_2 as a function of pH. The black dotted line is quoted from Seinfeld and Pandis [26].

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